Director's Report

Project Name: Gateway Crossing

Description: Preliminary site plan and special land use approvals

Date on Agenda this packet pertains to: April 4, 2024

 \boxtimes Public Hearing

 \boxtimes Special Land Use

⊠Initial Submittal

□Rezoning □Other:

 \Box Revised Plans

⊠Preliminary Approval

□Final Approval

Contact	Consultants &	Approval	Denial	Approved w/Conditions	Other	Comments
	Departments			,		
Sean	Planning				\boxtimes	
O'Neil	Director					
DLZ	Engineering			\boxtimes		See letter dated 03/27/24.
	Consultant					
Justin	Staff Planner			\boxtimes		See letter dated 03/28/24.
Quagliata						
Jason	WLT Fire			\boxtimes		See letter dated 03/26/24.
Hanifen	Marshal					

WHITE LAKE TOWNSHIP PLANNING COMMISSION

REPORT OF THE COMMUNITY DEVELOPMENT DEPARTMENT

TO:	Planning Commission
FROM:	Sean O'Neil, AICP, Community Development Director
	Justin Quagliata, Staff Planner
DATE:	March 28, 2024
RE:	Gateway Crossing Preliminary Site Plan and Special Land Uses – Review #4

Staff reviewed the revised site plan prepared by Boss Engineering (revision date January 12, 2024). The following comments from the first review dated January 23, 2023, second review dated September 26, 2023, and third review dated February 8, 2024 are listed below. Responses to those comments are provided in (green).

Najor Companies (Brian Najor) has requested preliminary site plan and special land use (2) approval to construct a commercial/retail center on Parcel Number 12-20-426-003 and Parcel Number 12-20-402-003, located at the southwest corner Bogie Lake Road and Highland Road. The two legal descriptions on Sheet 1 conflict with the combined legal description on Sheet 2 and the size of the parcels listed in the Site Data Table on Sheet 3. Revise for consistency. The lot width listed in the Site Data table is also inconsistent with the combined legal description on Sheet 2 and the dimension labeled on the drawing. Revise for consistency. (Comments addressed. Acreage is now consistent between plan sheets and the Site Data Table). Currently the parcels are zoned GB (General Business). Combined the parcels comprising the subject site are approximately 5.836 acres in size (to be confirmed based on previous comments). If the project proceeds to construction, an application to combine the parcels shall be submitted to the Assessing Department prior to issuance of a building permit. final site plan submission (comment remains as a notation). The design engineer stated the Applicant acknowledges this requirement.

The Applicant is proposing to construct-two one single-story buildings totaling-12,380 8,573 8,620 square feet in size. (Total area of the building and each tenant space size listed on Sheet 3 are all inconsistent with the preliminary floor plan. Revise for consistency). (Comment addressed. The total area of the building and each tenant space size listed on Sheet 4 are now consistent with the floor plan). <u>The size of the retail and coffee shop</u> building labeled on the drawing (8,320 square feet) is two square feet less than the size of the building listed in the Site Data table on Sheet 3 (8,322 square feet). Revise for consistency. (Comment addressed. The Site Data Table now shows the correct total area for the building and it matches what is shown on the site plan). Special land use approval is requested as-two one drive-thru-windows are is proposed; the easterly unit of the-east building is identified as a coffee shop and the westerly building is identified as a Culver's drive-thru restaurant. Special land use approval is also requested to allow outdoor dining at the retail and coffee shop building and Culver's. (The Culver's building is no longer being proposed on this site).

Based on the nature of the proposed project, the Applicant shall state whether the development would be a commercial condominium project or consist of another ownership arrangement. (Comment addressed. A note about the building having a single owner and leasable units as well as a west parcel for sale is now noted in the Site Data Table. However, it appears the proposed west parcel would share a driveway and drive aisle(s) with the east parcel; the appropriate easement agreements would need to be submitted for review and approval prior to scheduling a pre-construction meeting).

Master Plan

The Future Land Use Map from the Master Plan designates the subject site in the Planned Business category. All development in Planned Business is required to adhere to strict access management principles in order to minimize traffic conflict and maximize safety throughout the M-59 corridor. Connections to and segments of the Township community-wide pathway system are required as an integral part of all Planned Business development.

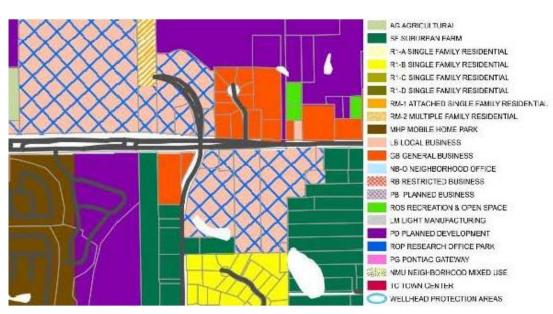
The Future Land Use Map from the draft 2024 Master Plan designates the subject site in the Commercial Corridor category, which is intended to provide regional goods and services (such as large box-stores and drive-thrus) to residents and non-residents.



FUTURE LAND USE MAP

Zoning

Both parcels comprising the subject site are located in the GB (General Business) zoning district, which requires a minimum of 200 feet of lot width and one acre of lot area. Both parcels meet the minimum standards for both lot area and lot width of the GB zoning district. Retail commercial uses are a permitted principal use in the GB zoning district. Beverage and restaurant establishments with drive-thru window service are a special land use in the GB zoning district.



ZONING MAP

Physical Features

There appear to be EGLE (Michigan Department of Environment, Great Lakes, and Energy) regulated wetlands on the site. However, a wetland delineation was not provided. A delineation prepared by a wetland specialist/ecologist must be provided by the Applicant at preliminary site plan. (Comment outstanding. Provide a copy of a delineation report). (Comment addressed. A delineation report dated November 3, 2023 has been provided). EGLE has regulatory authority regarding the wetland boundary location(s) and jurisdictional status of wetlands on this site. Prior to final site plan, wetland boundary verification shall be completed by EGLE. Note the proposed layout may require revision in response to the EGLE review. Based on the submitted plans, the Applicant proposes to grade within the Natural Features Setback. Grading activities should not occur in the Natural Features Setback as the intent is to, as much as possible, leave said area in its natural state. If grading is permitted to occur in the Natural Features Setback, the area must be restored to its natural, undisturbed state. A Natural Features Setback restoration plan is required and must be submitted at final site plan. (Comments remain as notations. These requirements were acknowledged by the Applicant's engineer in the response letter provided to the first and second review).

The following should be conditions of any approval:

- Prior to any construction or grading on the site, the Applicant shall install silt fencing at the upland edge of Natural Features Setbacks / limits of grading. The silt fencing shall be removed after construction once the area is stabilized and vegetation has been established.
- Wetland limits shall be clearly identified with permanent markers. The size, number, location, and language on the markers shall be subject to the approval of the Community Development Director.

Access

The site fronts on Highland Road and Bogie Lake Road. Highland Road (state trunkline) along the subject site is a four-lane divided highway designated as a Principal Arterial on the Township Thoroughfare Plan. Development of the subject site requires the installation of an eight-footwide sidewalk along the Highland Road property frontage (shown on plans; <u>the existing paved</u> <u>shoulder shall be removed and converted to greenbelt</u>). (Comment addressed. The existing paved shoulder along Highland Road will be removed and converted to greenbelt except for the area being used for the right-turn taper). Along the east side of the property the northern portion of Bogie Lake Road is a four-lane road (three lanes going north (two right-turn lanes to eastbound Highland Road, one northbound lane through Highland Road), and one lane going south). There is also an existing right-turn taper at the Bogie Lake Road driveway approach. Bogie Lake Road along the southern portion of the property is a two-lane road.

While the zoning ordinance requires site plans incorporate (where feasible and appropriate) cross-access with neighboring sites, the property to the west is owned by ITC. There is no opportunity for vehicle access through the ITC corridor, so constructing a frontage road to the west is not required.

The zoning ordinance requires a minimum six-foot-wide sidewalk placed one-foot from the inside edge of the right-of-way along the Bogie Lake Road property frontage. The plan shows eight-foot-wide sidewalk and boardwalk (195 linear feet of boardwalk) along Bogie Lake Road property frontage. Direct pedestrian access from the frontage sidewalks to the buildings should be provided. (Comment addressed. Direct pedestrian access is now provided from the sidewalks along Highland Road and Bogie Lake Road). Note it appears the Applicant is proposing to construct offsite sidewalk to the west along Highland Road (whether or not the offsite sidewalk is in the road right-of-way shall be clarified on the plan). Easements would be required from the adjacent property owner to construct offsite sidewalk (if not in the right-of-way). (Comment addressed. Per the design engineer, the sidewalk is located in the right-of-way). The boardwalk details on Sheet 9 conflict with the boardwalk width shown on Sheet 3. Revise for consistency. (Comment addressed. The boardwalk width on Sheet 9 is now shown to be eight-feet-wide). Additionally, some of the sidewalk (boardwalk) along Bogie Lake Road is proposed outside of the right-of-way; the sidewalk (boardwalk) must be relocated inside the road right-of-way or an easement be provided. Right-of-way/easement widths for public walkways when not adjacent to or a part of street rights-of-way must be at least 15 feet and dedicated to the use of the public. Only a 10-footwide sidewalk easement is proposed. Revise accordingly. (Comment addressed. The sidewalk easement has been changed to be 15 feet as required instead of the 10 feet previously proposed). Furthermore, sidewalk shall be constructed to the south property line, or a variance is required from the Zoning Board of Appeals. (Comment addressed. A portion of the sidewalk is now proposed to the south property line (south side of the church driveway).

DLZ reviewed the submitted traffic impact study (TIS) and stated the methodology is in line with standard practices and the findings are supported by the data provided. Additionally, DLZ was in agreement with the conclusions and recommended treatments.

The development would be accessed from a driveway on Highland Road and Bogie Lake Road. <u>Both driveways</u> The Highland Road driveway would require variances from the zoning ordinance access management standards. As a preface to the following comments regarding access management, the Planning Commission should note the zoning ordinance states direct access drives should generally be minimized in number and maximized in separation. Reasonable access is not necessarily the same as direct access. The number of driveways permitted for a site shall be the minimum number necessary to provide safe and efficient access for regular traffic and emergency vehicles.

The minimum distance between a proposed driveway and the nearest intersection shall not be less than 455 feet when the speed limit is greater than or equal to 50 miles per hour (mph). Along the Highland Road frontage the speed limit is 55 mph. The proposed distance of the Highland Road driveway to the Bogie Lake Road intersection is 300 feet. <u>Therefore, a 155-foot variance is required from the Zoning Board of Appeals.</u> (Comment outstanding; however, the Applicant intends to seek a variance from the Zoning Board of Appeals). The minimum distance between a proposed driveway and the nearest intersection shall not be less than 350 feet when the speed limit is 45 miles per hour (mph). Along the Bogie Lake Road frontage, the speed limit is 45 mph. <u>As the driveway is not 350 feet from the intersection, a variance is required from the Zoning Board of Appeals</u>. (Comment rescinded. See response to following comment). Note the dimension of the centerline of the Bogie Lake Road driveway to Highland Road on the site plan. (Comment addressed. A dimension (350.6 feet) has been added to the plan).

Utilities

The project would be served by both the municipal water and sanitary sewer systems. The Township Engineering Consultant will perform an analysis of stormwater, location and capacity of utilities, and grading to ensure compliance with all applicable ordinances as well as the Township Engineering Design Standards.

Staff Analysis – Preliminary Site Plan

The development standards for the GB district require 50-foot front yard setbacks, 20-foot rear yard setbacks, and 15-foot side yard setbacks. <u>The proposed front (east) setback listed in the Site Data table on Sheet 3 is incorrect. Revise accordingly.</u> (Comment addressed. The proposed east setback in the Site Data Table is now shown correctly). <u>General Note 2 on Sheet 7 identifies the west setback as a front yard and not a side yard. Revise accordingly.</u> (Comment addressed. The note has been revised). The maximum building height allowed is 35 feet or two stories, whichever is less. Article 4, Section 17 of the zoning ordinance provides additional standards for drive-in or drive-thru window service, including a front yard setback of 60 feet (see Page 8 of this report regarding this requirement).

Building Architecture and Design

Generally, exterior building materials should be comprised primarily of high quality, durable, low maintenance material, such as masonry, stone, brick, glass, or equivalent materials. Buildings should be completed on all sides with acceptable materials. The proposed building materials for the Culver's are a mix of stone (veneer) and EFIS (exterior insulation finishing system). Canvas awnings are also proposed. The proposed building materials for the multi-tenant building are a mix of brick (veneer), fiber cement siding, and hardie paneling. Metal canopies are also proposed.

While building materials will be reviewed in detail at final site plan, the Applicant should be aware of the Township's architectural character requirements. EFIS, fiber cement siding, and hardie panel are not considered high-quality materials. Seventy (70) percent of all elevations of both buildings should be covered with some combination of brick or stone or glass. (Comment outstanding. The building is unattractive in appearance, and the fiber cement paneling and siding are substandard materials. All sides of the building will be visible from adjacent roads and must be comprised of high-quality materials. Also, a brown/tan/taupe color scheme should be utilized on the building as opposed to dark grey, light grey, and black). (Comment addressed. The building materials have been revised to include almost all brick veneer with a light, medium, and dark brown color scheme). Furthermore, all buildings shall have windows at eve level covering at least 30 percent of the front facade (north and east elevations of the buildings). Calculations for window coverage on the front facades shall be provided on the elevations at final site plan. (Comment remains as a notation. This requirement was acknowledged by the Applicant's engineer in the response letter provided to the first review). While front facade window coverage calculations are not provided at this time, it appears the north elevation meets the 30% requirement. However, the east elevation does not meet the 30% requirement; if the east elevation is not updated to provide the required window coverage, a variance must be requested from the Zoning Board of Appeals. (Glass coverage calculations have been added to the preliminary elevations. The required window coverage is provided on the north elevation, but a variance is required on the east elevation as only 9.27% window coverage is proposed. The required variance has been added to the variance list on Sheet 4 of the plan set).

A sample board of building materials to be displayed at the Planning Commission meeting and elevations in color are required by the zoning ordinance and must be submitted at final site plan. Additionally, the address (street number) locations shall be shown on the building. Six-inch-tall numbers visible from the street shall be required. The address locations are subject to approval of the Fire Marshal. (Comments remain as notations. These requirements were acknowledged by the Applicant's engineer in the response letter provided to the first review).

Outdoor patios are located on the site. Details for the items to be located on the patios and details for the patios' surfacing shall be provided at final site plan. (Comment remains as a notation. This requirement was acknowledged by the Applicant's engineer in the response letter provided to the first review). An ornamental paving treatment should be required by the Planning Commission. The treatment should be something either decorative or something to provide aesthetic quality to the patios. Potential options for ornamental paving treatments include, but are not limited to, CMU pavers; brick; stone; or stamped, stained, and sealed concrete. Accessory items such as railings, benches, trash receptacles, outdoor seating (such as tables and chairs), or sidewalk planters located in the vicinity of sidewalks and/or outdoor seating areas are required to be of commercial quality and complement the building design and style. These details shall be provided at final site plan. (Comment remains as a notation. This requirement was acknowledged by the Applicant's engineer in the response letter provided to the first review).

Landscaping and Screening

Landscaping must comply with the provisions of the zoning ordinance and should be designed to preserve existing significant natural features and to buffer service areas, parking lots, and dumpsters. A mix of evergreen and deciduous plants and trees are preferred, along with seasonal accent plantings. A landscape plan will be provided and reviewed in detail during final site plan if the preliminary site plan is approved. Following are initial comments relative to a landscape plan:

A snow storage plan was not provided. Information on method of snow storage shall be provided at final site plan. Winter maintenance of parking lot landscape islands (insufficient parking lot landscape islands for plant material – variance required from the Zoning Board of Appeals (add to list of variances to be requested on Sheet 4 or demonstrate the required amount of parking lot landscaping can be provided (this can be demonstrated without having a landscape architect prepare a landscape plan)) (Comment addressed at this level of review. Proposed areas for parking lot landscaping have been shown on Sheet 4. Note not all of the proposed areas identified will count as parking lot landscaping; this will be reviewed further when a landscape plan is submitted at final site plan)) shall be required where heavy applications of salt and deicing products occur through the use of salt tarps which minimize soil absorption and ultimately reduce plant disorders. (Comments remain as notations. The response letter provided to the first review states a snow storage plan will be provided at final site plan).

Trash Receptacle Screening

The zoning ordinance requires dumpsters to be surrounded by a six-foot-tall wall on three sides and an obscuring wood gate on a steel frame on the fourth side, located on a six-inch concrete pad extending 10 feet in front of the gate, with six-inch concrete-filled steel bollards to protect the rear wall and gates. Furthermore, the zoning ordinance states dumpsters and trash storage enclosures shall be constructed of the same decorative masonry materials as the buildings to which they are accessory. Brickform concrete (simulated brick pattern) or stained, decorative CMU block are not permitted where the principal building contains masonry. Plain CMU block is also prohibited. A dumpster enclosure detail was provided on Sheet PP-1. (The aforementioned sheet has been renumbered as PP-3 with the second submittal). (The aforementioned sheet has been renumbered as PP-5 with the third submittal).

At the time of trash pick-up, the location of the dumpster enclosure could cause conflict with traffic entering and exiting the site. The dumpster enclosure location should be evaluated when considering circulation around the site. (Comment addressed. One dumpster enclosure has been eliminated and the other dumpster enclosure location has been revised to reduce conflict with traffic).

Parking

The parking calculations in the Site Data table on Sheet 3 are incorrect and shall be revised. (Comment outstanding. When units or measurements determining number of required parking spaces result in fractional space, any fraction up to and including onehalf shall be disregarded and fractions over one-half shall require one parking space). (Comment addressed. Required parking calculations have been updated. See following comments). 54 parking spaces are required for Culver's, not 46. 31 parking spaces are required for the coffee shop, not 19. The fast food standard shall be applied to the coffee shop. (Comment outstanding. Revise accordingly). (Comment addressed. Required parking calculations have been updated. See following comments).-Retail tenant space #1 requires 13-12 parking spaces, not 11-13. Retail tenant spaces #2 and #3 each require nine parking spaces, not seven. Additionally, gross floor area is utilized for fast food and retail uses, not useable floor area. It is unacceptable to remove 15 percent of the floor area from the parking calculations. (Comment addressed). 116 65 77 parking spaces and 8 stacking spaces are required to serve the development and 90 48 61 parking spaces and 16 stacking spaces are proposed; therefore, a 261716-parking space variance is required from the Zoning Board of Appeals. (Revise parking variance note on Sheet 3 accordingly). (Comment addressed. The applicable note on Sheet 4 has been updated).

The Planning Commission should note per the proposed zoning ordinance amendment to the off-street parking requirements, a maximum of 77 parking spaces would be allowed on the site and a minimum of 58 parking spaces would be required. Therefore, with 61 parking spaces proposed, a parking space variance would not be required.

Staff recommends the Planning Commission require the six easterly parking spaces be removed. Traffic circulation at the northeast corner of the site will make these spaces dangerous and difficult to access; vehicles attempting to access these spaces could cause traffic conflicts with vehicles exiting the drive-thru and bypass lane. Additionally, staff suggests the three northwesterly parking spaces be removed. Traffic circulation at the northwest corner of the site will make these spaces dangerous and difficult to access; vehicles attempting to access these spaces could cause traffic conflicts with vehicle ingress/egress from/to the Highland Road driveway and vehicles entering the drive-thru. (Comment outstanding. The nine aforementioned parking spaces remain as previously proposed. A dimension (19 feet) has been added to the back side of the six parking spaces on the east side of the site; this has been noted as an attempt to demonstrate reduced interference from these parking spaces with the bypass lane. Staff continues to recommend revisions to this area of the site plan; see recommendation on Page 15).

Two-way drives are required to be a minimum of 24 feet in width. At the east end of the northerly drive aisle, the proposed width is 22.8 feet. Revise the site plan to increase the width to 24 feet; if not revised, a variance is required from the Zoning Board of Appeals. (Comment addressed. The aforementioned two-way drive aisle has been revised to be 24 feet in width).

The one-way drive (approximately 40 feet in length) north of the Bogie Lake Road driveway shall be removed. (Comment outstanding. See third comment in green in this paragraph). One-way drives are required to be a minimum of 20 feet in width, so the proposed width of 12 feet would require a variance from the Zoning Board of Appeals. (Comment addressed. The one-way drive aisle has been increased to 20 feet in width). However, removing this drive will improve vehicle circulation around the site. Funneling traffic north through said area would conflict with drive-thru and bypass lane traffic (maintaining the bypass lane is important for the efficient and safe function of the drivethru). Also, vehicles attempting to enter the drive-thru from the Bogie Lake Road driveway would also have to traverse west across the drive aisle north of the building where pedestrians are accessing vehicles north of said drive aisle and vehicles on both sides of said drive aisle are entering/exiting the site from the west. **Removing** the aforementioned section of one-way drive aisle will also allow the landscape island in this area to be extended east to the east property line. (Staff concerns remain regarding the internal traffic circulation near the northeast corner of the site. Vehicles backing out of the easternmost parking spaces may have difficulties).

The zoning ordinance requires each individual parking space be delineated by dual stripes, two feet apart centered on the dividing lines and painted white. Revise the site plan and the typical parking space detail on Sheet 3. If the required striping is not provided, a variance is required from the Zoning Board of Appeals. (Comment addressed. The plans as well as the parking space detail on Sheet 3 (now Sheet 4) now show white dual striping).

All dimensions for drive widths and parking space depth shall be revised. The site plan measures drive widths to the face of curb; road measurement surface is taken between the edges of the gutter pan (drive width shall be provided between the edges of the gutter pan). (Comment partially addressed. There are still some drive aisles/maneuvering lanes with width measured to the curb, not the edge of the gutter pan. Revise accordingly). (Comment addressed. The measurements have been revised accordingly). Furthermore, gutter pan shall not be included in the measurement of parking space depth. Revise the site plan and the typical parking space detail on Sheet 3. (Comment partially addressed. Sheet 3 shows 18-foot-deep parking spaces in some areas of the site while other spaces are 17-feet in depth. Gutter pan is also being counted as width in parking space detail now shows the space length to be 17-feet and matching what is proposed on the site plan, and the space measurements have been revised accordingly).

<u>The typical parking space detail shows spaces 18 feet in length and the site plan shows the spaces 17 feet in length. Revise for consistency.</u> (See previous comment. While the typical parking space detail shows parking spaces 17 feet in depth, the plan shows 18-feet-deep spaces in some areas). (Comment addressed. See previous comment).

While provided on the typical angled parking space detail, label the length and width dimensions of the angled parking on the site plan. (Comment rescinded. Angled parking is no longer proposed).

The sidewalk north of the southernmost parking spaces shall be increased to seven feet in width to be eligible for 17-foot-deep parking spaces abutting the aforementioned sidewalk. Otherwise, 18-foot-deep parking spaces shall be required. (Comment outstanding. Clarification is required. While in the response letter provided to the second review the Applicant's engineer stated the sidewalk width has been increased to seven feet in width, on Sheet 4 there is a 6.5-foot dimension label appearing to indicate the width of said sidewalk). (Comment addressed. The dimension has been revised and now shows the full seven-foot width). Label the parking space depth and width, width of the sidewalk north of the spaces, and width of the sidewalk west of the spaces. (Comment partially addressed. Parking space depth and width have been added, but the sidewalk width west of the spaces is not labeled and the width of the sidewalk north of the spaces is unclear (see previous comment)). (Comment addressed. Additional sidewalk width dimensions have been added to the site plan). Additionally, staff recommends the 10 southernmost parking spaces be restricted to employee parking and designated/marked accordingly. (Comment partially addressed. The number of parking spaces south of the building has increased to 24. Staff continues to suggest the southernmost spaces (12) be restricted to employee parking and designated/marked accordingly. While in the response letter provided to the second review the Applicant's engineer stated they acknowledge this recommendation, a note stating such could not be located by staff on Sheet 4). (Comment addressed. Site Plan Note 4 has been added to Sheet 4 of the plan set).

For the proposed drive-thrus, eight vehicle stacking spaces inclusive of the vehicle at the window are required. The site plan shall show nine-foot-wide and 18-foot-long stacking spaces, and the parking calculations in the Site Data table on Sheet 3 shall be revised to show the required and proposed stacking spaces. (Comment addressed. The Site Data Table now shows the correct number of required and proposed stacking spaces).

Off-Street Loading Requirements

The zoning ordinance requires-two one loading spaces for a development of this size-(one for each building). Such loading and unloading spaces must be an area 10 feet by 50 feet, with a 15-foot height clearance. No loading spaces are proposed, so a variance is required from the Zoning Board of Appeals. (Comment partially addressed. A loading space is now provided northeast of the proposed dumpster enclosure (label the length and width); however, staff agrees with DLZ regarding the location presenting conflict with traffic entering and exiting the site from Bogie Lake Road). (Comment addressed. The loading space north of the proposed dumpster is now shown outside of the drive aisle).

Signs

The zoning ordinance requires the area, quantity, location, and dimensions of all signs to be provided with the preliminary site plan. The site plan shows the location of two one monument signs, each with a 10-foot setback from the Highland Road and Bogie Lake Road rights-of-way. (The proposed sign area of the monument sign is 125 square feet, which exceeds the allowed sign area by 65 square feet and would require a variance from the Zoning Board of Appeals (a note on Sheet 4 incorrectly states the allowed sign area is 65 square feet when the allowed sign area is 60 square feet based on the proposed sign setback; revise accordingly). (Comment addressed. The monument sign has been revised with additional setback and reduced sign area to comply with the zoning ordinance). Freestanding signs on parcels containing a multi-tenant building in the GB zoning district are allowed six square feet of sign area for each one foot of setback, up to a maximum of 150 square feet in area (with a 25-foot setback)). (The Applicant will be requesting a variance for sign area (has been added to the list of variances to be requested on Sheet 4)). (Comment rescinded. See previous comment in green in this paragraph). In instances where a parcel has frontage on two thoroughfares, a second freestanding sign may be permitted along the secondary thoroughfare. This provision is contingent upon the second sign being no more than 50 percent of the size permitted the first sign, a minimum 150 feet of separation exists between any freestanding signs on the site, and all other setback requirements are met. Sheet PP-1 shows a detail labeled "existing pylon sign." There is no existing pylon sign on the site. (The aforementioned sheet has been renumbered as PP-3 with the second submittal). Furthermore, the zoning ordinance prohibits pylon signs. Remove the aforementioned detail from the plan set. (Comment addressed. The aforementioned detail has been removed). Any proposed freestanding sign must be of the monument type (which is indicated on Sheet 3 of the site plan). While monument sign details were not provided (a detail is now provided on Sheet PP-3) (the aforementioned sheet has been renumbered as PP-4 with the third submittal) (the aforementioned sheet has been renumbered as PP-5 with the third submittal), staff can administratively review and approve signage. Any/all signage would be required to comply with the zoning ordinance.

The Culver's building elevations show three wall signs (one on every façade except the south elevation). In instances where a parcel has frontage on two streets, an additional wall sign may be permitted on the building facing the secondary thoroughfare, which is no greater than five percent of the wall area on which the sign is placed. Where permitted, wall signs must be located flat against the building's front façade or parallel to the front façade on a canopy. <u>The wall sign on the west elevation shall be removed, or a variance is required from the Zoning Board of Appeals.</u> Additionally, wall signs cannot extend above the roofline of a building. <u>Variances are required to install wall signs above the roofline of the building.</u> Staff does not support any variances for signage. <u>The building elevations should be revised to comply with the sign standards.</u> Note signage is not permitted on the awnings. (These comments are no longer applicable as the Culver's building is no longer being proposed on this site).

The multi-tenant (four tenants) retail and coffee shop building elevations show wall signs on every facade, except the south elevation. In the case of a building with two or more tenants, one wall sign is permitted per tenant. In instances where a parcel has frontage on two streets, an additional wall sign may be permitted on the building facing the secondary thoroughfare, which is no greater than five percent of the wall area on which the sign is placed. The wall sign on the west elevation shall be removed, or a variance is required from the Zoning Board of Appeals. (Comment outstanding). (The Applicant will be seeking a variance for this wall sign (has been added to the list of variances to be requested on Sheet 4)). (Comment rescinded. The wall sign on the west elevation has been removed). Additionally, wall signs cannot extend above the roofline of a building. Variances are required to install wall signs above the roofline of the building. (Comment outstanding). (The Applicant will be seeking a variance for the placement of walls signs (has been added to the list of variances to be requested on Sheet 4)). (Comment rescinded. The wall signs on the north elevation have been removed. The response letter provided to the third review stated until tenants are known sign placement is unknown, and sign permits will be sought as tenants are selected). Staff does not support any variances for signage. The building elevations should be revised to comply with the sign standards. (Comment remains as a notation). Note signage is not permitted on the canopies.

Outdoor Lighting

Site lighting is required to comply with the zoning ordinance. Information on site lighting will be provided and reviewed in detail during final site plan. While the building elevations show wall-mounted lighting, outdoor lighting is reviewed and approved via a photometric plan and required attachments. <u>All luminaries shall be removed from existing sheets in the plan set.</u> (Comment outstanding. Note the type of wall-mounted sconce lighting (appears to be outward, unshielded lighting) shown on the preliminary elevations is not permitted in the Township and would require a variance from the Zoning Board of Appeals). (Comment rescinded. The sconce lighting has been removed from the plans. A photometric plan indicating light sources and styles will be provided at final site plan).

Staff Analysis – Special Land Use (Drive-thru)

Special land uses for drive-thrus are evaluated using the general standards for all special land uses listed in Article 6, Section 10 of the zoning ordinance and the following specific standards for outdoor dining found in Article 4, Section 17 of the zoning ordinance:

A. A front yard setback of at least sixty (60) *feet shall be required.*

The coffee shop drive-thru tenant space is only 50 feet from the Bogie Lake Road right-of-way. However, the drive-thru window is over 60 feet from the Bogie Lake Road right-of-way. <u>The</u> <u>Applicant may request the Zoning Board of Appeals make an interpretation allowing the</u> <u>setback as proposed being conforming to the 60-foot front yard setback.</u> (Comment outstanding; however, the Applicant intends to seek an interpretation/variance from the Zoning Board of Appeals). The Culver's building is conforming.

B. Entrance and exit drives shall be at least one hundred (100) feet from any street intersection and two hundred (200) feet from any residential district.

The Highland Road driveway is not 200 feet from the residential zoning district to the west. <u>Therefore, a variance is required from the Zoning Board of Appeals.</u> (Comment outstanding; however, the Applicant intends to seek a variance from the Zoning Board of Appeals). The Bogie Lake Road driveway is compliant.

C. An outdoor lighting plan shall specify the type of fixtures to be used, light intensity, and method of shielding the fixtures so that light does not project onto adjoining properties or on any public or private street or right-of-way. Dropped fixtures shall not be allowed. The site plan shall include a photometric plan and catalog details for all proposed fixtures. Outdoor lights must meet the performance standards of Section 5.18.

Site lighting is required to comply with the zoning ordinance. Information on site lighting will be provided and reviewed in detail during final site plan.

Staff Analysis – Special Land Use (Outdoor Dining)

Special land uses for outdoor dining are evaluated using the general standards for all special land uses listed in Article 6, Section 10 of the zoning ordinance and the following specific standards for outdoor dining found in Article 4, Section 18 of the zoning ordinance:

- A. The Planning Commission shall determine that the use is designed and will be operated so as not to create a nuisance to property owners adjacent to or nearby the eating establishment. As such, the proposed use shall meet the following minimum criteria:
 - *i. The establishment may operate only during the following hours:*
 - Monday thru Thursday: 8:00 a.m. 12:00 midnight
 - Friday: 8:00 a.m. 2:00 a.m.
 - Saturday: 10:00 a.m. 2:00 a.m.
 - Sunday: 10:00 a.m. 10:00 p.m.

Culver's and tThe coffee shop would be required to adhere to said hours of operation. (Revise Site Plan Note 3 on Sheet 3. The hours of operation pertain to the outdoor dining hours, not hours of operation for the coffee shop). (Comment addressed. The note on Sheet 4 has been updated accordingly).

- ii. The use of exterior loudspeakers is prohibited where the site abuts a residential district or use. The noise level at the lot line shall not exceed 70 dB.
 Culver's and tThe coffee shop would be required to adhere to said performance standard.
- An outdoor lighting plan shall specify the type of fixtures to be used, light intensity, and method of shielding the fixtures so that light does not project onto adjoining properties or on any public or private street or right-of-way. Dropped fixtures shall not be allowed. The site plan shall include a photometric plan and catalog details for all proposed fixtures. Outdoor lights must meet the performance standards of Section 5.18.

Site lighting is required to comply with the zoning ordinance. Information on site lighting will be provided and reviewed in detail during final site plan.

- **B.** Additional parking spaces must be provided according to the following:
 - i. Outdoor dining areas for more than 30 people or which include either permanent or seasonal structures, such as awning, roofs, or canopies, may be required to provide additional parking according to the following:
 - a. If the outdoor seating is 25% of the indoor seating or less, no additional parking is necessary.
 - b. If the outdoor seating is 26%-50% of the indoor seating, the restaurant may be required to provide up to 125% of the parking required for the indoor space.
 - c. If the outdoor seating is over 50% of the indoor seating capacity, the restaurant may be required to provide up to 150% of the parking required for the indoor space.

According to the site plan, a 656 square foot patio is proposed on the northeast corner of the Culver's building and a 253 232 square foot patio is proposed on the northeast corner of the retail and coffee shop building. From an occupancy perspective, the Building Code states assembly without fixed seating – unconcentrated (tables and chairs) is F15 square feet per person. Maximum patio occupancy is subject to approval of the Building Official. The site plan shows seating for 16 patrons on the Culver's patio (four, four-top tables). Based on a restaurant dining room with 80 seats, the outdoor seating does not warrant additional parking. The site plan shows seating for eight patrons on the coffee shop patio (two, four-top tables). The submitted floor plan does not show the coffee shop seating capacity; however, the tenant space would be limited to 32 seats in order to not warrant additional parking to serve the outdoor seating. (Per the design engineer, the outdoor seating is less than 25% of the indoor seating. Therefore, no additional parking is required).

Planning Commission Options / Recommendation

The Planning Commission may recommend approval, approval with conditions, or denial of the preliminary site plan to the Township Board; action on the special land use is determined by the Planning Commission. <u>Staff recommends the plans be revised and resubmitted to address</u> the items identified in this memorandum. An updated list of any requested variances shall also be provided. The majority of staff comments have been addressed. While there are variances required, the plan demonstrates land use feasibility. Concerns remain regarding the internal traffic circulation, especially near the northeast corner of the site. At a minimum the southerly three parking spaces of the easternmost six parking spaces should be removed; doing so would also allow the direct pedestrian access to the building from the frontage sidewalk along Bogie Lake Road to be shifted north. As proposed, the location of the pedestrian access is a safety concern as it crosses the bypass lane just north of the drive-thru window. Eliminating the three aforementioned parking spaces and shifting the pedestrian access north would provide separation from vehicles at the drive-thru window.

The following plans were reviewed:

- Plans prepared by Boss Engineering dated January 5, 2023 (revision date-September 8, 2023 January 12February 28, 2024). The utility, grading, and drainage plans for the site are subject to the approval of the Township Engineering Consultant and shall be completed in accordance with the Township Engineering Design Standards. <u>Note 2 on Sheet 1 shall be removed (the zoning ordinance requires plans be to scale).</u> (Comment addressed. The note has been removed).
- Preliminary floor plan and elevations prepared by Detroit Architectural Group dated January <u>4Septembeer 6November 15, 2023</u>February 28, 2024. <u>These plans shall be sealed by the</u> <u>Registered Architect who prepared the plans.</u> (Comment addressed. The aforementioned plan sheets have been sealed).
- Floor plan and exterior elevations prepared by AMAG dated May 15, 2020 (revision date May 28, 2020). <u>These plans shall be sealed by the Registered Architect who prepared the plans.</u> (Comment rescinded. This comment is no longer applicable as the west building is no longer being proposed).



March 27, 2024

Sean O' Neil Community Development Department Charter Township of White Lake 7525 Highland Road White Lake, Michigan 48383

RE: Gateway Crossing- Preliminary Site Plan Review – 4th Review

Ref: DLZ No. 2345-7567-01

Design Professional: Boss Engineering

Dear Mr. O' Neil,

Our office has performed a Preliminary Site Plan review for the above-mentioned plan dated February 28, 2024. The plans were reviewed for feasibility based on general conformance with the Township Engineering Design Standards.

General Site Information

This site is located at the southwest corner of M-59 and Bogie Lake Road. Total site acreage is approximately 5.36 acres.

Site Improvement Information:

- Construction of a retail and coffee shop building (8,620 sq.ft.) with associated parking, including ADA parking.
- Site to be serviced by proposed water main and sanitary sewer.
- Storm water runoff is proposed to be routed via storm sewer to and detained underground located south of the proposed building.

The following items should be noted with respect to Planning Commission review:

Note that comments from our previous review dated February 13,2024 are in *italics*. Responses to those comments are in **bold**. New comments are in standard font.

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- a) Provide wetland delineation report. In addition, a wetland permit from EGLE will be required due to the construction of the boardwalk within the wetlands and wetland buffer and due to the proximity of site construction in general to the wetlands. Comment outstanding. Although a delineation has been provided, our office requests a copy of the wetland report. Comment addressed. A copy of the wetland report has now been provided. A wetland boundary verification shall be done by EGLE.
 Comment remains as a notation regarding EGLE wetland boundary verification and EGLE wetland permit requirement.
- b) We defer to the Township Fire Department regarding hydrant spacing/coverage. Comment remains.
- c) Show the location/continuation of the existing sanitary sewer to the south relative to the location of the proposed boardwalk. It appears that construction of the boardwalk may impact the existing sewer and that construction of the boardwalk may be in an existing sanitary sewer easement. Permission from the Township would be required for construction within the easement. Comment remains as a notation. The existing sanitary sewer is now shown. Per the design engineer response, the property owner acknowledges that permission from the Township will be required for work within the sanitary sewer easement.
- d) Provide fire truck turning plan to demonstrate adequate turning radii for fire trucks, please use a 40 foot long vehicle for the analysis. Comment addressed. A truck turning plan has been provided. We note that fire truck clearance will be tight in the area of the dumpster location. Per the current submittal, we now note that the fire truck clearance in the vicinity of the proposed dumpster location appears to be improved from the previous plan submittal. Comment remains as a notation.
- e) The proposed watermain stub to the west shall end with a blow off assembly or hydrant. Comment addressed. A GV&W as well as a temporary blowoff assembly have now been provided at the stub.
- f) The drive width near the northeastern portion of parking now shows a width less than the required 24'. Is the intent for the parking area in the NE corner to only be accessed from the south? (i.e. one way). In addition, the drive width near the SE area of the site has been reduced from 15' to 12'. Is one way circulation the intent? Current zoning standards for drives require one way circulation drives to be a minimum of 20' width and two way to be 24'. There are also circulation concerns relative to the 6 parking spaces near the NE corner of the site. We defer to the Township regarding these items. Comment addressed. The two way drive width near the southeastern area of the site is now shown as 20' wide. Both drive widths now meet ordinance requirements. We continue to defer to the Township regarding the internal traffic circulation concerns near the northeastern corner of the site. We do note that dimension (19.0') was added to the back side of the six parking spaces on



the east side to demonstrate reduction in interference from these parking spaces with the drive thru lane.

- g) We note that OCWRC Sanitary Sewer Details have been included in the plan submittal but are unnecessary as the White Lake details are what apply to this site. Comment addressed. OCWRC sanitary sewer details have been removed from the plan set.
- h) Sheet 9-Basin Summary- Basin size provided (26,207 cu. ft.) should be 27,646 cu.ft. based on DHWL. Comment addressed. The basin size provided has now been revised to that based on the DHWL.

Recommendation

The plan now demonstrates feasibility from an engineering perspective. We defer to the Township regarding the remainder of comment f) above.

Please feel free to contact our office should you have any questions.

Sincerely,

DLZ Michigan

M fear

Michael Leuffgen, P.E. Department Manager

Encl. None

Un fourfles

Victoria Loemker, P.E. Senior Engineer

Cc: Justin Quagliata, Community Development, via email Hannah Kennedy-Galley, Community Development, via email Aaron Potter, DPS Director, White Lake Township, via email Jason Hanifen, Fire Marshall, White Lake Township, via email

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January 19, 2023

Sean O'Neil, Director Community Development Department Charter Township of White Lake 7525 Highland Road White Lake, Michigan 48383

Re: Gateway Crossing Development TIS Memorandum Response

Ref: DLZ File No. 2345-7567-01

Date of Memo: 1/3/23

Design Professional: Jacob Swanson, PE and Kyle Paulson; Fleis & VandenBrink

The applicant has submitted a Traffic Impact Study (TIS) for the Gateway Crossings Development located in the southwest quadrant of the Bogie Lake Road and Highland Road (M-59) intersection. The proposed development in the TIS includes 6,031 square feet of retail, 4,060 square feet of restaurant with a drive- through, and 2,289 square feet of coffee shop with a drive-through. The TIS utilized turning movement traffic counts at the Bogie Lake Road and Highland Road (M-59) and WB-EB Crossover (west of Bogie Lake Road), WB Highland Road (M-59) & Nordic Drive / EB-WB Crossover (east of Bogie Lake Road), and the SB Bogie Lake Road and NB-SB Crossover (north of Highland Road (M-59)) on Thursday, November 3, 2022.

DLZ has reviewed the analysis; the methodology is in line with standard practices, and the findings are supported by the data provided. Based on data from the Shopping Plaza and Fast Food with Drive-Through sections of the 11th edition of the "ITE Trip Generation Manual", the additional daily trips are 2,835 trips per day. Additionally, 109 AM Peak Hour trips per day and 111 PM Peak Hour trips per day are anticipated to be added to the existing traffic volumes. Based on the White Lake Zoning Ordinance, the number of daily trips generated by the site is above the minimum threshold for requiring a Traffic Impact Study (750+ daily trips).

The TIS evaluated the existing traffic conditions at each intersection, the future background conditions (existing conditions with natural traffic volume growth) at each intersection and the future conditions at each intersection with the full proposed build-out of the site. The TIS data indicates that with traffic signal optimization, each intersection will operate in a similar manner to the future background condition. It also shows that no traffic movements will operate below a level of service (LOS) of "D", with the exception of the southbound right turn movement, which will continue to operate a LOS of "E".

The future traffic conditions were also evaluated at proposed site drives along both Bogie Lake Road and Highland Road (M-59). During both the AM and PM peak hours, the site drives operate with all turning movements at a LOS of "C" or greater.

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White Lake Plaza Traffic Impact Study Review Page 2 of 2

The TIS also evaluated the need for turn lanes or tapers at the proposed site driveways based on MDOT and Road Commission for Oakland County (RCOC). Based on the trip generation peak hour's traffic, it was determined that a right turn lane is warranted at the site driveway along Highland Road (M-59), but no treatment is required at the site driveway along Bogie Lake Road. However, while the TIS indicates a right turn taper is not warranted along Bogie There appears to be an existing right turn taper at the Bogie Lake Road site drive location, but the owner should evaluate the existing right turn taper to ensure it meets current RCOC dimensional requirements. RCOC and MDOT ROW permits will be required prior to construction.

As previously stated, we are in agreement with the conclusions and recommended treatments, with the exception of the right turn taper on Bogie Lake Road.

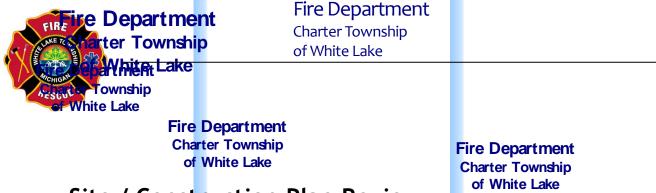
If you have any questions, please feel free to contact to me.

Respectfully, DLZ Michigan, Inc.

[Moniel -

Leigh Merrill, P.E. Project Manager

Cc: Michael Leuffgen, P.E., DLZ via email Craig Burnside, Community Development via e-mail



Site / Construction Plan Review

To: Sean O'Neil, Planning Department Director

Date: 03/26/2024

Project: Gateway Crossing

Job #: 22-029-1

Date on Plans: 02/28/2024

The Fire Department has the following comments with regards to the 4th review of preliminary site plans for the project known as Gateway Crossing

The Fire Department has no further comments at this time.

Jason Hanifen Fire Marshal Charter Township of White Lake (248)698-3993 jhanifen@whitelaketwp.com

Plans are reviewed using the International Fire Code (IFC), 2015 Edition and Referenced NFPA Standards.

CHARTER TOWNSHIP OF WHITE LAKE **SITE PLAN REVIEW APPLICATION** Community Development Department, 7525 Highland Road, White Lake, Michigan 48383 (248) 698-3300 x5

APPLICANT AND PROPERTY INFORMATION				
Applicant: Najor Companies, Brian Najor				
Phone: 248-433-7000 / 248-703-8900 Email Address: brian@najorcompanies.com				
Address: 600 N. Old Woodward, Suite 100 Birmingham, MI 48009				
(Street) (City) (State) (Zip)				
Applicant's Legal Interest in Property: Owner				
Property Owner: Same as above Phone:				
Address:				
Project Name: Gateway Commons Parcel I.D. No.:				
Proposed Use: General Business				
Existing Use: Vacant Parcel Size: 4.79 AC & 1.07 AC Floor Area / No. of Units				
TYPE OF DEVELOPMENT				
Subdivision Site Condominium Commercial				
Multiple Family Special Land Use Industrial				
Adult Entertainment				
SITE PLAN SUBMITTAL CHECKLIST				
T₩0 □ PDF File and One Paper Copy (sealed and no larger than 24x36)				
Application Review Fees (to be calculated by the Community Development Department)				
* PLANS WILL NOT BE ACCEPTED UNLESS FOLDED *				
m				
REQUIRED SIGNATURES				
(Signature of Property Owner) (Date)				
(Signature of Applicant) (Date)				
SIGNATURES TO BE VERIFIED BY THE TOWNSHIP				

WETLAND DELINEATION FOR:



Owner: Gateway Crossing, LLC 600 North Old Woodward, Suite 101 Birmingham, MI 48009 Contact: Brian Najor Email: brian@najorcompanies.com Phone: 248-433-7000

Prepared By:



3121 E. Grand River Howell, MI 48843 517.546.4836 fax 517.548.1670 www.bosseng.com

Contact: Patrick Cleary, PLA - Landscape Architect

November 3, 2023

Gateway Crossing Highland Road and Bogie Lake Road White Lake Township, Oakland County, MI

I. Summary

A wetland delineation was conducted at the property (parcel #'s 12-20-402-003 & 12-20-426-003) in White Lake, MI. The site location is shown in the map figure at left. The study area is on the west parcel (12-20-402-003). The study area was currently undeveloped but disturbed. There was evidence of previous development at the top of slope that defined the north/northwest borders of the wetland, a constructed driveway along the south, and a mowed field along the west / southwest border of the wetland. The purpose of the delineation was to determine existing conditions and establish development limits.

Report Index:

- I. Summary
- II. Wetland Description
- III. Reference Maps
- IV. Representative Photos
- V. Drawing / Boundary Map (excerpt)
- VI. Data Sheets

As part of the work the following information was reviewed and is included in this report:

- National Wetland Inventory (NWI) Map 1
- USDA NRCS Soil Survey Map 2
- Aerial Maps / Photos

A site visit was conducted on June 3, 2022, and the wetland flagged. Further documentation was collected during a second site visit on November 3, 2023. Conditions were drier than normal during the initial visit and considered normal for the season during the second visit but there was no change to the wetland boundary.

The site investigation substantiated the Palustrine environment and also determined a a likely Riverine condition that runs northwest to southeast through the western corner of the site, the entire area included in an area determined to be a wetland. The delineation was completed in accordance with the 1987 U.S. Army Corps of Engineers (USACOE) Wetland Delineation Manual, the Regional Supplement for the Midwest Region August 2010, and USACOE MI State Plan List 2018. Wetlands were determined by the soil, vegetation and hydrology criteria that have been established by the USACOE - and adopted by the Michigan Department of Environment, Great Lakes and Energy (EGLE).

There are larger Palustrine wetlands directly west of the study area as shown on the NWI map excerpt (Map 1) that most likely include more than 5- acres. This size of connected wetlands along with the potential Riverine environment indicates that this wetland would be regulated by EGLE. EGLE is the final arbiter for wetland determinations in the state (non-coastal) and it is recommended that they be consulted for an official determination if any wetland impact is contemplated.

The White Lake Township Zoning Ordinance contains provisions for natural features including wetlands. Section 3.11 (Q) states "*No building or structure shall be located closer than 25-feet to any regulated wetland, submerged land, watercourse, pond, stream, lake or like body of water. The setback shall be measured from the edge of the established wetland boundary as reviewed and approved by the Township.*" This setback is shown and noted on the Wetland Boundary Map in Section V of this report. This setback should be taken into account with any development scenario.

II. Wetland Descriptions

Two wetlands were flagged in the field. Wetland 'A' with three transects, A1 to A3 and Wetland 'B' with two transects, B1 and B2. Wetland 'A' is the primary depressional area that includes approximately 1.33 acres on site, and substantially more off-site. Wetland 'B' can be described as essentially a left over 'hole' from some previous construction activity with steep 3:1 or steeper sides, rounded shape (+-15-ft x 30-ft) and a flat bottom, in total measuring only approximately 375 sq ft. However, due to its configuration it does not appear to drain well and therefore exhibits wetland characteristics.

Wetland 'A': This wetland is a well-defined depression. Near the northwest corner of the site, it is at the bottom of a steep constructed fill slope located near the west property line and continues south and then east towards Bogie Lake Road. At the east side, bordering the road, and then along its south side it appears to be a more natural depression with flatter bank slopes (5-8%). The sampling points were taken at the first at the steep fill slope at the west side of the site (northeast area of the wetland), further east where there was a change in vegetation, and then along the south side of the wetland where it appeared as a more natural depression with shallower slopes and another change in vegetation.

TRANSECT A1:

This transect was taken near the northern end of the site and wetland, near the west property line, along a steep (3:1) embankment probably fill embankment (See 'Wetland Boundary Map' for specific location.)

<u>Soils & Hydrology:</u> Upland soils were a 10YR 5/3 loamy sand to sand, possible fill, although the color was consistent with Oakland County NRCS description of 18B Fox Sandy Loam at depths greater than 9-inches. The upland sample was taken near the toe of the slope with a 10YR 4/1 loamy clay transition at 11-inches, consistent with the soil color and texture further downslope at the wetland edge. Due to the sandy texture the soil was quite dry. Down slope to the wetland edge soil saturation and standing water occurred before hydric soil indicators were prominent – a 10YR 4/1 silty/loamy clay. Approximately 8-10 further downslope it became a much more defined Houghton/Adrian Muck with 10YR 2/1 color and mucky texture. The boundary was confirmed where the hydrology & hydric soil characteristics agreed, meeting the 'F1' Loamy Mucky Mineral criteria, and consistent with the 6-2-22 site visit flagging.

<u>Vegetation:</u> The vegetation going up the slope was a mixture of invasives & lawn-type grasses. There was a quick transition from a near monoculture of Phragmites to a near monoculture of Goldenrod (Solidago canadensis) then more Autumn Olive (Elaeagnus umbellate) and Cottonwood (Populus) further up to the top of the slope along with an increasing density of lawntype grasses (Festuca & Poa). At the wetland edge, at the transect, there was a large clump of Willow (Salix alba) along with smaller amounts of Green Ash (Saplings only), Red and Gray Dogwoods (Cornus alba / sericea & racemosa). Just above the wetland edge the general area was dominated by Phragmites for approximately 15-20-ft up slope.

TRANSECT A2:

This transect was taken further east through the toe of a less steep slope (10-15%+-) primarily where was a change in the vegetation mix. (See 'Wetland Boundary Map' for specific location.)

<u>Soils & Hydrology:</u> Upland soils were consistent with Transect A1-1 with a 10YR 5/3 color, sandy texture, and dry condition. At the wetland edge the same soil and hydrologic conditions continued with an approximately 6-8-inch layer of 10YR 4/1 silty/loamy clay between the 10YR 2/1 Muck and the 10YR 5/3 Loamy Sand above, again meeting the 'F1' hydric soil indicator.

<u>Vegetation:</u> The vegetation at this transect generally became more woody with more in the tree stratum dominated by Cottonwood of varying sizes, and Russian Olive. The herbaceous layer was still dominated by Phragmites at the wetland edge, then Goldenrod, and lawn-type grasses further up slope, but then Crown Vetch became much more prevalent near and the top of the slope.

TRANSECT A3:

This transect was taken along the south side of the wetland with more moderate boundary slopes (5-8%). Although dominated by invasives this boundary appeared to be more natural and less disturbed (See 'Wetland Boundary Map' for specific location.)

<u>Soils & Hydrology:</u> Upland soils were similar to the previous transects with a 10YR 5/2 color, sandy texture, and dry condition. At the wetland edge, however, it continued sandy but darker at 10YR 3/1 with soil saturation (approximately 10-15-ft further downslope soil was inundated). The 11-inches of 10YR 3/1 met the Dark Surface (S7) hydric soil indicator. Other hydrologic evidence included water-stained leaves and geomorphic position. Generally the entire wetland – saturation if not inundation was evident on aerial images going back 20-years or more.

<u>Vegetation:</u> The vegetation at this transect generally became more scrubby /woody with more in the tree stratum dominated by Boxelder (Acer negundo) along with the Cottonwood and Green Ash. Vines became dominant – Riverbank Grape (Vitis riparia) along with Blackberry (Rubus occidentalis). The herbaceous layer was still dominated by Phragmites at the wetland edge, but with scattered Sedges (Carex lacustris) then much more Buckthorn and Honeysuckle (Lonicera japonica) scattered Gray Dogwood, and several prominent clumps of Sumac (Rhus typhina) nearer the road.

Wetland 'B' Adjacent to Wetland Flags 'A13' & 'A14', separated by a ridge/mound there was a small (+-375 sq ft) 'hole', most likely left over from some previous construction. Highly disturbed, irregularly rounded in shape and with steep 3:1 plus side slopes. This area is the result of construction, and its 'borderline' wetland status may need further confirmation by EGLE.

<u>TRANSECT B1:</u> One transect was taken for this wetland including representative upland conditions data sheet and a sampling wetland data sheet near the middle of the flat bottom to document existing conditions.

<u>Soils & Hydrology</u>: Soils around the 'hole' and in it are the same 10YR 5/3 sandy soils as other upland areas on the site, including the flat bottom of this area. Except a hardpan was encountered at 8-inches precluding further determination of the soil conditions. Hydrologically, however, it was sparsely vegetated (B8), contained water-stained leaves (B9) and met the conditions of Geomorphic Position (D2). The encountered hardpan may be precluding adequate drainage.

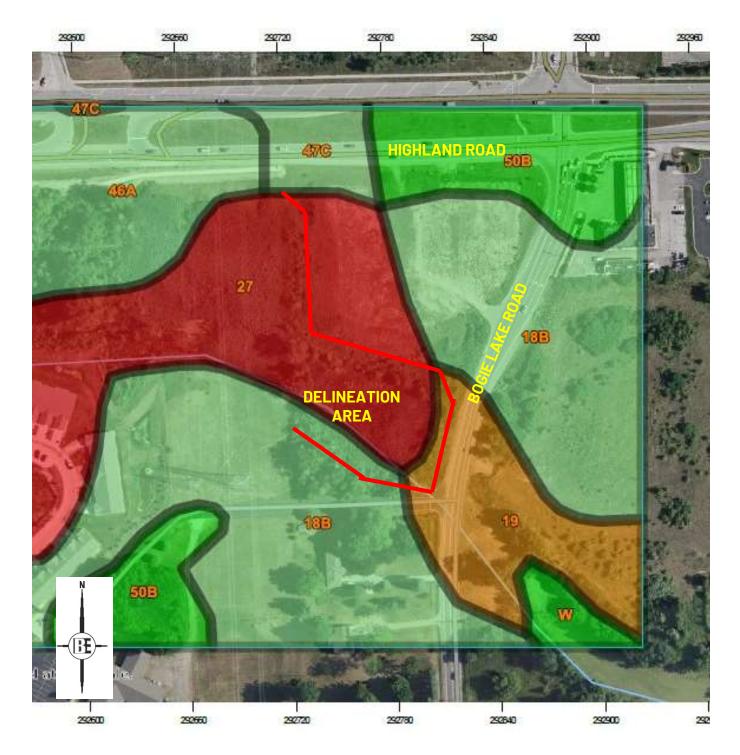
<u>Vegetation:</u> The vegetation could be discounted as inside the hole it was dominated by volunteer invasives Buckthorn, Phragmites, Boxelder, but also Riverbank Grape and some Green Ash to meet the FAC neutral test criteria. Outside was more of the same but also with Sumac supporting the dry surrounding conditions.

III. Reference Maps



MAP 1 – National Wetland Inventory (NWI) Map

Hydric Rating by Map Unit—Oakland County, Michigan (22-029_Hyrdic Soils)



MAP 2 – USDA NRCS Hydric Soils Map

Hydric Rating by Map Unit

Map unit symbol	Map unit name	Rating	Acres In AOI	Percent of AOI
168	Fox sandy loam, till plain, 2 to 6 percent slopes	4	11.3	39.6%
19	Sebewa loam, disintegration moraine, 0 to 2 percent slopes	94	2.7	9.4%
27	Houghton and Adrian mucks	100	6.3	22.2%
46A	Dixboro loamy fine sand, 0 to 3 percent slopes	7	3.2	11.2%
47C	Fox-Riddles sandy loams, 6 to 12 percent slopes	3	0.8	3.0%
50B	Udipsamments, undulating	0	3.7	12.9%
w	Water	0	0.5	1.7%
Totals for Area of Inter	est		28.4	100.0%

Area of Interest (AOI) Transportation Area of Interest (AOI) +++ Rails Soils Interstate Highways ~ Soil Rating Polygons ~ US Routes Hydric (100%) \approx Major Roads Hydric (66 to 99%) Local Roads \sim Hydric (33 to 65%) Background Hydric (1 to 32%) Aerial Photography Man Not Hydric (0%) Not rated or not available Soil Rating Lines Hydric (100%) Hydric (66 to 99%) Hydric (33 to 65%) Hydric (1 to 32%) Not Hydric (0%) Not rated or not available Soil Rating Points Hydric (100%) Hydric (66 to 99%) Hydric (33 to 65%) Hydric (1 to 32%) Not Hydric (0%) Not rated or not available Water Features Streams and Canals \sim

MAP LEGEND

IV. Site Photos



PHOTO 1 – Near Northwest Corner, At Toe of Steep Slope – Looking West



PHOTO 2 – Southeast Side, Near Culvert Crossing – Looking North

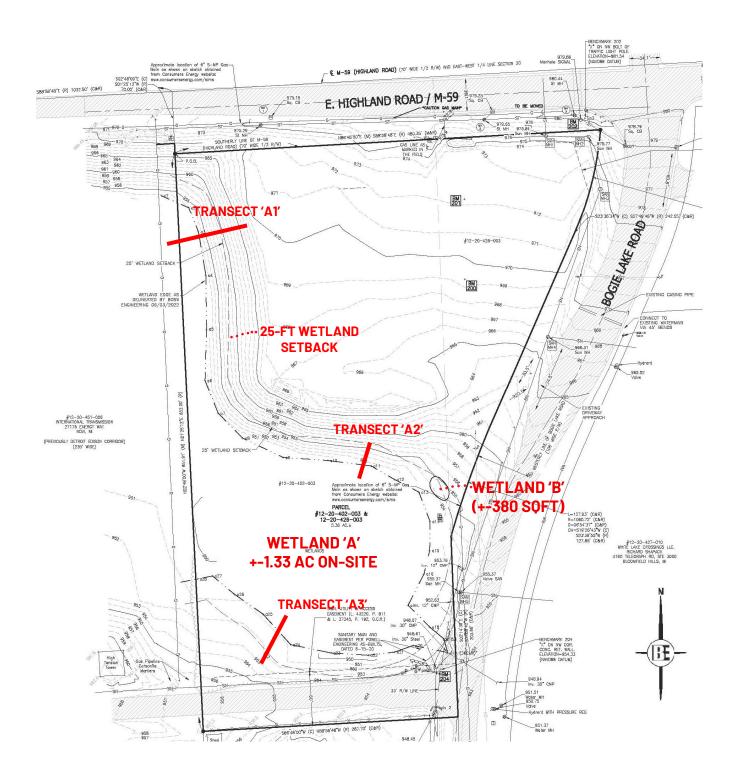


PHOTO 3 – South Side – Looking North



PHOTO 4 – Southwest Corner – Looking North

V. WETLAND BOUNDARY MAP





ME	MO
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		VIA EMAIL keith@najorcompanies.com
То:	Keith Maziasz Gateway Crossing, LLC	
From:	Jacob Swanson, PE Kyle Paulson Fleis & VandenBrink	
Date:	January 3, 2023	
Re:	Gateway Crossing Development White Lake Township, Michigan Traffic Impact Study	

1 INTRODUCTION

This memorandum presents the results of the Traffic Impact Study (TIS) for the Gateway Crossing Development located in the southwest quadrant of the Highland Road (M-59) & Bogie Lake Road intersection, in White Lake Township, Michigan. The proposed development includes retail and restaurant land uses, including two (2) restaurants with drive-through services. Site access is proposed via one (1) right-in/right-out (RIRO) driveway on EB Highland Road (M-59) and one (1) full access driveway on Bogie Lake Road, as shown on the attached **Figure 1**. The study section of Highland Road (M-59) and Bogie Lake Road are under the jurisdiction of the Michigan Department of Transportation (MDOT) and the Road Commission for Oakland County (RCOC), respectively. The completion of a TIS has been required (in accordance with the MDOT Geometric Design Guidance Section 1.2.4) as part of the site plan approvals and driveway permitting process.

The scope of work for this study was developed based on the requirements and input provided by MDOT, Fleis & VandenBrink's (F&V) knowledge of the study area, understanding of the development program, accepted traffic engineering practices, and information published by the Institute of Transportation Engineers (ITE). The study analyses were completed using Synchro/SimTraffic (Version 11). Sources of data for this study include F&V subconsultant Quality Counts, LLC (QC), MDOT, ITE, RCOC, and the Southeast Michigan Council of Governments (SEMCOG).

2 BACKGROUND

2.1 EXISTING ROAD NETWORK

Vehicle transportation for the study area is provided by Highland Road (M-59) and Bogie Lake Road. The lane uses and traffic control at the study intersections are shown on the attached **Figure 2** and the study roadways are further described below. For the purposes of this study, all minor streets, crossovers, and site driveways are assumed to have an operating speed of 25 miles per hour (mph), unless otherwise noted.

Highland Road (M-59) generally runs in the east and west directions, adjacent to the north side of the project site. The roadway is classified as an *Other Principal Arterial* and is under the jurisdiction of MDOT. The study section of Highland Road (M-59) has a posted speed limit of 55 mph and an Average Annual Daily Traffic (AADT) volume of approximately 40,000 vehicles per day (SEMCOG 2016). The roadway provides a four-lane, median divided cross-section, with two (2) lanes in each direction; left-turns are facilitated via exclusive left-turn lanes provided at the crossovers (U-turns) intersections.

Bogie Lake Road generally runs in the north and south directions, adjacent to the east side of the project site. Bogie Lake Road begins/ends, to the north of Highland Road (M-59), at the Meijer parking lot. Left turn movements are prohibited at the signalized intersection with Highland Road (M-59); these movements are facilitated via the median crossovers (U-turns) intersections along Highland Road (M-59).

- <u>South of Highland Road (M-59)</u>: The study section of Bogie Lake Road, south of M-59, has a posted speed limit of 45mph, is classified as a *Minor Arterial*, is under the jurisdiction of MDOT, and has an AADT volume of approximately 10,200 vehicles per day (SEMCOG 2021). Bogie Lake Road provides a two-lane cross-section, with one (1) lane in each direction. At the intersection with Highland Road (M-59), Bogie Lake Road widens to provide three (3) northbound lanes; one (1) exclusive through lane and dual (2) right-turn lanes.
- <u>North of Highland Road (M-59)</u>: This study section of Bogie Lake Road has a posted speed limit of 25mph, is classified as a *Local Road*, and is under the jurisdiction of RCOC. Bogie Lake Road provides a four-lane, median divided cross-section, with two (2) lanes in each direction. At the intersection with Highland Road (M-59), Bogie Lake Road widens to provide three (3) southbound lanes; one (1) exclusive through lane and dual (2) right-turn lanes. Additionally, at the NB-to-SB crossover, north of Highland Road (M-59), northbound Bogie Lake Road widens to provide an exclusive left-turn lane.

<u>Nordic Drive</u> intersects WB Highland Road (M-59), serving as the 4th-leg of the EB-to-WB Crossover intersection. Southbound Nordic Drive provides right-turn egress-only onto WB Highland Road (M-59).

2.2 EXISTING TRAFFIC VOLUMES

F&V subconsultant QC collected existing Turning Movement Count (TMC) data at the following study intersections on Thursday, November 3, 2022, during the AM (7:00 AM-9:00 AM) and PM (4:00 PM-6:00 PM) peak periods:

- EB Highland Road (M-59) & WB-to-EB Crossover, West of Bogie Lake Road
- Highland Road (M-59) & Bogie Lake Road
- WB Highland Road (M-59) & Nordic Drive / EB-to-WB Crossover, East of Bogie Lake Road
- SB Bogie Lake Road & NB-to-SB X/O, North of Highland Road (M-59)

During collection of the turning movement counts, Peak Hour Factors (PHFs) and commercial truck percentages were recorded and used in the traffic analysis. The peak hours of the study intersections were utilized and the through volumes were carried through the roadway network and balanced upwards at the proposed site driveway. Therefore, the traffic volumes used in the analysis and shown on the attached traffic volume figures may not match the raw traffic volumes shown in the data collection. The weekday AM and PM peak hours for the adjacent roadway network were observed to generally occur between 7:15 AM to 8:15 AM and 4:30 PM to 5:30 PM, respectively. F&V collected an inventory of existing lane use and traffic controls, as shown on the attached **Figure 2**. Additionally, F&V obtained the current signal timing permits from RCOC for the signalized study intersection. The existing 2022 peak hour traffic volumes used in the analysis are shown on the attached **Figure 3**.

3 EXISTING CONDITIONS

Existing peak hour vehicle delays and Levels of Service (LOS) were calculated at the study intersections using Synchro/SimTraffic (Version 11) traffic analysis software. This analysis was based on the existing lane use and traffic control shown on the attached **Figure 2**, the existing peak hour traffic volumes shown on the attached **Figure 3**, and the methodologies presented in the *Highway Capacity Manual*, 6th Edition (HCM6). The signalized intersections within the study roadway network operate with non-NEMA phasing and clustered signals, which are not supported by HCM6; therefore, HCM2000 was determined to be more appropriate for use at these intersections. Descriptions of LOS "A" through "F" as defined in the HCM6, are attached. Typically, LOS D is considered acceptable, with LOS A representing minimal delay and LOS F indicating failing conditions. The existing conditions results are attached and summarized in **Table 1**.

The results of the existing conditions analysis indicates that all approaches and movements are currently operating acceptably, at LOS D or better during both peak periods, with the exception of the following:

Highland Road (M-59) & Bogie Lake Road

• During the AM peak hour: The southbound right-turn movement is currently operating at LOS E.



• <u>During the PM peak hour</u>: The northbound through movement, the southbound through movement, and the southbound right-turn movement are currently operating at LOS E.

Although the Synchro LOS analysis indicates poor operations, a review of SimTraffic network simulations indicates generally acceptable operations during both the AM and PM peak hours. SimTraffic microsimulations indicate that all vehicle queues along the northbound and southbound approaches were observed to be processed through the intersection within each cycle length.

WB Highland Road (M-59) & EB-to-WB Crossover / Nordic Drive

• <u>During the PM peak hour</u>: The northbound (crossover) approach is currently operating at LOS E.

Review of SimTraffic microsimulations indicates generally acceptable operations at this signalized study intersection. Occasional periods of vehicle queues were present during the PM peak hour; however, the majority of queues were observed to be serviced each cycle, leaving minimal residual vehicle queueing. Additionally, vehicle queues were observed to dissipate and were not present throughout the PM peak hour.

SimTraffic network simulations indicate acceptable operations throughout the remainder of the study roadway network during both the AM and PM peak hours. All vehicles at the remaining signalized study intersections were observed to be serviced within each cycle length.

				Exis	ting C	ondition	s
	Intersection	Control	Approach	AM Pe	eak	PM Pe	ak
				Delay (s/veh)	LOS	Delay (s/veh)	LOS
10	EB Highland Road (M-59)		EBT	15.3	В	9.6	Α
&	&	Signalized	SBL	0.4	Α	0.3	Α
11	WB-to-EB X/O		Overall	13.6	В	8.3	Α
			EBT	3.2	Α	2.9	Α
			EBR	3.0	Α	2.0	Α
			WBT	6.5	Α	14.2	В
20	Highland Road		WBR	3.7	Α	2.1	Α
&	(M-59) &	Signalized	NBT	31.8	С	59.3	Е
21	Bogie Lake Road		NBR	33.7	С	51.8	D
			SBT	36.8	D	61.2	Е
			SBR	59.6	Е	66.4	Е
			Overall	9.6	Α	17.3	В
	WB Highland Road (M-59)		WBT	9.5	Α	11.2	В
30	&		WBR	6.1	А	5.0	Α
&	EB-to-WB X/O	Signalized	NBTL	36.9	D	65.0	Е
31	/		SBR	26.4	С	42.2	D
	Nordic Drive		Overall	13.3	В	19.7	В
40	Bogie Lake Road		WBL	0.3	Α	0.3	Α
&	&	Signalized	SB	5.9	Α	4.7	Α
41	NB-to-SB X/O		Overall	1.5	Α	1.0	Α

Table 1: Existing Intersection Operations

4 BACKGROUND CONDITIONS (2024 NO BUILD)

Historical population and economic profile data was obtained for White Lake Township from SEMCOG in order to calculate a background growth rate to project the existing 2022 peak hour traffic volumes to the site buildout year of 2024. Population and employment projections from 2020 to 2045 were reviewed and show an average annual growth of 0.16% and 0.01%, respectively. Therefore, a conservative background growth rate of **0.5%** per year was applied to the existing peak hour traffic volumes to forecast the background 2024 traffic volume *without the proposed development*, as shown on the attached **Figure 4**.



In addition to the background traffic growth, it is important to account for traffic that will be generated by developments within the vicinity of the study area that are currently under construction or will be within the buildout year. At the time of this study, neither MDOT nor White Lake Township identified any planned background developments within the vicinity of the project site.

Background peak hour vehicles delays and LOS *without the proposed development* were calculated at the study intersections based on the existing lane use and traffic control shown on the attached **Figure 2**, the background peak hour traffic volumes shown on the attached **Figure 4**, and the methodologies presented in the HCM. The results of the background conditions analysis are attached and summarized in **Table 2**.

						ondition			· ·	l Conditi	lono		Diffe	rence	
	Intersection	Control	Approach	AM Pe	eak	PM Pe	ak	AM P	eak	PM P	eak	AM P	eak	PM P	eak
				Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS
10	EB Highland Rd.		EBT	15.3	В	9.6	Α	15.6	В	9.7	Α	0.3	-	0.1	-
&	(M-59) &	Signal	SBL	0.4	Α	0.3	Α	0.4	Α	0.3	Α	0.0	-	0.0	-
11	WB-to-EB X/O		Overall	13.6	В	8.3	Α	13.9	В	8.4	Α	0.3	-	0.1	-
			EBT	3.2	Α	2.9	Α	3.1	Α	2.9	Α	-0.1	-	0.0	-
			EBR	3.0	Α	2.0	Α	3.0	Α	2.0	Α	0.0	-	0.0	-
			WBT	6.5	Α	14.2	В	6.6	Α	14.4	В	0.1	-	0.2	-
20	Highland Road		WBR	3.7	Α	2.1	Α	3.7	Α	2.0	Α	0.0	-	-0.1	-
&	(M-59) &	Signal	NBT	31.8	С	59.3	Е	31.9	С	59.6	Е	0.1	-	0.3	-
21	Bogie Lake Rd.		NBR	33.7	С	51.8	D	33.8	С	52.2	D	0.1	-	0.4	-
			SBT	36.8	D	61.2	Е	36.7	D	61.0	Е	-0.1	-	-0.2	-
			SBR	59.6	Е	66.4	Е	60.4	Е	66.1	Е	0.8	-	-0.3	-
			Overall	9.6	Α	17.3	В	9.8	Α	17.5	В	0.2	-	0.2	-
	WB Highland Rd.		WBT	9.5	Α	11.2	В	9.6	Α	11.4	В	0.1	-	0.2	-
30	(M-59) &		WBR	6.1	Α	5.0	Α	6.1	Α	5.0	Α	0.0	-	0.0	-
&	EB-to-WB X/O	Signal	NBTL	36.9	D	65.0	Е	36.0	D	65.7	Е	-0.9	-	0.7	-
31	/		SBR	26.4	С	42.2	D	26.4	С	42.3	D	0.0	-	0.1	-
	Nordic Drive		Overall	13.3	В	19.7	В	13.2	В	19.9	В	-0.1	-	0.2	-
40	Bogie Lake Rd.		WBL	0.3	Α	0.3	Α	0.3	Α	0.3	Α	0.0	-	0.0	-
&	&	Signal	SB	5.9	Α	4.7	Α	5.9	Α	4.7	Α	0.0	-	0.0	-
41	NB-to-SB X/O		Overall	1.5	Α	1.0	Α	1.5	Α	0.9	Α	0.0	-	-0.1	-

Table 2: Background Intersection Operations

* Decreased delays are the result of improved progression and/or HCM weighting methodologies

The results of the background conditions analysis indicates that all approaches and movements at the study intersections are expected to continue operating acceptably, in a manner similar to the existing conditions analysis. Additionally, review of SimTraffic network simulations indicates acceptable operations throughout the study roadway network, similar to the observations made during existing conditions.

5 SITE TRIP GENERATION

The number of weekday peak hour (AM and PM) and daily vehicle trips generated by the proposed development were calculated using the rates published by the Institute of Transportation Engineers (ITE) in *Trip Generation*, *11th Edition*. The proposed development includes retail and restaurant land uses, including two (2) restaurants with drive-through service. Additionally, one (1) of the proposed drive-through restaurants is currently planned to be a Culver's restaurant, which does not operate during the AM peak hours (7AM-9AM); therefore, the AM peak trip generation was excluded. Site access is proposed via one (1) right-in/right-out (RIRO) driveway on Highland Road (M-59) and one (1) full access driveway on Bogie Lake Road. The site trip generation forecast utilized for the proposed development is summarized in **Table 3**.



Land Use	ITE	Amount	Units	Average Daily	AM P	Peak Ho	our (vph)	PM F	Peak Ho	our (vph)
	Code	Amount	Units	Traffic (vpd)	In	Out	Total	In	Out	Total
Strip Retail Plaza (<40k SF)	822	6,031	SF	484	8	6	14	27	27	54
				Internal Capture	1	1	2	14	8	22
Pass-By	0%	5 AM, 40%	РM	97	0	0	0	6	6	12
		Ne	w Trips	387	7	5	12	7	13	20
Fast Food with Drive-Through	934	4,060	SF	1,898	0	0	0	70	64	134
				Internal Capture	0	0	0	5	8	13
Pass-By	0%	5 AM, 55%	РM	408	0	0	0	33	33	66
		Ne	w Trips	1,490	0	0	0	32	23	55
Coffee Shop with Drive-Through	937	2,289	SF	1,221	100	97	197	45	44	89
				Internal Capture	1	1	2	3	6	9
Pass-By	50%	% AM; 55%	РМ	263	49	49	98	22	22	44
		Ne	w Trips	958	50	47	97	20	16	36
		Tota	al Trips	3,603	108	103	211	142	135	277
			Total	Internal Capture	2	2	4	22	22	44
		Total P	ass-By	768	49	49	98	61	61	122
		Total Nev	v Trips	2,835	57	52	109	59	52	111

Table 3: Site Trip Generation Summary

As is typical of commercial developments, a portion of the trips generated by the proposed development are from vehicles currently on the adjacent roadway that will pass the site on the way from an origin to their ultimate destination. Therefore, not all traffic at the site driveways is necessarily new traffic added to the street system. This percentage of the trips generated by the development are considered "pass-by" trips and do not add new traffic to the adjacent street system. The percentage of pass-by trips used in this analysis was determined based on the rates published by ITE in the *Trip Generation Manual*, *11th Edition*. However, ITE does not provide pass-by data for either LUC 822: Strip Retail Plaza or LUC 937: Coffee Shop with Drive-Through; therefore, the pass-by data for LUC 821: Shopping Plaza and LUC 934: Fast Food with Drive-Through were utilized for this analysis, respectively.

Additionally, the table also presents internal trip capture estimates, which are the portion of trips generated by a mixed-used development that would begin and end within the development site, resulting in no additional trips added to the adjacent road network. The internal trip capture projections follow the Transportation Research Board's (TRB) *Report 684: Enhancing Internal Trip Capture Estimation for Mixed-Use Development*. The internal trips estimation calculations spreadsheets are attached.

These pass-by trips and the internal trips were reduced from the total trips generated by the site, in order to calculate the total new trip generation that was distributed to the study roadway network.

6 SITE TRIP DISTRIBUTION

The vehicular trips that would be generated by the proposed development were assigned to the study roads based on the proposed site access plan and driveway configurations, the existing peak hour traffic patterns in the adjacent roadway network, and the methodologies published by ITE. The ITE trip distribution methodology assumes that new trips will enter the network and access the development, then leave the development and return to their direction of origin, whereas pass-by trips will enter and exit the development in their original direction of travel. The site trip distributions utilized in the analysis are summarized in **Table 6**.

The vehicular traffic volumes shown in **Table 3** were distributed to the study roadway network according to the distribution shown in **Table 4**. The site-generated trips shown on the attached **Figure 5** were added to the background peak hour traffic volumes shown on the attached **Figure 4**, in order to calculate the future peak hour traffic volumes, with the addition of the proposed development. Future peak hour traffic volumes are shown on the attached **Figure 6**.



To/From	Via	New	Trips	Pas	s-By
TO/TTOIL	Vid	AM	PM	AM	PM
East	Highland Road (M-59)	34%	46%	47% (EB)	38% (EB)
West	Highland Road (M-59)	53%	39%	27% (WB)	41% (WB)
South	Bogie Lake Road	13%	15%	15% (SB)	9% (SB)
North	Bogie Lake Road	N/A	N/A	11% (NB)	12% (NB)
	Total	100%	100%	100%	100%
	Trip	o Volume	s		
East	Highland Road (M-59)	36	51	46	46
West	Highland Road (M-59)	58	43	23	50
South	Bogie Lake Road	15	17	10	14
North	Bogie Lake Road	0	0	16	12
	Total	109	111	98	122

Table 4: Site Trip Distribution

7 FUTURE CONDITIONS (2024 BUILDOUT)

Future peak hour vehicle delays and LOS *with the proposed development* were calculated based on the proposed lane use and traffic controls shown on the attached **Figure 2**, future peak hour traffic volumes shown on the attached **Figure 6**, and the methodologies presented in the HCM. The results of the future conditions analysis are attached and summarized in **Table 5**.

				Backgr	ound	Conditi	ons	Fut	ure C	ondition	S	Difference			
	Intersection	Control	Approach	AM Pe	ak	PM P		AM P	eak	PM P	eak	AM P	eak	PM P	eak
			PP	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS
10	EB Highland Rd.		EBT	15.6	В	9.7	Α	16.1	В	9.9	А	0.5	-	0.2	-
&	(M-59) &	Signal	SBL	0.4	А	0.3	Α	0.5	А	0.3	А	0.1	-	0.0	-
11	WB-to-EB X/O		Overall	13.9	В	8.4	Α	14.1	Α	8.3	Α	0.2	В→А	-0.1	-
			EBT	3.1	Α	2.9	Α	4.1	А	3.8	Α	1.0	-	0.9	-
			EBR	3.0	А	2.0	А	2.5	А	1.7	Α	-0.5	-	-0.3	-
			WBT	6.6	Α	14.4	В	8.3	А	16.6	В	1.7	-	2.2	-
20	Highland Road		WBR	3.7	Α	2.0	Α	3.3	А	3.0	Α	-0.4	-	1.0	-
&	(M-59) &	Signal	NBT	31.9	С	59.6	Е	31.9	С	59.6	Е	0.0	-	0.0	-
21	Bogie Lake Rd.		NBR	33.8	С	52.2	D	34.1	С	53.3	D	0.3	-	1.1	-
	0		SBT	36.7	D	61.0	Е	36.4	D	61.2	Е	-0.3	-	0.2	-
			SBR	60.4	Е	66.1	Е	60.7	Е	66.0	Е	0.3	-	-0.1	-
			Overall	9.8	Α	17.5	В	11.0	В	19.2	В	1.2	А→В	1.7	-
	WB Highland Rd.		WBT	9.6	Α	11.4	В	9.7	А	11.6	В	0.1	-	0.2	-
30	(M-59) &		WBR	6.1	А	5.0	А	6.1	А	5.0	А	0.0	-	0.0	-
&	EB-to-WB X/O	Signal	NBTL	36.0	D	65.7	Е	32.6	С	91.2	F	-3.4	$D \rightarrow C$	25.5	$E{\rightarrow}F$
31	/		SBR	26.4	С	42.3	D	26.4	С	42.4	D	0.0	-	0.1	-
	Nordic Drive		Overall	13.2	В	19.9	В	13.6	В	25.2	С	0.4	-	5.3	В→С
40	Bogie Lake Rd.		WBL	0.3	А	0.3	А	0.3	А	0.3	Α	0.0	-	0.0	-
&	&	Signal	SB	5.9	А	4.7	Α	5.9	А	4.7	Α	0.0	-	0.0	-
41	NB-to-SB X/O		Overall	1.5	Α	0.9	Α	1.5	Α	0.9	Α	0.0	-	0.0	-

Table 5: Future Intersection Operations



				Backgr	ound	Condit	ions	Fut	ure C	ondition	S		Diffe	rence	
	Intersection	Control	Approach	AM Pe	eak	PM P	eak	AM P	eak	PM P	eak	AM P	eak	PM P	eak
				Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS
50	EB M-59 &	Stop	EB		N1/	٨			Fr	ee			N	/ ^	
50	W. Site Drive	(Minor)	NBR		N/.	A		15.2	С	15.0	С		IN	/A	
	Bogie Lake Rd.	•	EB					14.0	В	13.8	В				
60	&	Stop (Minor)	NBL		N/	A		8.9	А	8.2	Α		N	/A	
	E. Site Drive	(1011101)	SB						Fr	ee					

* Decreased delays are the result of improved progression and/or HCM weighting methodologies

The results of the future conditions analysis indicates that all the study intersection approaches and movements will continue to operate acceptably, in a manner similar to the background conditions analysis, with the exception of the following:

WB Highland Road (M-59) & EB-to-WB Crossover / Nordic Drive

• During the PM peak hour: The northbound (crossover) approach is expected to operate at LOS F.

Although the Synchro LOS analysis indicates failing operations, a review of SimTraffic network simulations indicates generally acceptable operations. Occasional periods of long vehicle queues were present during the PM peak hour; however, the majority of queues were observed to be serviced each cycle, leaving minimal residual vehicle queueing. Additionally, any vehicle queues present were contained within the available left-turn storage area and were observed to dissipate within the PM peak hour.

SimTraffic network simulations indicate acceptable operations throughout the remainder of the study roadway network during both the AM and PM peak hours. All vehicles at the remaining signalized study intersections were observed to be serviced within each cycle length. Additionally, all approaches and movements at the proposed site driveways are expected to operate acceptably at LOS D or better during both peak periods; the stop-controlled egress traffic was observed to find adequate gaps within the through traffic.

7.1 FUTURE CONDITIONS WITH IMPROVEMENTS

Mitigation measures were investigated in order to improve the projected future traffic operations to LOS D or better for all approaches and movements during both peak periods. Signal timing adjustments, geometric improvements, and traffic control modifications were investigated at the study intersections. The results of the evaluation indicates that signal timing optimizations alone will adequately mitigate increases in delay due to the additional traffic generated by the proposed development.

				Fut	Future Co		s	Future w/ IMPs				Difference			
	Intersection	Control	Approach	AM P	eak	PM P	eak	AM P	eak	PM P	eak	AM P	eak	PM P	Peak
				Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS
			EBT	4.1	А	3.8	А	11.5	В	9.5	Α	7.4	A→B	5.7	-
			EBR	2.5	Α	1.7	А	3.8	Α	2.2	Α	1.3	-	0.5	-
			WBT	8.3	А	16.6	В	14.7	В	23.5	С	6.4	А→В	6.9	$B \rightarrow C$
20	Highland Road		WBR	3.3	А	3.0	А	3.1	А	10.1	В	-0.2	-	7.1	$A {\rightarrow} B$
&	(M-59) &	Signal	NBT	31.9	С	59.6	Е	24.4	С	41.8	D	-7.5	-	-17.8	$E \rightarrow D$
21	Bogie Lake Rd.		NBR	34.1	С	53.3	D	26.1	С	41.1	D	-8.0	-	-12.2	-
	0		SBT	36.4	D	61.2	Е	31.8	D	53.3	D	-4.6	-	-7.9	$E{\rightarrow}D$
			SBR	60.7	Е	66.0	Е	52.9	D	58.2	Е	-7.8	$E \rightarrow D$	-7.8	-
			Overall	11.0	В	19.2	В	15.6	В	24.1	С	4.6	-	4.9	B→C

Table 6: Future Intersection Operations with Improvements



				Future Conditions Future w/ IMPs								Difference				
	Intersection	Control	Approach	AM P	eak	PM P	eak	AM P	eak	PM P	eak	AM P	eak	PM P	eak	
				Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)		Delay (s/veh)		Delay (s/veh)	LOS	Delay (s/veh)	LOS	
			WBT	9.7	А	11.6	В			28.5	С			16.9	B→C	
30	WB Highland Rd. (M-59) &		WBR	6.1	А	5.0	А			11.2	В			6.2	А→В	
&	EB-to-WB X/O	Signal	NBTL	32.6	С	91.2	F	No Ch	ange	53.0	D	No Ch	ange	-38.2	F→D	
31	/ Nordic Drive		SBR	26.4	С	42.4	D			28.8	С			-13.6	D→C	
			Overall	13.6	В	25.2	С			32.1	С			6.9	-	

With the implementation of the recommended signal timing optimizations, all study intersection approaches and movements are expected to operate acceptably, at LOS D or better during both peak periods, with the exception of the following:

Highland Road (M-59) & Bogie Lake Road

• <u>During the PM peak hour</u>: The southbound right-turn movement is expected to continue operating at LOS E.

Although the Synchro LOS analysis still indicates poor operations, a review of SimTraffic network simulations indicates acceptable operations during the PM peak hour. SimTraffic microsimulations indicate that all southbound vehicle queues were observed to be processed through the intersection within each cycle length, leaving no residual vehicle queues.

With the implementation of the recommended mitigation measures, SimTraffic network simulations indicate acceptable operations throughout the remainder of the study roadway network and proposed site driveways during both peak periods.

8 ACCESS MANAGEMENT

8.1 AUXILIARY TURN LANE EVALUATION

Highland Road (M-59) and Bogie Lake Road are under the jurisdiction of MDOT and RCOC, respectively; therefore, the MDOT and RCOC warranting criteria were utilized in order to determine the need for auxiliary turn lanes at the proposed site driveways. Highland Road (M-59) is a four-lane, median-divided roadway; therefore, the left-turn warrants were not evaluated at the proposed W. Site Drive. The result of the analyses shown on the attached MDOT/RCOC warrant charts and are summarized in **Table 7**.

		,
Site Driveway Intersection	Right-Turn Treatment	Left-Turn Treatment
EB Highland Road (M-59) & W. Site Drive	Right-Turn Lane	N/A
Bogie Lake Road & E. Site Drive	No Treatment	No Treatment

The results of the auxiliary turn lane evaluation indicates that a full-width right-turn deceleration lane is recommended along eastbound Highland Road (M-59) at the proposed W. Site Drive.

8.2 DRIVEWAY SPACING EVALUATION

The MDOT Geometric Design Guidance (Section 1.2.2) was utilized to evaluate the location of the proposed site driveways in relation to nearby intersections, crossovers, and driveways within close proximity to the project site. The AASHTO intersection corner clearance criteria were evaluated for the 55-mph section of Highland Road (M-59) and the 45-mph section of Bogie Lake Road. The proposed development plans include two (2) proposed access points: one (1) right-in/right-out (RIRO) site driveway along EB Highland Road (M-59) and one (1) full access driveway along Bogie Lake Road. The distance of the proposed site driveways from nearby access points and the warranting criteria are summarized in **Table 8** and displayed in **Exhibit 1**.



Adjacent Dr	iveways	s & Intersections	Distance	Criteria	Meets
W. Site Drive	to	WB-to-EB Crossover	400 feet	150 feet	YES
W. Site Drive	to	Bogie Lake Road	360 feet	230 feet	YES
E. Site Drive	to	Shell Gas Station	250 feet	630 feet	NO
E. Site Drive	to	Grace Church	360 feet	350 feet	YES

Table 8: Desirable Corner Clearance Summary

The results of the analysis indicates that the proposed E. Site Drive is not expected to meet the desirable MDOT spacing criteria in relation to the nearby Shell Gas Station driveway on the opposite side of Bogie Lake Road. However, the proposed location of the E. Site Drive location currently meets the driveway spacing requirements from the Grace Church driveway; therefore, shifting the driveway location further south to increase the spacing from the Shell Drive would result in the driveway no longer meeting spacing requirements to the south.

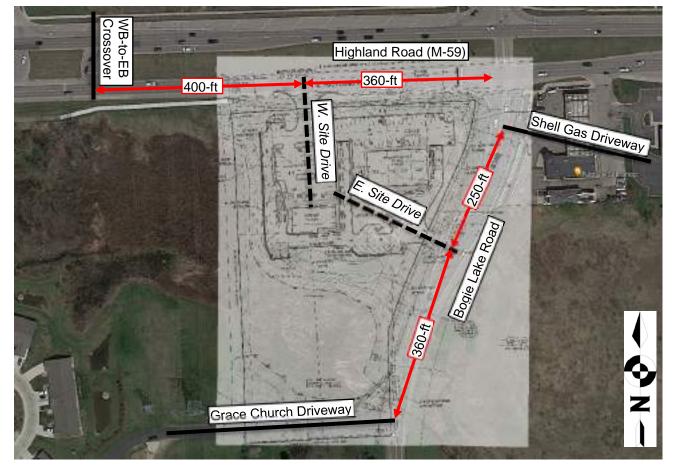


Exhibit 1: Proposed Driveway Spacing

9 SITE CIRCULATION AND QUEUEING

9.1 COFFEE SHOP DRIVE-THROUGH

The projected drive-through vehicle queuing was reviewed to determine if the proposed on-site drive-through storage is adequate to accommodate the projected operations. Typical restaurants with drive-through have an average service rate of approximately 60 vehicles/hour; additionally, approximately 70% of customers will utilize a drive-through. Therefore, of the total of 100 vehicles generated by the coffee shop during the AM peak hour, it is estimated that approximately 70 vehicles per hour will use the drive-through facility, with the remaining 30 vehicles using walk-in service. The evaluation of the queue length included two criteria:



- 1) A queuing analysis was performed to determine if the projected demand of the proposed development exceeds the service rate and calculate the projected queuing. The projected demand (70 veh/hr) is greater than the service rate (60 veh/hr) of the site; therefore, a surplus of 10 vehicles is expected.
- 2) In addition, a Poisson Distribution was performed to determine the probability of random arrivals; the results indicate a maximum potential of five (5) vehicles arriving at any given time.

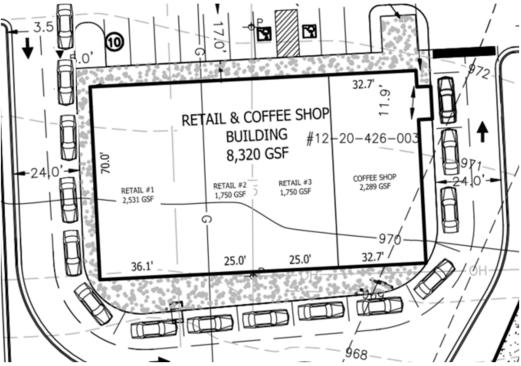
Therefore, providing queueing for a total drive-through queue of 15 vehicles is recommended. The proposed drive-through provides vehicle queueing storage, at 25-ft each vehicle, for four (4) vehicles from the order board to the pick-up window and 11 vehicles past the order boards, for a total drive-through queue of 15 vehicles (375 feet) within the allotted drive-through area without impacting the parking spaces or internal site circulation.

The proposed vehicle queueing storage for this project site can adequately accommodate the projected vehicle queue lengths for the proposed development. In the event that the vehicle demands exceed the drive-through capacity, the internal site circulation has adequate space to accommodate the additional vehicle storage lengths on-site without impacting the adjacent street operations on Highland Road (M-59). The projected vehicle queueing is summarized in **Table 9** and the expected queueing is shown in the attached site plan.

Number of Arrivals	70
Time per Vehicle (s)	60
Service Rate (veh/hr)	60
Drive-Through Queue (veh)	10
Peak Arrival (veh)	5
Vehicle Length	25
TOTAL QUEUE (ft)	375

Table 9: Coffee Shop Vehicle Queuing Analysis

Exhibit 2: Coffee Shop Vehicle Queueing





9.2 CULVERS DRIVE-THROUGH

The peak trip generation for the proposed Culver's restaurant is expected during the PM peak period; therefore, the projected drive-through vehicle queuing for the PM was reviewed to determine if the proposed on-site queue length for the drive-through is adequate to accommodate the projected operations.

Fast-food restaurants with drive-through windows typically service approximately 70% of customers via a drivethrough, with the remaining patrons choosing to dine-in. Therefore, of the total of 70 vehicles generated by the fast-food restaurant during the PM peak hour, it is estimated that approximately 49 vehicles per hour will use the drive-through facility, with the remaining 21 vehicles using walk-in service.

Culver's operates similar to a typical fast-food restaurant, wherein food is ordered at menu board and drivers pay for their orders at the window. Upon receipt of payment, drivers that order food (not drinks or frozen custard) are issued an order number and must pull ahead to wait for their food to be delivered to their vehicle in the queue past the pickup window. Therefore, the vehicle queue for Culver's is calculated two ways: Before the Payment Window and After the Payment Window

Before the Payment Window

The estimated service rate for a typical fast-food restaurant (90 veh/hr) is greater than the projected arrival rate at the drive-through (49 veh/hr); therefore, the required queueing for the drive-through is based on the maximum potential for random arrivals.

A Poisson Distribution was performed to determine the probability of random arrivals; the results are attached and indicate a maximum potential of four (4) vehicles arriving simultaneously at any given time. The proposed site utilizes two (2) menu order boards and one (1) pick up window. The proposed drive-through provides vehicle queueing storage, at 25-ft each vehicle, for eight (8) vehicles from the order boards to the pick-up window and seven (7) vehicles past the order boards, for a total drive-through queue of 15 vehicles (375 feet) within the allotted drive-through area without impacting the parking spaces or internal site circulation.

After the Payment Window

The estimated service rate is one (1) vehicle served food every 120 seconds (2 min) past the payment window. It was assumed that 80% of the vehicles in the drive-through will order food, then will enter the food queue lane past the payment window. The results of the analysis are summarized below and show a projected peak queue of nine (9) vehicles past the payment window.

CULVER'S DRIVE-THROUGH STACK	ING SPACE CALCULATOR
	Before Payment Window
Number of Arrivals	49
Time per Vehicle (s)	40
Service Rate (veh/hr)	90
Order Board to Pick-up Window (veh)	8
Peak Arrival (veh)	4
Vehicle Length	25
TOTAL QUEUE (ft)	300
	After Payment Window
Number of Arrivals	39
Time per Vehicle (s)	120
Vehicle Queue Past Window (veh)	9
Vehicle Length	25
TOTAL QUEUE (ft)	225

Table 10: Culver's Vehicle Queuing Analysis



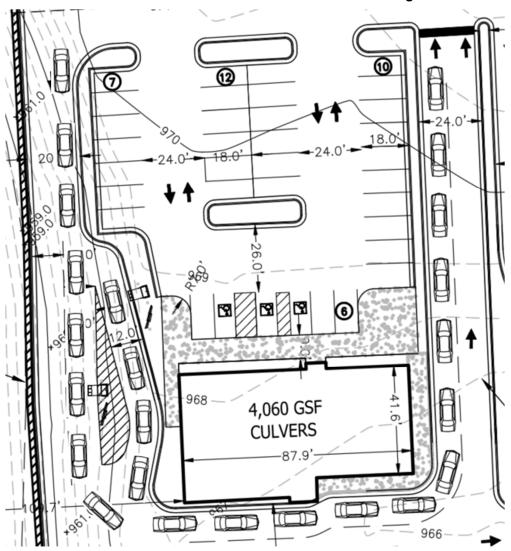


Exhibit 3: Fast-Food Restaurant Vehicle Queueing

10 CONCLUSIONS

The conclusions of this TIS are as follows:

10.1 EXISTING CONDITIONS (2022)

The result of the existing conditions analysis indicates that all of the study intersections, approaches, and movements, are currently operating acceptably at LOS D or better during both peak periods, with the exception of the following:

Highland Road (M-59) & Bogie Lake Road

- <u>During AM peak hour</u>: The SB right-turn movement is currently operating at LOS E.
- <u>During PM peak hour</u>: The NB through, SB through, and SB right-turn movements are currently operating at LOS E.

Review of SimTraffic network simulations indicates generally acceptable operations throughout the study roadway network. All vehicle queues along the northbound/southbound approaches were observed to be serviced within each cycle length, leaving no residual queueing.



WB Highland Road (M-59) & EB-to-WB Crossover / Nordic Drive

• During PM peak hour: The NB (crossover) approach is currently operating at LOS E.

Although the Synchro LOS analysis indicates poor operations, a review of SimTraffic network simulations indicates generally acceptable operations. SimTraffic microsimulations indicate that occasional periods of vehicle queues were present during the PM peak hour; however, the majority observed to be serviced each cycle, leaving minimal residual vehicle queueing. Additionally, vehicle queues were observed to dissipate and were not present throughout the peak hour.

10.2 BACKGROUND CONDITIONS (2024 NO BUILD):

- A conservative 0.5% annual background growth rate was utilized in order to project the existing 2022 peak hour traffic volumes to the buildout year of 2024. Additionally, no planned developments were identified within the vicinity of the project site.
- The results of the background conditions analysis indicates that all approaches and movements at the study intersections will continue to operate in a manner similar to existing conditions. Additionally, review of SimTraffic microsimulations indicates acceptable operations, with minimal vehicle queueing.

10.3 FUTURE CONDITIONS (2024 BUILDOUT)

The results of the future conditions analysis indicates that all of the study intersection approaches and movements will continue to operate in a manner similar to background conditions with the following additional delays:

Highland Road (M-59) & EB-to-WB Crossover / Nordic Drive

• During PM peak hour: The NB approach is expected to operate at LOS F.

Review of SimTraffic network simulations indicates generally acceptable operations, similar to those observations made during the background conditions analysis. Occasional periods of long vehicle queues were present; however, the majority of queues were observed to be serviced each cycle, leaving minimal residual vehicle queueing. Additionally, any vehicle queues present were contained within the available left-turn storage area and were observed to dissipate within the PM peak hour.

The proposed site driveways are expected to operate acceptably, at LOS D or better during both peak periods.

10.4 FUTURE CONDITIONS WITH IMPROVEMENTS

- Mitigation measures were reviewed at the study intersections in order to mitigate the impact that the site-generated traffic from the proposed development.
- Signal timing optimizations were reviewed during both peak periods and were determined to adequately mitigate increases in delay due to the additional traffic generated by the proposed development.

10.5 ACCESS MANAGEMENT

- The MDOT and RCOC auxiliary turn lane warranting criteria were reviewed at the proposed site driveways on Highland Road (M-59) and Bogie Lake Road, respectively. The results of the evaluation indicates the following:
 - A full-width right-turn deceleration lane is recommended at the proposed W. Site Drive on eastbound Highland Road (M-59).
 - No treatments are recommended at the proposed E. Site Drive on Bogie Lake Road.
- Review of the proposed driveway location and adjacent crossover intersections indicates that the proposed E. Site Drive does not meet the MDOT minimum desirable spacing criteria, in relation to the existing Shell Gas Station driveway. However, shifting the driveway further south to increase the spacing would result in insufficient spacing to the south (from existing Grace Church driveway).



10.6 SITE CIRCULATION

• The results of the drive-through queueing evaluation indicates that the proposed site plan can adequately accommodate the projected vehicle queueing generated by the fast-food restaurant and the coffee shop drive-through operations, without impacting the internal site circulation or the adjacent roadway network.

11 RECOMMENDATIONS

The recommendation of this TIS are as follows:

Recomm	mended Improvements
Highlan	d Road (M-59) & Bogie Lake Road
• (Optimize the traffic signal timing during both peak periods
WB High	hland Road (M-59) & EB-to-WB Crossover / Nordic Drive
• (Optimize the traffic signal timing during the PM peak hour
EB High	nland Road (M-59) & W. Site Drive
• F	Provide a full-width right-turn deceleration lane at the proposed E. Site Drive

Any questions related to this memorandum, study, analysis, and results should be addressed to Fleis & VandenBrink.

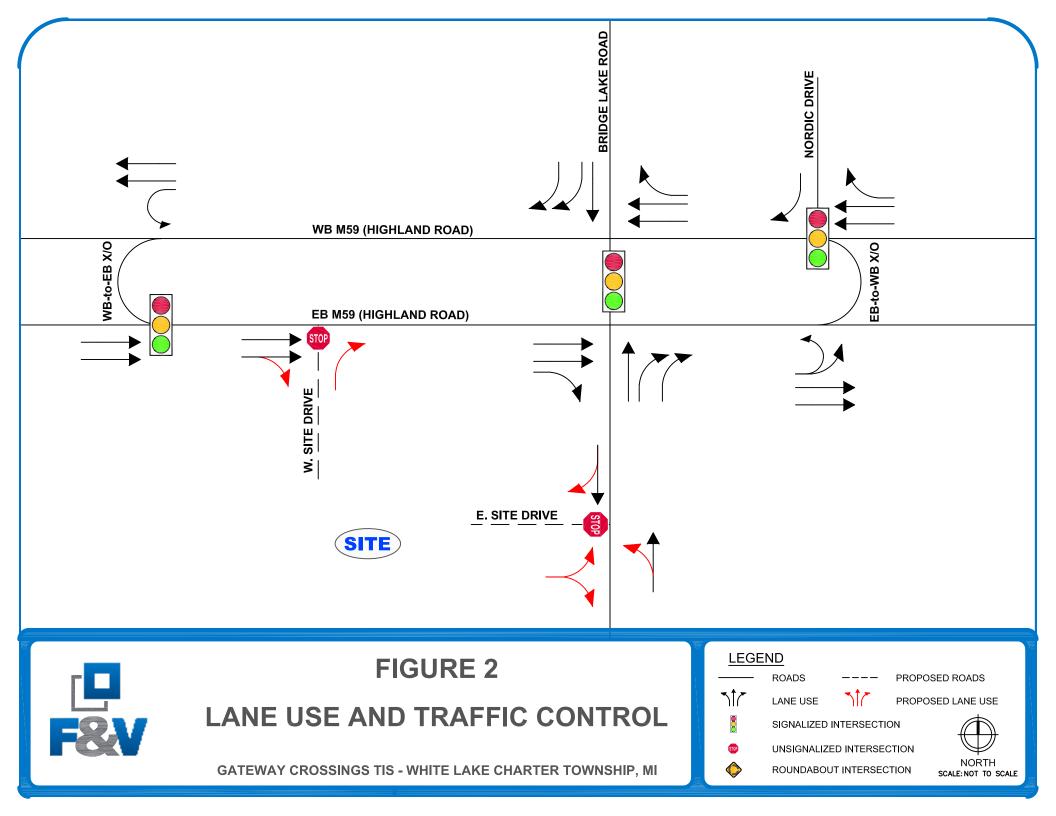


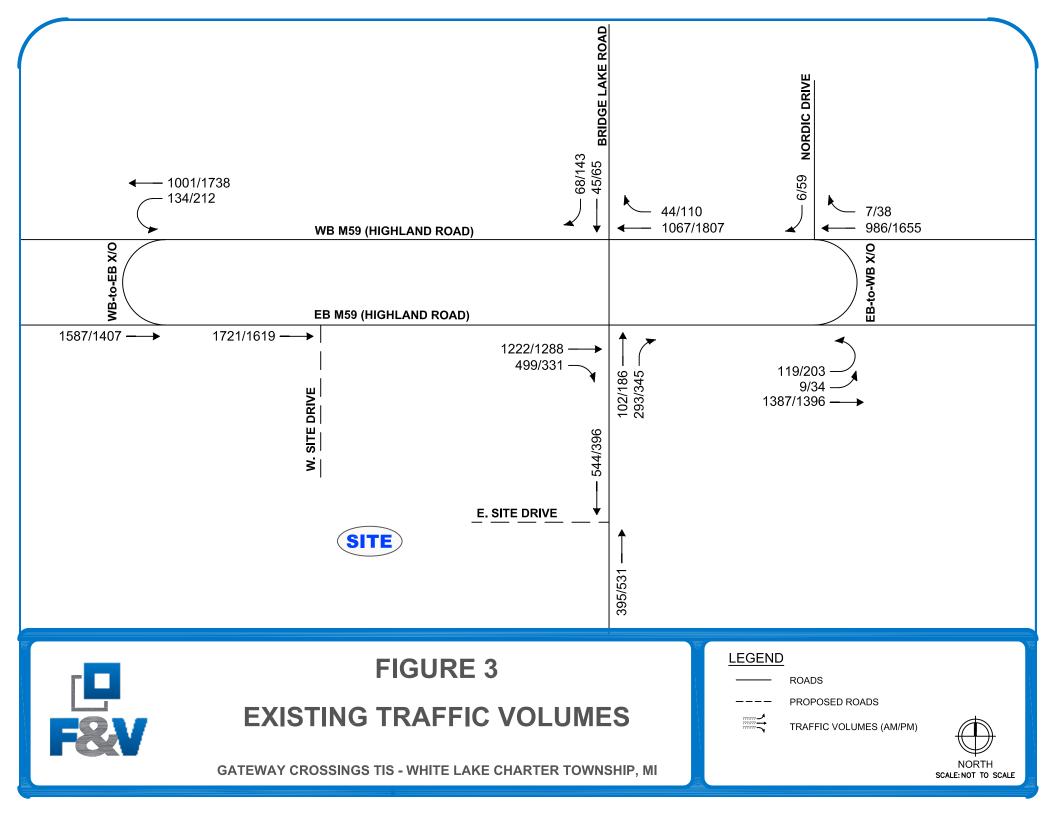
I hereby certify that this engineering document was prepared by me or under my direct personal supervision and that I am a duly licensed Professional Engineer under the laws of the State of Michigan.

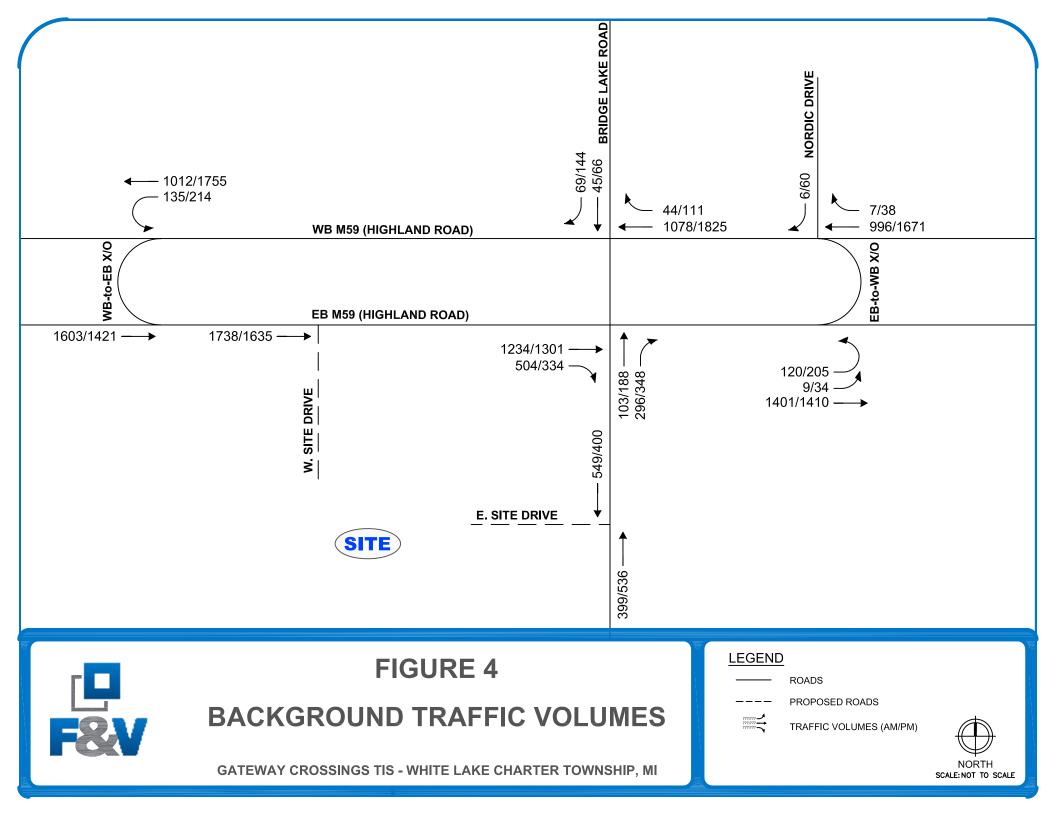
Attached: Figures 1 – 6 Proposed Site Plan Traffic Volume Data Signal Timing Permits Internal Capture Spreadsheet Synchro / SimTraffic Results Auxiliary Lane Warrant Poisson Distribution

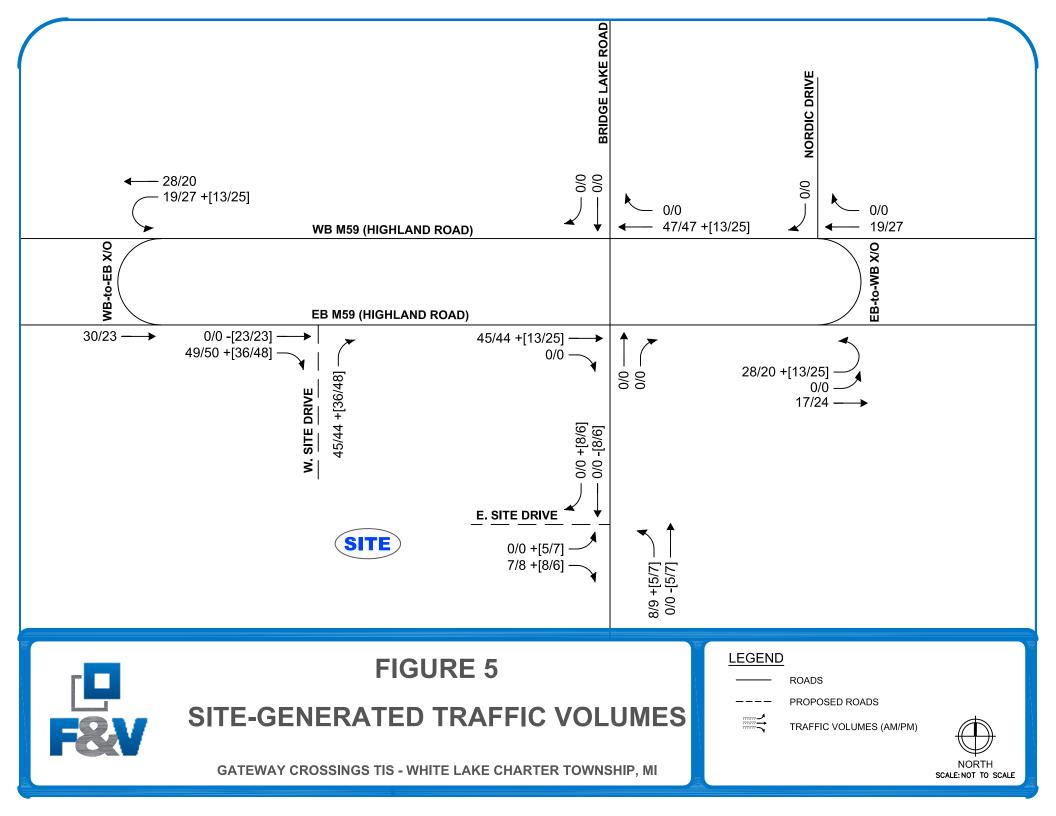


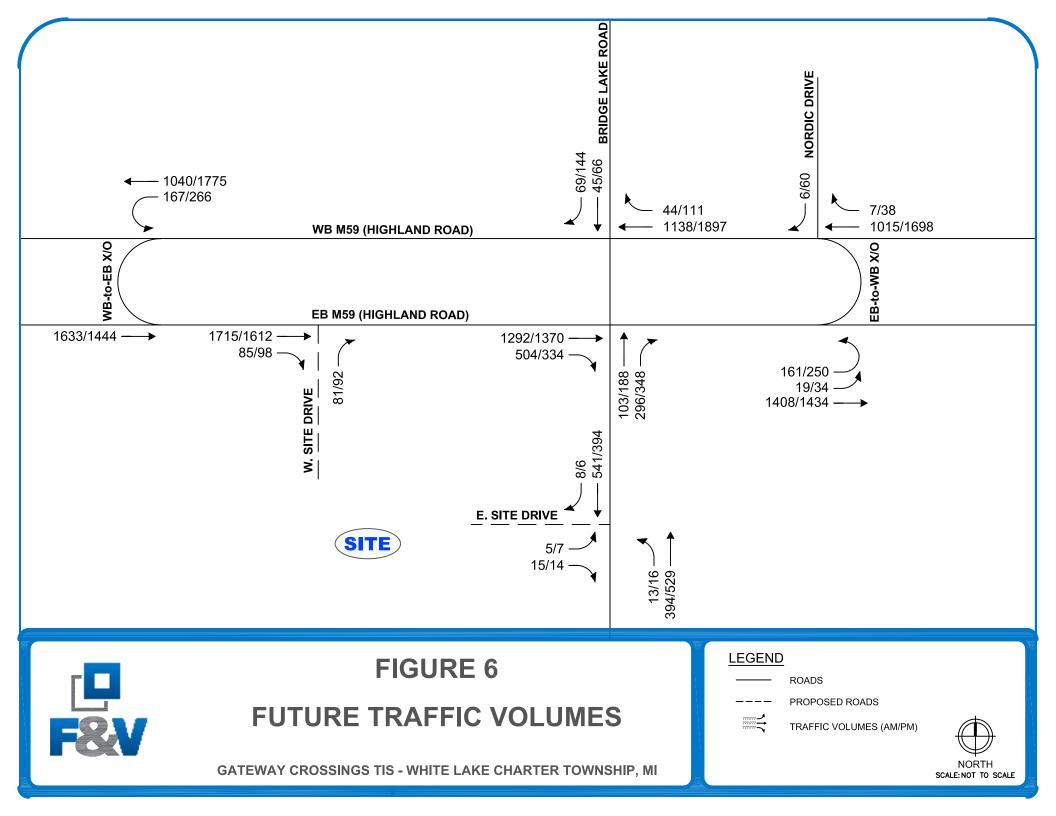


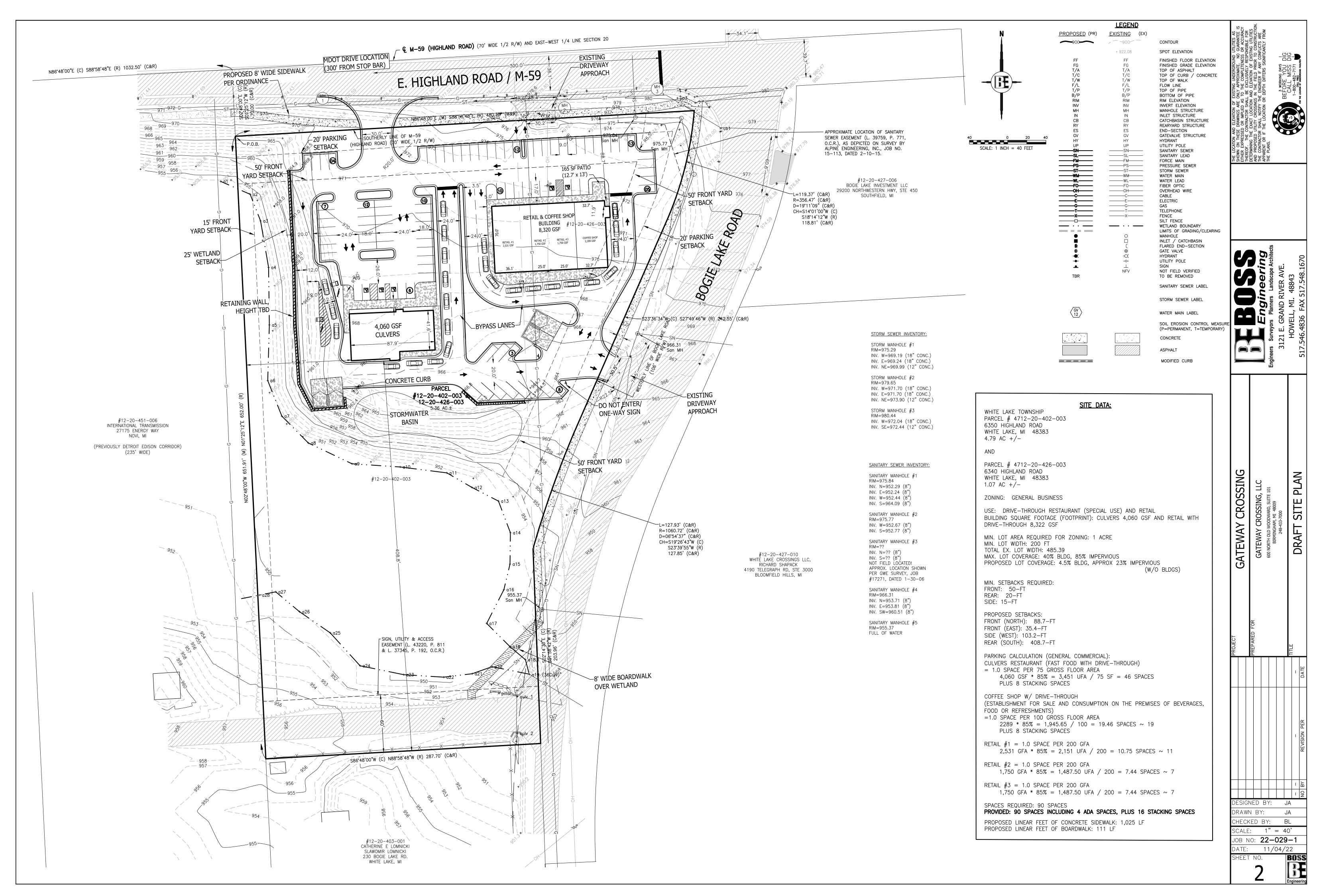






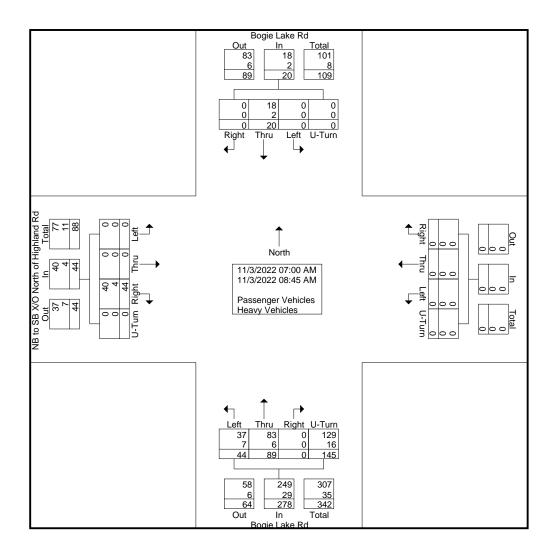






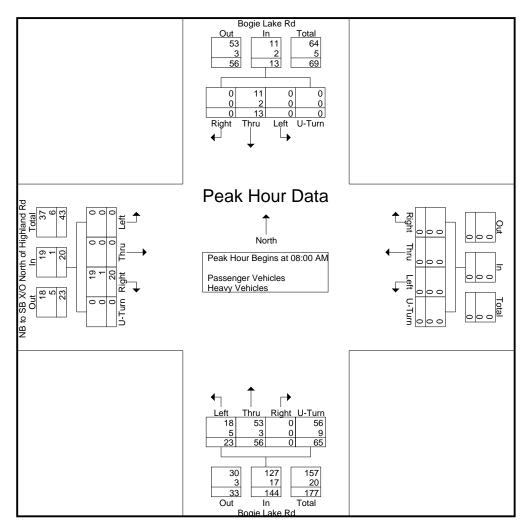


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Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
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Grand Total	0	0	44	0	44	0	0	0	0	0	44	89	0	145	278	0	20	0	0	20	342
Apprch %	0	0	100	0		0	0	0	0		15.8	32	0	52.2		0	100	0	0		
Total %	0	0	12.9	0	12.9	0	0	0	0	0	12.9	26	0	42.4	81.3	0	5.8	0	0	5.8	
Passenger Vehicles	0	0	40	0	40	0	0	0	0	0	37	83	0	129	249	0	18	0	0	18	307
% Passenger Vehicles	0	0	90.9	0	90.9	0	0	0	0	0	84.1	93.3	0	89	89.6	0	90	0	0	90	89.8
Heavy Vehicles	0	0	4	0	4	0	0	0	0	0	7	6	0	16	29	0	2	0	0	2	35
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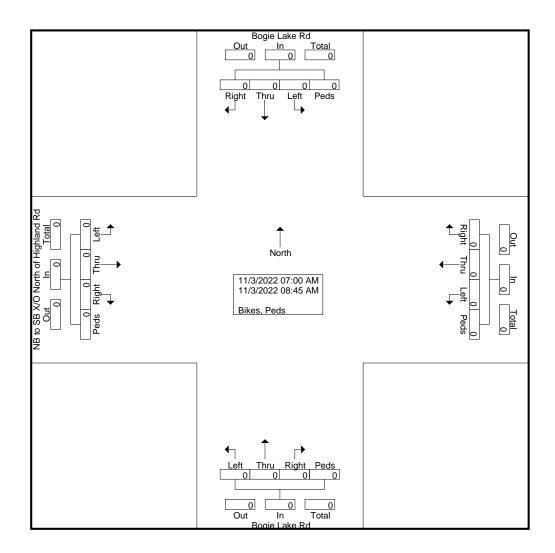


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Peak Hour fo	or Entir	e Inter	section	n Begi	ns at 08	:00 AN	/														
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Total Volume	0	0	20	0	20	0	0	0	0	0	23	56	0	65	144	0	13	0	0	13	177
% App. Total	0	0	100	0		0	0	0	0		16	38.9	0	45.1		0	100	0	0		
PHF	.000	.000	.714	.000	.714	.000	.000	.000	.000	.000	.821	.824	.000	.677	.818	.000	.813	.000	.000	.813	.903
Passenger Vehicles	0	0	19	0	19	0	0	0	0	0	18	53	0	56	127	0	11	0	0	11	157
% Passenger Vehicles	0	0	95.0	0	95.0	0	0	0	0	0	78.3	94.6	0	86.2	88.2	0	84.6	0	0	84.6	88.7
Heavy Vehicles	0	0	1	0	1	0	0	0	0	0	5	3	0	9	17	0	2	0	0	2	20
% Heavy Vehicles	0	0	5.0	0	5.0	0	0	0	0	0	21.7	5.4	0	13.8	11.8	0	15.4	0	0	15.4	11.3



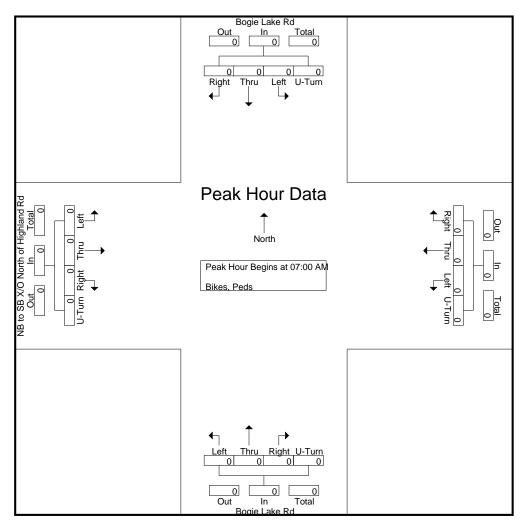


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08:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
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08:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Grand Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
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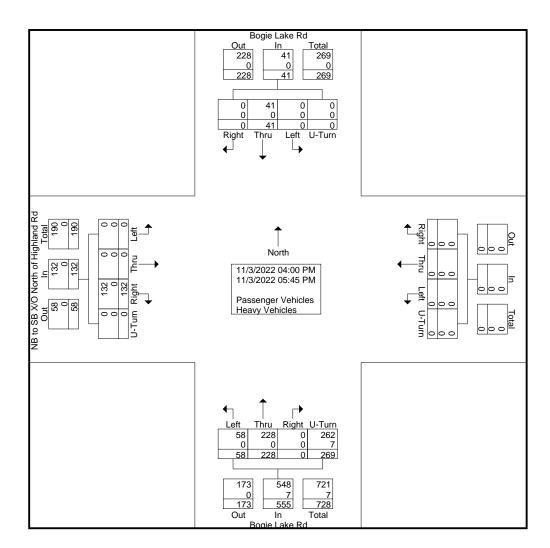


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Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A								of 1													
Peak Hour fo	pr Entir	e Inter	sectio	n Begi	ns at 07	:00 AN	1														
07:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total Volume	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% App. Total	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
PHF	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000



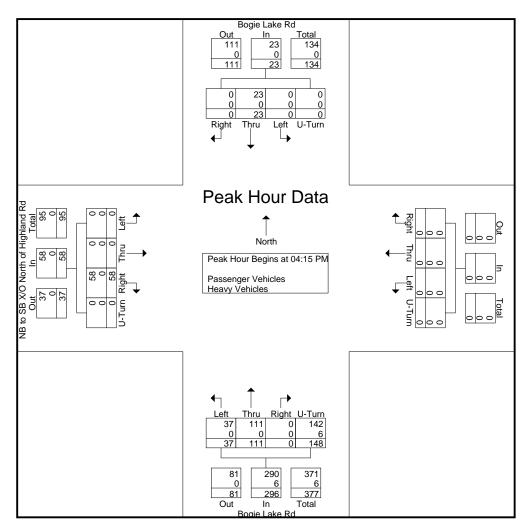


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Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
04:00 PM	0	0	18	0	18	0	0	0	0	0	4	28	0	30	62	0	2	0	0	2	82
04:15 PM	0	0	12	0	12	0	0	0	0	0	7	34	0	43	84	0	11	0	0	11	107
04:30 PM	0	0	13	0	13	0	0	0	0	0	8	16	0	36	60	0	3	0	0	3	76
04:45 PM	0	0	18	0	18	0	0	0	0	0	12	34	0	40	86	0	4	0	0	4	108
Total	0	0	61	0	61	0	0	0	0	0	31	112	0	149	292	0	20	0	0	20	373
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Grand Total	0	0	132	0	132	0	0	0	0	0	58	228	0	269	555	0	41	0	0	41	728
Apprch %	0	0	100	0	-	0	0	0	0	-	10.5	41.1	0	48.5		0	100	0	0		-
Total %	Ō	Ō	18.1	Ō	18.1	Ō	Ō	Ō	Ō	0	8	31.3	Ō	37	76.2	Ō	5.6	Ō	Ō	5.6	
Passenger Vehicles	0	0	132	0	132	0	0	0	0	0	58	228	0	262	548	0	41	0	0	41	721
% Passenger Vehicles	0	0	100	0	100	0	0	0	0	0	100	100	0	97.4	98.7	0	100	0	0	100	99
Heavy Vehicles	0	0	0	0	0	0	0	0	0	0	0	0	0	7	7	0	0	0	0	0	7
% Heavy Vehicles	0	0	0	0	0	0	0	0	0	0	0	0	0	2.6	1.3	0	0	0	0	0	1



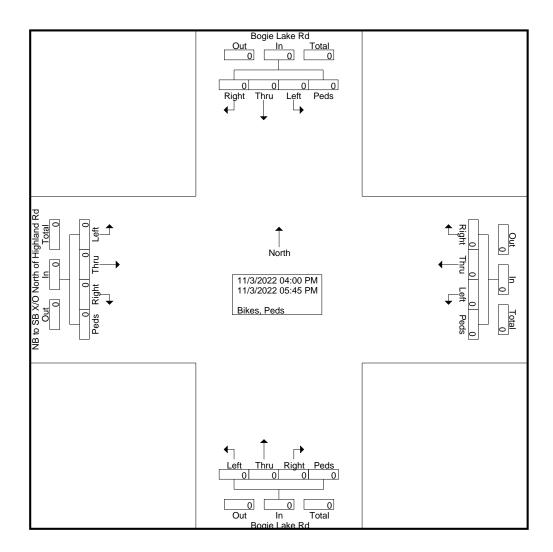


	Ν	Hi	B X/O ghland astbou	Rd	of		W	/estboi	und				jie Lak orthbo					gie Lak outhbo			
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
Peak Hour A								of 1													
Peak Hour fo	or Entir	e Inter	sectio	n Begi	ns at 04	:15 PN	1														
04:15 PM	0	0	12	0	12	0	0	0	0	0	7	34	0	43	84	0	11	0	0	11	107
04:30 PM	0	0	13	0	13	0	0	0	0	0	8	16	0	36	60	0	3	0	0	3	76
04:45 PM	0	0	18	0	18	0	0	0	0	0	12	34	0	40	86	0	4	0	0	4	108
05:00 PM	0	0	15	0	15	0	0	0	0	0	10	27	0	29	66	0	5	0	0	5	86
Total Volume	0	0	58	0	58	0	0	0	0	0	37	111	0	148	296	0	23	0	0	23	377
% App. Total	0	0	100	0		0	0	0	0		12.5	37.5	0	50		0	100	0	0		
PHF	.000	.000	.806	.000	.806	.000	.000	.000	.000	.000	.771	.816	.000	.860	.860	.000	.523	.000	.000	.523	.873
Passenger Vehicles	0	0	58	0	58	0	0	0	0	0	37	111	0	142	290	0	23	0	0	23	371
% Passenger Vehicles	0	0	100	0	100	0	0	0	0	0	100	100	0	95.9	98.0	0	100	0	0	100	98.4
Heavy Vehicles	0	0	0	0	0	0	0	0	0	0	0	0	0	6	6	0	0	0	0	0	6
% Heavy Vehicles	0	0	0	0	0	0	0	0	0	0	0	0	0	4.1	2.0	0	0	0	0	0	1.6



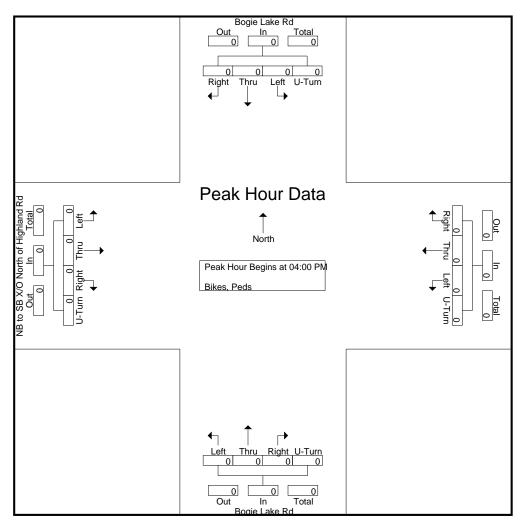


								G	roups	Printed-	Bikes	, Peds									
	٢		B X/O ghland astbou	Rd	of		W	/estbo	und				gie Lak orthbo					jie Lak outhbo			
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Grand Total Apprch % Total %	0 0	0 0	0 0	0 0	0	0 0	0 0	0 0	0 0	0	0 0	0 0	0 0	0 0	0	0 0	0 0	0 0	0 0	0	0



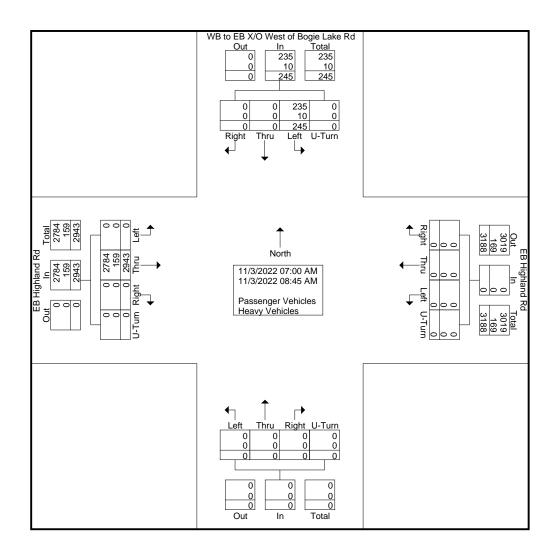


	Ν	Hię	B X/O ghland astbou		of		W	estbo	und				jie Lak orthbo					gie Lak outhbo			
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A	nalysis	From	04:00	PM to	05:45 F	PM - P	eak 1 o	of 1													
Peak Hour fo	or Entir	e Inter	sectio	n Begiı	ns at 04	:00 PN	/														
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total Volume	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% App. Total	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
PHF	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000



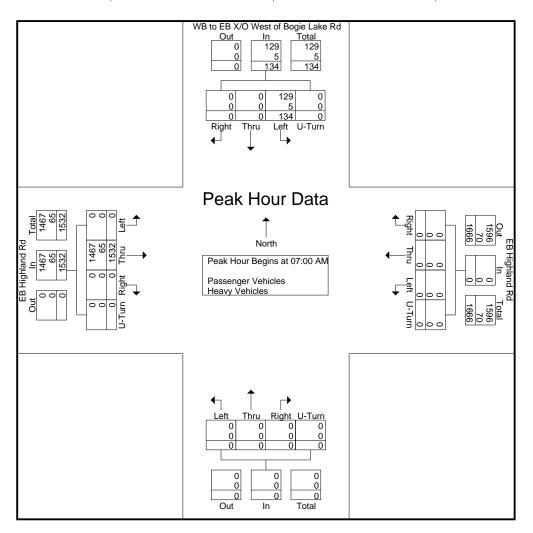


						G	roups	Printe	d- Pas	senger	/ehicle	es - He	avy Ve	ehicles	;						_
		EBH	Highlar	nd Rd			EB	Highla	nd Rd	-						WB	to EB 2			Bogie	
			astbou					estbo				N	orthbo	und				_ake R outhbou			
Ctort Times	1	Thru	Dista			1	Thru	District			1	Thru	District			1	Thru				[
Start Time	Left		Right	U-Turn	App. Total	Left		Right	U-Turn	App. Total	Left		Right	U-Turn	App. Total	Left		Right	U-Turn	App. Total	Int. Total
07:00 AM	0	423	0	0	423	0	0	0	0	0	0	0	0	0	0	55	0	0	0	55	478
07:15 AM	0	369	0	0	369	0	0	0	0	0	0	0	0	0	0	25	0	0	0	25	394
07:30 AM	0	393	0	0	393	0	0	0	0	0	0	0	0	0	0	20	0	0	0	20	413
07:45 AM	0	347	0	0	347	0	0	0	0	0	0	0	0	0	0	34	0	0	0	34	381
Total	0	1532	0	0	1532	0	0	0	0	0	0	0	0	0	0	134	0	0	0	134	1666
1																					
08:00 AM	0	356	0	0	356	0	0	0	0	0	0	0	0	0	0	41	0	0	0	41	397
08:15 AM	0	361	0	0	361	0	0	0	0	0	0	0	0	0	0	28	0	0	0	28	389
08:30 AM	0	343	0	0	343	0	0	0	0	0	0	0	0	0	0	11	0	0	0	11	354
08:45 AM	0	351	0	0	351	0	0	0	0	0	0	0	0	0	0	31	0	0	0	31	382
Total	0	1411	0	0	1411	0	0	0	0	0	0	0	0	0	0	111	0	0	0	111	1522
Grand Total	0	2943	0	0	2943	0	0	0	0	0	0	0	0	0	0	245	0	0	0	245	3188
Apprch %	0	100	0	0		0	0	0	0		0	0	0	0		100	0	0	0		1
Total %	0	92.3	0	0	92.3	0	0	0	0	0	0	0	0	0	0	7.7	0	0	0	7.7	
Passenger Vehicles	0	2784	0	0	2784	0	0	0	0	0	0	0	0	0	0	235	0	0	0	235	3019
% Passenger Vehicles	0	94.6	0	0	94.6	0	0	0	0	0	0	0	0	0	0	95.9	0	0	0	95.9	94.7
Heavy Vehicles	0	159	0	0	159	0	0	0	0	0	0	0	0	0	0	10	0	0	0	10	169
% Heavy Vehicles	0	5.4	0	0	5.4	0	0	0	0	0	0	0	0	0	0	4.1	0	0	0	4.1	5.3



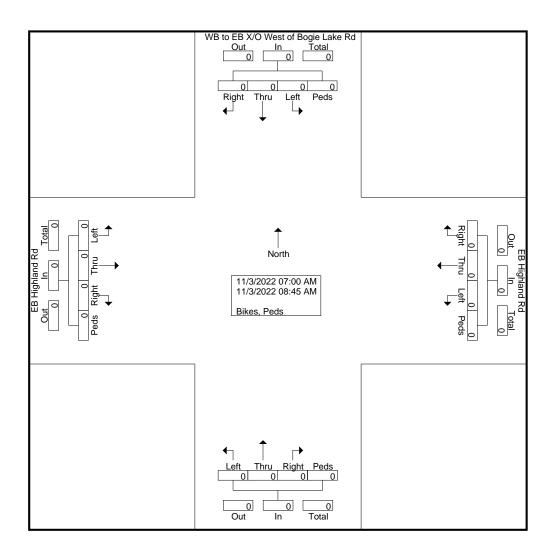


			-lighlar astbou					Highlai /estboi				N	orthbo	und		WB	I	X/O W Lake R outhbo	۲d	Bogie	
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
Peak Hour A								of 1													
Peak Hour fo	or Entir	e Inter	sectio	n Begi	ns at 07	:00 AN	/														
07:00 AM	0	423	0	0	423	0	0	0	0	0	0	0	0	0	0	55	0	0	0	55	478
07:15 AM	0	369	0	0	369	0	0	0	0	0	0	0	0	0	0	25	0	0	0	25	394
07:30 AM	0	393	0	0	393	0	0	0	0	0	0	0	0	0	0	20	0	0	0	20	413
07:45 AM	0	347	0	0	347	0	0	0	0	0	0	0	0	0	0	34	0	0	0	34	381
Total Volume	0	1532	0	0	1532	0	0	0	0	0	0	0	0	0	0	134	0	0	0	134	1666
% App. Total	0	100	0	0		0	0	0	0		0	0	0	0		100	0	0	0		
PHF	.000	.905	.000	.000	.905	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.609	.000	.000	.000	.609	.871
Passenger Vehicles	0	1467	0	0	1467	0	0	0	0	0	0	0	0	0	0	129	0	0	0	129	1596
% Passenger Vehicles	0	95.8	0	0	95.8	0	0	0	0	0	0	0	0	0	0	96.3	0	0	0	96.3	95.8
Heavy Vehicles	0	65	0	0	65	0	0	0	0	0	0	0	0	0	0	5	0	0	0	5	70
% Heavy Vehicles	0	4.2	0	0	4.2	0	0	0	0	0	0	0	0	0	0	3.7	0	0	0	3.7	4.2



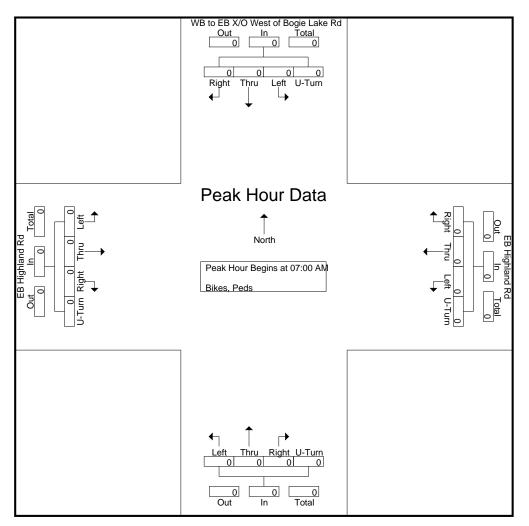


								G	roups	Printed-	Bikes	, Peds									
			Highla astboເ					Highla /estbo				N	orthbo	und		WB	I	X/O W Lake R	۲d	Bogie	
			401000					00100										<u>outhbo</u>	und		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
07:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Grand Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Apprch % Total %	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		



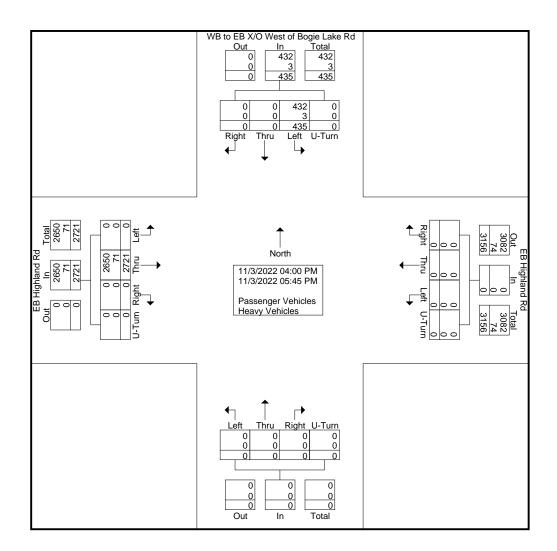


			Highlar astbou					lighlai estbo				N	orthbo	und		WB	I	X/O W Lake R outhbo		Bogie	
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A								of 1													
Peak Hour fo	pr Entir	e Inter	section	n Begir	ns at 07	:00 AN	Λ														
07:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total Volume	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% App. Total	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
PHF	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000



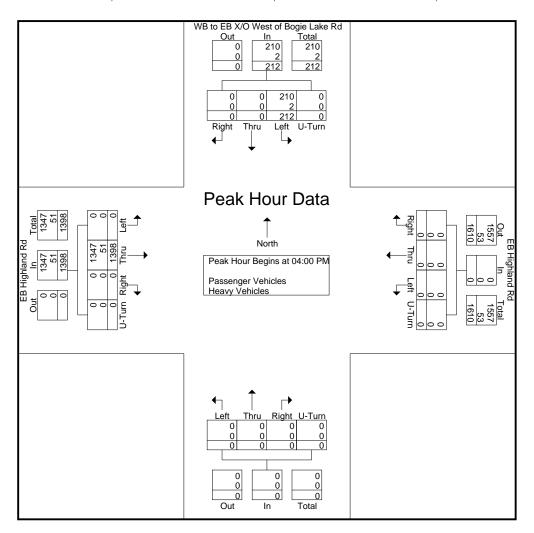


						G	roups	Printe	d- Pas	senger	/ehicle	es - He	avy Ve	ehicles	;						
		FBF	Highlar	nd Rd			FB	Highla	nd Rd	-						WB	to EB 2			Bogie	
			astbou					estbo				N	orthboi	und				_ake R			
				-			-											outhbou			
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
04:00 PM	0	352	0	0	352	0	0	0	0	0	0	0	0	0	0	52	0	0	0	52	404
04:15 PM	0	338	0	0	338	0	0	0	0	0	0	0	0	0	0	60	0	0	0	60	398
04:30 PM	0	373	0	0	373	0	0	0	0	0	0	0	0	0	0	43	0	0	0	43	416
04:45 PM	0	335	0	0	335	0	0	0	0	0	0	0	0	0	0	57	0	0	0	57	392
Total	0	1398	0	0	1398	0	0	0	0	0	0	0	0	0	0	212	0	0	0	212	1610
05:00 PM	0	309	0	0	309	0	0	0	0	0	0	0	0	0	0	64	0	0	0	64	373
05:15 PM	0	355	0	0	355	0	0	0	0	0	0	0	0	0	0	61	0	0	0	61	416
05:30 PM	0	334	0	0	334	0	0	0	0	0	0	0	0	0	0	60	0	0	0	60	394
05:45 PM	0	325	0	0	325	0	0	0	0	0	0	0	0	0	0	38	0	0	0	38	363
Total	0	1323	0	0	1323	0	0	0	0	0	0	0	0	0	0	223	0	0	0	223	1546
Grand Total	0	2721	0	0	2721	0	0	0	0	0	0	0	0	0	0	435	0	0	0	435	3156
Apprch %	0	100	0	0		0	0	0	0		0	0	0	0		100	0	0	0		
Total %	0	86.2	0	0	86.2	0	0	0	0	0	0	0	0	0	0	13.8	0	0	0	13.8	
Passenger Vehicles	0	2650	0	0	2650	0	0	0	0	0	0	0	0	0	0	432	0	0	0	432	3082
% Passenger Vehicles	0	97.4	0	0	97.4	0	0	0	0	0	0	0	0	0	0	99.3	0	0	0	99.3	97.7
Heavy Vehicles	0	71	0	0	71	0	0	0	0	0	0	0	0	0	0	3	0	0	0	3	74
% Heavy Vehicles	0	2.6	0	0	2.6	0	0	0	0	0	0	0	0	0	0	0.7	0	0	0	0.7	2.3



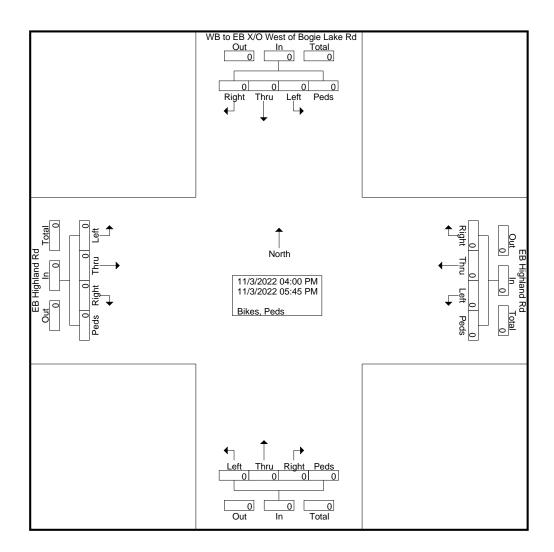


			-lighlar astbou					Highlai estbou				N	orthbo	und		WB		X/O W Lake F outhbo	۲d	Bogie	
Start Time	Left	Thru	Right	U-Turn	App. Total	Left							Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
Peak Hour A								of 1													
Peak Hour fo	or Entir	e Inter	section	n Begi	ns at 04	:00 PN	Λ														
04:00 PM	0	352	0	0	352	0	0	0	0	0	0	0	0	0	0	52	0	0	0	52	404
04:15 PM	0	338	0	0	338	0	0	0	0	0	0	0	0	0	0	60	0	0	0	60	398
04:30 PM	0	373	0	0	373	0	0	0	0	0	0	0	0	0	0	43	0	0	0	43	416
04:45 PM	0	335	0	0	335	0	0	0	0	0	0	0	0	0	0	57	0	0	0	57	392
Total Volume	0	1398	0	0	1398	0	0	0	0	0	0	0	0	0	0	212	0	0	0	212	1610
% App. Total	0	100	0	0		0	0	0	0		0	0	0	0		100	0	0	0		
PHF	.000	.937	.000	.000	.937	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.883	.000	.000	.000	.883	.968
Passenger Vehicles	0	1347	0	0	1347	0	0	0	0	0	0	0	0	0	0	210	0	0	0	210	1557
% Passenger Vehicles	0	96.4	0	0	96.4	0	0	0	0	0	0	0	0	0	0	99.1	0	0	0	99.1	96.7
Heavy Vehicles	0	51	0	0	51	0	0	0	0	0	0	0	0	0	0	2	0	0	0	2	53
% Heavy Vehicles	0	3.6	0	0	3.6	0	0	0	0	0	0	0	0	0	0	0.9	0	0	0	0.9	3.3



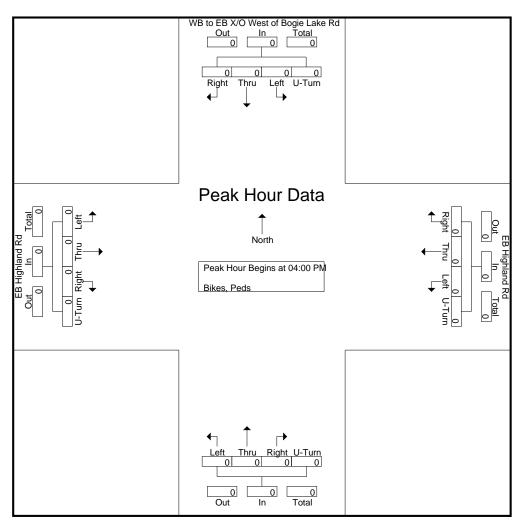


								G	Groups	Printed-	Bikes	, Peds									_
			Highlai astbou					Highla /estbo				N	orthbo	und		WB	1	X/O W Lake R	۲d	Bogie	
Ctort Time	1	Thru	Disht	Peds		1	Thru	Disht	Peds		1	Thru	Disht	Peds		1	Thru	Diabt	Peds		
Start Time	Left		Right		App. Total	Left	-	Right		App. Total	Left		Right		App. Total	Left		Right	Peus	App. Total	Int. Total
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Grand Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Apprch % Total %	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		

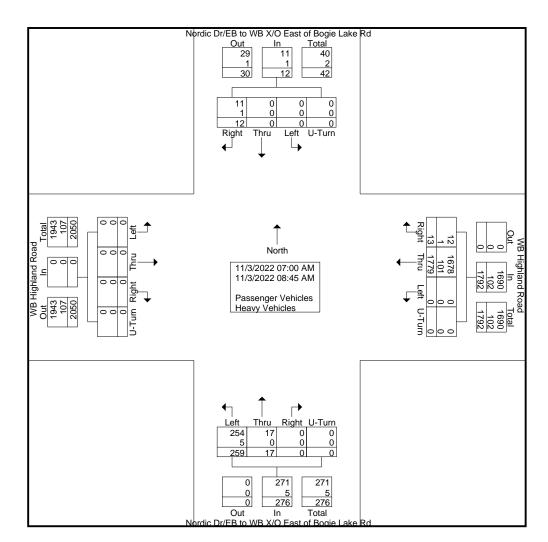




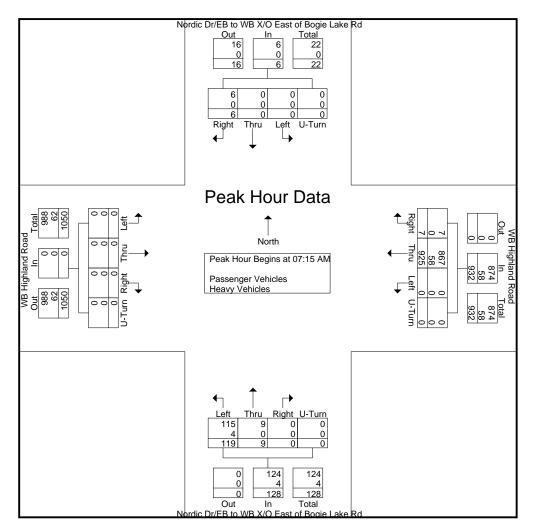
			lighlaı astbou					-lighla ′estbo				N	orthbo	und		WB	I	X/O W Lake F outhbo		Bogie	
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A	nalysis	s From	04:00	PM to	05:45 F	PM - P	eak 1	of 1													
Peak Hour fo	or Entir	e Inter	sectio	n Begi	ns at 04	:00 PN	1														
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total Volume	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% App. Total	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
PHF	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000



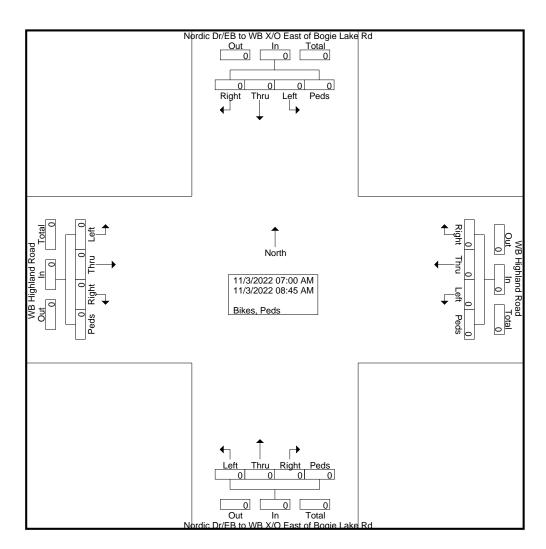
						G	roups	Printe	d- Pas	senger '	Vehicle	es - He	avy Ve	ehicles	5						
		WB Hi	iahlan	1 Road	ч		wвн	iahlan	d Road	4	Nord				D East	Nord			VB X/C) East	
			astbou		^			estbo		A			0	ke Rd					ike Rd		
				inu					unu				orthbo	und				outhbo	und		
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
07:00 AM	0	0	0	0	0	0	189	1	0	190	28	0	0	0	28	0	0	1	0	1	219
07:15 AM	0	0	0	0	0	0	220	1	0	221	37	4	0	0	41	0	0	2	0	2	264
07:30 AM	0	0	0	0	0	0	231	2	0	233	27	1	0	0	28	0	0	1	0	1	262
07:45 AM	0	0	0	0	0	0	243	3	0	246	30	3	0	0	33	0	0	2	0	2	281
Total	0	0	0	0	0	0	883	7	0	890	122	8	0	0	130	0	0	6	0	6	1026
1																					
08:00 AM	0	0	0	0	0	0	231	1	0	232	25	1	0	0	26	0	0	1	0	1	259
08:15 AM	0	0	0	0	0	0	208	0	0	208	46	2	0	0	48	0	0	1	0	1	257
08:30 AM	0	0	0	0	0	0	226	2	0	228	29	1	0	0	30	0	0	0	0	0	258
08:45 AM	0	0	0	0	0	0	231	3	0	234	37	5	0	0	42	0	0	4	0	4	280
Total	0	0	0	0	0	0	896	6	0	902	137	9	0	0	146	0	0	6	0	6	1054
Grand Total	0	0	0	0	0	0	1779	13	0	1792	259	17	0	0	276	0	0	12	0	12	2080
Apprch %	0	0	0	0		0	99.3	0.7	0		93.8	6.2	0	0		0	0	100	0		
Total %	0	0	0	0	0	0	85.5	0.6	0	86.2	12.5	0.8	0	0	13.3	0	0	0.6	0	0.6	
Passenger Vehicles	0	0	0	0	0	0	1678	12	0	1690	254	17	0	0	271	0	0	11	0	11	1972
% Passenger Vehicles	0	0	0	0	0	0	94.3	92.3	0	94.3	98.1	100	0	0	98.2	0	0	91.7	0	91.7	94.8
Heavy Vehicles	0	0	0	0	0	0	101	1	0	102	5	0	0	0	5	0	0	1	0	1	108
% Heavy Vehicles	0	0	0	0	0	0	5.7	7.7	0	5.7	1.9	0	0	0	1.8	0	0	8.3	0	8.3	5.2



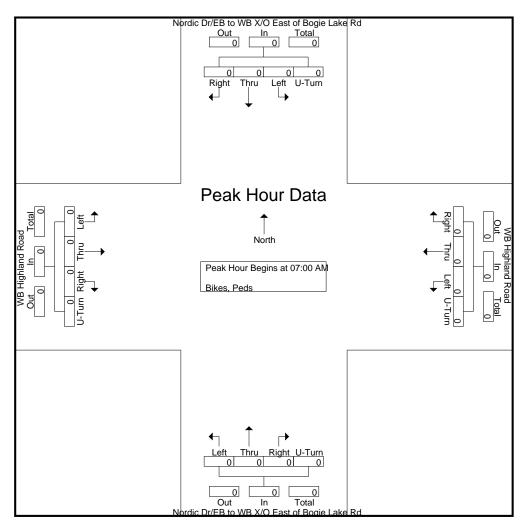
			ighland astbou	d Road Ind	1			ighland estbou		1	Nord	of Bo		VB X/C ke Rd und) East	Nord	of Bo		ke Rd) East	
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
Peak Hour A	nalysis	s From	07:00	AM to	08:45 A	λM - Ρ	eak 1	of 1													
Peak Hour fo	pr Entir	e Inter	sectio	n Begiı	ns at 07	:15 AN	1														
07:15 AM	0	0	0	0	0	0	220	1	0	221	37	4	0	0	41	0	0	2	0	2	264
07:30 AM	0	0	0	0	0	0	231	2	0	233	27	1	0	0	28	0	0	1	0	1	262
07:45 AM	0	0	0	0	0	0	243	3	0	246	30	3	0	0	33	0	0	2	0	2	281
08:00 AM	0	0	0	0	0	0	231	1	0	232	25	1	0	0	26	0	0	1	0	1	259
Total Volume	0	0	0	0	0	0	925	7	0	932	119	9	0	0	128	0	0	6	0	6	1066
% App. Total	0	0	0	0		0	99.2	0.8	0		93	7	0	0		0	0	100	0		
PHF	.000	.000	.000	.000	.000	.000	.952	.583	.000	.947	.804	.563	.000	.000	.780	.000	.000	.750	.000	.750	.948
Passenger Vehicles	0	0	0	0	0	0	867	7	0	874	115	9	0	0	124	0	0	6	0	6	1004
% Passenger Vehicles	0	0	0	0	0	0	93.7	100	0	93.8	96.6	100	0	0	96.9	0	0	100	0	100	94.2
Heavy Vehicles	0	0	0	0	0	0	58	0	0	58	4	0	0	0	4	0	0	0	0	0	62
% Heavy Vehicles	0	0	0	0	0	0	6.3	0	0	6.2	3.4	0	0	0	3.1	0	0	0	0	0	5.8



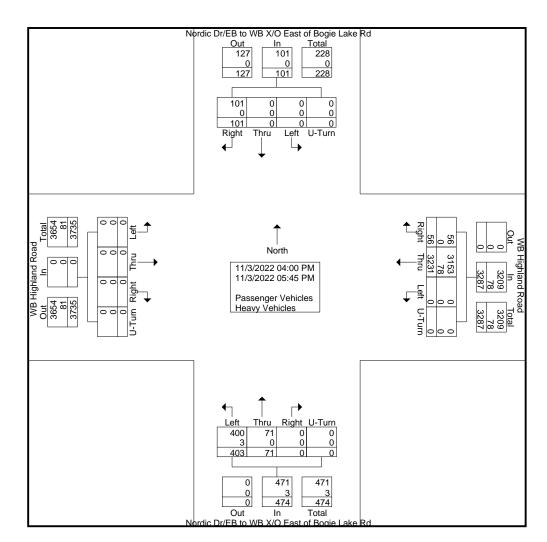
								G	iroups	Printed-	Bikes	, Peds									
		WB H	iahlan	d Road	4		WR H	ighland	d Road	4	Nord) East	Nord) East	
			astbou		1			/estboi		1				ike Rd				ogie La			
			431501										orthbo	und				outhbo			
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
07:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:15 AM	0	0	0	0	0	0	0 0 0 0 0					0	0	0	0	0	0	0	0	0	0
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Grand Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Apprch %	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
Total %																					



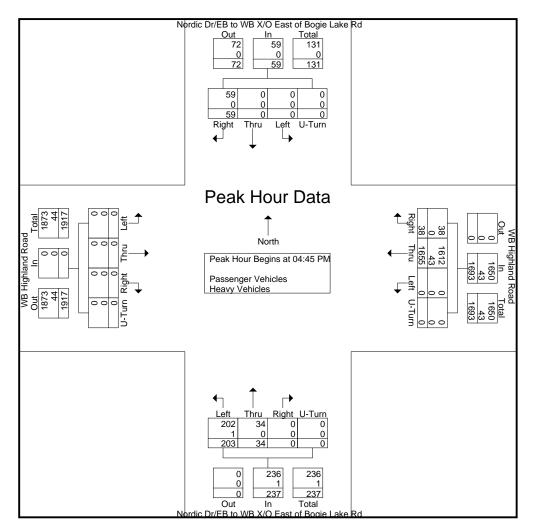
			ighlano astbou	d Road Ind	l			ighlan 'estboi	d Road und	I	Norc	of Bo		ke Rd) East	Nord	of Bo		ke Rd) East	
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A								of 1													
Peak Hour fo	or Entir	e Inter	section	n Begiı	ns at 07	:00 AN	1														
07:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total Volume	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% App. Total	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
PHF	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000



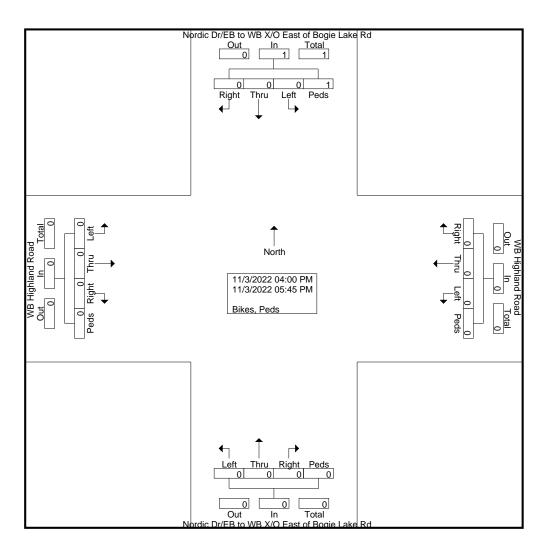
						G	roups	Printe	d- Pas	senger '	Vehicle	es - He	avy Ve	ehicles	5						
		WB Hi	iahlan	d Road	4		WВН	iahlan	d Road	4	Nord				D East	Nord				D East	
			astbou		۲ ×			estbol		•			ogie La					ogie La			
			a31001					631001					orthbo	und				outhbo	und		
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
04:00 PM	0	0	0	0	0	0	426	4	0	430	50	7	0	0	57	0	0	6	0	6	493
04:15 PM	0	0	0	0	0	0	438	3	0	441	58	7	0	0	65	0	0	14	0	14	520
04:30 PM	0	0	0	0	0	0	381	5	0	386	45	11	0	0	56	0	0	10	0	10	452
04:45 PM	0	0	0	0	0	0	438	7	0	445	45	12	0	0	57	0	0	19	0	19	521
Total	0	0	0	0	0	0	1683	19	0	1702	198	37	0	0	235	0	0	49	0	49	1986
05:00 PM	0	0	0	0	0	0	416	7	0	423	46	8	0	0	54	0	0	8	0	8	485
05:15 PM	0	0	0	0	0	0	411	13	0	424	67	8	0	0	75	0	0	12	0	12	511
05:30 PM	0	0	0	0	0	0	390	11	0	401	45	6	0	0	51	0	0	20	0	20	472
05:45 PM	0	0	0	0	0	0	331	6	0	337	47	12	0	0	59	0	0	12	0	12	408
Total	0	0	0	0	0	0	1548	37	0	1585	205	34	0	0	239	0	0	52	0	52	1876
Grand Total	0	0	0	0	0	0	3231	56	0	3287	403	71	0	0	474	0	0	101	0	101	3862
Apprch %	0	0	0	0		0	98.3	1.7	0		85	15	0	0		0	0	100	0		
Total %	0	0	0	0	0	0	83.7	1.5	0	85.1	10.4	1.8	0	0	12.3	0	0	2.6	0	2.6	
Passenger Vehicles	0	0	0	0	0	0	3153	56	0	3209	400	71	0	0	471	0	0	101	0	101	3781
% Passenger Vehicles	0	0	0	0	0	0	97.6	100	0	97.6	99.3	100	0	0	99.4	0	0	100	0	100	97.9
Heavy Vehicles	0	0	0	0	0	0	78	0	0	78	3	0	0	0	3	0	0	0	0	0	81
% Heavy Vehicles	0	0	0	0	0	0	2.4	0	0	2.4	0.7	0	0	0	0.6	0	0	0	0	0	2.1



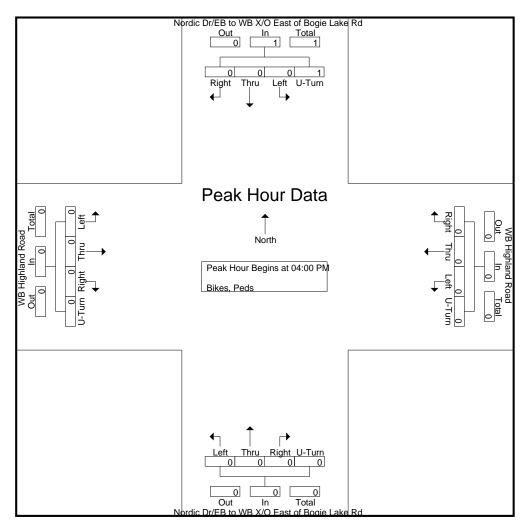
			ighland astbou	d Roac Ind	1			ighlan /estboi	d Road und	1	Norc	of Bo		VB X/C ike Rd und) East	Nord	of Bo	B to V gie La outhbo	ke Rd) East	
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
Peak Hour A	nalysis	s From	04:00	PM to	05:45 F	PM - P	eak 1	of 1													
Peak Hour fo	or Entir	e Inter	sectio	n Begii	ns at 04	:45 PN	/														
04:45 PM	0	0	0	0	0	0	438	7	0	445	45	12	0	0	57	0	0	19	0	19	521
05:00 PM	0	0	0	0	0	0	416	7	0	423	46	8	0	0	54	0	0	8	0	8	485
05:15 PM	0	0	0	0	0	0	411	13	0	424	67	8	0	0	75	0	0	12	0	12	511
05:30 PM	0	0	0	0	0	0	390	11	0	401	45	6	0	0	51	0	0	20	0	20	472
Total Volume	0	0	0	0	0	0	1655	38	0	1693	203	34	0	0	237	0	0	59	0	59	1989
% App. Total	0	0	0	0		0	97.8	2.2	0		85.7	14.3	0	0		0	0	100	0		
PHF	.000	.000	.000	.000	.000	.000	.945	.731	.000	.951	.757	.708	.000	.000	.790	.000	.000	.738	.000	.738	.954
Passenger Vehicles	0	0	0	0	0	0	1612	38	0	1650	202	34	0	0	236	0	0	59	0	59	1945
% Passenger Vehicles	0	0	0	0	0	0	97.4	100	0	97.5	99.5	100	0	0	99.6	0	0	100	0	100	97.8
Heavy Vehicles	0	0	0	0	0	0	43	0	0	43	1	0	0	0	1	0	0	0	0	0	44
% Heavy Vehicles	0	0	0	0	0	0	2.6	0	0	2.5	0.5	0	0	0	0.4	0	0	0	0	0	2.2



								G	iroups	Printed-	Bikes	, Peds									
		WB Hi	iablan		4		м р ц	ighlan	d Door	4	Nord	lic Dr/E	EB to V	VB X/C) East	Nord	lic Dr/E	EB to V	VB X/C	D East	
			astbou		, I			estbo				of Bo	ogie La	ake Rd			of Bo	ogie La	ke Rd		
			asibol	ina			vv	esibol	una			No	orthbo	und			Sc	outhbo	und		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1
04:15 PM	0	0	0	0	0						0	0	0	0	0	0	0	0	0	0	0
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1
05:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Grand Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1
Apprch %	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	100		
Total %	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	100	100	

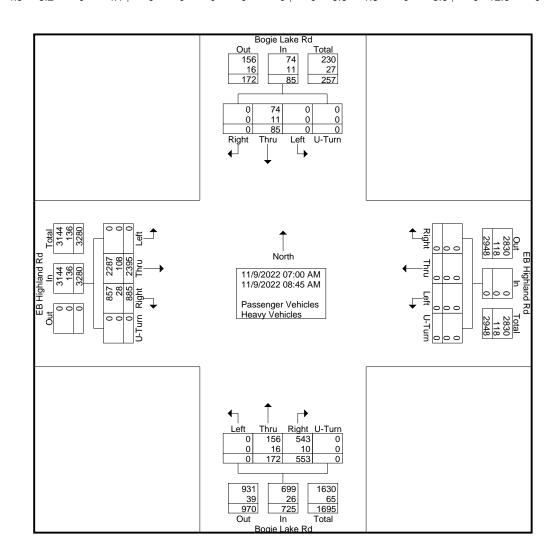


			ighlan astbou	d Road Ind	l			ighlan 'estboi	d Road und	1	Norc	of Bo		ke Rd) East	Nord	of Bo	EB to V ogie La outhbo	ke Rd) East	
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A	nalysis	s From	04:00	PM to	05:45 F	PM - P	eak 1	of 1													
Peak Hour fo	or Entir	e Inter	sectio	n Begiı	ns at 04	:00 PN	1														
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total Volume	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1
% App. Total	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	100		
PHF	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.250	.250	.250



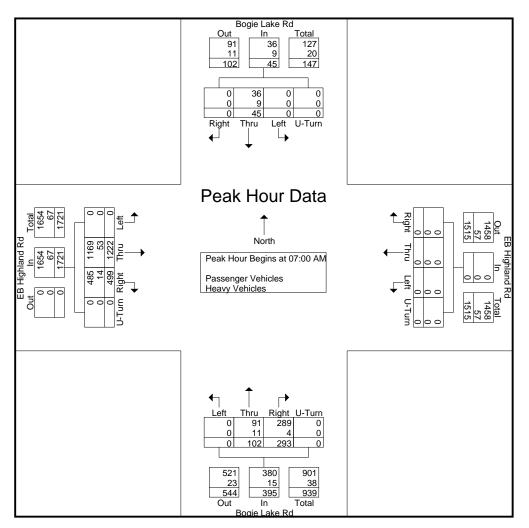


						G	roups	Printe	d- Pas	senger	/ehicle	es - He	avv V	ehicles							
		EB I	Highlar	nd Rd				Highlar		J			gie Lak				Boo	jie Lak	e Rd		[
			astbou				W	estbou	und				orthbo					outhbo			
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
07:00 AM	0	294	190	0	484	0	0	0	0	0	0	32	76	0	108	0	14	0	0	14	606
07:15 AM	0	331	85	0	416	0	0	0	0	0	0	29	84	0	113	0	7	0	0	7	536
07:30 AM	0	313	110	0	423	0	0	0	0	0	0	24	69	0	93	0	10	0	0	10	526
07:45 AM	0	284	114	0	398	0	0	0	0	0	0	17	64	0	81	0	14	0	0	14	493
Total	0	1222	499	0	1721	0	0	0	0	0	0	102	293	0	395	0	45	0	0	45	2161
08:00 AM	0	293	130	0	423	0	0	0	0	0	0	26	78	0	104	0	11	0	0	11	538
08:15 AM	0	317	91	0	408	0	0	0	0	0	0	19	64	0	83	0	7	0	0	7	498
08:30 AM	0	283	68	0	351	0	0	0	0	0	0	14	49	0	63	0	7	0	0	7	421
08:45 AM	0	280	97	0	377	0	0	0	0	0	0	11	69	0	80	0	15	0	0	15	472
Total	0	1173	386	0	1559	0	0	0	0	0	0	70	260	0	330	0	40	0	0	40	1929
Grand Total	0	2395	885	0	3280	0	0	0	0	0	0	172	553	0	725	0	85	0	0	85	4090
Apprch %	0	73	27	0		0	0	0	0		0	23.7	76.3	0		0	100	0	0		
Total %	0	58.6	21.6	0	80.2	0	0	0	0	0	0	4.2	13.5	0	17.7	0	2.1	0	0	2.1	
Passenger Vehicles	0	2287	857	0	3144	0	0	0	0	0	0	156	543	0	699	0	74	0	0	74	3917
% Passenger Vehicles	0	95.5	96.8	0	95.9	0	0	0	0	0	0	90.7	98.2	0	96.4	0	87.1	0	0	87.1	95.8
Heavy Vehicles	0	108	28	0	136	0	0	0	0	0	0	16	10	0	26	0	11	0	0	11	173
% Heavy Vehicles	0	4.5	3.2	0	4.1	0	0	0	0	0	0	9.3	1.8	0	3.6	0	12.9	0	0	12.9	4.2



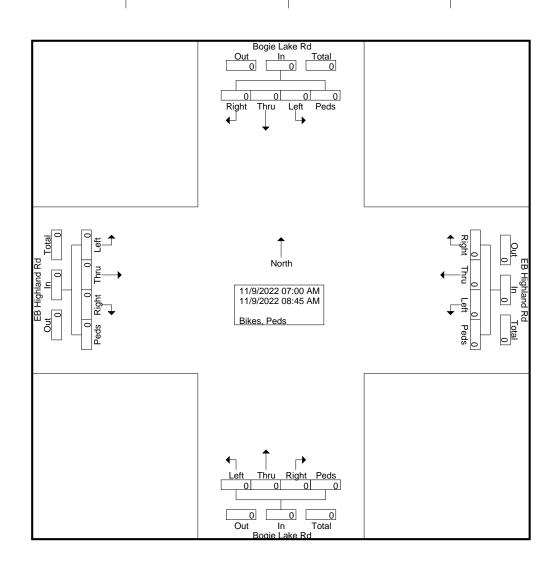


			Highlar astbou					Highla /estbo					gie Lak orthbo					gie Lak outhbo			
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
Peak Hour A	nalysis	s From	07:00	AM to	08:45 A	4M - Ρ	eak 1	of 1													
Peak Hour fo	or Entir	e Inter	rsection	n Begir	ns at 07	:00 AN	1														
07:00 AM	0	294	190	0	484	0	0	0	0	0	0	32	76	0	108	0	14	0	0	14	606
07:15 AM	0	331	85	0	416	0	0	0	0	0	0	29	84	0	113	0	7	0	0	7	536
07:30 AM	0	313	110	0	423	0	0	0	0	0	0	24	69	0	93	0	10	0	0	10	526
07:45 AM	0	284	114	0	398	0	0	0	0	0	0	17	64	0	81	0	14	0	0	14	493
Total Volume	0	1222	499	0	1721	0	0	0	0	0	0	102	293	0	395	0	45	0	0	45	2161
% App. Total	0	71	29	0		0	0	0	0		0	25.8	74.2	0		0	100	0	0		
PHF	.000	.923	.657	.000	.889	.000	.000	.000	.000	.000	.000	.797	.872	.000	.874	.000	.804	.000	.000	.804	.892
Passenger Vehicles	0	1169	485	0	1654	0	0	0	0	0	0	91	289	0	380	0	36	0	0	36	2070
% Passenger Vehicles	0	95.7	97.2	0	96.1	0	0	0	0	0	0	89.2	98.6	0	96.2	0	80.0	0	0	80.0	95.8
Heavy Vehicles	0	53	14	0	67	0	0	0	0	0	0	11	4	0	15	0	9	0	0	9	91
% Heavy Vehicles	0	4.3	2.8	0	3.9	0	0	0	0	0	0	10.8	1.4	0	3.8	0	20.0	0	0	20.0	4.2



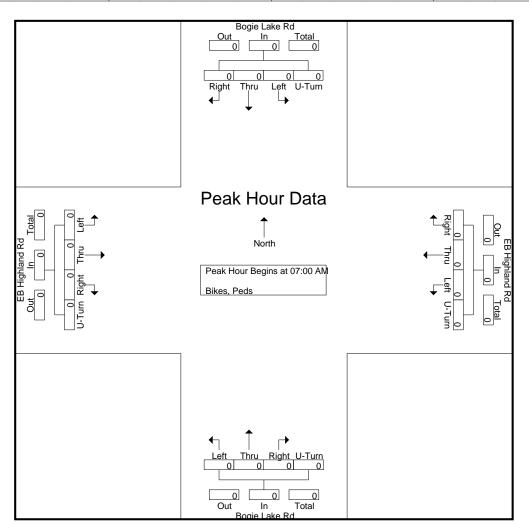


								G	iroups	Printed-	Bikes	, Peds									
		EB	Highlar	nd Rd			EB	Highla	nd Rd			Bog	jie Lak	e Rd			Bog	gie Lak	e Rd		
		E	astbou	Ind			W	estbo	und			N	orthbo	und			Sc	outhbo	und		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
07:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Grand Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Apprch % Total %	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		



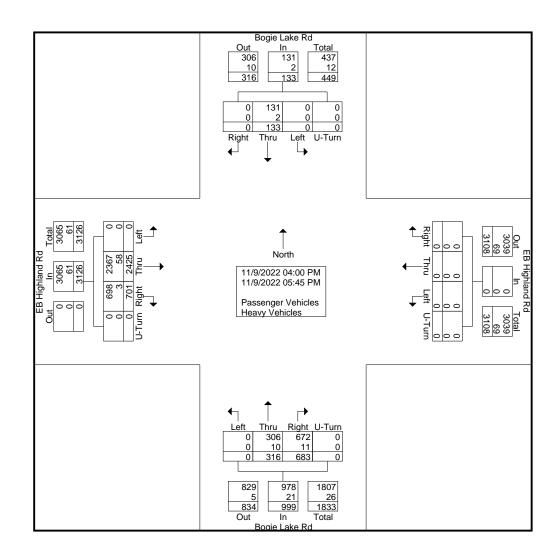


			Highlar astbou					Highla /estbo					jie Lak					gie Lak outhbo			
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru			App. Total	Int. Total
Peak Hour A	nalysis	s From	07:00	AM to	08:45	4M - P	1 - Peak 1 of 1														
Peak Hour fo	or Entir	e Inter	section	n Begi	ns at 07	:00 AN	Λ														
07:00 AM	0	0	0	Ō	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total Volume	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% App. Total	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
PHF	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000



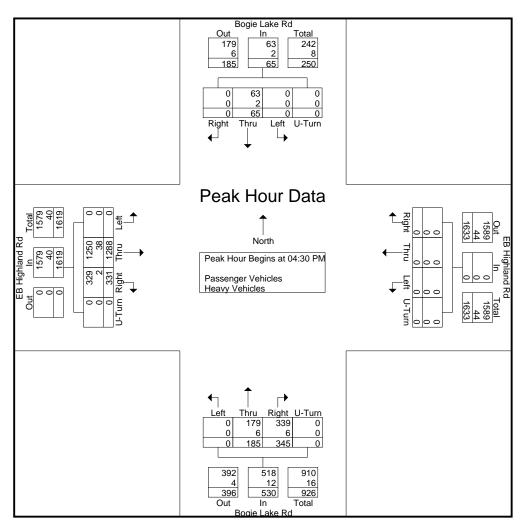


						G	roups	Printe	d- Pas	senger \	/ehicle	es - He	avy V	ehicles							
		EB I	Highlar	nd Rd			EB H	Highla	nd Rd			Bog	gie Lak	ke Rd			Bog	jie Lak	e Rd		
		E	astbou	und			W	estbou	und			N	orthbo	und			Sc	outhbo	und		
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
04:00 PM	0	266	64	0	330	0	0	0	0	0	0	31	106	0	137	0	18	0	0	18	485
04:15 PM	0	291	82	0	373	0	0	0	0	0	0	40	100	0	140	0	15	0	0	15	528
04:30 PM	0	336	80	0	416	0	0	0	0	0	0	48	87	0	135	0	19	0	0	19	570
04:45 PM	0	334	82	0	416	0	0	0	0	0	0	44	86	0	130	0	15	0	0	15	561
Total	0	1227	308	0	1535	0	0	0	0	0	0	163	379	0	542	0	67	0	0	67	2144
05:00 PM	0	295	85	0	380	0	0	0	0	0	0	54	88	0	142	0	16	0	0	16	538
05:15 PM	0	323	84	0	407	0	0	0	0	0	0	39	84	0	123	0	15	0	0	15	545
05:30 PM	0	306	100	0	406	0	0	0	0	0	0	39	66	0	105	0	16	0	0	16	527
05:45 PM	0	274	124	0	398	0	0	0	0	0	0	21	66	0	87	0	19	0	0	19	504
Total	0	1198	393	0	1591	0	0	0	0	0	0	153	304	0	457	0	66	0	0	66	2114
Grand Total	0	2425	701	0	3126	0	0	0	0	0	0	316	683	0	999	0	133	0	0	133	4258
Apprch %	0	77.6	22.4	0		0	0	0	0		0	31.6	68.4	0		0	100	0	0		
Total %	0	57	16.5	0	73.4	0	0	0	0	0	0	7.4	16	0	23.5	0	3.1	0	0	3.1	
Passenger Vehicles	0	2367	698	0	3065	0	0	0	0	0	0	306	672	0	978	0	131	0	0	131	4174
% Passenger Vehicles	0	97.6	99.6	0	98	0	0	0	0	0	0	96.8	98.4	0	97.9	0	98.5	0	0	98.5	98
Heavy Vehicles	0	58	3	0	61	0	0	0	0	0	0	10	11	0	21	0	2	0	0	2	84
% Heavy Vehicles	0	2.4	0.4	0	2	0	0	0	0	0	0	3.2	1.6	0	2.1	0	1.5	0	0	1.5	2



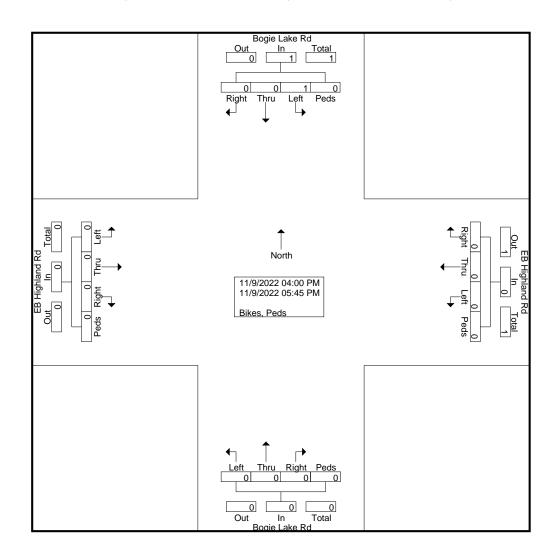


			Highlar astbou					Highla /estboi					gie Lak orthbo					gie Lak			
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
Peak Hour A	nalysis	s From	04:00	PM to	05:45 F	PM - P	eak 1	of 1													
Peak Hour fo	or Entir	e Inter	section	n Begir	ns at 04	:30 PN	1														
04:30 PM	0	336	80	Ō	416	0	0	0	0	0	0	48	87	0	135	0	19	0	0	19	570
04:45 PM	0	334	82	0	416	0	0	0	0	0	0	44	86	0	130	0	15	0	0	15	561
05:00 PM	0	295	85	0	380	0	0	0	0	0	0	54	88	0	142	0	16	0	0	16	538
05:15 PM	0	323	84	0	407	0	0	0	0	0	0	39	84	0	123	0	15	0	0	15	545
Total Volume	0	1288	331	0	1619	0	0	0	0	0	0	185	345	0	530	0	65	0	0	65	2214
% App. Total	0	79.6	20.4	0		0	0	0	0		0	34.9	65.1	0		0	100	0	0		
PHF	.000	.958	.974	.000	.973	.000	.000	.000	.000	.000	.000	.856	.980	.000	.933	.000	.855	.000	.000	.855	.971
Passenger Vehicles	0	1250	329	0	1579	0	0	0	0	0	0	179	339	0	518	0	63	0	0	63	2160
% Passenger Vehicles	0	97.0	99.4	0	97.5	0	0	0	0	0	0	96.8	98.3	0	97.7	0	96.9	0	0	96.9	97.6
Heavy Vehicles	0	38	2	0	40	0	0	0	0	0	0	6	6	0	12	0	2	0	0	2	54
% Heavy Vehicles	0	3.0	0.6	0	2.5	0	0	0	0	0	0	3.2	1.7	0	2.3	0	3.1	0	0	3.1	2.4



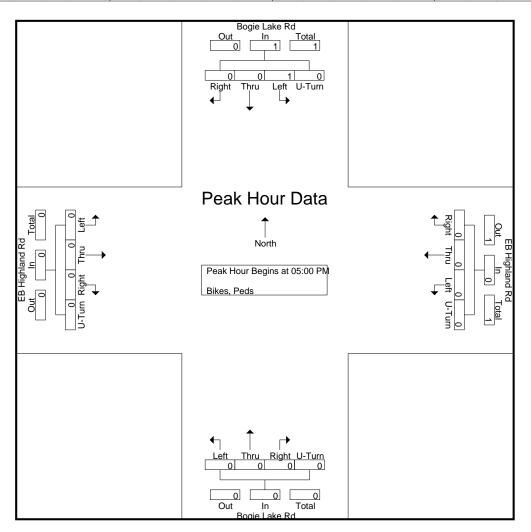


								G	roups	Printed-	Bikes	, Peds									
		EB	Highla	nd Rd			EB	Highla	nd Rd			Bog	jie Lak	ke Rd			Bog	jie Lak	e Rd		
		E	astbou	und			W	estbo	und			No	orthbo	und			Sc	outhbo	und		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1	1
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1	1
Crond Total	0	0	0	0	0		0	0	0	0	0	0	0	0		4	0	0	0	4	4
Grand Total	0	0	0	0	0		0	0	0	0	0	0	0	0	0	1	0	0	0	1	1
Apprch %	0	0	0	0		0	0	0	0		0	0	0	0		100	0	0	0	100	
Total %	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	100	0	0	0	100	



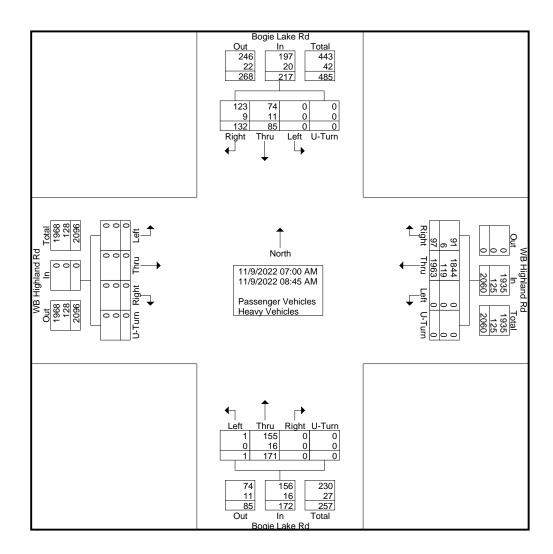


			-lighlar astbou					-lighlai estbo					jie Lak					gie Lak outhbo			
Start Time	Left	Thru			App. Total	Left				App. Total	Left	Thru	Right		App. Total	Left			Peds	App. Total	Int. Total
Peak Hour A	nalysis	s From	04:00	PM to	05:45 F	PM - P	eak 1	of 1													
Peak Hour fo	or Entir	e Inter	section	n Begi	ns at 05	:00 PN	/														
05:00 PM	0	0	0	Ō	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1	1
Total Volume	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1	1
% App. Total	0	0	0	0		0	0	0	0		0	0	0	0		100	0	0	0		Ĺ
PHF	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.250	.000	.000	.000	.250	.250



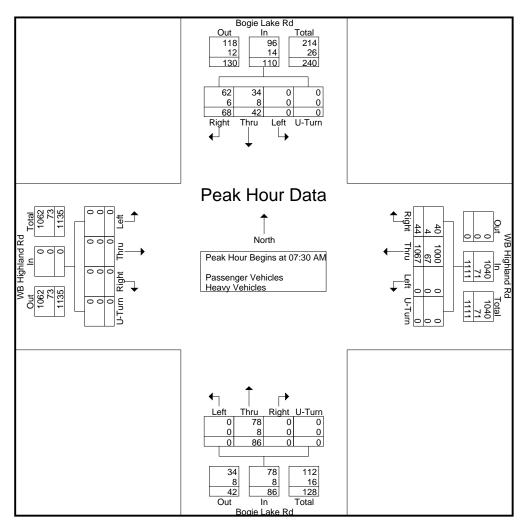


						G	roups	Printe	d- Pas	senger	/ehicle	es - He	avy V	ehicles							
		WB	Highla	nd Rd			WB	Highla	nd Rd			Bog	gie Lak	e Rd			Bog	gie Lak	e Rd		
		E	astbou	und			W	estbo	und			N	orthbo	und			Sc	outhbo	und		
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
07:00 AM	0	0	0	0	0	0	211	9	0	220	1	31	0	0	32	0	14	24	0	38	290
07:15 AM	0	0	0	0	0	0	218	9	0	227	0	29	0	0	29	0	7	23	0	30	286
07:30 AM	0	0	0	0	0	0	290	11	0	301	0	24	0	0	24	0	10	16	0	26	351
07:45 AM	0	0	0	0	0	0	282	9	0	291	0	17	0	0	17	0	14	14	0	28	336
Total	0	0	0	0	0	0	1001	38	0	1039	1	101	0	0	102	0	45	77	0	122	1263
08:00 AM	0	0	0	0	0	0	247	14	0	261	0	26	0	0	26	0	11	18	0	29	316
08:15 AM	0	0	0	0	0	0	248	10	0	258	0	19	0	0	19	0	7	20	0	27	304
08:30 AM	0	0	0	0	0	0	229	16	0	245	0	14	0	0	14	0	7	9	0	16	275
08:45 AM	0	0	0	0	0	0	238	19	0	257	0	11	0	0	11	0	15	8	0	23	291
Total	0	0	0	0	0	0	962	59	0	1021	0	70	0	0	70	0	40	55	0	95	1186
i																					
Grand Total	0	0	0	0	0	0	1963	97	0	2060	1	171	0	0	172	0	85	132	0	217	2449
Apprch %	0	0	0	0		0	95.3	4.7	0		0.6	99.4	0	0		0	39.2	60.8	0		
Total %	0	0	0	0	0	0	80.2	4	0	84.1	0	7	0	0	7	0	3.5	5.4	0	8.9	
Passenger Vehicles	0	0	0	0	0	0	1844	91	0	1935	1	155	0	0	156	0	74	123	0	197	2288
% Passenger Vehicles	0	0	0	0	0	0	93.9	93.8	0	93.9	100	90.6	0	0	90.7	0	87.1	93.2	0	90.8	93.4
Heavy Vehicles	0	0	0	0	0	0	119	6	0	125	0	16	0	0	16	0	11	9	0	20	161
% Heavy Vehicles	0	0	0	0	0	0	6.1	6.2	0	6.1	0	9.4	0	0	9.3	0	12.9	6.8	0	9.2	6.6



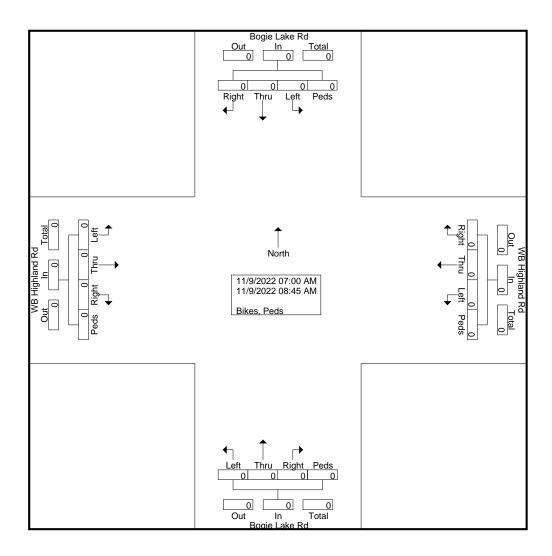


			Highlai astbou					Highla /estbou					jie Lak					gie Lak			
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
Peak Hour A								of 1													
Peak Hour fo	or Entir	e Inter	section	n Begir	ns at 07	:30 AN	/														
07:30 AM	0	0	0	Ō	0	0	290	11	0	301	0	24	0	0	24	0	10	16	0	26	351
07:45 AM	0	0	0	0	0	0	282	9	0	291	0	17	0	0	17	0	14	14	0	28	336
08:00 AM	0	0	0	0	0	0	247	14	0	261	0	26	0	0	26	0	11	18	0	29	316
08:15 AM	0	0	0	0	0	0	248	10	0	258	0	19	0	0	19	0	7	20	0	27	304
Total Volume	0	0	0	0	0	0	1067	44	0	1111	0	86	0	0	86	0	42	68	0	110	1307
% App. Total	0	0	0	0		0	96	4	0		0	100	0	0		0	38.2	61.8	0		
PHF	.000	.000	.000	.000	.000	.000	.920	.786	.000	.923	.000	.827	.000	.000	.827	.000	.750	.850	.000	.948	.931
Passenger Vehicles	0	0	0	0	0	0	1000	40	0	1040	0	78	0	0	78	0	34	62	0	96	1214
% Passenger Vehicles	0	0	0	0	0	0	93.7	90.9	0	93.6	0	90.7	0	0	90.7	0	81.0	91.2	0	87.3	92.9
Heavy Vehicles	0	0	0	0	0	0	67	4	0	71	0	8	0	0	8	0	8	6	0	14	93
% Heavy Vehicles	0	0	0	0	0	0	6.3	9.1	0	6.4	0	9.3	0	0	9.3	0	19.0	8.8	0	12.7	7.1



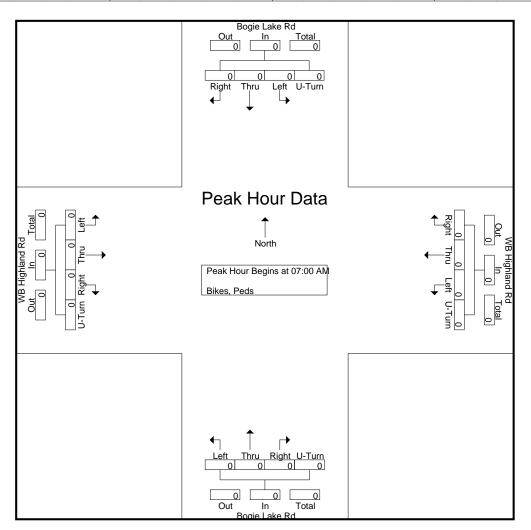


								G	roups	Printed-	Bikes	, Peds									
		WB	Highla	nd Rd			WB		nd Rd				jie Lał	ke Rd			Bog	gie Lak	e Rd		
		E	<u>astbou</u>	und			W	estbo	und			N	orthbo	und			<u> </u>	outhbo	und		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
07:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
										1											i
Grand Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Apprch %	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
Total %																					



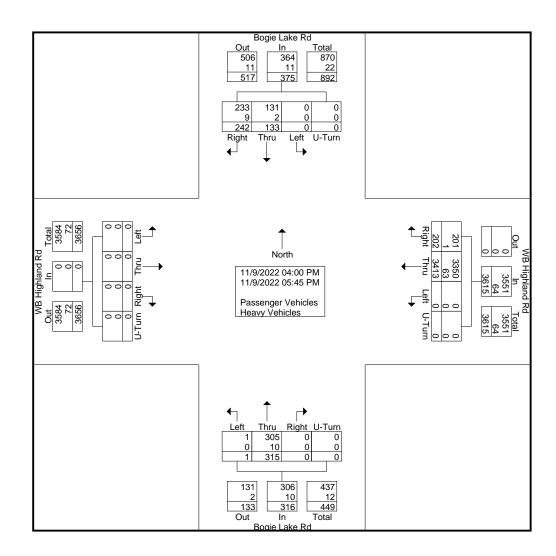


			Highla astbou					Highla /estbo	nd Rd und				gie Lak orthbo					gie Lak outhbo			
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A	nalysis	s From	07:00	AM to	08:45	AM - P	eak 1	of 1													
Peak Hour fo	or Entir	e Inter	section	n Begi	ns at 07	:00 AN	Λ														
07:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total Volume	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% App. Total	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
PHF	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000



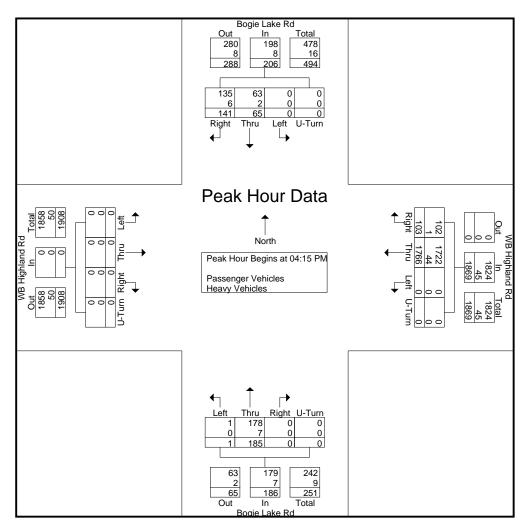


						G	roups	Printed	d- Pas	senger	Vehicle	es - He	eavv Ve	ehicles							
		WB	Highla	nd Rd				Highla					gie Lak				Bog	gie Lak	e Rd		
		E	astbou	und			W	estbou	Ind			N	orthbo	und			S	outhbo	und		
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
04:00 PM	0	0	0	0	0	0	378	21	0	399	0	31	0	0	31	0	18	23	0	41	471
04:15 PM	0	0	0	0	0	0	489	29	0	518	1	39	0	0	40	0	15	30	0	45	603
04:30 PM	0	0	0	0	0	0	390	24	0	414	0	48	0	0	48	0	19	34	0	53	515
04:45 PM	0	0	0	0	0	0	454	29	0	483	0	44	0	0	44	0	15	37	0	52	579
Total	0	0	0	0	0	0	1711	103	0	1814	1	162	0	0	163	0	67	124	0	191	2168
05:00 PM	0	0	0	0	0	0	433	21	0	454	0	54	0	0	54	0	16	40	0	56	564
05:15 PM	0	0	0	0	0	0	456	26	0	482	0	39	0	0	39	0	15	34	0	49	570
05:30 PM	0	0	0	0	0	0	420	36	0	456	0	39	0	0	39	0	16	30	0	46	541
05:45 PM	0	0	0	0	0	0	393	16	0	409	0	21	0	0	21	0	19	14	0	33	463
Total	0	0	0	0	0	0	1702	99	0	1801	0	153	0	0	153	0	66	118	0	184	2138
Grand Total	0	0	0	0	0	0	3413	202	0	3615	1	315	0	0	316	0	133	242	0	375	4306
Apprch %	0	0	0	0		0	94.4	5.6	0		0.3	99.7	0	0		0	35.5	64.5	0		
Total %	0	0	0	0	0	0	79.3	4.7	0	84	0	7.3	0	0	7.3	0	3.1	5.6	0	8.7	
Passenger Vehicles	0	0	0	0	0	0	3350	201	0	3551	1	305	0	0	306	0	131	233	0	364	4221
% Passenger Vehicles	0	0	0	0	0	0	98.2	99.5	0	98.2	100	96.8	0	0	96.8	0	98.5	96.3	0	97.1	98
Heavy Vehicles	0	0	0	0	0	0	63	1	0	64	0	10	0	0	10	0	2	9	0	11	85
% Heavy Vehicles	0	0	0	0	0	0	1.8	0.5	0	1.8	0	3.2	0	0	3.2	0	1.5	3.7	0	2.9	2





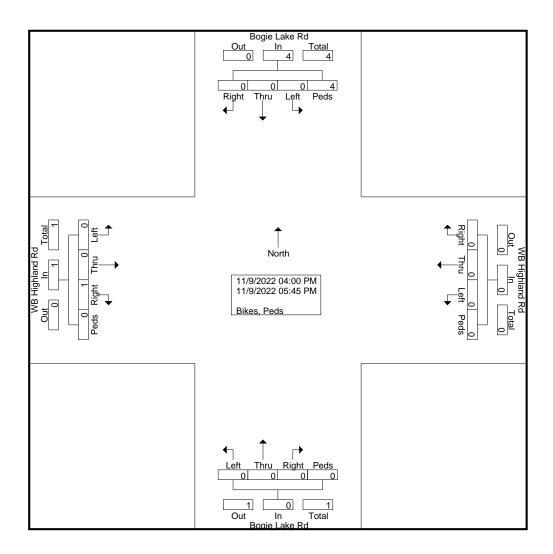
			Highlai astbou					Highla /estboi					jie Lak					jie Lak outhbo			
Start Time	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Left	Thru	Right	U-Turn	App. Total	Int. Total
Peak Hour A	nalysis	s From	04:00	PM to	05:45 F	PM - P	eak 1	of 1													
Peak Hour fo	or Entir	e Inter	sectior	n Begir	ns at 04	:15 PN	1														
04:15 PM	0	0	0	0	0	0	489	29	0	518	1	39	0	0	40	0	15	30	0	45	603
04:30 PM	0	0	0	0	0	0	390	24	0	414	0	48	0	0	48	0	19	34	0	53	515
04:45 PM	0	0	0	0	0	0	454	29	0	483	0	44	0	0	44	0	15	37	0	52	579
05:00 PM	0	0	0	0	0	0	433	21	0	454	0	54	0	0	54	0	16	40	0	56	564
Total Volume	0	0	0	0	0	0	1766	103	0	1869	1	185	0	0	186	0	65	141	0	206	2261
% App. Total	0	0	0	0		0	94.5	5.5	0		0.5	99.5	0	0		0	31.6	68.4	0		
PHF	.000	.000	.000	.000	.000	.000	.903	.888.	.000	.902	.250	.856	.000	.000	.861	.000	.855	.881	.000	.920	.937
Passenger Vehicles	0	0	0	0	0	0	1722	102	0	1824	1	178	0	0	179	0	63	135	0	198	2201
% Passenger Vehicles	0	0	0	0	0	0	97.5	99.0	0	97.6	100	96.2	0	0	96.2	0	96.9	95.7	0	96.1	97.3
Heavy Vehicles	0	0	0	0	0	0	44	1	0	45	0	7	0	0	7	0	2	6	0	8	60
% Heavy Vehicles	0	0	0	0	0	0	2.5	1.0	0	2.4	0	3.8	0	0	3.8	0	3.1	4.3	0	3.9	2.7





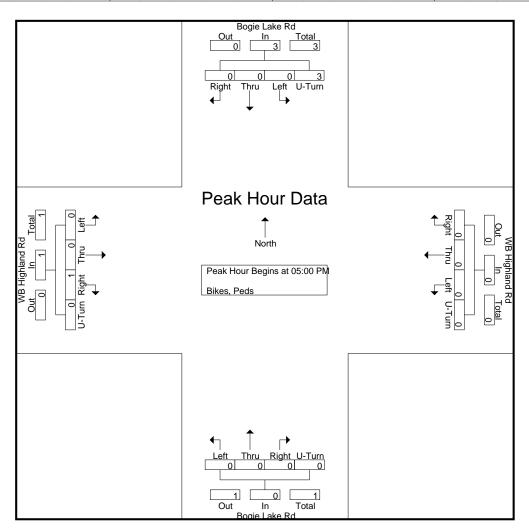
Groups	Printed-	Rikos	Dode	
Gloubs	FIIIILEU-	DINES.	r eus	

				nd Rd				Highla	nd Rd			Bog	jie Lak					gie Lak			
		<u> </u>	<u>astbou</u>	und			W	estbo	und			<u> </u>	orthbo	und			<u>Sc</u>	outhbo	und		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1
05:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	3	3
05:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:45 PM	0	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Total	0	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	3	3	4
Grand Total	0	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	4	5
Apprch %	0	0	100	0		0	0	0	0		0	0	0	0		0	0	0	100		
Total %	0	0	20	0	20	0	0	0	0	0	0	0	0	0	0	0	0	0	80	80	





			Highla					0	nd Rd				gie Lak					gie Lak			
		<u> </u>	<u>astbou</u>	ina			V	estbo	una			N	<u>orthbo</u>	<u>una</u>			50	outhbo	una		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A	nalysis	s From	04:00	PM to	05:45 F	PM - P	eak 1	of 1													
Peak Hour fo	or Entir	e Inter	section	n Begi	ns at 05	:00 PN	Л														
05:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	3	3
05:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:45 PM	0	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Total Volume	0	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	3	3	4
% App. Total	0	0	100	0		0	0	0	0		0	0	0	0		0	0	0	100		
PHF	.000	.000	.250	.000	.250	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.250	.250	.333



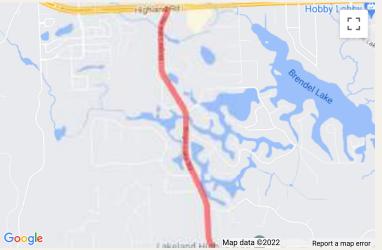
Crash and Road Data

Road Segment Report

Bogie Lake Rd, (PR Number 703507)

From:	Bogie Lake Rd 0.000 BMP
To:	Highland Rd 1.555 EMP
Jurisdiction:	County
FALINK ID:	2902
Community:	White Lake Township
County:	Oakland
Functional Class:	4 - Minor Arterial
Direction:	1 Way
Length:	1.555 miles
Number of Lanes:	2
Posted Speed:	45 (source: TCO)
Route Classification:	Not a route
Annual Crash Average 2017-2021:	<u>21</u>
Traffic Volume (2021)*:	10,200 (Observed AADT)
Pavement Type (2021):	Asphalt
Pavement Rating (2021):	Fair
Short Range (TIP) Projects:	No TIP projects for this segment.
Long Range (RTP) Projects:	No long-range projects for this segment.

Street View



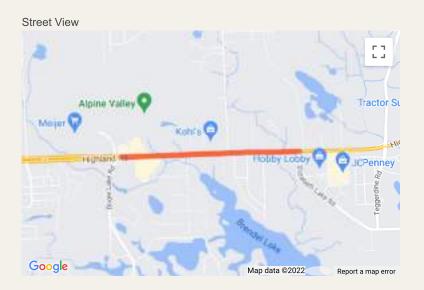
* AADT values are derived from Traffic Counts

Crash and Road Data

Road Segment Report

Highland Rd, (PR Number 648906)

From:	Highland Rd 8.294 BMP
То:	Elizabeth Lake Rd 9.396 EMP
Jurisdiction:	State
FALINK ID:	1764
Community:	White Lake Township
County:	Oakland
Functional Class:	3 - Other Principal Arterial
Direction:	2 Way
Length:	1.102 miles
Number of Lanes:	5
Posted Speed:	50 (source: TCO)
Route Classification:	I-75
Annual Crash Average 2017-2021:	<u>42</u>
Traffic Volume (2016)*:	40,000 (Observed AADT)
Pavement Type (2021):	Asphalt
Pavement Rating (2021):	Poor
Short Range (TIP) Projects:	No TIP projects for this segment.
Long Range (RTP) Projects:	No long-range projects for this segment.



Q

* AADT values are derived from Traffic Counts

<u>O</u>		AFFI	C-	SAF	TY ROA ETY D WORK	EPA	RTM					ŝ.	,					
LOCATION: BOGIE LAKE	8	X	0	N	10	1-9	59						DAT	:	9-	25	5-19	8
CITY/TOWNSHIP: WHITE LAN	KE.	TL	JP	5						_	В	Y:	RA	CHE	2_	Jo	NE	c
COUNTY#: 1228 STATE#:																		
P																		
ELECTRICAL DEVICE: IN										NT	EN	ANC	B					
UNDERGROUND:																		
EDISON OK: YES N			-	-										2	-	-		-
									-								_	-
COORDINATE W/DISTRICT 7:	-	-	_			_	-		_		_		_		_	_		-
	÷		_							_				_				
DIAL SPLIT.	-	1	1.3	1	2	2	2	2		3	3	3	3	+	4	4	4	4
CHANGE TIMING	Ē		1	-	-	-	1	1		1		-		-	-	-	3	4
CHANGE OFFSET									3		- 1						-	-
CHANGE CYCLE LENGTH		-	-	-	-			-		-	-	_	-	-	-			
CHANGE BREAKOUT OR EPROM:	_	-	-	_			-			-	-		_	-	_	-	_	
CHANGE HOURS OF OPERATION: OLD:												-						
NEW:	_		-				_				-	_					_	
REPROGRAM TBC								1.8 										
INSTALL INTERCONNECT:T	BC		_2	IN	TROL	Lan		TON	в									
MBT OK: YES NO									-83	2								
NO CHANGE - RECORD CORRECTI	ON					15		.1	*: 1									1
			0		- 10		~	U.		i Nati	09722			0-				
X OTHER: CREW INSTALLED	-11	3	-	2-1	3-18		PL	ER	SE	C	He	:cr	. 0	21	-	_		
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APPROVED BY:	0	1	-				-	-	1					a		-		
DATE INSTALLED: 9/25/18	y			-							_	DA	TE:	5	125	11	8	
INSTALLED BY: RICHARDON WIG		1	,			-						-			-		-	
	act	10	-	-				-				-			-		-	

INTERSECT	ION:	BOG	EL	A	LE	8	XI	0	NI	1 (1-5	9	_			_	_			-
CITY/VILLA	GE/TO	WNSH		NH	ITE	LA	KE	T	we)									_	
COUNTY#:_	1228	MD	от#:			14	-				REV	#:	5	DE	TRO	TE	oisc)N#:_		
DRAWN BY	Ra	lado	Ja	es	A	PPR	OVE	DB	Y:		J	J.	0		DA	TE D	RAV	VN:_	91	25/18
INSTALLED	BY: _			_			_			_		2050.		_	DA	TE IN	ISTI	.D:	1	1
HOURS OF	OPER	ATION:	M-1	F:	GAR	n - {	3pm	15	TAC	85	UN	: 1	8Ar	n-{	Spr)	_		_	
HOURS OF	FLASH	IING:	M-	F:	80r	n-(DAT	nis	SAT	25	SUN	: 8	Ren	1-8	RAN	n				
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PHASE 1: PHASE 2:		1	1	4	-	-	-	-	-	-	-	-		-	-	-	-	-	2	\square
PHASE 2: PHASE 3:		4		1	1	-	-	-	-	-	-	-	-	-			-	-	14	
PHASE 4:	1	2	+	-	-	1	-	-	-	-	-	-	-	-	-	-	-	-	4	\square
PHASE 5:				-		- 1	1	-	-	-	-	-					-	-		
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PHASE 8:	3									1							-			
PHASE 9:											1									
PHASE 10:		1.1.1										1						1.1		
PHASE 11:													1				_			
PHASE 12:		-			1				_	_				1	-		_			
PHASE 13:										_	_		1	_	1		_	-		
PHASE 14:		1		_	_	_		_	_	_	-	_		_	_	1	_	-		
PHASE 15:			-	_	_	_	_	_	-	_	-	_	-	_	-	-	1	-	-	
PHASE 16:						_		_	_		_	_			L	_	_	1		
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laximum #1		-	50	-	25	2	-	-	-	-	-	+	-	-	-	-	-	-		0-999
laximum #2		_	0.0	+	0.0	-	+	+-	+	+-	-	+	-	-	-	-	+	-	- Internet and the second	0-999
ellow Cleara		-	3.5		3.5		+	-	-	-	-	+	+	+	+	+	+	-	-	0-9.9
ed Glearanc	0		1.9		11.4	-		1.1											- U.I	0-9.9

Phase	T	1	2	3	4	5 DA	6	3. P		9	10	1100	12		14	15	16	RANGE (SEC)
Walk	-	-	-	5	-	5	0	-	~	~	10	1		10			1.0	00-99
Pedest Clearance	+	+	+	-	-	-	-	-	-			-					-	00-99
Flashing Walk	+	+	-	-	-	-	-		-	-	-				2 - 2	-	-	00-00
Extend Ped Clear	-	-	-	-	-	-			-	-	-		-	-	~	1	-	(0-no, 1-Y+R, 2-
Act Rest in Walk																		
111111111111111111111111111111111111111				ШШ		IIIII	ш		IIII	IIII				HIII	IIII	IIII	IIIII	1111111111111111
	3.	PHA	SE I	DAT	A - 4	. INI	TIAL	IZE .	& NC	DN A	ACTI	JATE	DR	ESPO	ONS	E		
Phase	11	2	3	4	1 5	6	17	1 8	-	-		the second se	and the second second	3 1			16	
Initial		4	1	T	1	17	-		-		1							
NA Response		1	-	1	1	1												
CODES:	1.3	0	-	-	1		-	2			3		-	4				
Initial	n	one		ina	activ	е		red		у	rello	w	\$	reen	1			
NA Response	. no	one		1	01			to 2		n.Å	both	1	iner:		l.	stard	enne	
		3. P	HAS			HHH - 5.	VE	HICLE	- 8 F	ED PED	EST	HIII RIAN	RE		.s			
Phase	1	2	3	4	5		-	8	9		and the second s	and and a local data		3 1	_	5	16	
Vehicle Recall		3	1	3	T	1	T	1	T	1								
Pedestrian Recall			-	T	1			1	1									
CODES:	1 8	0	-	-	1	-		2	-	1	3	1	-	4	-		-	
Vehicle	no	one		1	call			min			max	Ē.		soft				
Pedestrian	2023	one			call			ped		bot	N. /							
				IIII				IIIII		IIII	1111	1111		11111	###	Ш	1111	
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Nonlock Memory										-								/
Dual Entry					1													/
Last Car Passage																		/
Conditional Service																		/
CODES:	No.	= NC			1=	YE	S	mm							ш	U P F	6	
	mm	in the		3. PH	IAS	EDA	TA	- 7. S	PEC	IAL	SEC	UEN	VCE		/			
Phase	1	2	3	4	5	16	7	8	9	or the second	and the second second			3 1	4 1	5	16	
Omit		-	-	N	-	1	+	-	-	1	-	-		1	-	1	-	
Yel	-		-	1	1	-	+-	+-	-	+	-		1	-	-			
Dcal	-	_	-	-	1	1	+	-	1		+	1	-		-	+		
							Sin				1101	~						
				TA.				UIII	ECT		min	IIIII SDC	1.0	TC4		i Wi	mm	
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		-6		1			1		T	C+ D	-	8						
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Extend Time	_	- 1		A. 0	P	T	1	-	1	1	-		-99					
Delay Time	-	-	-		-	+	+	-	+	+-	+		-999	1				
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ssigned Phase									1	T								1
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peration Mede: Nor	m V	eh I						t Bar	A	St B	lar B	83						1
/	_	_		A. C	ONT	RO	LS			1	101			-			F	RANGE (SEC)
xtend Time													-					00-99
Jelay Time									1		1		18	1				00-999

	÷.,		-					_	_			COUN AL CO				_				-	_	_	_
					-	-	2.0	-								-	_	-	_				
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MOL		-				+	+			-	1			-	omai	ns (ON a	fter th	ne b	eain	ning	arn	Gree
the second se	k Offse	t MO	DE:	0 =	Adv	ance	Wal	k	1 = 0)elay	Wa	lk		10		-	-	_	10.7				oree
	Y/10		-	-		T	T	T		T	T	TI		Y	DLY	= A	mt o	ftime	the	Ad	vanc	e W	arni
YDL	Y/10	~																re the					2211
		Au	to p	p tim ed cl me re	ear	4. U	_		(00-99	9) S F	UP & I State Red re = Yes	vert		_	0	- 0	0 = fi, 2.0 - 9	9.9)				
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Phas	0			1	2	3	4	5	6	7	8	9		11	-	13	14	15	16	1			
FLAS	SH																1				No; 1:	=R. 3	2=Y)
ALT																							Off/O
ENTE							1								-		-						
EXIT					1			6 8															
					Te	st A	= Re	mote	Fla	sh:	0	-	(0 =	no	& 1	= y	es)						
				AS	8-15						- 6. /	ALT S	EQ. (1		creer	n. 	
	SEQ	1 pp		202	00	EP	AC		SEQ	(PH		PAIR	TO	RE	VER		1			Dr	DD		
	ord					3. M. P	F4. J	PPD	- - P	PO.							P3 .	1.PP4	h P	PD.		5.	
	08	-	1. 1.1	PZ.		1				-		the second se	.PP		-	1	100		-		PPC		
	08			PZ.			N		-	-	-	12	.PP		/	4	-	_	-		.FFG	-	
10	09						1			-		12 13	.pp		/	1					.FFQ	-	
10	09 10						1	1		_	100	12 13 14	.pp	2	2								
	09			-PZ.						-		12 13			2								
	09 10			IIIII						1	QVE	12 13 14		2	2								
	09 10 11	1	2	3	4					- 3. CH#		12 13 14 15	PSTA	2	2		3	4	5	6	7	8	СН#
VLAP	09 10 11	1			4							12 13 14 15 RLAF Phas Over	e Iap I				3	4	5	6	7	8	СН#
VL A F	09 10 11 11 Phses Phses	1			4							12 13 14 15 RLAF Phas Over	e Iap I				3	4	5	6	7	8	СН#
VLAF GRN P VLBF	09 10 11 Phses Phses Phses	1			4							12 13 14 15 RLAF Phas Over Over	e lap J lap k				3	4	5	6	7	8	СН#
VLAP GRNP VLBP GRNP	09 10 11 Phses Phses Phses Phses	1			4							12 13 14 15 RLAF Phas Over Over Over	e lap I lap L				3	4	5	6	7	8	CH#
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VLAP GRNP VLBP GRNP VLCP GRNP	09 10 11 Phses Phses Phses Phses Phses Phses	1			4							12 13 14 15 Phas Over Over Over Over Over	e lap I lap L lap L lap N lap N				3	4	5	6	7	8	CH#
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VL A P GRN P VL B P GRN P VL C P SRN P VL D P GRN P	09 10 11 Phses Phses Phses Phses Phses Phses Phses Phses Phses Phses Phses	1	2	3	4	5		IT D. 7	8	CH#	Tase	12 13 14 15 Over Over Over Over Over Over Over Over	e lap I lap I lap I lap M lap N lap N lap P sing			2		4	■ ■ ■ ■		7	8	CH#
VL A F GRN P VL B F GRN P VL C F GRN F GRN F GRN F F GRN F GRN F F GRN F F GRN F GRN F	09 10 11 11 Phses Phses Phses Phses Phses Phses Phses Phses Phses Phses Phses Phses Phses Phses Phses	1	2	3	4 '+GF		1. UN 6 ntry 4. U		e thi	CH#		12 13 14 15 Over Over Over Over Over Over Over Over	e lap I lap I lap I lap M lap N lap N lap P sing			2	hase		5	6		8	CH#
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verla rail gr rail ye rail ye	09 10 11 11 Phses		2	3	4 '+GF		1. UN 6 ntry 4. U		e thi	CH#		12 13 14 15 Over Over Over Over Over Over Over Over	e lap I lap I lap I lap M lap N lap N lap P sing			2	hase		5	6			CH#
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* For FYA operation, '-G/Y' entry defines the phase that is the green arrow

4. UNIT DATA - 7. PORT 1	/ ITS DATA (TS2 ONLY)	1
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ADDRESS	DESCRIPTION	PRES	M40
0	T&F BIU #1 TS2		
X	T&F BIU #2 TS2		/
2	T&F BIU #3 TS2		X
3	T&E BIU #4 TS2	/	
4	T&F BIU #5 RESERVED	1	
5	T&F BIU #6 RESERVED		0
6	T&F BIU #7 MFG USE		
7	T&F BIU #8 MFG USE		
8	DET BIU #1 TS2		
9	DET BIU #2 TS2		
10	DET BIU #3 TS2	1	
11 /	DET BIU #4 TS2		1
12/	DET BIU #5 RESERVED		
13	DET BIU #6 RESERVED		
14	DET BIU #7 MFG USE		
15	DET BIU #8 MFG USE		
16	MALFUNCTION UNIT		
17	DIAGNOSTIC (MSG 30)		
18	CONTROLLER UNIT		

CODES: 0=NO / 1=YES

4. (INIT DAT	4-0. 101	MISCELL	ANEUUa
Ring#	1	2	3	4
Input Response	1			
Output Select				

I/O Modes	INPUT	OUTPUT
"ABC" Connector		
"D" Connector		

Controller with Detection (TS1 ONLY): EPAC300/M52 enter "1" under D Conn Input 2070 enter "0" under D Conn Input

5. COORDINATION DATA - 1. COORD SETUP

		0	1	2	3	4	5	
OPER:	1	FRE	AUT	MAN				
MODE:	0	PRM	YLD	PYL	POM	SOM	FAC	
MAX :	0	INH	MX1	MX2	*******			
CORR:	2	DWL	MDW	SWY	SW+		*******	
OFST:	1000	BEG	END	OF GRE	EN			
FRCE:		PLN C	YC LE	TIME				
MX DWE	LL:	es libridades	YIELI	D PERIOD):			

5. COORDINATION DATA - 3. DIAL/SPLIT DATA

Mode: 0 = actuated

- 1 = coord phase
- 2 = minimum recall
- 3 = maximum recall
- 4 = pedestrain recall
- 5 = maximum + pedestrain recall
- 6 = phase omit
- 7 = dual coord phase

Sequence: 00 - 15 (Unit data has definition) Ring Lag: Ring offset from local cycle zero when not barrier locked to Ring #1. Time: 00 - 99 seconds.

5. COORDINATION DATA - 3. DIAL/SPLIT DATA

LEVEL 2

DIAL 1/SPLIT 1 CYCLE LENGTH: 110 SEC

PHASE	1	2	3	4	5	6	7	8
TIME		86		24		0.000		
MODE		1		3	10.11	5 8		

DIAL 1 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE				8	1	1.1.1		

DIAL 1 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME					1			
MODE				1.11				

DIAL 1 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME			1.1.1	3				
MODE								

DIAL 2/ SPLIT 1 CYCLE LENGTH: 90 SEC.

PHASE	1	2	3	4	5	6	7	8
TIME		63		27				
MODE			1	3	1		- 1	

DIAL 2 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME	12 12	1	1.1	1.1				
MODE								1

DIAL 2 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME			12 3				-	
MODE								-

DIAL 2 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE		2		-			1	

OFFSET	1	2	3
TIME	21		
SEQUENCE			
RING 2 LAG		1	
RING 3 LAG	1		
RING 4 LAG	1		
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG	1		
RING 3 LAG			
RING 4 LAG	1		
OFFSET	1	2	3
TIME		1000	_
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			

OFFSET	1	2	3
TIME	1		
SEQUENCE			
RING 2 LAG			1.1
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			-
RING 2 LAG			1
RING 3 LAG			
RING 4 LAG	3		
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG	1		2

5. COORDINATION DATA - 3. DIAL/SPLIT DATA I EVEL 4

LEVEL 2

DIAL 3/SPLIT 1 CYCLE LENGTH: 120 SEC.

PHASE	1	2	3	4	5	6	7	8
TIME		92		28				
MODE		1		3				

DIAL 3 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE			12 1					

DIAL 3 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE		1		1				

DIAL 3 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME	1.1		1				6	1.
MODE			120			_		

OFFSET	1	2	3
TIME	40		
SEQUENCE		2	
RING 2 LAG			
RING 3 LAG			-
RING 4 LAG		- 22-1	
OFFSET	1	2	3
TIME		2	
SEQUENCE			
RING 2 LAG		(1
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			2
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			100
RING 4 LAG			

DIAL-4 / SPLIT 1 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME			1.00					
MODE			-	1.1			2	

DIAL 4 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8	1
TIME									1
MODE		1					i	/	1

DIAL 4 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME				/			1	
MODE			1					

DIAL 4 / SPLIT 4 GYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME				S		-		1
MODE					1			8

OFFSET	1	2	3
TIME		/	_
SEQUENCE		/	
RING 2 LAG	/		(s=
RING 3 LAG			
RING 4 LAG		1	
OFESET	1	2	3
TIME			5
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			-
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG	1		
RING 3 LAG			
RING 4 LAG		1	

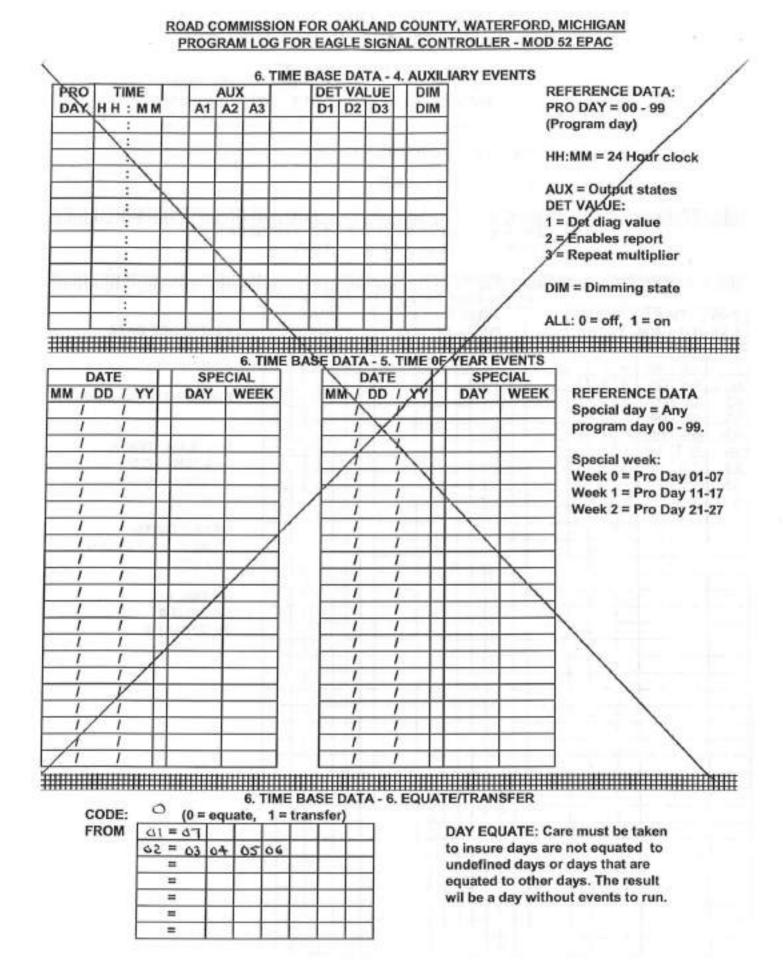
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20	06:00	2/1/1						Γ																				
02		1/1/1																		F	TTA						1	
52	15:00	and the second process of the second s									-		1	_	_	1		1	1		FL/							
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02	20:00	5/5/	-	1	\square	+	+	+	1	Ц	_	_	4	-	4	4	-	+	-									
_		1 1	-		+	+	+	+	-	-	-	-	+	-	+	+	-	+	-	2	AX		-					
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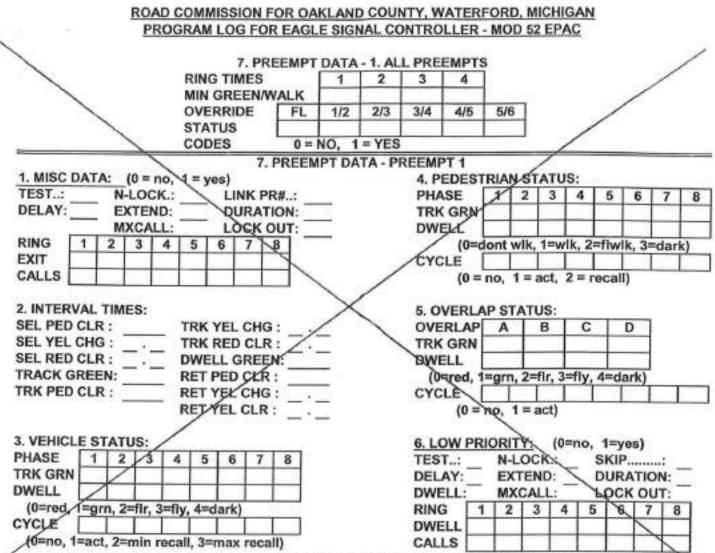
2

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PHASE#	ROAD	PHASE	LOAD SW	FLASH
1				
2	BOGIE LAKE	A	2	FLA
3				1 -11
4	×10 N/0 M-59	B	4	FLR
5	and the state of the			-
6				1
7				
8				
OLA				
OLB				2
OLC				
OLD				1
1PED				
2PED				-
3PED				1
4PED				
5PED				
6PED				
7PED				4
8PED				

Controller Information Sheet For Mod 52 EPAC Pole Mount "M" Cabinet

Intersection:	Bogie Lake & X/O N/O M-59
County No:	1228
State No:	-
Prepared By:	Dawn Bierlein
Date:	12-09-17

Phasing:

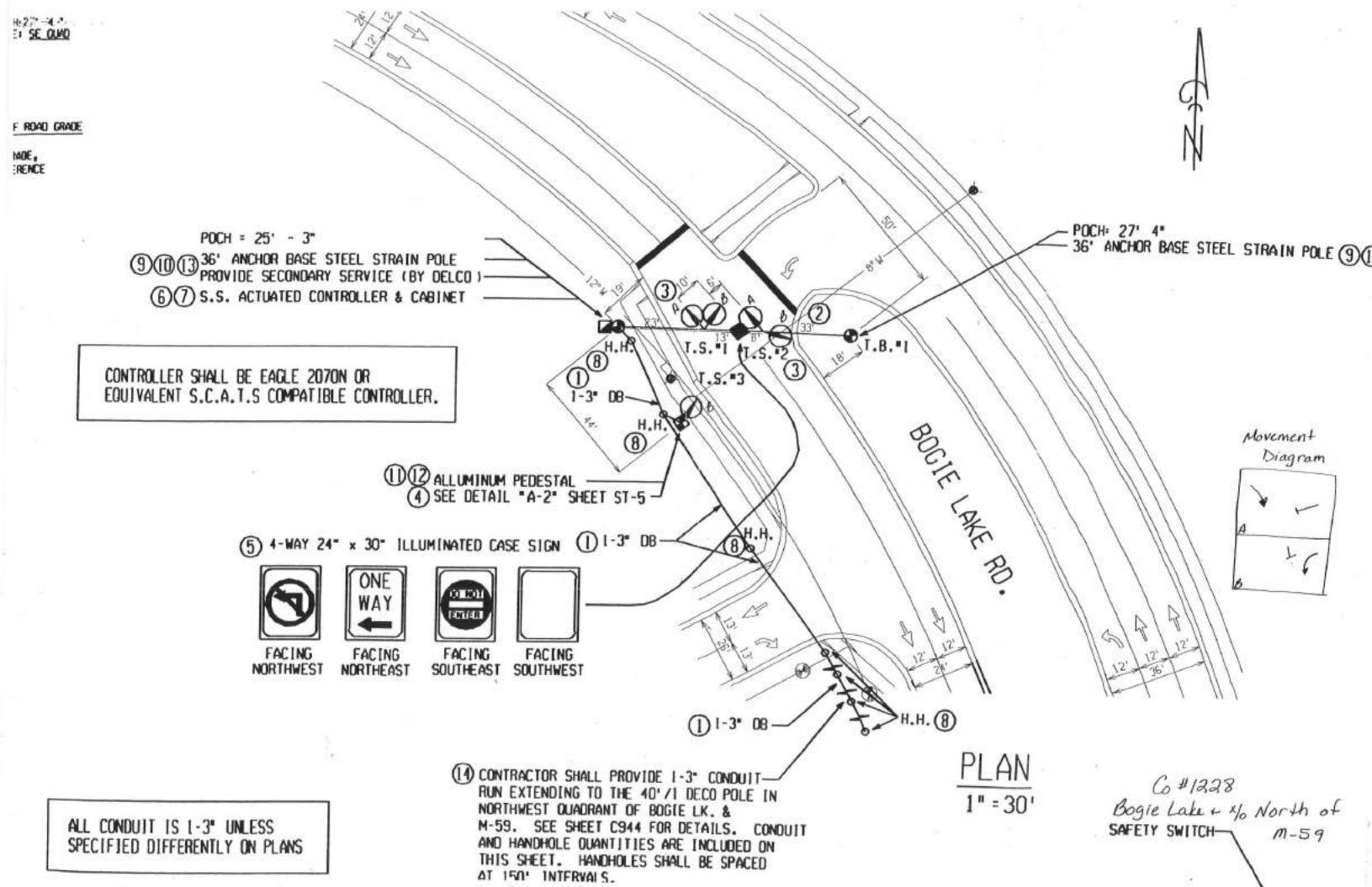
Load Switch 2:	Bogie Lake	A	FLA
Load Switch 4:	X/O N/O M-59	в	FLR

Jumpers:

121-213, 151-152, 153-154, 155-156, 173-174, 175-176, 177-178, 233-PB1, 237-PB1, 241-PB1, 255-256, 257-258, 259-260, 261-262, 263-PB1.

Conflict Monitor: None.

All switches OFF EXCEPT: Dual Select A&B; G&Y Enable; SSM 2,4. Minimum Flash = 4 + 2 + 1

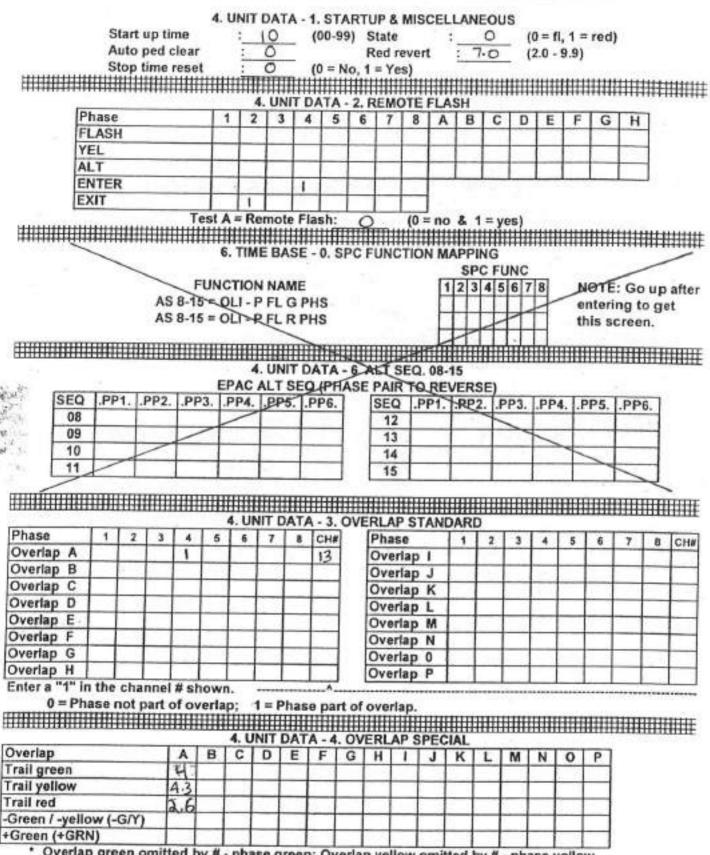


LOCATION: <u>Bogie LK É</u> CITY/TOWNSHIP: White L	aK							-		sγ:					10		
COUNTY#: <u>4110</u> STATE#:	04	1-1	01-	029	_сн/	RG	ES:	w	0	16	58	6	12				
PLI	EASE	PE	RFO	RM T	HE FO)LL	IWC	NG:									
ELECTRICAL DEVICE: INS	TALI	£ _		MO	DERN	IZE	_	_1	MAIN	ENA	NCI	3					
UNDERGROUND:						_	_										-
EDISON OK:YESN	0					JO	B#:	_				_					-
COORDINATE W/DISTRICT 7:		-				_							-				
DIAL.		1			2	2	2	2	3	3	3	3		4	4	4	4
SPLIT.	1	2	3	4	1	2	3	4	1	2	3	4		1	2	3	4
CHANGE TIMING								_									
CHANGE CYCLE LENGTH	_	_	_		_	-	_	-	-	+	-	-		x		-	-
OLD: <u>5am - Mid.</u> NEW: <u>5:30am - 1</u> X REPROGRAM TBC (TraFI INSTALL INTERCONNECT: MBT OK: <u>YES</u> NO NO CHANGE - RECORD CORRE X OTHER: <u>Res</u> 23	Пр.	S E		_MIN	ITRO								1.2			.*	
& MOOT RETIMING - FINA																15	

INTERSEC	TION:	BOG	IE I	AY.	E 8	N H	-59	3								_				
CITYNILLA	GE/TO	WNSH	IIP:	h	HIT	E	LAK	e			_									
COUNTY#:	4110	M	DOT#	:_6	304	-0	1-0	29			RE	/#:	23.	DET	ROI	TED	ISO	N#:		104:
DRAWN BY	E	Lab	iar	0	_^	PP	ROV	ED B	Y:	3	0	1	\$		DAT	EDF	NAS	/N:_)	11	11
INSTALLED	BY:							1						_	DAT	EIN	STL	D:	1	1
HOURS OF	OPER	ATION	8	7	DA	15	. 5	5:3	OA	m -	11	; 00	PA	1						
HOURS OF																11				
CODE					4. L				ES - \ 1	1. AC	CCES 2	S IIII CTU		DDE:	Fou	ır diç	jits IIIII			999)
CHANNEL:	RING	IPHNXT	1			****		*****	2010		******	*****	*****	*****	*****	*****	**	-		in the second
STRATCE.	Mino	PHAAT	11	2	3	4	5	a	ONC	RRE	9	10		12	12	14	15	16	CHA	PED
PHASE 1:		3 1525	11	-	5	-		0	1	0	3	10		12	13	14	15	10	VEH	PED
PHASE 2:	1	4	- 1	1		-	-	-	-	-		-	-	-	-	-	-	-	2	0
PHASE 3:				-	1	-	-	-				-	-	-	-	-	-	-	4	9
PHASE 4:	1	2		-	-	1						-	-	-	-		-	-	4	10
PHASE 5:			-	-	-		1	-	-	-	-	-	-	-	-	-	-		4	10
PHASE 6:		-		-	-			1		-	-	-	-+	-	-	-	-	-	-	-
PHASE 7:				-	-		-		1		-	-+	-	-	-	-	-		-	-
PHASE 8:	-	-		-	-	-	-	-		1	-	+	+	-	-	-	-	-	-	-
PHASE 9:	_	-	-	-	-	-			-		1	+	-	-	-	-	-	-	-	
HASE 10:	-	-	-	-		-	-	-	-	-	-	1	-	-+	-	-	-		-	-
HASE 11:	-	-	-	-	-	-	-	-	-	-	-	-+	1	+	-+	-	-	-	-	-
HASE 12:	-	-	-	-	-	-		-	-	-	-	+	·+	1	-	-	-			-
HASE 13:	-	-	-	-	-	-	-	-	-	-	-	+	-	1	1	-	-	-	-	-
HASE 14:	-		-	-	-	-	-	-	-	-	-	+	+	+	-+	1	-		-	-
HASE 15:	-	-	-	-	-	-	-	-		-	-	-+	-	+	-	-+	1			-
HASE 16:	-	-	-	-	-+	-	-	-	-	-	-	+	-+	+	-	-	·	1	-	-
DDES:			-		-					_			_	_		_	_		A	T
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ssage			10-	-	12.0	-	-	-	+	-	-	-	-	-	-	-	-	-	the second se	-9.9
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d Clearance			2.0		6.6									1					0.0	-9.9

Phase		11	2	3	HASI	5	6	71	8					13	14	15	16	5 RA	NGE	(SEC
Walk			7	-	7	-	-	-	-	-	1		-	-			1	1.4	00-	
Pedest Clearance	1	1	20	-	12	-	-	-	-	-	-	+	-	-	-	-	-	-	00-	
Flashing Walk	-	1	-		-			-		-	-		1	+	-	-	-	1		
Extend Ped Clear			0		0	-		-	-	-	-	+	-	-		-	-	-		-
Act Rest in Walk			-		~		+	-		-	+	+	+	-	-	-	-	+		
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Phase	1	2	3	14			17	18	19	110	_	12			1		6			
Initial	1	4	1	1	-	1	1	1	-	1.0	1		+	1	+	+	-			
NA Response	1	1	-	1	-	1	1	1			-	-	+	1	+	-				
CODES:	-	0		-	1	-	1	2	-	-	3	141	-	4		-	-			
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NA Response	no	ne			to 1	20		02			oth									
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Vehicle Recall		3	1	3	_	1	1	-	-	1			-		t "	-	-			
Pedestrian Recall		0		Ō	_	1	1	-	-		-	-	-	1	1	-	-			
CODES:	-	0	-	1.8	1	-	-	2	-		3		-	4	-	-	-			
Vehicle	no	ne		1	call			nin		11-5	ax	4		oft	8					
Pedestrian	по	пе		1	call			ed	1	ot N			1							
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	1	2	3	4	5	6	7	8	9	10	11	.12	13	14	15	1	6			/
Ionlock Memory	1	2	3	4	5	6	7	8	9	10	11	.12	13	14	15	1	6		/	/
Ionlock Memory Dual Entry	1	2	3	4	5	6	7	8	9	10	11	.12	13	14	15	1	6		/	/
Ionlock Memory Dual Entry ast Car Passage	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15		6	/	/	/
Vonlock Memory Dual Entry ast Car Passage Conditional Service				4		YES	7	8	9	10	11	.12	13	14	15		6	/	/	/
Phase Nonlock Memory Dual Entry ast Car Passage Conditional Service CODES:		N			1=	YES					+++++							/	/	
ionlock Memory Dual Entry ast Car Passage Conditional Service ODES:		N			1=					0. SF	+++++			300	ШН (М5)					
Ionlock Memory Dual Entry ast Car Passage Conditional Service CODES: 	0 IASE	N		8.5	1=			ECTO 6	DR - 7	0. SF	+++++			300	M52			ectio	n sh	
Vonlock Memory Dual Entry ast Car Passage Conditional Service CODES: UIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	0 IASE	N		2	1=	IAL 4	DET			0. SF	+++++			300	M5: tach	2) ned o		ectio ctor j	n sh	
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International Service International Service	o tASE ctor m Ve			2 6 n Pe A. C	1= 377 201	call ROL	DETI 5 4 3 St 1 S	G 5 Bar	DR-72	0. Sf 83 Bar	B RAN	B (E GE 00-9		300 fe at fo	M52 tach r D- as	2) med o con sign	det nem	ectic ctor j ents	on sho pin	eet
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* Overlap green omitted by # - phase green; Overlap yellow omitted by # - phase yellow

* For FYA operation, '-G/Y' entry defines the phase that is the green arrow

* For FYA operation, '+GRN' entry is the thru phase opposing the FYA phase

4. UNIT DATA - 8. I/O MISCELLANEOUS

Ring#	1	2	3	4	CONN	MODE
Input Response	1				"D"	
Output Select	1				"D"	

Connector "D": 0 = Standard & 1 = Alternate

I/O Modes	INPUT	OUTPUT
"ABC" Connector	1	
"D" Connector		

Controller with Solo Detection: EPAC300/M52 enter "1" under D Conn Input 2070 enter "0" under D Conn Input

5. COORDINATION DATA - 1. COORD SETUP

			0	1	2	3	4	5	
	OPER:	1	FRE	AUT	MAN	-			
	MODE:	2	PRM	YLD	PYL	POM	SOM	FAC	
	MAX :	0	INH	MX1	MX2				
	CORR:	2	DWL	MDW	SWY	SW+		*******	
	OFST:		BEG	END	OF GRE	EN			
	FRCE:		PLN C	YCLET	TIME				
1	MX DWE	L:		YIELI	PERIOD):			
		111111111					THURSDAY		
200 L. 201 L. 201	5.	COORD	INATION D	ATA - 2	MANILA	CONTR	01		

DIAL: SPLIT: OFFSET: SYNC:

To set cycle zero in manual control enter "1" for sync then press "E".

5. COORDINATION DATA - 3. DIAL/SPLIT DATA

Mode: 0 = actuated, 1 = coord phase, 2 = minimum recall, 3 = maximum recall, 4 = pedestrian recall, 5 = maximum + pedestrian recall, 6 = phase omit,

7 = dual coord phase.

Sequence: 00 - 15 (Unit data has definition) Ring Lag: Ring offset from local cycle zero when not barrier locked to Ring #1. Time: 00 - 99 seconds.

5. COORDINATION DATA - 3. DIAL/SPLIT DATA

DIAL 1/SP	LIT 1 C	YCLEL	ENG	гн: 11	0 5	es	PROC	E LENGTH
PHASE	1	2	3	4	5	6	7	8
TIME		80		24	1.1.1.1	-	1000	
MODE		1	1.1	3				

DIAL 1 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME		-					1	
MODE						11		

DIAL 1 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME					1000	000	12.00	
MODE				1				

DIAL 1 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE				1	1.5			

SEQUENCE RING 2 LAG RING 3 LAG **RING 4 LAG** OFFSET 1 2 3 TIME SEQUENCE **RING 2 LAG RING 3 LAG RING 4 LAG** OFFSET 1 2 3 TIME SEQUENCE RING 2 LAG **RING 3 LAG RING 4 LAG** OFFSET 1 2 3 TIME SEQUENCE RING 2 LAG

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LEVEL 1 OFFSET

RING 3 LAG RING 4 LAG

TIME

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PROGRAM

DIAL 2/SP	LIT 1 C	YCLEL	ENG	rh: 70	USC	cs	aya	ELEN	GTH
PHASE	1	2	3	4	5	6	7	8	1
TIME		60	-	27	2000				
MODE		1		3			1		1

00

DIAL 2 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME					1151			
MODE		1.1			2123		1	

DIAL 2 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME						200		1
MODE					1.1.1			

DIAL 2 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME	112	1, i i			100	1.55	-	-
MODE							10	

OFFSET	1	2	3
TIME	56		
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG		2	4
OFFSET	1	2	3
TIME		ę	
SEQUENCE			
RING 2 LAG		7	
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME		1	
SEQUENCE			2 2
RING 2 LAG			
RING 3 LAG			
RING 4 LAG	1	15.0	
OFFSET	1	2	3
TIME	1.1		
SEQUENCE	11.		
RING 2 LAG			10.5
RING 3 LAG			
RING 4 LAG			

5. COORDINATION DATA - 3. DIAL/SPLIT DATA

DIAL 3 / SP	LIT 1 C	YCLE L	ENGT	H:17	0 5	ecs	PR	ELEN	7 Kiilu
PHASE	11	2	3	4	5	6	7	8	
TIME	1	90	2	28	-			1	1
MODE		1		3				1.	1

DIAL 3 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								-
MODE						3.1		

DIAL 3 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME						1		-
MODE								

DIAL 3 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME		1	1		1.11	1		
MODE .						S 71		

TIME 93 SEQUENCE RING 2 LAG RING 3 LAG **RING 4 LAG** OFFSET 1 2 3 TIME SEQUENCE RING 2 LAG RING 3 LAG **RING 4 LAG** OFFSET 1 2 3 TIME SEQUENCE RING 2 LAG RING 3 LAG **RING 4 LAG** OFFSET 1 2 3 TIME SEQUENCE RING 2 LAG RING 3 LAG RING 4 LAG

1

2

3

LEVEL 1

DIAL 4/SPLIT 1 CYCLE LENGTH: 110 SCS

PHASE	1	2	3	4	5	6	7	8
TIME		75		35	1125.00			-
MODE		II		3				-

DIAL 4 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME		1			1000			-
MODE			1.1.22	1.1.1		12123		

DIAL 4 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8	1
TIME				1000	1945		1.1	1.4.00 (1.1	1
MODE	11.12		1.1	- 100 C	* . T .	100		1	1

DIAL 4 / SPLIT 4 CYCLE LENGTH:

PHASE	1 1	2	3	4	5	6	7	8	
TIME	1 2 2 - 1	12421	1.11	1.	1.24	100	1 1	111111	
MODE	1232013	1000	1 520	19044	(CLA) 2.8	19283			

OFFSET	1	2	3
TIME	36	1.1	
SEQUENCE			
RING 2 LAG			
RING 3 LAG	1	1	
RING 4 LAG		1.22	
OFFSET	1	2	3
TIME	12.20	19-19-1	0.00
SEQUENCE	1.1.1	1.1.1.1	
RING 2 LAG	10000	2.0	12
RING 3 LAG	1.11	1.4	
RING 4 LAG	10000		
OFFSET	1	2	3
THME	(* 15 Kither	1000	12-
SEQUENCE	N.C. MARK	22.27	145
RING 2 LAG	12.00	6.010	12-
RING 3 LAG	1.1.1.1		125
RING 4 LAG	1.2.2.2	i and a	
OFFSET	1	2	3
TIME	目的な分配	140.14	作為を
SEQUENCE	19.20	14-26-2	1.45
RING 2 LAG	1. A. L.		d're
RING 3 LAG	1.00	1.1	-
RING 4 LAG		1.1	-

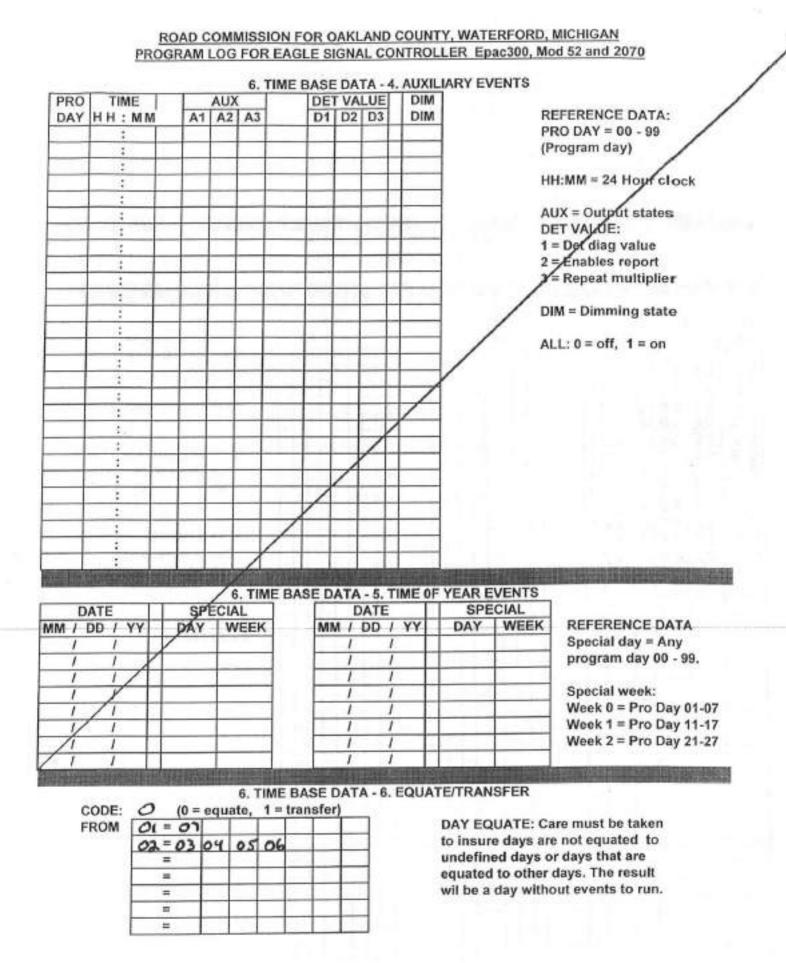
ROAD COMMISSION FOR OAKLAND COUNTY, W	ATERFORD, MICHIGAN
PROGRAM LOG FOR EAGLE SIGNAL CONTROLLER	Epac300, Mod 52 and 2070

DATE	6. TIME BASE TIME	DATA - 2. SET TIM			ST El	ND
MM/DD/YY	HH:MM:SS	MON & WEEK:	MM 3	sw	MM][sw
CYCLE ZERO:	24:00	(HH:MM - EVENT)			

STZ DIFF: ______ (GPS OFFSET)

2. UTILITIES - 8. CONFIGURE PORTS - 8. GPS CONFIGURATION GPS: 1 (0-NO, 1-YES) PORT: 4

PRO	TIME	COORD	6. TH		AX 2	_		1		OMI			
	HH : MN		1.8	PHA						ASE			REFERENCE DATA
	* * * * * *	DISIO	1.1	111				*	111				PRO DAY = 01 - 99
01	00:00		++	++	++	+		-	++	+	H	+	(Program day)
01		11111	++	++	++	+		-	++	+	H		(riogram day)
01	23:00		++	+	++	+			+	+	+	-	HH:MM = 24 Hour clock
02			++	++	++	-	-	-++		+	H	+	The stride clock
0a			++	Ħ	+		-	-		+	Ħ	-	
	06:00			Ħ	++					+	H		PATTERN: (D/S/O)
02		1/1/1	++	Ħ	$^{++}$		-		++	+	Ħ		FLASH =5/5/
02	13:55	the second se		11	Ħ					+	Ħ		FREE =0/0/4
60	14:25				tt	Ħ	-			+	Ħ		
02	15:00												
	19:00	1/1/		T	Ħ		-			1	Ħ		MAX2 & OMITS:
	23:00			T	11					1	П		Call free, set pattern
	:	1 1				П					П		to 0/0/0.
	: 1	1 1								T	П		
	:	1 1				П			T		Π		D = DIAL #
	- 1	1 1								-			S = SPLIT #
	:	1 1											0 = OFFSET #
	:	1 1											
	:	1 1											
	4	1 1								_	Ц		
	1	1 1				Ц	-				Ц		
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_	:	1 1				\square	-		11				
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-	:	1 1			-	4	-		++	-			
	:	1 1			-	++	-	++	++	+-	-		
	:	1 1	+++	-	-	++	-	++	++	+	+		
-	:	1 1			-	-			++	+	-		
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-	:	11		++	+	+	-		++	+	-		
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-			+++		-	++	-		++		-		



Page 8

	PROGRAM	LOG FOR EAGL	SIGNAL C		Auto Lat's	c.pat			100		010			
		7. PREE	MPT DATA	- 1. AL	L PRE	EMPT	S						2	/
		RING TIMES	1	2	3	4	1					/	/	
		MIN GREEN/WA	and the second se		and and		-				1	/		
		OVERRIDE	FL 1/2	2/3	3/4	4/5	5/	5		1	/			
		STATUS	-		_				1	/				
-		CODES	0 = NO,		And in case of the local division of the loc	-	-		1			_		-
1 MICC	DATA: (0		REEMPT D/	ATA - PF			-	1						
TEST:	DATA: (0 = no N-LOCK.				100000	EDES	100000					0		
DELAY:	EXTEND:					GRN	1	2	3	4	5	6	7	8
CELAT.	MXCALL				DW		-	-	-		-	-	-	-
RING	1 2 3 4	the second se	1-1		/		dont	wik	1=-	lk 2	flw	k 3:	=dar	-
EXIT				1	CYC		(11.		14, 5	Gar	<u>~</u>
CALLS			E	\times			no,	1=:	act.	2 = r	ecal	0		_
			· /	/	< · · ·					100.00				
	VAL TIMES:		/		5.0	VERL	AP S	TAT	JS:					
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BEL YEL		TRK RED CLR :	_ •			GRN							8	
SEL RED		DWELL GREEN:			DWE		2			-			ŝ.	
RACK	9.000 000 0N	RET PED CLR :				=red,	1=grì	h.2=	fir, 3	=fly,	4=d;	ark)		_
RK PEC		REF YEL CHG :			CYC	LE .							· · · · · · · · · · · · · · · · · · ·	
		BET VEL CLD.						1	1			_		-
	/	RET YEL CLR :	<u></u> _				no,	1=1	ict)					
VEHIC	E STATUS	RET YEL CLR :	<u> </u>			(0 =	1000		20/63		1-1	arl.		
	LE STATUS:		 		<u>6. L(</u>	: 0) OW P	RIOR	TY:	(0	=no,				
HASE	1 2 3				<u>6. L(</u> TES	(0 = <u>0W P</u> T:	RIOR	TY:	(0 :K.:		SKIF	L		_
. VEHIC PHASE RK GRN	1 2 3				<u>6. L(</u> TES DEL	(0 = 0 <u>W P</u> T AY:	N-E	TY: LOC	(0 :K.: ID:	_	SKIF	AH	ON:	_
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Controller Information Sheet For 4 Phase EPAC Pole Mount Cabinet

Intersection:	M-59 and Bogie Lake Rd
County No:	04110
State No:	63041-01-029
Prepared By:	Rachel Jones
Date:	11-30-11

Phasing:

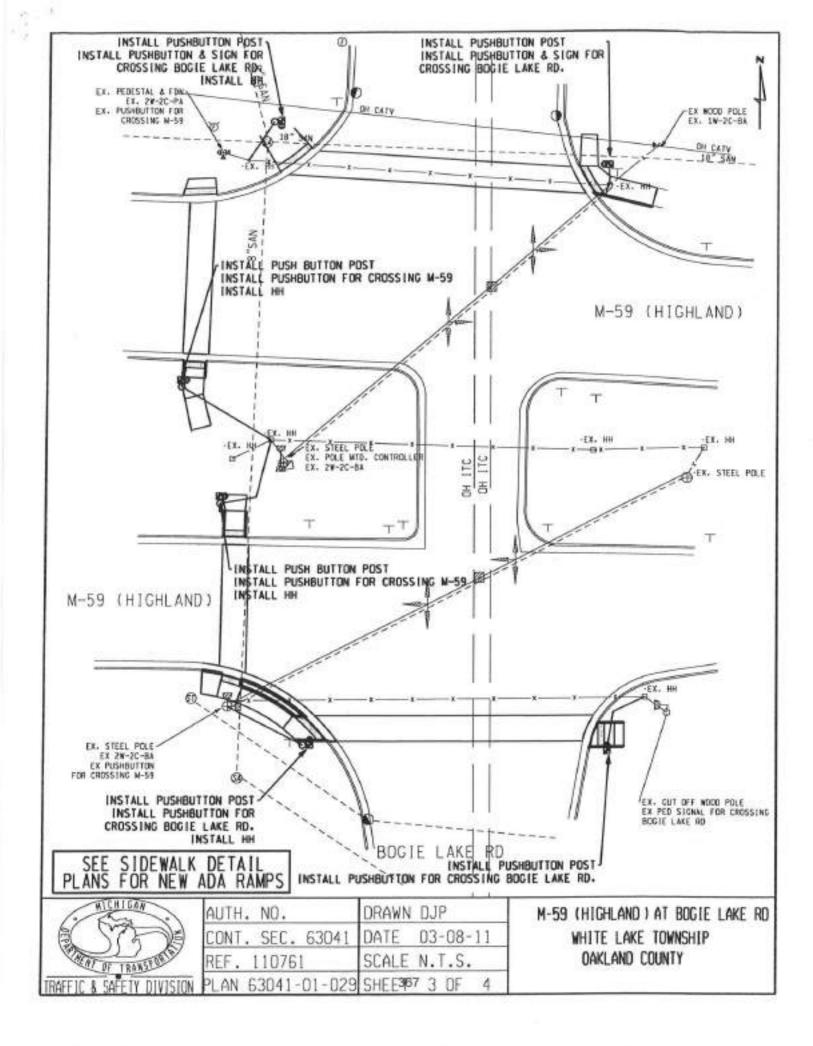
Load Switch 2:	M-59	Å	FLA
Load Switch 4:	Bogie Lake Near	в	FLR
Load Switch 5:(OLA)	Bogie Lake Far	C	FLR
Load Switch 6:	M-59 Peds	WA	
Load Switch 8:	Bogie Lake Ped West	WB	

Jumpers:

121-213, 151-152, 153-154, 155-156, 158-159, 161-162, 164-165, 173-174, 175-176, 177-178, 179-180, 185-186, 223-224, 229-230, 233-PB1, 237-PB1, 241-242, 243-244, 245-246, 255-256, 257-258, 259-260, 261-262, 263-PB1, 268-269, 273-274.

Conflict Monitor: 4-5.

All switches OFF EXCEPT: Dual Select A&B; G&Y Enable; SSM 2,4,5. Minimum Flash = 4 + 2 + 1



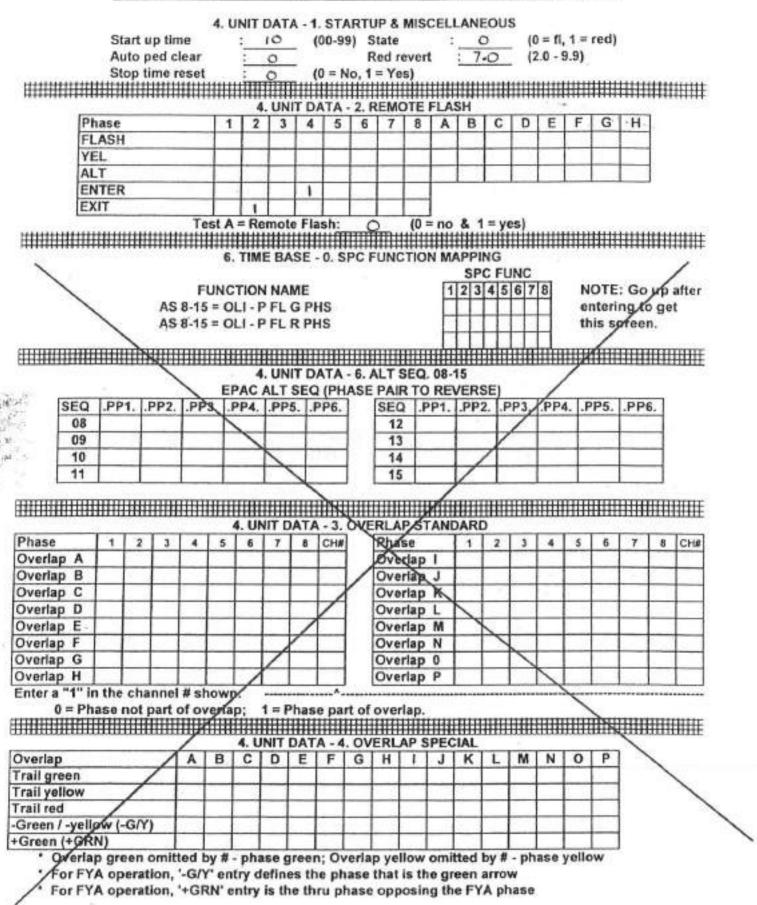
		OAKL TR	AFFIC	- S/	AFETY	/ DEP	ART	ME	NT	-020						AN 13			
LOCATION: <u>E</u>	3 M-5	१ ई	X/c	5	w	0	B	0	gi	e L	K	_D/	ATE	A	De	19	科	24	
CITY/TOWNSHIP:	Whit	c L	ake	_					~		_B'	ť:	Е	L	ab	ie		0	
COUNTY#: 4136	STATE	1: 630	41-0	ol -	129	_CH	ARG	ES:	6) (0	1	6	8	6	12	-		
		PLEA	ASE P	ERFO	DRM 1	HE F	OLL	ow	ING	ż.									
ELECTRICAL	DEVICE:	_ INST	ALL		_мо	DERN	IZ.E	_		MAI	NTE	NA	NC	E					
UNDERGROUT	ND;																		
EDISON OK:	YES _	NO					JO	B#:											
COORDINATE	W/DISTRIC	7:																	
													_						
		DIAL	1 1	1	1 4	2	2	2	2	_	3	3	3	3	-	4	4	4	4
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CHANGE OFFS			^																
CHANGE BRE			-			_				-	_		L.,		L	×	_	-	-
CHANGE HOU TOAYS: OLD: 5 NEW: 5	an-	Mid	nic	34	ł	2													
X REPROGRAM T					ts)														
INSTALL INTE	RCONNECT:	3	FBC _	_	MIN	TROI	-	_	TON	٩E									
MBT OK:	YES	NO																	
NO CHANGE -	RECORD CO	RRECT	ION																
K OTHER: R	cv12	7 4	<u>.</u>	S.	No.	- 5,	T	1	-	-	1			0.77				4	1
* MOOT RETIM	NHG - FI	AL *	4					_											
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ATE INSTALLED:	1/2/17										_		_				-	-	5

Phase	-	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	RAT	VGE (SEC
Walk			-	-	_	_					1		-	-	-				00-9	
Pedest Clearance							-	-	_	-									00-99	9
Flashing Walk						-	-				-	-								
Extend Ped Clear	-	-	-										T	-	-	_				
Act Rest in Walk																		-	-	_
ERRENTERENTER	3.	HH PH/	IIII SE	DAT	A - 4	INI	TIAL		NO	N AC	TUA	TED		SPO	IIII NSE					
Phase	1	2	3	4	5	_		the second second	9	the second second	and second se	112	the second second	Concernance in the		-	16			
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NA Response							1	T				1			1	Т				
CODES:		0			1			2			3			4	-		-			
nitial	no	ne		ina	activ	e	1	red		yel	low		g	reen						
NA Response	no	ne			0 1			0 2			oth									
NUMBER OF STREET		3. F	PHA:	SE D	ATA	- 5.	VEH	ICLE	& P	EDES	TRI	AN F	REC	ALL	S					
hase	1	2	3	-		6	7	8	9	10	11	12	13	14	15	1	16			
/ehicle Recall		3		3												T				
Pedestrian Recall			1	1		1	1					-				T				
CODES:		0		1	1			2			3			4						
/ehicle	no	ne		1	call			nin		m	ax		s	oft						
Pedestrian	no	ne		1	call		F	ed	1	bot N	I. A.									
				ШШ	HIII				Ш	11111	Ш		HIII			ĦĦ	1111			11111
· · · · · · · · · · · · · · · · · · ·	See. St.	3	PH	ASE	DAT	TA -	6. NC	DNLC	CK	& MI	SC C	ONT	RO	LS						-
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Jual Entry		1.1		1					1.1									/		
ast Car Passage				-	-	+	+	-			-	-	-	-	-	+	L	/		
ast Car Passage					-	-	-	-				_	_	-	-		7	/		
Dual Entry ast Car Passage Conditional Service CODES:	6	NO			1=	YES											ł			
ast Car Passage Conditional Service CODES:			Ш				11111										ł	/		
ast Car Passage Conditional Service CODES: 			TA		SPEC		DET			0. SI	PC 1	-8 (E		300	M52	2)				
ast Car Passage Conditional Service CODES: 	HASE			2			11111	6	7	8	2C 1	-8 (E		300 e at	M52 tach	2) ed	dete	ection	shee	
ast Car Passage Conditional Service CODES: HHHHHHHHHHHHHH 3. Pl Betector # on Print PAC/M52 "D" Conne	HASE		TA		SPEC		DET			and the second se	2C1	-8 (E		300 e at	M52 tach r D-	2) ed cor	dete	ection tor pi	shee	
ast Car Passage Conditional Service CODES: 	HASE			6			DET	6	7	8		-8 (E		300 e at	M52 tach r D-	2) ed cor	dete	ection tor pi	shee	
ast Car Passage Conditional Service CODES: CODES: CODES: CODES: Connection # on Print PAC/M52 "D" Connection ssigned Phase CODES:	HASE Inctor			6	SPEC 77		DET 5 4	6 5	7 2	83	/	-8 (E		300 e at	M52 tach r D-	2) ed cor	dete	ection tor pi	shee	
ast Car Passage Conditional Service CODES: CODES: CODES: CODES: Content PAC/M52 "D" Conne ssigned Phase CODES:	HASE Inctor		1 1 Nor	6 n Pe	PEC 7		DET	6 5	7 2	8 3 t Bar	В	/	Se	300 e at fo	M52 tach r D-	2) ed cor	dete	ection tor pi	shee	
ast Car Passage Conditional Service ODES: UIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	HASE Inctor		1 1 Nor	6 n Pe	PEC 7		DET	6 5	7 2	8 3 t Bar	B	IGE	SE	300 e at fo	M52 tach r D-	2) ed cor	dete	ection tor pi	shee	
ast Car Passage Conditional Service CODES: 	HASE Inctor		1 1 Nori	6 n Pe	PEC 7		DET 5 4 St	6 5	7 2	8 3 t Bar	BRAN	IGE 00-9	Se (SEC 9	300 e at fo	M52 tach r D-	2) ed cor	dete	ection tor pi	shee	
ast Car Passage Conditional Service ODES: UIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	HASE Inctor		1 1 Nori	6 n Pe	PEC 7		DET 5 4 St	6 5	7 2	8 3 t Bar	BRAN	IGE	Se (SEC 9	300 e at fo	M52 tach r D-	2) ed cor	dete	ection tor pi	shee	
ast Car Passage conditional Service ODES: detector # on Print PAC/M52 "D" Conne ssigned Phase ODES: peration Mode: Nor xtend Time elay Time	ASE ector 0 m Ve	n h	1 1 Non	2 6 A. C		CIAL 4 2 Call ROL	DET 5 4 St St	6 5 Bar		8 3 t Bar	BRAN	IGE 00-9	Se (SE 9	300 ee at fo	/M52 tach r D- as	2) ed cor	dete	ection tor pi	shee	
ast Car Passage conditional Service ODES: 3. Pl etector # on Print PAC/M52 "D" Conne ssigned Phase ODES: peration Mode: Nor xtend Time elay Time 3	ASE ector 0 m Ve	n h	1 1 Non	2 6 A. C		CIAL 4 2 Call ROL	DET 5 4 St St	6 5 Bar		8 3 t Bar R - 2	BRAN	IGE 00-9	(SE) 9	300 te at fo	/M52 tach r D- as	2) ed cor sig	deta nnec nme	ection tor pi ents	n shee In	et
ast Car Passage conditional Service ODES: 3. Pl etector # on Print PAC/M52 "D" Conne ssigned Phase ODES: peration Mode: Nor xtend Time elay Time 111111111111111111111111111111111111	ASE ector 0 m Ve	n h	1 1 Non	2 6 A. C		CIAL 4 8 Call ROL PECI		6 5 Bar ETE	7 2 	8 3 4 Bar R - 2 8	BRAN	IGE 00-9	(SE) 9	300 ee at fo C)	IM52 tach r D-4 as	2) ed cor sig	deta nnec nme	ection tor pi ents	n shee In	et
ast Car Passage Conditional Service ODES: UIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	ASE ector 0 m Ve	n h		2 6 A. C		CIAL 4 8 Call ROL PECI		6 5 Bar	7 2 	8 3 4 Bar R - 2 8	BRAN	IGE 00-9	(SE) 9	300 ee at fo C)	tach r D-as	2) ed cor sig	deta nnec nme	ection tor pi ents	n shee In	et
ast Car Passage Conditional Service CODES: UIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	ASE ector 0 m Ve	n h		2 6 A. C		CIAL 4 8 Call ROL PECI	DET 5 4 St S AL C 5 13	6 5 Bar ETE 6 14	7 2 	8 3 4 Bar R - 2 8	BRAN	IGE 00-9	(SE) 9	300 e at fo C)	tach r D-as	2) ed cor sig	deta nnec nme	ection tor pi ents	n shee In	et
ast Car Passage Conditional Service CODES: 3. Pl etector # on Print PAC/M52 "D" Conne ssigned Phase ODES: peration Mode: Nor xtend Time elay Time 111111111111111111111111111111111111	I ASE octor 0 m Ve	#DA ah		2 6 A. C TA - 10		Cial 4 Cial 4 Cial Cial Cial Cial Cial Cial Cial Cial	DET 5 4 St S St AL D St S St	6 5 Bar ETE 6 14	7 2 CTO 7 15	8 3 4 Bar 8 16 4 8 16	B RAN	IGE 00-9 0-99 H 9-1	(SEC 9 99 16 (2 5e	300 ee at fo C) 2078 ee at fo	tach r D-as	2) ed cor sig	deta nnec nme	ection tor pi ents	n shee In	et
ast Car Passage Conditional Service CODES: IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	I ASE octor 0 m Ve	#DA ah		2 6 A. C TA - 10		Cial 4 2 call ROL PECI 4 12 2	DET 5 4 St S St AL D St S St	6 5 Bar ETE 6 14	7 2 CTO 7 15	8 3 4 Bar 8 16 4 8 16	B RAN	IGE 00-9	(SEC 9 9 16 (2 5 6	300 ee at fo C) 2078 ee at fo	tach r D-as	2) ed cor sig	deta nnec nme	ection tor pi ents	n shee In	et
ast Car Passage Conditional Service CODES: UIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	I ASE octor 0 m Ve	#DA ah		2 6 A. C TA - 10		Cial 4 Cial 4 Cial Cial Cial Cial Cial Cial Cial Cial	DET 5 4 St S St AL D St S St	6 5 Bar ETE 6 14	7 2 CTO 7 15	8 3 4 Bar 8 16 4 8 16	B RAN	IGE 00-9 0-99 H 9-1	(SEC 9 99 16 (2 Sec 9	300 ee at fo C) 2078 ee at fo	tach r D-as	2) ed cor sig	deta nnec nme	ection tor pi ents	n shee In	et

1

1

1



4. UNIT DATA - 8. I/O MISCELLANEOUS

Ring#	1	2	3	4	CONN	MODE
Input Response	t				"D"	
Output Select	1				"D"	

I/O Modes INPUT OUTPUT "ABC" Connector "D" Connector

Controller with Solo Detection: EPAC300/M52 enter "1" under D Conn Input 2070 enter "0" under D Conn Input

COOPD SETUS

	0.000.	0	1	2	3	4	5
OPER:	1	FRE	AUT	MAN			
MODE:	0	PRM	YLD	PYL	POM	SOM	FAC
MAX :	0	INH	MX1	MX2	*******	-	*******
CORR:	2	DWL	MDW	SWY	SW+		
OFST:	1000	BEG	END	OF GRE	EN		
FRCE:		PLN C	YCLET	TIME			
MX DWE	.L.:		YIELI	PERIOD	:		

5. COORDINATION DATA - 2. MANUAL CONTROL

DIAL: SPLIT: OFFSET: SYNC:

To set cycle zero in manual control enter "1" for sync then press "E".

5. COORDINATION DATA - 3. DIAL/SPLIT DATA

Mode: 0 = actuated, 1 = coord phase, 2 = minimum recall, 3 = maximum recall,

4 = pedestrian recall, 5 = maximum + pedestrian recall, 6 = phase omit,

7 = dual coord phase.

Sequence: 00 - 15 (Unit data has definition)

Ring Lag: Ring offset from local cycle zero when not barrier locked to Ring #1. Time: 00 - 99 seconds.

5. COORDINATION DATA - 3. DIAL/SPLIT DATA

PHASE	1	2	3	H; 11	5	6	7	8
TIME	1	86		24				-
MODE		1		3				

DIAL 1 / SPLIT 2 CYCLE LENGTH:

......

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE								

DIAL 1 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE		-						-

DIAL 1 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME	16 8				1			
MODE								

DIAL 2/ SPLIT 1 CYCLE LENGTH: 90 Secs

PHASE	1	2	3	4	5	6	7	8
TIME		63		27				
MODE		II		3				-

DIAL 2 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME						1		
MODE								

DIAL 2 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE								

DIAL 2 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME					-			
MODE					1			

OFFSET	1	2	3
TIME	25		
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME		100	
SEQUENCE			
RING 2 LAG		2	
RING 3 LAG			
RING 4 LAG		1.1	
OFFSET	1	2	3
TIME			
SEQUENCE			125
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE		2	
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			

OFFSET	1	2	3
TIME	41		
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG		1	
OFFSET	1	2	3
TIME			1
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			

5. COORDINATION DATA - 3. DIAL/SPLIT DATA

PHASE	1	2	3	4	5	6	7	8
TIME		92		28	-			
MODE		1		3				

DIAL 3 / SPLIT 2 CYCLE LENGTH:

LEVEL 2

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE								

DIAL 3 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE								

DIAL 3 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								-
MODE							-	-

DIAL 4/SPLIT 1 CYCLE LENGTH: 110 505

PHASE	1	2	3	4	5	6	7	8
TIME		75		35			-	
MODE		1		3				

DIAL 4/ SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								-
MODE	1				1100			-

DIAL 4 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME	1			-				100-0
MODE				12				1.1

DIAL 4 / SPLIT 4 CYCLE LENGTH:

PHASE	1 1	2	3	4	5	6	7	8
TIME	1000	and the second	1	100	1	2000	2 4	1
MODE	1.20	1 - 64	5 61	-12/200	11.27		100	141-21

OFFSET	11	2	3
TIME	78		-
SEQUENCE	1.2		-
RING 2 LAG			
RING 3 LAG			-
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			1
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			2
SEQUENCE			1
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			

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1	1218	-
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<u>इन्हेलिक</u>	26-37	***
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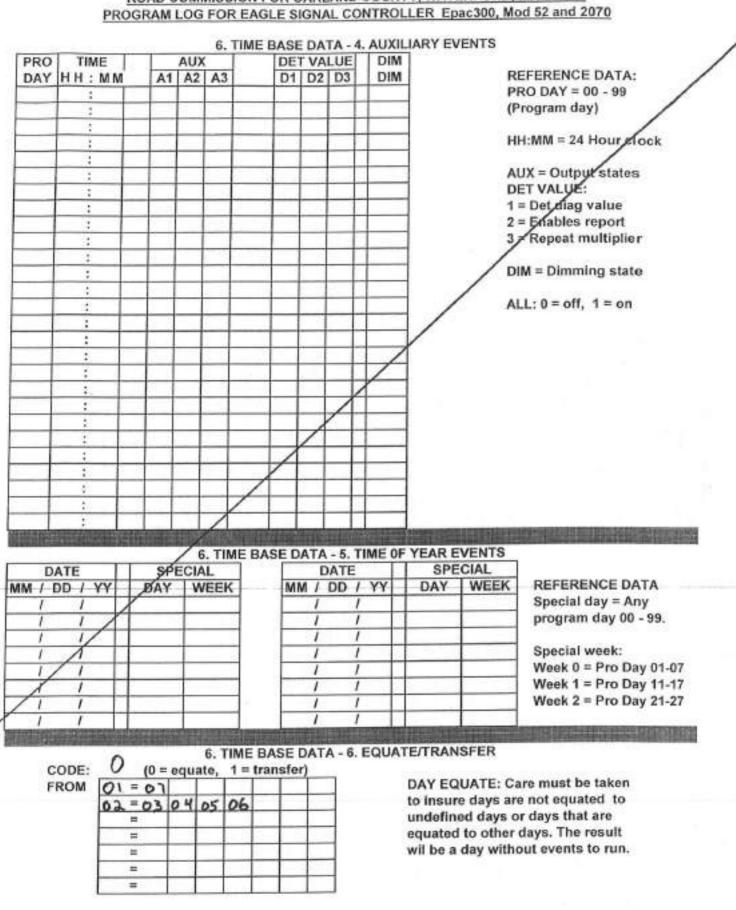
ROAD COMMISSION FOR OAKLAND COUNTY, W	ATERFORD, MICHIGAN
PROGRAM LOG FOR EAGLE SIGNAL CONTROLLER	Epac300, Mod 52 and 2070

DATE	6. TIME BASE	DATA - 2. SET TIM			ST EN	ND
MM/DD/YY	HH:MM:SS	MON & WEEK:	3	sw	MM _[1	sw
CYCLE ZERO	24:00	(HH:MM - EVENT)			

STZ DIFF: ______ (GPS OFFSET)

2. UTILITIES - 8. CONFIGURE PORTS - 8. GPS CONFIGURATION GPS: 1 (0-NO, 1-YES) PORT: 4

1000		Contraction and	6	TIME		ACE	DA	TA - 3	TP	AFE	IC I	EVE	NTS	
PPO	TIME	COORD	0,	1 HAIR	_		_	1A	5, 110	AFT	OM	And the second second	NIO	
PRO			- 1			X 2				- Di				REFERENCE DATA
DAY	HH:MN	PATRN	-		_	SE #	and the local division of the local division	-	-			E#	* *	PRO DAY = 01 - 99
		DISIO		* *	1	1.1.	1.	-	-1-	-1-	1-1	-		
DI	00:00	and the second se				4		-		-		-		(Program day)
01		1/1/1		\square				_		-	\square	_		
01	23:00							_		_				HH:MM = 24 Hour clock
0a	00:00													
62	05:30	1/1/1												1111111111111111
02	06:00	2/1/1												PATTERN: (D/S/O)
02	09:00	1/1/1												FLASH =5/5/
02	13:55													FREE =0/0/4
	14:25	1/1/1		TT										
	15:00													
02	19:00	1/1/1			T									MAX2 & OMITS:
02	23:00	5151					П							Call free, set pattern
	:	1 1					П							to 0/0/0.
	1	1 1	_	TT			П							
	:	1 1		tt		-	Ħ							D = DIAL #
		11		11			Ħ	-				-		S = SPLIT #
	:	1 1		T	T	-	Ħ	-			T			0 = OFFSET #
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-	:	11	-		H	-	H	-	++	1	Ħ			
		11		-	Ħ	-	H	1	++	+	Ħ			
	:	11			H	-	H	-	++	t	tt	Ħ		
-	:	11			H	-	H	-	++	+	H	Ħ		
-	:	11			H	+	+	1	++	+	H	H		



ROAD COMMISSION FOR OAKLAND COUNTY, WATERFORD, MICHIGAN

	ROAD COMMISSION FO										
PRO	GRAM LOG FOR EAGL	E SIGNAL	CONTR	OLLER	Epac	300, Mod	1 52 a	nd 20	070		/
	7. PREE	EMPT DAT	A - 1 A	I PRF	EMPTS	1.61				6	/
	RING TIMES	1	2	3	4	1				/	
	MIN GREEN/WA	ALK		1					/		
	OVERRIDE	FL 1/	2 2/3	3/4	4/5	5/6		/	/		
	SUTATE							/			
	CÓRES	0 = NO,	1 = YE	S			/	· · ·			
		REEMPT	DATA - F	REEMP	T1	/	_				-
1. MISC DATA: (0						RIAN ST	TATU	S:			102-2-4
THE REPORT OF A DESCRIPTION OF A DESCRIP	OCK .: LINK PR#	Contraction and the second second		PHA		1 2	3	4	5	6 3	8
Contraction of the second s	END: DURATIO				GRN	_			_	_	
and a second sec	CALL: LOCK OU	and an and a second		DW			I				
CONCRETE THE REPORT OF THE REP	3 4 5 6 7 8			/		lont wik	1=w	lk, 2=	flwik	, 3=d	ark)
CALLS		- °	\checkmark	CYC	10 C				_	_	_
ALLS		1	X		(0 =	no, 1 =	act,	z = re	call)		
INTERVAL TIMES	e.	/	1			D OTAT					
SEL PED CLR :	TRK YEL CHG :	/			RLAP	A	B	С	TD		
EL YEL CHG :	TRK RED CLR	£ -			GRN	-	Б	6	1-0	-	
EL RED CLR :	DWELL GBEEN:			DWE					-		
RACK GREEN:	RET PER CLR :					€grn, 2=	flr 3	=fly d	f=da	rkt	
RK PED CLR :	RET YEL CHG :				LE	U	1 1	1	1		
380801/257/310742803	BET YEL CLR :					N				_	_
	pile i i le le viert .				(0 =	no. 15	act)		-		
					(0 =	no, A	act)				
. VEHICLE STATUS	/			6. L(1000	no, A	1	€no,	1=ye	es)	
a fair and the second se		-'- 8]		<u>6. L0</u> TES	OW PR		To	€no,			
HASE 1 2 RK GRN	s.	8			0W PR	IORITY:	CK.:	15	KIP.	s)	.—
HASE 1 2 RK GRN WELL	3 4 5 6 7 1	8		TES	<u>DW PR</u> T: AY:	IORITY: N-LOG	CK.:	->	KIP.		
HASE 1 2 RK GRN WELL (0=red, 1=grn, 2=f	3 4 5 6 7 1	8		TES	DW PR	IORITY: N-LOO EXTE MXCA	CK.:		KIP.	TION	
HASE 1 2 RK GRN WELL (0=refl, 1=grn, 2=fl YELE	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark)	- ' 8 		TES DEL DWE RING DWE	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOO EXTE MXCA	CK.: ND:		KIP.	TION	:
HASE 1 2 RK GRN WELL (0=refl, 1=grn, 2=f VELE	3 4 5 6 7 1	- ' 8 		TES DEL DWE RING	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOO EXTE MXCA	CK.: ND:		KIP.	TION	:
HASE RK GRN WELL (0=refl, 1=grn, 2=fl yeLE (0=no, 1=act, 2=m	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark)	B B SIGNAL	PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOO EXTE MXCA	CK.: ND:		KIP.	TION	:
HASE RK GRN WELL (0=red, 1=grn, 2=f VCLE (0=no, 1=act, 2=m	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark)		PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOO EXTEI MXCA	CK.: ND:				:
HASE RK GRN WELL (0=red, 1=grn, 2=f yele (0=no, 1=act, 2=m PHASE# 1	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark) in recall, 3=max recall)		PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOC EXTEI MXCA 2 2	ND: ND: ULL: 3 4 SE				8
HASE RK GRN WELL (0=refl, 1=grn, 2=fl yeLE (0=no, 1=act, 2=m HASE# 1 2 EB M-	S. 3 4 5 6 7 1 ir, 3=fly, 4=dark) in recall, 3=max recall) RO		PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOO EXTEI MXCA	ND: ND: ULL: 3 4 SE				8
HASE 1 2 RK GRN WELL (0=refl, 1=grn, 2=fl yelle (0=no, 1=act, 2=m HASE# 1 2 5 6 1 3	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark) in recall, 3=max recall) RO	SIGNAL	PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOC EXTEL MXCA 2	CK.: ND: NLL: 3 4 SE	LOA	D SV		ASH
HASE 1 2 RK GRN WELL (0=refl, 1=grn, 2=fl YELE (0=no, 1=act, 2=m HASE# 1 2 2 3 4 X (0 V	S. 3 4 5 6 7 1 ir, 3=fly, 4=dark) in recall, 3=max recall) RO	SIGNAL	PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOC EXTEI MXCA 2 2 PHA	CK.: ND: NLL: 3 4 SE	LOA	SKIP. SURA OCK		ASH
HASE RK GRN WELL (0=refl, 1=grn, 2=fl yeLE (0=no, 1=act, 2=m HASE# 1 2 2 3 4 X (0 V 5	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark) in recall, 3=max recall) RO	SIGNAL	PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOC EXTEL MXCA 2	CK.: ND: NLL: 3 4 SE	LOA	D SV		ASH
HASE RK GRN WELL (0=refl, 1=grn, 2=fl yeLE (0=no, 1=act, 2=m HASE# 1 2 2 3 4 X fo 5 6	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark) in recall, 3=max recall) RO	SIGNAL	PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOC EXTEL MXCA 2	CK.: ND: NLL: 3 4 SE	LOA	D SV		ASH
HASE RK GRN WELL (0=refl, 1=grn, 2=fl yeLe (0=no, 1=act, 2=m HASE# 1 2 2 5 6 7	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark) in recall, 3=max recall) RO	SIGNAL	PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOC EXTEL MXCA 2	CK.: ND: NLL: 3 4 SE	LOA	D SV		ASH
HASE 1 2 RK GRN WELL (0=refl, 1=grn, 2=fl yeLE (0=no, 1=act, 2=m HASE# 1 2 5 6 7 8	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark) in recall, 3=max recall) RO	SIGNAL	PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOC EXTEL MXCA 2	CK.: ND: NLL: 3 4 SE		D SV		ASH
HASE 1 2 RK GRN WELL (0=refl, 1=grn, 2=fl yeLE 1 (0=no, 1=act, 2=m HASE# 1 2 EB 11- 3 4 X fo V 5 6 7 8 OLA	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark) in recall, 3=max recall) RO	SIGNAL	PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOC EXTEL MXCA 2	CK.: ND: NLL: 3 4 SE		D SV		ASH
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HASE 1 2 RK GRN WELL (0=refl, 1=grn, 2=fl yelle (0=no, 1=act, 2=m PHASE# 1 2 5 6 7 8	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark) in recall, 3=max recall) RO	SIGNAL	PHASI	TES DEL DWE RING DWE CAL	DW PR T: AY: ELL: 3 ELL	IORITY: N-LOC EXTEL MXCA 2	CK.: ND: NLL: 3 4 SE		D SV		ASH
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HASE 1 2 RK GRN WELL (0=refl, 1=grn, 2=fl YELE (0=no, 1=act, 2=m HASE# 1 2 C G M- 3 4 X f O V 5 6 7 8 OLA OLB OLC OLD PED PED PED	S. 3 4 5 6 7 1 Ir, 3=fly, 4=dark) in recall, 3=max recall) RO	SIGNAL	PHASI	TES DEL DWE RING DWE CAL	OW PR T: AY: ELL: 3 ELL	IORITY: N-LOC EXTEL MXCA 2	CK.: ND: NLL: 3 4 SE		D SV		ASH

Controller Information Sheet 4 Phase EPAC

1	EB M-59 & X/O W/O Bogie Lake
÷.	White Lake
1	63041-01-129
-	4136
	Rachel Jones
	11/1/11

Phasing:

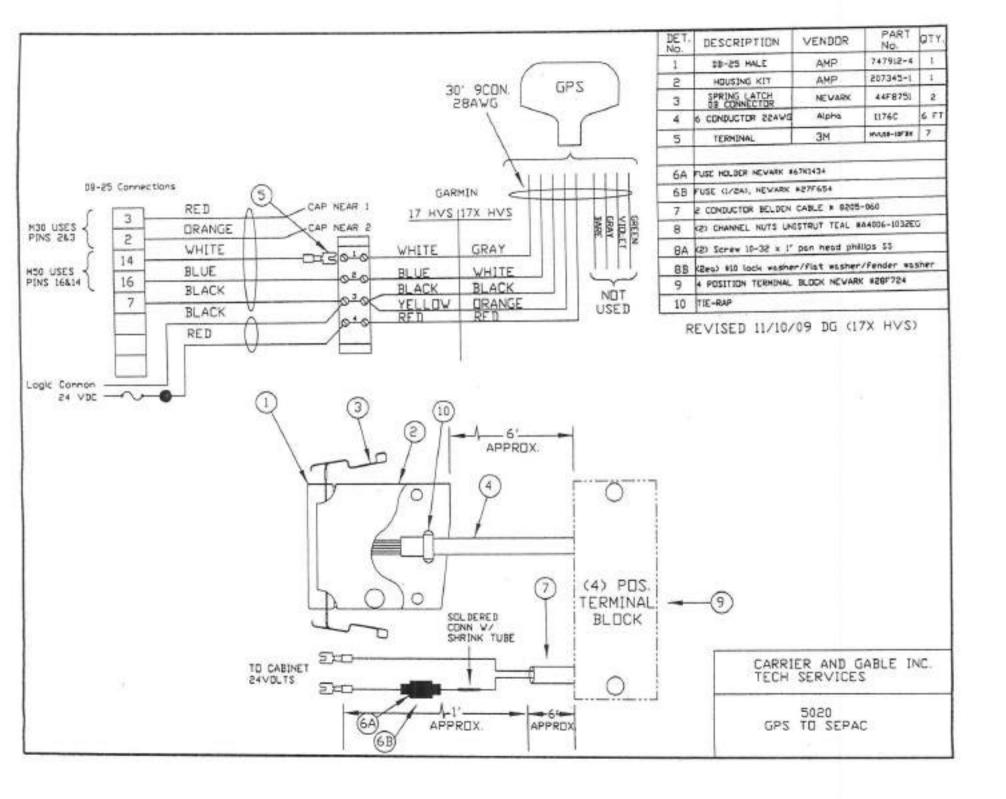
Load Switch 2:	EB M-59	A	FLA
Load Switch 4:	X/O W/O Bogie Lake	в	FLR

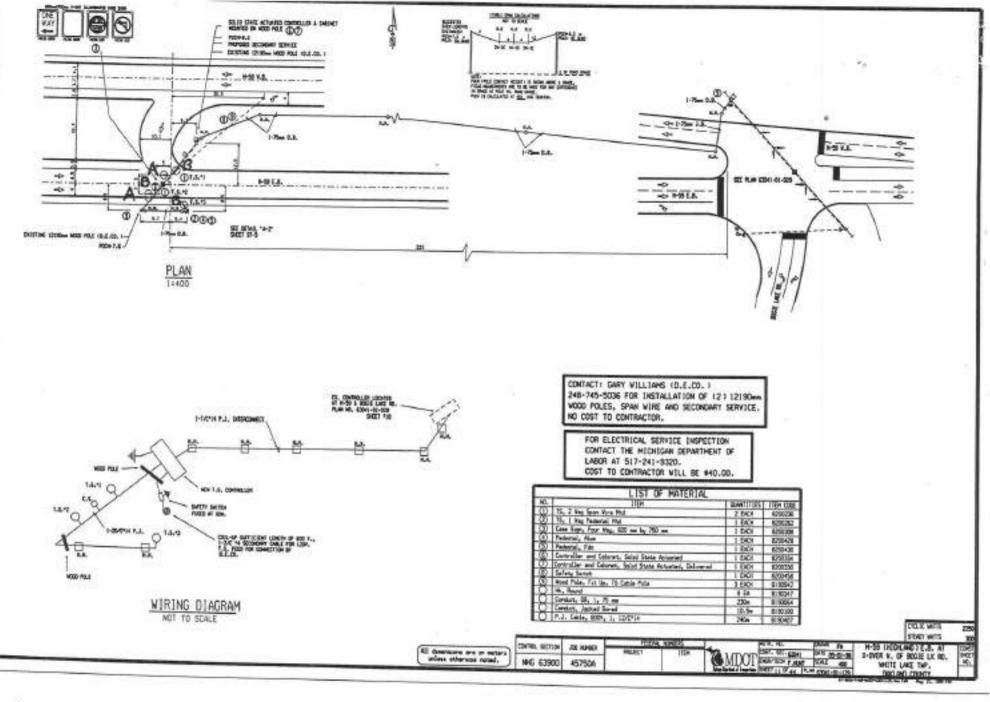
Jumpers:

121-213, 151-152, 153-154, 155-156, 173-174, 175-176, 177-178, 233-PB1, 237-PB1, 241-PB1, 255-256, 257-258, 259-260, 261-262, 263-PB1.

Signal Monitor : NONE

All switched OFF EXCEPT: Dual Select A&B; G&Y Enable; SSM 2,4. Minimum Flash = 4+2+1





4 .

CITY/TOWNSHIP: White Lak	¢	200									20		a r	0
COUNTY#: 4139 STATE#: 630								0	10	0	61	de .		
				THE FO				4 A INIT	ENA	NCT				
ELECTRICAL DEVICE:INST	ALL		MO	DERN	IZE	-		AINT	La ser	TACT.		1 2 3	20	17
UNDERGROUND:				_	101					-				
EDISON_OK:YESNO					101	BW:	-							
COORDINATE W/DISTRICT 7:														-
DIAL.	1	1 1	1	2	2	2	2	3	3	3	3	4	4	4
SPLIT.	1	2 3	4	1	2	3	4		2	3	4	1	2	3
X CHANGE OFFSET	x	-		-		-	-		-	-		-	-	
ADD DIAL/SPLIT							_					X		
CHANGE BREAKOUT OR EPROM	÷					_	_	_						
▲ CHANGE HOURS OF OPERATION	1													
OLD: Sam- Mid	nia	4+			_				_	_				
OLD: <u>5am-Mid</u> NEW: <u>5:30am-</u>	11	pm								_		1		
X REPROGRAM TBC (Traffic	E	Je	ts)										
INSTALL INTERCONNECT:					L		TO	NE						
MBT OK:YESNO														
	CTIO	N											1	
NO CHANGE - RECORD CORREC				4		£4.,	1	1.				. K		
NO CHANGE - RECORD CORREC														
NO CHANGE - RECORD CORREC														
X OTHER: Rev 9														
NO CHANGE - RECORD CORRECT X OTHER: Rev 9 * MOOT RETIMING - FINAL			-						1					

ROAD COMMISSION FOR O	OAKLAND COUNTY	Y, WATERFOR	RD, MICHIGAN
PROGRAM LOG FOR EAGLE SI	SIGNAL CONTROLI	LER Epac300,	Mod 52 and 2070

INTERSEC	TION:	WBN	59 (1	нан	LAJ	2 (0	XIC	E	OB	OGIE	LAN	El	NORI	DIC			_			
CITY/VILLA	GE/TO	WNSH	IP:	WH	ITE	U	W.G													
COUNTY#:										F	REV	¥: 4	7 0	ETF	105	ED	ISO	N#:		
DRAWN BY												0.0							1 /	17/1
NSTALLED	BY: _														AT	EIN	STL	D:	1	1
IOURS OF	OPER/	ATION:	7	DAM	<u>s:</u>	5:	30	AM	- 11	:00	em	3								
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		*******	*****		*****	*****		*****	*****	******	*****		*****	*****	****	*****	••	_		
HANNEL:	RING	PHNXT						C	ONCU	RREN									CHA	
			1	2	3	4	5	6	7	8	9	10	11	12 '	13	14	15	16	VEH	PED
PHASE 1:	-	_	1														_			
HASE 2:	1	4	1.12	1															2	9
HASE 3:					1	1.1		1.1												
HASE 4:	1	2				1													4	
HASE 5:			1.1				1	5.6										-		
HASE 6:								1										11		
HASE 7:	1					-			1										1.12	
HASE 8:										1				1	_					
HASE 9:						1					1									
HASE 10:												1								
HASE 11:													1							
HASE 12:	3		5											1			13			
HASE 13:				_											1			_	1	
HASE 14:			_	_		-			_							1				
HASE 15:																	1			
HASE 16:																		1		
DES: RING PHNXT CONCUR P	Ph	ng Nun lase Ne lases T	ext In	Con	g (1- icuri	16) rent	(0=N	IIII		S)		und	11111	nnel	l, en nel#	ter '	'1" wn.		<u>小</u>	 ₩₩₩
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kimum #1			92		26	2	1	1	1			1	-	-	-	1	1	1	_	0-999
dmum #2			1.0	1	100	-	1	-	-			-	-	-	1	1	T			0-999
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Pedest Clearance			i	-			-	-1	-	-	-	-		-	-	-	+	00-99
Flashing Walk		-	-				-	-		-	-	-		-	1.11	-	+	00-00
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Act Rest in Walk			-				-	-	-	-	-	-			-	-	+	-
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	3.	PHA	SE	DAT	A - 4	INI	TIAI		LNC	N A	CTU	ATE	DR	SPC	NSI	####		*****
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NA Response	-		-	1	-	+	+	+	+	-	+	+	-	+	+	+	-	
CODES:	-	0	-	-	1	-	-	2	-	-	3	-	-	4	-	-	_	
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NA Response	- 10.22	ne			to 1	•		0 2			both		9	reer	÷			
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Vehicle Recall	-	3	-	3		10	+	1.	1-	+"	+	+	-		+	-	10	
Pedestrian Recall		2		13	+	-	-	+	-	+	-	+	-	+	-	+	-	
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Pedestrian	no	8878		- 2.74	call		- 13	bed		bot			1	son				
	HIII	IIIII	1111	mi	1111		mi	IIIII		illi		iiiiii		11111				
	mm	3	PH	ASE	DAT	CA	5 N/	INI C	DCK	2 54	ISC	CO	NTRO		1111	HH	1111	
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		-	-	-	-		-	-	-	-	-	+	-	-	-	+	-	/
Dual Entry			_													+		/
Dual Entry Last Car Passage		_						-									-	/
Dual Entry Last Car Passage Conditional Service		NO				VER		-										/
Dual Entry ast Car Passage Conditional Service CODES:	0 ·	NO			1=	YES												
Dual Entry Last Car Passage Conditional Service CODES:	INH					####												
Dual Entry Last Car Passage Conditional Service CODES: 	INH				BPEC	####	DET				PC	1-8			ØM5	2)		
Dual Entry Last Car Passage Conditional Service CODES: 	IASE		TA .	8.5	PEC 3		DET	6	7	8	IIII IIII IIII	1-8		ce'a	dM5	2) hed	det	ection sheet
Detector # on Print PAC/M52 "D" Conne	IASE				BPEC	####	DET				IIII IIII	1-8		ce'a	ttacl or D	2) hed -cor	det	ection sheet stor pin
Dual Entry Last Car Passage Conditional Service CODES: IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	ASE		TA .		PEC 3		DET	6	7	8	#	1-8		ce'a	ttacl or D	2) hed -cor	det	ection sheet
Dual Entry Last Car Passage Conditional Service CODES: 	ASE ctor	DA		2 6	PEC 3 7		DET 5 4	65	72	83		1-8		ce'a	ttacl or D	2) hed -cor	det	ection sheet stor pin
Dual Entry ast Car Passage Conditional Service CODES: 	ASE ctor	DA		2 6 n Pe	BPEC 3 7	AL 4 8 Call	DET 5	65	72	83	-	/	S	ce a fo	ttacl or D	2) hed -cor	det	ection sheet stor pin
Dual Entry Last Car Passage Conditional Service CODES: IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	ASE ctor	DA		2 6 n Pe	BPEC 3 7		DET 5	65	72	83	-	NGI	S (SE	ce a fo	ttacl	2) hed -cor	det	ection sheet stor pin
Dual Entry Last Car Passage Conditional Service CODES: 	ASE ctor	DA		2 6 n Pe	BPEC 3 7	AL 4 8 Call	DET 5	65	72	83	-	NGE	S (SE 99	ce a fo	ttacl	2) hed -cor	det	ection sheet stor pin
Dual Entry Last Car Passage Conditional Service CODES: 	ASE ctor	DA		2 6 n Pe	BPEC 3 7	AL 4 8 Call	DET 5	65	72	83	-	NGI	S (SE 99	ce a fo	ttacl	2) hed -cor	det	ection sheet stor pin
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Dual Entry Last Car Passage Conditional Service CODES: 	ASE ctor			2 6 A. C	ad 1 ONT	Call ROL		6 5 Bar	7 2 A S	8 3 4 t Ba	RA	NGE 00-	S (SE 99 999	C)	(MS ttacl or D at	2) hed -cor ssig	det nnec inm	ection sheet stor pin ents
Dual Entry Last Car Passage Conditional Service CODES: 	o m Ve			2 6 A. C	ad 1 ONT	AL 4 8 call ROL	DET 5 4 S S S S S S S S S S S S S S S S S S S	6 5 Bar ETE	A S	8 3 4 t Ba	RA	NGE 00-	S (SE 99 999	C) 2070 ce al	(MS ttacl or D at at	2) hed cor ssig	det inned inmed	ection sheet stor pin ents
Dual Entry ast Car Passage Conditional Service CODES: 	o m Ve			2 6 A. C	ad 1 ONT	AL 4 8 Call ROL		6 5 Bar	A S	8 3 4 t Ba	RA	NGE 00-	S (SE 99 999	C) 2070 ce al	(WIS ttacl or D at) tacl or D-	2) hed cor ssig	det inned inm det	ection sheet stor pin ents ####################################
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Dual Entry Last Car Passage Conditional Service CODES: IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	Ctor 0 m Ve	h N		2 6 Pe A. C	BPEC 3 7 on 1 million 1 mi	LAL 4 8 call ROL ECC 4 12	DET 5 4 S S AL D 5 13 3	6 5 Bar ETE 6 14	7 2 A S CTC 7 15	8 3 4 4 HB A HB		NGE 00-	S (SE 99 999	C) 2070 ce al	(WIS ttacl or D at) tacl or D-	2) hed cor ssig	det inned inm det	ection sheet stor pin ents ####################################
Dual Entry ast Car Passage Conditional Service CODES: UNINE Service CODES: Detector # on Print PAC/M52 "D" Conne ssigned Phase CODES: Deration Mode: Nor xtend Time elay Time CODES: aster on Print CODES: CODES	Ctor 0 m Ve	h N		2 6 n Pe A. C		LAL 4 8 call ROL EC 4 12 call call	S S S S S S S S	6 5 Bar ETE 6 14	7 2 A S CTC 7 15	8 3 4 t Ba	rB RA 2.V	NGE 00-	S (SE 99 999 -16 (S	C) 2070 co at fc	(WIS ttacl or D at) tacl or D-	2) hed cor ssig	det inned inm det	ection sheet stor pin ents ####################################
Dual Entry Last Car Passage Conditional Service CODES: IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	Ctor 0 m Ve	h N		2 6 n Pe A. C		LAL 4 8 call ROL ECC 4 12	S S S S S S S	6 5 Bar ETE 6 14	7 2 A S CTC 7 15	8 3 4 4 HB A HB	rB RA 2.V		S (SE 99 999 -16 (SE	C) 2070 co at fc	(WIS ttacl or D at) tacl or D-	2) hed cor ssig	det inned inm det	ection sheet stor pin ents ####################################
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ROAD COMMISSION FOR OAKLAND COUNTY, WATERFORD, MICHIGAN PROGRAM LOG FOR EAGLE SIGNAL CONTROLLER Epac300, Mod 52 and 2070 4. UNIT DATA - 1. STARTUP & MISCELLANEOUS Start up time (00-99) State 10 : 0 (0 = fi, 1 = red)Auto ped clear 0 Red revert : 7.0 (2.0 - 9.9)Stop time reset 0 (0 = No, 1 = Yes)4. UNIT DATA - 2. REMOTE FLASH Phase 2 3 4 5 6 7 8 A B C G D E F H 1 FLASH YEL ALT ENTER 1 EXIT Test A = Remote Flash: Test A = Remote Flash: 0 (0 = no & 1 = yes) (0 = no & 1 = yes) 6. TIME BASE - 0. SPC FUNCTION MAPPING SPC FUNC FUNCTION NAME 12345678 NOTE: Go up after AS 8-15 = OLI - P FL G PHS entering to get AS 8-15 = OLI - P FL R PHS this screen. 4. UNIT DATA - 6. ALT SEQ. 08-15 EPAC ALT SEQ (PHASE PAIR TO REVERSE) .PP1. .PP2. .PP3. .PP4. .PP5. .PP6. SEQ SEQ .PP1. .PP2. .PP3. .PP4. .PP5. .PP6. 08 12 09 13 10 14 11 15 4. UNIT DATA - 3. OVERLAP STANDARD Phase 1 2 3 7 8 CHN Phase 4 5 8. 1 2 4 5 6 7 CH# 8 Overlap A Overlap | Overlap B Overlap J Overlap C Overlap K Overlap X Overlap D Overlap E Overlap M Overlap F Overlap N Overlap 0 Overlap G Overlap H Overlap R Enter a "1" in the channel # shown. 0 = Phase not part of overlap; 1 = Phase part of overlap. \mathcal{A} 4. UNIT DATA - 4. OVERLAP SPECIAL & DEFGHI Overlap JKL M А в 'N 0 Trail green Trail yellow Trail red -Green / -yellow (-G/Y) +Green (+GRN) * Overlap green omitted by # - phase green; Overlap yellow omitted by # - phase yellow * For FYA operation, '-G/Y' entry defines the phase that is the green arrow

' For PYA operation, '+GRN' entry is the thru phase opposing the FYA phase

4. UNIT DATA - 8. I/O MISCELLANEOUS

Ring#	1	2	3	4	CONN	MODE
Input Response	1				"D"	
Output Select	1				"D"	

Connector "D": 0 = Standard & 1 = Alternate

I/O Modes	INPUT	OUTPUT
"ABC" Connector	1	
"D" Connector		

Controller with Solo Detection: EPAC300/M52 enter "1" under D Conn Input 2070 enter "0" under D Conn Input

5. COORDINATION DATA - 1. COORD SETUP

						10-11-11-11-11-11-11-11-11-11-11-11-11-1	
		0	1	2	3	4	5
OPER:	1	FRE	AUT	MAN			
MODE:	0	PRM	YLD	PYL	POM	SOM	FAC
MAX :	0	INH	MX1	MX2			
CORR:	2	DWL	MDW	SWY	SW+		
OFST:	0	BEG	END	OF GRE	EN		
FRCE:	0	PLN C	YCLET	ГІМЕ			
MX DWE	LL: O		YIEL	D PERIOD	: 0		
TRAFFIC TO TA		TTTTTTTTTTTTTTT					***********

	5. COURDINATION DAT	A - Z. MANUAL CONTRO	UL.	
DIAL:	SPLIT:	OFFSET:	SYNC:	
			And and a second se	

To set cycle zero in manual control enter "1" for sync then press "E".

5. COORDINATION DATA - 3. DIAL/SPLIT DATA

Mode: 0 = actuated, 1 = coord phase, 2 = minimum recall, 3 = maximum recall,

4 = pedestrian recall, 5 = maximum + pedestrian recall, 6 = phase omit,

7 = dual coord phase.

Sequence: 00 - 15 (Unit data has definition)

Ring Lag: Ring offset from local cycle zero when not barrier locked to Ring #1. Time: 00 - 99 seconds.

5. COORDINATION DATA - 3. DIAL/SPLIT DATA

LEVEL 2 DIAL 1 / SP	LIT 1 C	YCLEL	ENG	TH: ()	0 5	ess		
PHASE	1	2	3	4	5	6	7	8
TIME		86		24	1	1		
MODE		1		3				

DIAL 1 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME			1		11111			
MODE				1	1	1.1.1.1		-

DIAL 1 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE			1					-

DIAL 1 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME			1					3
MODE					-			-

12.1

DIAL 2/SPLIT 1 CYCLE LENGTH: 90 Secs

PHASE	1	2	3	4	5	6	7	8
TIME		63		27				
MODE		1		3				

DIAL 2 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME	1					2.182.1	8 10	1.
MODE								

DIAL 2 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE					1	5	1	1

DIAL 2 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME							1	
MODE							1	

LEVEL 1	-		
OFFSET	1	2	3
TIME	29		
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG		S	
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG		-	3-12
OFFSET	1	2	3
TIME			
SEQUENCE			1 + 1
RING 2 LAG		1	
RING 3 LAG			1.5.2
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE		1	
RING 2 LAG			
RING 3 LAG			1
RING 4 LAG			1

OFFSET	1	2	3
TIME	45	2	
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			0.00
OFFSET	1	2	3
TIME			
SEQUENCE		-	
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG	1		
RING 4 LAG			

5. COORDINATION DATA - 3. DIAL/SPLIT DATA

PHASE	1	2	3	4	5	6	7	8
TIME	1	92	1	28	-			-
MODE		1		2				

DIAL 3 / SPLIT 2 CYCLE LENGTH:

LEVEL 2

PHASE	1	2	3	4	5	6	7	8
TIME								-
MODE		1	-			-	-	-

DIAL 3 / SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								-
MODE								

DIAL 3 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME								
MODE .				-		1		

DIAL 4/ SPLIT 1 CYCLE LENGTH: 10 SOCS

PHASE	1	2	3	4	5	6	7	8
TIME	1	75		35		-		-
MODE		11		2				-

DIAL 4 / SPLIT 2 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME				_				-
MODE	1 A 8				1			-

DIAL 4/ SPLIT 3 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME		-			1000	1		112.00
MODE					10 20			-

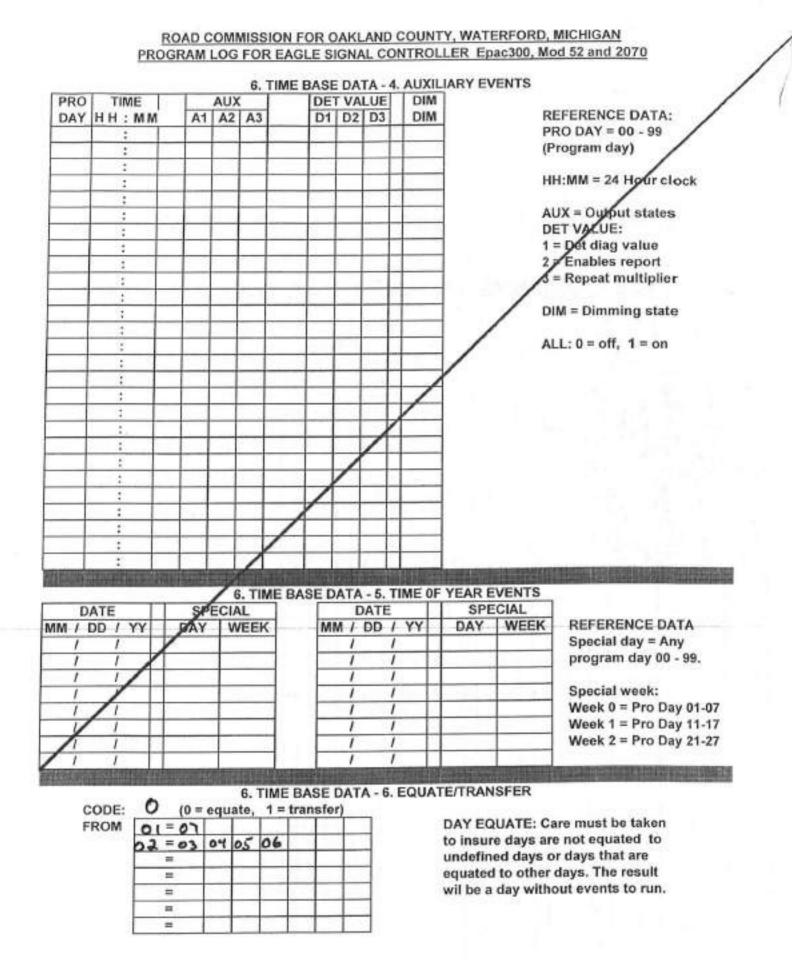
DIAL 4 / SPLIT 4 CYCLE LENGTH:

PHASE	1	2	3	4	5	6	7	8
TIME		4144		1.002.3	1			12.00
MODE		1-0-c	1	NP-X-C	1.014	1.1.1.1		

LEVEL 1			
OFFSET	1	2	3
TIME	81		
SEQUENCE			
RING 2 LAG			
RING 3 LAG	-		
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			100
OFFSET	1	2	3
TIME			
SEQUENCE			
RING 2 LAG			
RING 3 LAG			
RING 4 LAG			

OFFSET	1	2	3
TIME	29	1	
SEQUENCE	1.4.		1
RING 2 LAG			
RING 3 LAG		1	
RING 4 LAG		1	-
OFFSET	1	2	3
TIME	1000	1	1.1.5.1
SEQUENCE			
RING 2 LAG			
RING 3 LAG		121	1000
RING 4 LAG			
OFFSET	1	2	3
THME	1. 1. 1.	1541	
SEQUENCE	1.0		18.14
RING 2 LAG		1.111	102.40
RING 3 LAG		100	
RING 4 LAG	1.1.1	the of the	1.2
OFFSET	1	2	3
TIME	10/2/45	いわりま	498.5 M
SEQUENCE	12:246-	10183	-
RING 2 LAG	- Alter	14-14-14-15-15-15-15-15-15-15-15-15-15-15-15-15-	17.1
RING 3 LAG	1	12-21	
RING 4 LAG			

	Pf						D, MICHIGAN Mod 52 and 2070
		DATE MM/DD/YY	T HH:	IME	A - 2. SET TIM ON & WEEK:	BEG	DST END MM SW
		CYCLE ZERO): <u>24</u> : (0 (HH:I	MM - EVENT		
		STZ DIFF:	-18000	(GPS OF	SET)		
			and the second			and the second	
		2. UTILITIES			rs - 8. GPS CO 1-YES) P		TION
DO-110					In the second	-	and the second se
and the second second			6, TIME	BASE DATA	- 3. TRAFFIC	EVENTS	A STATEMENT AND A STATEMENT AN
PRO	Call and the second sec	COORD		MAX 2	1. A 10 A	TIN	DEFERING SATA
DAY	HH:MN	D / S / O		ASE #S	the second se	SE #S	REFERENCE DATA PRO DAY = 01 - 99
01	00:00						(Program day)
01	05:30			++++++			(i togram day)
01	23:00	5151					HH:MM = 24 Hour clock
02	00:00	5151					
	05:30						DATTERNI, IDISION
02		2/1/1					PATTERN: (D/S/O) FLASH =5/5/
02	09:00	49/1 /1					FREE =0/0/4
	14:25						terrare states
02	15:00	3/1 /1					
02	19:60	1/1/1					MAX2 & OMITS:
02	23:00						Call free, set pattern
		1 1					to 0/0/0.
		1 1					D = DIAL #
	1	i i					S = SPLIT #
	:	1 1					0 = OFFSET #
	:	1 1					
	:	11					
	:	11					1. Sec. 1. Sec
		1 1					
	:	1 1					
	:	1 1	_				
-		1 1				+++	
-	:	1 1				++++	
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Page 8

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														/
		7. PREEMPT RING TIMES	DATA 1	- 1. AL	L PRE	EMPTS						-	/	
		MIN GREEN/WALK		6	3						1	/		
		OVERRIDE FL	1/2	2/3	3/4	4/5	5/6			8	/			
		STATUS	116	23	3/4	400	0/0	-		/				
			NO. 1	= YES				-	/					
Part		7. PREEN	address of the same	and the second second	REEMP	T 1		1	<u> </u>	-	-	-		-
1. MISC	DATA: (0 = no		1 1 27			EDEST	RIAN	STA	TU	S:				
TEST:	N-LOCK				PHA		11	2	3	4	5	6	7	8
DELAY:	EXTEND					GRN	-		-			-	-	-
UNCLUSED .	MXCALL				DW	ELL								
RING	1 2 3 4	5 6 7 8	7		/	(0=d	ont v	vik, 1	=wl	k, 2=	-flwlk	. 3:	dark	3
EXIT			1	/	CYC	LE		T		1				
CALLS				\times		(0 =	no, 1	1 = a	ct, i	2 = n	ecall)			
			/	1										
	VAL TIMES:		/	1		VERLA	_	and the second second	-	-				
SEL PED	1.2017.2017	TRK YEL CHG : Z.				RLAP	A	E	3	С	0)		
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SEL RED	the second s	DWELL GREEN:	_		DWE	~ ~ ~		_			1			
TRACK G	1000 and 100	RET PED CLR :				=red, h	egrn,	, 2=fl	r, 3-	=fly,	4=da	rk)	-	-
TRK PED	CLR:	RET YEL CHG :			CYC		X	_		_		_		
		BET YEL CLR :	-			(0 = 1	no, 1	- a	(1)					
DWELL		4 5 6 7 8			6. LO TES DEL DWE	AY:	N-L EX	TENI	(.: D: _	-	1=ye SKIP. DUR/ LOCH	ATIO	ON:	
(0=red,	1=grn, 2=fir, 3=	fly, 4=dark)			RING		-	3	4	5	distant in the local distance in the local d	TY	18	٦
CYELE					DWE	LL	1	1	1	1		1	X	
(0=no, 1	=act, 2=min ree	call, 3=max recall)			CAL	LS				1		t		4
		SIC	GNAL P	HASIN	G		-	-	-	-	-	-		
PHASE#		ROAD					P	HAS	E	LO	AD SI	N	FLAS	SH
1						_	1			and the second				
2	M59							A			2		A	
3			12							-				
4	XIO 510 B	OGIE LAKE / NORDA	c				B	SC			4		R	
5													_	
6								_					1.1	
7			1.1				-	-	-		1.1	-		_2
8							-		-			_		
OLA							-		-			-		
OLB							1	_	-	-		-	1	-
OLD							-	-	+	-		-	-	_
1PED							-		+	-		-		-
2PED	WALK MA-SO D	ED (NORTH LEG)					w	0	-	6		+	-	-
3PED	1010 1-3-1	ED [NOKIN LEG]		-			w	m.	+	4		-	14	-
4PED	1100000				1	1000	-	1.14	+	2.00	5	-	10.11	-
5PED	N. Sec.						1	1	+	-	112.	1	100	-
6PED			0.200	1	115	1.1	-	-	-	1.00	115		1	
7PED	S. I. IE				11		-			-	10.55	-	1.5	-
8PED														
						and the second se	and the second se	and the second division of the second divisio	and the local division of the local division	and the second division of the second divisio				

Controller Information Sheet 4 Phase EPAC M Cabinet

Intersection CityiTwp State No. County No. Prepared By Date WB M-59 & XIO EIO Bogie Lake / Nordic White Lake 63041-01-229 4139 Dawn Bierlein 11/16/15

Phasing:

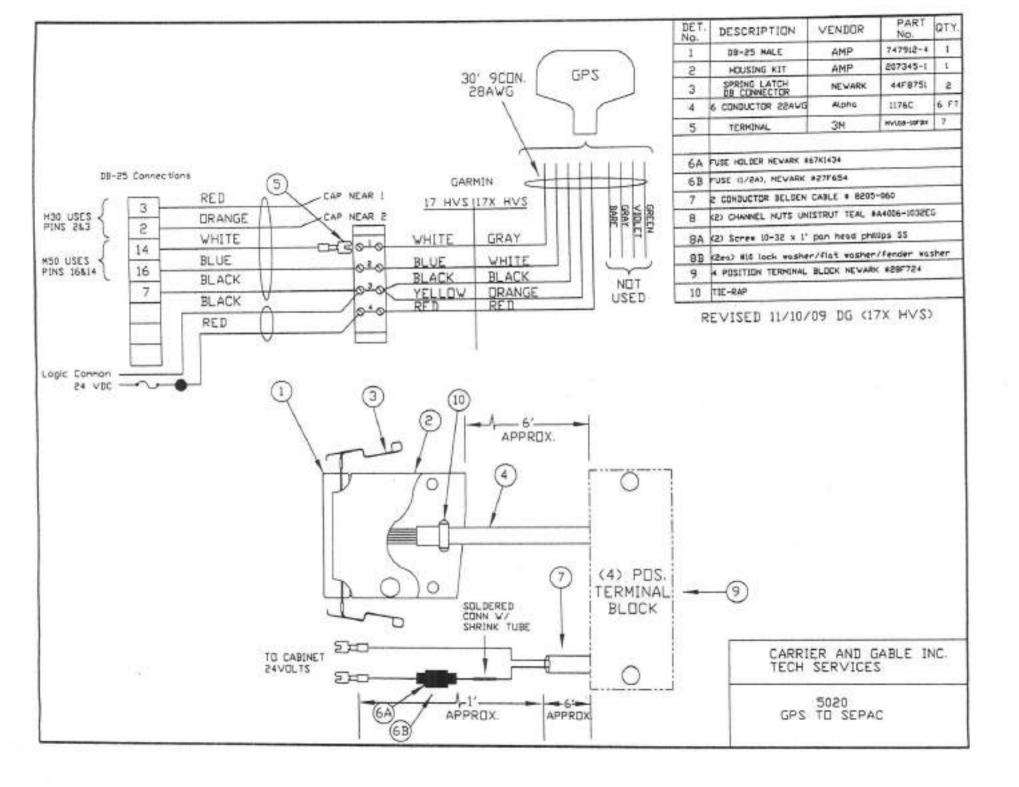
Load Switch 2: M-59	A	FLA
Load Switch 4: XTO EIO Bogie Lake / Nordic	B&C	FLR
Load Switch 6: WB M-59 Ped (North Leg)	WA	

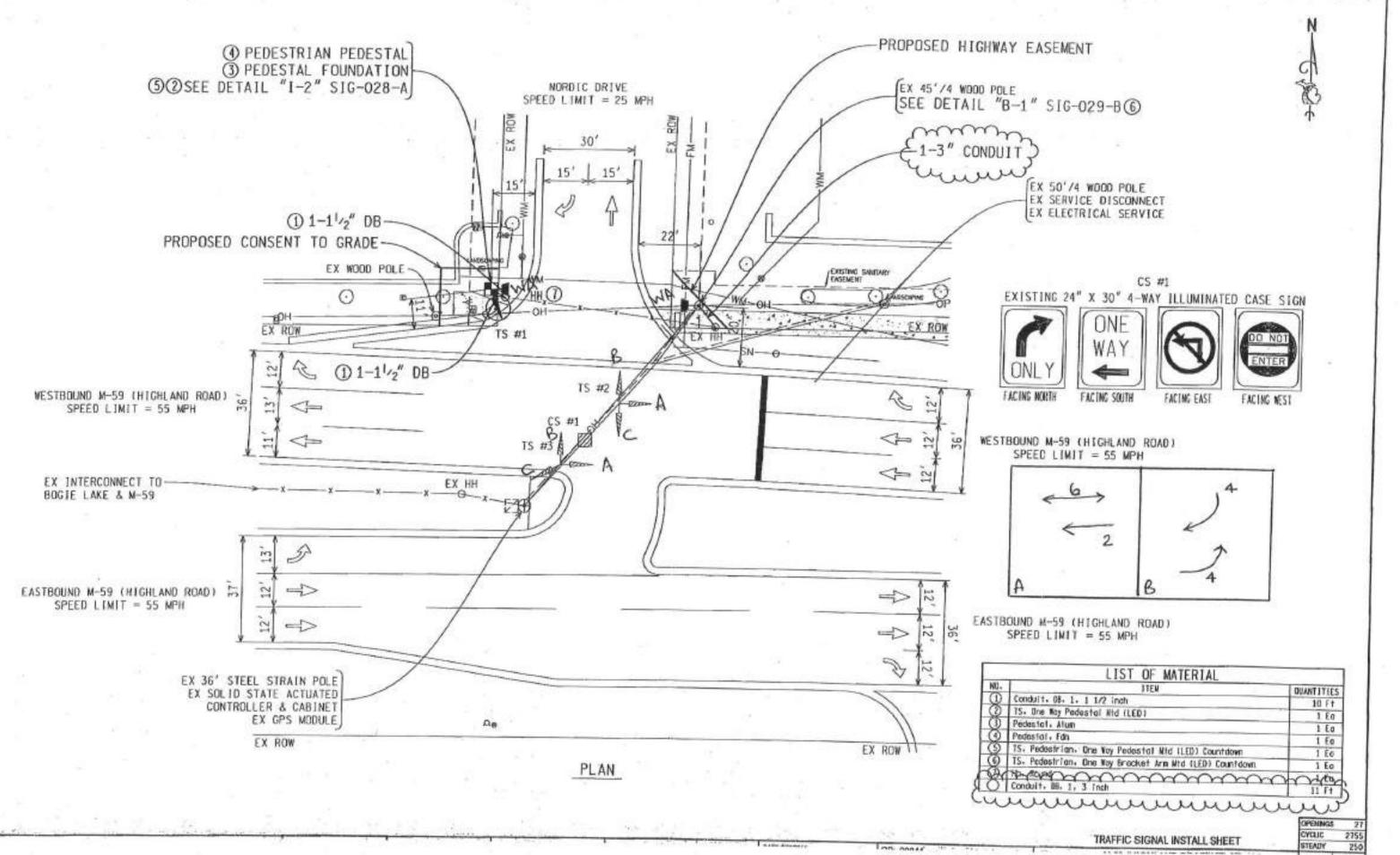
Jumpers:

121-213, 151-152, 153-154, 155-156, 173-174, 175-176, 177-178, 179-180, 185-186, 233-PB1, 237-PB1, 241-PB1, 255-256, 257-258, 259-260, 261-262, 263-PB1, 268-269.

Signal Monitor : NONE

All switched OFF EXCEPT: Dual Select A&B; G&Y Enable; SSM 2,4. Minimum Flash =4+2+1





	NCHRP 684 Internal Trip Capture Estimation Tool								
Project Name: Gateway Crossing TIS Organization:									
Project Location:	White Lake Twp		Performed By:	Fleis & VandenBrink Engineering					
Scenario Description:			Date:	12/13/2022					
Analysis Year:			Checked By:						
Analysis Period:	AM Street Peak Hour		Date:						

Table 1-A: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate)

Land Use	Developme	ent Data (For Info	ormation Only)		Estimated Vehicle-Trips ³	
Lanu Use	ITE LUCs ¹	Quantity	Units	Total	Entering	Exiting
Office				0		
Retail				14	8	6
Restaurant				197	100	97
Cinema/Entertainment				0		
Residential				0		
Hotel				0		
All Other Land Uses ²				0		
				211	108	103

	Table 2-A: Mode Split and Vehicle Occupancy Estimates									
Land Use		Entering Tri	ps		Exiting Trips					
Lanu Use	Veh. Occ.4	% Transit	% Non-Motorized		Veh. Occ. ⁴	% Transit	% Non-Motorized			
Office										
Retail										
Restaurant										
Cinema/Entertainment										
Residential										
Hotel										
All Other Land Uses ²										

Table 3-A: Average Land Use Interchange Distances (Feet Walking Distance)								
Origin (France)				Destination (To)				
Origin (From)	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel		
Office								
Retail								
Restaurant								
Cinema/Entertainment								
Residential								
Hotel								

	Table 4-A: Internal Person-Trip Origin-Destination Matrix*										
Origin (From)		Destination (To)									
Origin (From)	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel					
Office		0	0	0	0	0					
Retail	0		1	0	0	0					
Restaurant	0	1		0	0	0					
Cinema/Entertainment	0	0	0		0	0					
Residential	0	0	0	0		0					
Hotel	0	0	0	0	0						

Table 5-A	: Computatio	ons Summary	Table 5-A: Computations Summary			
	Total	Entering	Exiting	Land Use	Entering Trips	Exiting Trips
All Person-Trips	211	108	103	Office	N/A	N/A
Internal Capture Percentage	2%	2%	2%	Retail	13%	17%
				Restaurant	1%	1%
External Vehicle-Trips ⁵	207	106	101	Cinema/Entertainment	N/A	N/A
External Transit-Trips ⁶	0	0	0	Residential	N/A	N/A
External Non-Motorized Trips ⁶	0	0	0	Hotel	N/A	N/A

¹ Land Use Codes (LUCs) from <i>Trip Generation Manual</i> , published by the Institute of Transportation Engineers.
² Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator.
³ Enter trips assuming no transit or non-motorized trips (as assumed in ITE <i>Trip Generation Manual</i>).
⁴ Enter vehicle occupancy assumed in Table 1-A vehicle trips. If vehicle occupancy changes for proposed mixed-use project, manual adjustments must be made to Tables 5-A, 9-A (O and D). Enter transit, non-motorized percentages that will result with proposed mixed-use project complete.
⁵ Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A.
⁶ Person-Trips
*Indicates computation that has been rounded to the nearest whole number.

Estimation Tool Developed by the Texas A&M Transportation Institute - Version 2013.1

	NCHRP 684 Internal Trip Capture Estimation Tool								
Project Name:			Organization:						
Project Location:			Performed By:						
Scenario Description:			Date:						
Analysis Year:			Checked By:						
Analysis Period:	PM Street Peak Hour		Date:						

	Table 1-P: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate)									
Land Use	Developme	Development Data (For Information Only)				Estimated Vehicle-Trips ³				
Land Use	ITE LUCs ¹	Quantity	Units		Total	Entering	Exiting			
Office					0					
Retail					54	27	27			
Restaurant					223	115	108			
Cinema/Entertainment					0					
Residential					0					
Hotel					0					
All Other Land Uses ²					0					
					277	142	135			

Table 2-P: Mode Split and Vehicle Occupancy Estimates									
		Entering Tr	ips		Exiting Trips				
Land Use	Veh. Occ.4	% Transit	% Non-Motorized	Veh. Occ.4	% Transit	% Non-Motorized			
Office									
Retail									
Restaurant									
Cinema/Entertainment									
Residential									
Hotel									
All Other Land Uses ²									

	Table 3-P: Average Land Use Interchange Distances (Feet Walking Distance)								
Origin (From)				Destination (To)					
Oligin (Floin)	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel			
Office									
Retail									
Restaurant									
Cinema/Entertainment									
Residential									
Hotel									

Table 4-P: Internal Person-Trip Origin-Destination Matrix*										
Origin (From)		Destination (To)								
Origin (From)	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel				
Office		0	0	0	0	0				
Retail	0		8	0	0	0				
Restaurant	0	14		0	0	0				
Cinema/Entertainment	0	0	0		0	0				
Residential	0	0	0	0		0				
Hotel	0	0	0	0	0					

Table 5-P	: Computatio	ns Summary		Table 6-P: Internal	Trip Capture Percenta	ges by Land Use
	Total	Entering	Exiting	Land Use	Entering Trips	Exiting Trips
All Person-Trips	277	142	135	Office	N/A	N/A
Internal Capture Percentage	16%	15%	16%	Retail	52%	30%
				Restaurant	7%	13%
External Vehicle-Trips ⁵	233	120	113	Cinema/Entertainment	N/A	N/A
External Transit-Trips ⁶	0	0	0	Residential	N/A	N/A
External Non-Motorized Trips ⁶	0	0	0	Hotel	N/A	N/A

¹Land Use Codes (LUCs) from *Trip Generation Manual*, published by the Institute of Transportation Engineers.

²Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator.

³Enter trips assuming no transit or non-motorized trips (as assumed in ITE *Trip Generation Manual*).

⁴Enter vehicle occupancy assumed in Table 1-P vehicle trips. If vehicle occupancy changes for proposed mixed-use project, manual adjustments must be ⁵Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P.

⁶Person-Trips

*Indicates computation that has been rounded to the nearest whole number.

Estimation Tool Developed by the Texas A&M Transportation Institute - Version 2013.1

	≯	-	-	•	1	<		
Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations		^			<u> </u>	OBIX		
Traffic Volume (vph)	0	1587	0	0	134	0		
Future Volume (vph)	0	1587	0	0	134	0		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)	1000	6.1	1000	1000	5.9	1000		
Lane Util. Factor		0.95			1.00			
Frt		1.00			1.00			
Flt Protected		1.00			0.95			
Satd. Flow (prot)		3471			1736			
Flt Permitted		1.00			0.95			
Satd. Flow (perm)		3471			1736			
Peak-hour factor, PHF	0.91	0.91	0.92	0.92	0.61	0.61		
Adj. Flow (vph)	0	1744	0	0	220	0		
RTOR Reduction (vph)	0	0	0	0	0	0		
Lane Group Flow (vph)	0	1744	0	0	220	0		
Heavy Vehicles (%)	4%	4%	2%	2%	4%	4%		
Turn Type		NA			Prot			
Protected Phases		2!			4 2!			
Permitted Phases								
Actuated Green, G (s)		56.9			90.0			
Effective Green, g (s)		56.9			83.9			
Actuated g/C Ratio		0.63			0.93			
Clearance Time (s)		6.1						
Vehicle Extension (s)		3.0						
Lane Grp Cap (vph)		2194			1618			
v/s Ratio Prot		c0.50			c0.13			
v/s Ratio Perm								
v/c Ratio		0.79			0.14			
Uniform Delay, d1		12.2			0.2			
Progression Factor		1.00			1.00			
Incremental Delay, d2		3.1			0.2			
Delay (s)		15.3			0.4			
Level of Service		В	• (А			
Approach Delay (s)		15.3	0.0		0.4			
Approach LOS		В	A		А			
Intersection Summary								
HCM 2000 Control Delay			13.6	H	CM 2000	Level of Service)	В
HCM 2000 Volume to Capacit	y ratio		0.62					
Actuated Cycle Length (s)			90.0		um of lost			12.0
Intersection Capacity Utilization	on		80.0%	IC	U Level o	of Service		D
Analysis Period (min)			15					
! Phase conflict between lan	e groups							

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		<u></u>	1					•	77		•	
Traffic Volume (vph)	0	1222	499	0	0	0	0	102	293	0	45	0
Future Volume (vph)	0	1222	499	0	0	0	0	102	293	0	45	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.7	6.7					10.9	10.9		6.9	
Lane Util. Factor		0.95	1.00					1.00	0.88		1.00	
Frt		1.00	0.85					1.00	0.85		1.00	
Flt Protected		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (prot)		3471	1553					1827	2733		1681	
Flt Permitted		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (perm)		3471	1553					1827	2733		1681	
Peak-hour factor, PHF	0.89	0.89	0.89	0.92	0.92	0.92	0.87	0.87	0.87	0.95	0.95	0.95
Adj. Flow (vph)	0	1373	561	0	0	0	0	117	337	0	47	0
RTOR Reduction (vph)	0	0	229	0	0	0	0	0	67	0	0	0
Lane Group Flow (vph)	0	1373	332	0	0	0	0	117	270	0	47	0
Heavy Vehicles (%)	4%	4%	4%	2%	2%	2%	4%	4%	4%	13%	13%	13%
Turn Type		NA	Perm					NA	Perm		NA	
Protected Phases		2						4			8	
Permitted Phases			2						4			
Actuated Green, G (s)		53.3	53.3					19.1	19.1		23.1	
Effective Green, g (s)		53.3	53.3					19.1	19.1		23.1	
Actuated g/C Ratio		0.59	0.59					0.21	0.21		0.26	
Clearance Time (s)		6.7	6.7					10.9	10.9		6.9	_
Vehicle Extension (s)		3.0	3.0					3.0	3.0		3.0	
Lane Grp Cap (vph)		2055	919					387	580		431	_
v/s Ratio Prot		c0.40	0.04					0.06	0.40		0.03	
v/s Ratio Perm		0.07	0.21					0.00	c0.10		0.44	_
v/c Ratio		0.67	0.36					0.30	0.47		0.11	
Uniform Delay, d1		12.4	9.5					29.8	31.0		25.6	
Progression Factor		0.16	0.24					1.00	1.00		0.00	
Incremental Delay, d2		1.2 3.2	0.7					2.0	2.7		0.5	
Delay (s) Level of Service		э.z А	3.0 A					31.8 C	33.7 C		0.5	
Approach Delay (s)		3.1	A		0.0			33.2	U		A 0.5	
Approach LOS		3.1 A			0.0 A			55.Z C			0.5 A	
		A			~			U			A	
Intersection Summary			0.7		014 0000		<u></u>					
HCM 2000 Control Delay	t'a		8.7	Н	CM 2000	Level of S	Service		А			
HCM 2000 Volume to Capacity	ratio		0.61	0		(47.0			
Actuated Cycle Length (s)			90.0		um of losi				17.6			
Intersection Capacity Utilization	I		58.7%	IC	U Level (of Service			В			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					- † †	1		↑			↑	77
Traffic Volume (vph)	0	0	0	0	1067	44	0	102	0	0	45	68
Future Volume (vph)	0	0	0	0	1067	44	0	102	0	0	45	68
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.7	6.7		6.9			10.9	10.9
Lane Util. Factor					0.95	1.00		1.00			1.00	0.88
Frt					1.00	0.85		1.00			1.00	0.85
Flt Protected					1.00	1.00		1.00			1.00	1.00
Satd. Flow (prot)					3406	1524		1827			1681	2515
Flt Permitted					1.00	1.00		1.00			1.00	1.00
Satd. Flow (perm)					3406	1524		1827			1681	2515
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.87	0.87	0.87	0.95	0.95	0.95
Adj. Flow (vph)	0	0	0	0	1160	48	0	117	0	0	47	72
RTOR Reduction (vph)	0	0	0	0	0	20	0	0	0	0	0	57
Lane Group Flow (vph)	0	0	0	0	1160	28	0	117	0	0	47	15
Heavy Vehicles (%)	2%	2%	2%	6%	6%	6%	4%	4%	4%	13%	13%	13%
Turn Type					NA	Perm		NA			NA	Perm
Protected Phases					6			8			4	
Permitted Phases						6		00.4			40.4	4
Actuated Green, G (s)					53.3	53.3		23.1			19.1	19.1
Effective Green, g (s)					53.3	53.3		23.1			19.1	19.1
Actuated g/C Ratio					0.59	0.59		0.26			0.21	0.21
Clearance Time (s)					6.7	6.7		6.9			10.9	10.9
Vehicle Extension (s)					3.0	3.0		3.0			3.0	3.0
Lane Grp Cap (vph)					2017	902		468			356	533
v/s Ratio Prot					c0.34	0.00		c0.06			0.03	0.04
v/s Ratio Perm					0.50	0.02		0.05			0.40	0.01
v/c Ratio					0.58	0.03		0.25			0.13	0.03
Uniform Delay, d1					11.3	7.6		26.6			28.7	28.1
Progression Factor					0.48	0.47 0.1		0.00 1.2			1.25 0.8	2.12 0.1
Incremental Delay, d2					1.1 6.5	3.7		1.2			0.0 36.8	59.6
Delay (s) Level of Service					0.5 A	3.7 A		1.5 A			30.0 D	59.0 E
Approach Delay (s)		0.0			6.4	A		1.3			50.6	E
Approach LOS		0.0 A			0.4 A			1.3 A			50.0 D	
Intersection Summary												
HCM 2000 Control Delay			9.6	H	CM 2000	Level of S	Service		A			
HCM 2000 Volume to Capacity	v ratio		0.50									
Actuated Cycle Length (s)			90.0	S	um of los	t time (s)			17.6			
Intersection Capacity Utilizatio	n		58.7%			of Service			В			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					<u></u>	1		4				1
Traffic Volume (vph)	0	0	0	0	986	7	119	9	0	0	0	6
Future Volume (vph)	0	0	0	0	986	7	119	9	0	0	0	6
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.1	6.1		5.9				5.9
Lane Util. Factor					0.95	1.00		1.00				1.00
Frt					1.00	0.85		1.00				0.86
Flt Protected					1.00	1.00		0.96				1.00
Satd. Flow (prot)					3406	1524		1763				1644
Flt Permitted					1.00	1.00		0.96				1.00
Satd. Flow (perm)					3406	1524		1763				1644
Peak-hour factor, PHF	0.92	0.92	0.92	0.95	0.95	0.95	0.78	0.78	0.78	0.75	0.75	0.75
Adj. Flow (vph)	0	0	0	0	1038	7	153	12	0	0	0	8
RTOR Reduction (vph)	0	0	0	0	0	3	0	96	0	0	0	6
Lane Group Flow (vph)	0	0	0	0	1038	4	0	69	0	0	0	2
Heavy Vehicles (%)	2%	2%	2%	6%	6%	6%	3%	3%	3%	0%	0%	0%
Turn Type					NA	Perm	custom	NA				Perm
Protected Phases					2!			4				
Permitted Phases						2	4 2!					4
Actuated Green, G (s)					56.9	56.9		21.1				21.1
Effective Green, g (s)					56.9	56.9		21.1				21.1
Actuated g/C Ratio					0.63	0.63		0.23				0.23
Clearance Time (s)					6.1	6.1		5.9				5.9
Vehicle Extension (s)					3.0	3.0		3.0				3.0
Lane Grp Cap (vph)					2153	963		413				385
v/s Ratio Prot					c0.30							
v/s Ratio Perm						0.00		0.04				0.00
v/c Ratio					0.48	0.00		0.17				0.00
Uniform Delay, d1					8.8	6.1		27.5				26.4
Progression Factor					1.00	1.00		1.32				1.00
Incremental Delay, d2					0.8	0.0		0.7				0.0
Delay (s)					9.5	6.1		36.9				26.4
Level of Service					A	A		D				С
Approach Delay (s)		0.0			9.5			36.9			26.4	
Approach LOS		A			A			D			С	
Intersection Summary												
HCM 2000 Control Delay			13.3	Н	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capaci	ty ratio		0.40									
Actuated Cycle Length (s)			90.0		um of los				12.0			
Intersection Capacity Utilizati	on		55.1%	IC	U Level	of Servic	е		В			
Analysis Period (min)			15									
Phase conflict between lar	ne groups											

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Movement	WBL	WBR	NBT	NBR	SBL	SBT			
Lane Configurations	۲					<u>††</u>			
Traffic Volume (vph)	88	0	0	0	0	25			
Future Volume (vph)	88	0	0	0	0	25			
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900			
Total Lost time (s)	4.9					5.4			
Lane Util. Factor	1.00					0.95			
Frt	1.00					1.00			
Flt Protected	0.95					1.00			
Satd. Flow (prot)	1556					3139			
Flt Permitted	0.95					1.00			
Satd. Flow (perm)	1556					3139			
Peak-hour factor, PHF	0.82	0.82	0.92	0.92	0.81	0.81			
Adj. Flow (vph)	107	0	0	0	0	31			
RTOR Reduction (vph)	0	0	0	0	0	0			
Lane Group Flow (vph)	107	0	0	0	0	31			
Heavy Vehicles (%)	16%	16%	2%	2%	15%	15%			
Turn Type	Prot					NA			
Protected Phases	4 2!					2!			
Permitted Phases									
Actuated Green, G (s)	90.0					57.6			
Effective Green, g (s)	84.6					57.6			
Actuated g/C Ratio	0.94					0.64			
Clearance Time (s)						5.4			
Vehicle Extension (s)						3.0			
Lane Grp Cap (vph)	1462					2008			
v/s Ratio Prot	c0.07					0.01			
v/s Ratio Perm									
v/c Ratio	0.07					0.02			
Uniform Delay, d1	0.2					5.9			
Progression Factor	1.00					1.00			
Incremental Delay, d2	0.1					0.0			
Delay (s)	0.3					5.9			
Level of Service	А					А			
Approach Delay (s)	0.3		0.0			5.9			
Approach LOS	А		А			А			
Intersection Summary									
HCM 2000 Control Delay			1.5	H	CM 2000	Level of Servic	e	Α	
HCM 2000 Volume to Capa	acity ratio		0.08						
Actuated Cycle Length (s)			90.0		um of lost		1	0.3	
Intersection Capacity Utilization	ation		25.2%	IC	U Level o	of Service		А	
Analysis Period (min)			15						
! Phase conflict between	lane groups								
 Critical Lana Group 									

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Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations		^			<u> </u>	OBIX		
Traffic Volume (vph)	0	1407	0	0	212	0		
Future Volume (vph)	0	1407	0	0	212	0		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)		6.1			5.9			
Lane Util. Factor		0.95			1.00			
Frt		1.00			1.00			
Flt Protected		1.00			0.95			
Satd. Flow (prot)		3471			1787			
Flt Permitted		1.00			0.95			
Satd. Flow (perm)		3471			1787			
Peak-hour factor, PHF	0.94	0.94	0.92	0.92	0.88	0.88		
Adj. Flow (vph)	0	1497	0	0	241	0		
RTOR Reduction (vph)	0	0	0	0	0	0		
Lane Group Flow (vph)	0	1497	0	0	241	0		
Heavy Vehicles (%)	4%	4%	2%	2%	1%	1%		
Turn Type		NA			Prot			
Protected Phases		2!			4 2!			
Permitted Phases								
Actuated Green, G (s)		85.9			120.0			
Effective Green, g (s)		85.9			113.9			
Actuated g/C Ratio		0.72			0.95			
Clearance Time (s)		6.1						
Vehicle Extension (s)		3.0						
Lane Grp Cap (vph)		2484			1696			
v/s Ratio Prot		c0.43			c0.13			
v/s Ratio Perm								
v/c Ratio		0.60			0.14			
Uniform Delay, d1		8.5			0.2			
Progression Factor		1.00			1.00			
Incremental Delay, d2		1.1			0.1			
Delay (s)		9.6			0.3			
Level of Service		Α			Α			
Approach Delay (s)		9.6	0.0		0.3			
Approach LOS		A	А		А			
Intersection Summary								
HCM 2000 Control Delay			8.3	Н	CM 2000	Level of Service)	А
HCM 2000 Volume to Capacit	y ratio		0.51					
Actuated Cycle Length (s)			120.0	S	um of lost	time (s)		12.0
Intersection Capacity Utilization	n		95.4%	IC	CU Level o	of Service		F
Analysis Period (min)			15					
! Phase conflict between lan	e groups							

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		<u></u>	1					↑	77		•	
Traffic Volume (vph)	0	1288	331	0	0	0	0	186	345	0	65	0
Future Volume (vph)	0	1288	331	0	0	0	0	186	345	0	65	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.7	6.7					10.9	10.9		6.9	
Lane Util. Factor		0.95	1.00					1.00	0.88		1.00	
Frt		1.00	0.85					1.00	0.85		1.00	
Flt Protected		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (prot)		3505	1568					1863	2787		1827	
Flt Permitted		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (perm)		3505	1568					1863	2787		1827	
Peak-hour factor, PHF	0.95	0.95	0.95	0.92	0.92	0.92	0.93	0.93	0.93	0.92	0.92	0.92
Adj. Flow (vph)	0	1356	348	0	0	0	0	200	371	0	71	0
RTOR Reduction (vph)	0	0	106	0	0	0	0	0	120	0	0	0
Lane Group Flow (vph)	0	1356	242	0	0	0	0	200	251	0	71	0
Heavy Vehicles (%)	3%	3%	3%	2%	2%	2%	2%	2%	2%	4%	4%	4%
Turn Type		NA	Perm					NA	Perm		NA	
Protected Phases		2						4			8	
Permitted Phases			2						4			
Actuated Green, G (s)		83.3	83.3					19.1	19.1		23.1	
Effective Green, g (s)		83.3	83.3					19.1	19.1		23.1	
Actuated g/C Ratio		0.69	0.69					0.16	0.16		0.19	
Clearance Time (s)		6.7	6.7					10.9	10.9		6.9	
Vehicle Extension (s)		3.0	3.0					3.0	3.0		3.0	
Lane Grp Cap (vph)		2433	1088					296	443		351	
v/s Ratio Prot		c0.39						c0.11			0.04	
v/s Ratio Perm			0.15						0.09			
v/c Ratio		0.56	0.22					0.68	0.57		0.20	
Uniform Delay, d1		9.2	6.6					47.5	46.6		40.7	
Progression Factor		0.23	0.24					1.00	1.00		0.00	
Incremental Delay, d2		0.8	0.4					11.7	5.2		1.3	
Delay (s)		2.9	2.0					59.3	51.8		1.3	
Level of Service		А	А					E	D		А	
Approach Delay (s)		2.7			0.0			54.4			1.3	
Approach LOS		A			Α			D			А	
Intersection Summary												
HCM 2000 Control Delay			15.2	Н	CM 2000	Level of \$	Service		В			
HCM 2000 Volume to Capacity	/ ratio		0.58									
Actuated Cycle Length (s)			120.0	S	um of lost	t time (s)			17.6			
Intersection Capacity Utilization	n		71.1%	IC	CU Level of	of Service			С			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					- ††	1		↑			↑	77
Traffic Volume (vph)	0	0	0	0	1807	110	0	186	0	0	65	143
Future Volume (vph)	0	0	0	0	1807	110	0	186	0	0	65	143
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.7	6.7		6.9			10.9	10.9
Lane Util. Factor					0.95	1.00		1.00			1.00	0.88
Frpb, ped/bikes					1.00	0.99		1.00			1.00	0.98
Flpb, ped/bikes					1.00	1.00		1.00			1.00	1.00
Frt					1.00	0.85		1.00			1.00	0.85
Flt Protected					1.00	1.00		1.00			1.00	1.00
Satd. Flow (prot)					3539	1562		1863			1827	2670
Flt Permitted					1.00	1.00		1.00			1.00	1.00
Satd. Flow (perm)					3539	1562		1863			1827	2670
Peak-hour factor, PHF	0.92	0.92	0.92	0.90	0.90	0.90	0.93	0.93	0.93	0.92	0.92	0.92
Adj. Flow (vph)	0	0	0	0	2008	122	0	200	0	0	71	155
RTOR Reduction (vph)	0	0	0	0	0	37	0	0	0	0	0	31
Lane Group Flow (vph)	0	0	0	0	2008	85	0	200	0	0	71	124
Confl. Peds. (#/hr)						3						1
Heavy Vehicles (%)	2%	2%	2%	2%	2%	2%	2%	2%	2%	4%	4%	4%
Turn Type					NA	Perm		NA			NA	Perm
Protected Phases					6			8			4	
Permitted Phases						6						4
Actuated Green, G (s)					83.3	83.3		23.1			19.1	19.1
Effective Green, g (s)					83.3	83.3		23.1			19.1	19.1
Actuated g/C Ratio					0.69	0.69		0.19			0.16	0.16
Clearance Time (s)					6.7	6.7		6.9			10.9	10.9
Vehicle Extension (s)					3.0	3.0		3.0			3.0	3.0
Lane Grp Cap (vph)					2456	1084		358			290	424
v/s Ratio Prot					c0.57			c0.11			0.04	
v/s Ratio Perm						0.05						0.05
v/c Ratio					0.82	0.08		0.56			0.24	0.29
Uniform Delay, d1					13.0	5.9		43.8			44.1	44.5
Progression Factor					0.91	0.33		0.00			1.34	1.45
Incremental Delay, d2					2.3	0.1		4.5			2.0	1.7
Delay (s)					14.2	2.1		4.6			61.2	66.4
Level of Service					В	A		A			E	E
Approach Delay (s)		0.0			13.5			4.6			64.8	_
Approach LOS		A			В			A			E	
Intersection Summary												
HCM 2000 Control Delay			17.3	Н	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capacity	v ratio		0.79									
Actuated Cycle Length (s)			120.0	S	um of los	t time (s)			17.6			
Intersection Capacity Utilizatio	n		71.1%			of Service			С			
Analysis Period (min)			15						-			
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					^	1		र्भ				1
Traffic Volume (vph)	0	0	0	0	1655	38	203	34	0	0	0	59
Future Volume (vph)	0	0	0	0	1655	38	203	34	0	0	0	59
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.1	6.1		5.9				5.9
Lane Util. Factor					0.95	1.00		1.00				1.00
Frpb, ped/bikes					1.00	0.98		1.00				1.00
Flpb, ped/bikes					1.00	1.00		1.00				1.00
Frt					1.00	0.85		1.00				0.86
Flt Protected					1.00	1.00		0.96				1.00
Satd. Flow (prot)					3505	1536		1822				1644
Flt Permitted					1.00	1.00		0.96				1.00
Satd. Flow (perm)					3505	1536		1822				1644
Peak-hour factor, PHF	0.92	0.92	0.92	0.95	0.95	0.95	0.79	0.79	0.79	0.74	0.74	0.74
Adj. Flow (vph)	0	0.02	0	0	1742	40	257	43	0	0	0	80
RTOR Reduction (vph)	0	0	0	0	0	7	0	33	0	0	0	33
Lane Group Flow (vph)	0	0	0	0	1742	33	0	267	0	0	0	47
Confl. Peds. (#/hr)	Ű	Ŭ	Ű	Ŭ		1	Ŭ	201	Ű	Ű	Ŭ	
Heavy Vehicles (%)	2%	2%	2%	3%	3%	3%	0%	0%	0%	0%	0%	0%
Turn Type	270	270	270	070	NA	Perm		NA	0,10	0,0	0 /0	Perm
Protected Phases					2!	I CIIII	Custom	4				I CIIII
Permitted Phases					۷:	2	4 2!	T				4
Actuated Green, G (s)					85.9	85.9	7 2:	22.1				22.1
Effective Green, g (s)					85.9	85.9		22.1				22.1
Actuated g/C Ratio					0.72	0.72		0.18				0.18
Clearance Time (s)					6.1	6.1		5.9				5.9
Vehicle Extension (s)					3.0	3.0		3.0				3.0
Lane Grp Cap (vph)					2508	1099		335				302
v/s Ratio Prot					c0.50	1099		335				302
v/s Ratio Perm					0.50	0.02		0.15				0.03
v/c Ratio					0.69	0.02		0.15				0.05
					9.6	0.03 5.0		46.8				41.1
Uniform Delay, d1 Progression Factor					9.0 1.00	5.0 1.00		40.0				41.1
Incremental Delay, d2					1.6			15.1				
					11.2	0.1		65.0				1.1 42.2
Delay (s)						5.0 A		65.0 E				42.2 D
Level of Service		0.0			B 11.1	A		⊏ 65.0			42.2	U
Approach Delay (s)												
Approach LOS		А			В			E			D	
Intersection Summary												
HCM 2000 Control Delay			19.7	Н	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capacit	v ratio		0.71									
Actuated Cycle Length (s)	,		120.0	S	um of lost	t time (s)			12.0			
Intersection Capacity Utilizatio	n		79.5%		U Level o				D			
Analysis Period (min)			15									
Phase conflict between lan	e groups											
c Critical Lane Group	0											

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Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	5					<u>††</u>		
Traffic Volume (vph)	185	0	0	0	0	23		
Future Volume (vph)	185	0	0	0	0	23		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)	4.9					5.4		
Lane Util. Factor	1.00					0.95		
Frt	1.00					1.00		
Flt Protected	0.95					1.00		
Satd. Flow (prot)	1752					3610		
Flt Permitted	0.95					1.00		
Satd. Flow (perm)	1752					3610		
Peak-hour factor, PHF	0.86	0.86	0.92	0.92	0.60	0.60		
Adj. Flow (vph)	215	0	0	0	0	38		
RTOR Reduction (vph)	0	0	0	0	0	0		
Lane Group Flow (vph)	215	0	0	0	0	38		
Heavy Vehicles (%)	3%	3%	2%	2%	0%	0%		
Turn Type	Prot					NA		
Protected Phases	4 2!					2!		
Permitted Phases								
Actuated Green, G (s)	120.0					86.6		
Effective Green, g (s)	114.6					86.6		
Actuated g/C Ratio	0.95					0.72		
Clearance Time (s)						5.4		
Vehicle Extension (s)						3.0		
Lane Grp Cap (vph)	1673					2605		
v/s Ratio Prot	c0.12					0.01		
v/s Ratio Perm								
v/c Ratio	0.13					0.01		
Uniform Delay, d1	0.1					4.7		
Progression Factor	1.00					1.00		
Incremental Delay, d2	0.2					0.0		
Delay (s)	0.3					4.7		
Level of Service	А					А		
Approach Delay (s)	0.3		0.0			4.7		
Approach LOS	А		А			А		
Intersection Summary								
HCM 2000 Control Delay			1.0	Н	CM 2000	Level of Servic	e	
HCM 2000 Volume to Capa	city ratio		0.13					
Actuated Cycle Length (s)			120.0	Sı	um of lost	t time (s)		
Intersection Capacity Utiliza	ation		30.6%			of Service		
Analysis Period (min)			15					
Phase conflict between la	ane groups							
c Critical Lane Group	0.0.00							

Intersection: 10: EB Highland Road & WB-to-EB X/O

Movement	EB	EB	SB
Directions Served	Т	Т	L
Maximum Queue (ft)	295	316	69
Average Queue (ft)	152	150	36
95th Queue (ft)	250	258	68
Link Distance (ft)	708	708	35
Upstream Blk Time (%)			12
Queuing Penalty (veh)			20
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 11: WB-to-EB X/O & WB Highland Road

Movement	WB
Directions Served	L
Maximum Queue (ft)	100
Average Queue (ft)	21
95th Queue (ft)	73
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	325
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 20: Bogie Lake Road & EB Highland Road

Movement	EB	EB	EB	NB	NB	NB	SB
Directions Served	Т	Т	R	Т	R	R	Т
Maximum Queue (ft)	132	138	95	130	136	120	14
Average Queue (ft)	35	42	41	55	61	48	0
95th Queue (ft)	88	94	75	108	109	94	10
Link Distance (ft)	330	330	330	291	291	291	37
Upstream Blk Time (%)							0
Queuing Penalty (veh)							0
Storage Bay Dist (ft)							
Storage Blk Time (%)							
Queuing Penalty (veh)							

Intersection: 21: Bogie Lake Road & WB Highland Road

	14/5	14/5	14/5	00	^	0.5
Movement	WB	WB	WB	SB	SB	SB
Directions Served	Т	Т	R	Т	R	R
Maximum Queue (ft)	114	100	39	94	67	47
Average Queue (ft)	28	29	3	30	25	16
95th Queue (ft)	79	82	18	73	55	42
Link Distance (ft)	477	477	477	152	152	152
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)						
Storage Blk Time (%)						
Queuing Penalty (veh)						

Intersection: 30: EB-to-WB X/O/Nordic Drive & WB Highland Road

Movement	WB	WB	WB	NB	SB
Directions Served	Т	Т	R	LT	R
Maximum Queue (ft)	196	180	21	55	30
Average Queue (ft)	112	64	1	35	5
95th Queue (ft)	180	132	11	62	23
Link Distance (ft)	905	905		11	94
Upstream Blk Time (%)				17	
Queuing Penalty (veh)				23	
Storage Bay Dist (ft)			50		
Storage Blk Time (%)		9			
Queuing Penalty (veh)		1			

Intersection: 31: EB Highland Road & EB-to-WB X/O

Movement	EB
Directions Served	L
Maximum Queue (ft)	114
Average Queue (ft)	23
95th Queue (ft)	73
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	300
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 40: Bogie Lake Road & NB-to-SB X/O

Movement	WB	SB	SB
Directions Served	L	Т	Т
Maximum Queue (ft)	10	54	6
Average Queue (ft)	0	8	0
95th Queue (ft)	5	34	4
Link Distance (ft)	28	192	192
Upstream Blk Time (%)	0		
Queuing Penalty (veh)	0		
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 41: Bogie Lake Road & NB-to-SB X/O

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)

Intersection: 50: W. Site Drive & EB Highland Road

vement
ections Served
ximum Queue (ft)
erage Queue (ft)
h Queue (ft)
k Distance (ft)
stream Blk Time (%)
euing Penalty (veh)
rage Bay Dist (ft)
rage Blk Time (%)
euing Penalty (veh)

Intersection: 60: Bogie Lake Road & E. Site Drive

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)
Zone Summary

Zone wide Queuing Penalty: 44

Intersection: 10: EB Highland Road & WB-to-EB X/O

Movement	EB	EB	SB
Directions Served	Т	Т	L
Maximum Queue (ft)	255	250	56
Average Queue (ft)	148	120	45
95th Queue (ft)	231	214	61
Link Distance (ft)	708	708	35
Upstream Blk Time (%)			22
Queuing Penalty (veh)			47
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 11: WB-to-EB X/O & WB Highland Road

	14/5	
Movement	WB	WB
Directions Served	L	Т
Maximum Queue (ft)	127	10
Average Queue (ft)	31	0
95th Queue (ft)	89	7
Link Distance (ft)		745
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)	325	
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 20: Bogie Lake Road & EB Highland Road

Movement	EB	EB	EB	NB	NB	NB
Directions Served	Т	Т	R	Т	R	R
Maximum Queue (ft)	90	104	62	238	154	137
Average Queue (ft)	35	39	24	124	77	62
95th Queue (ft)	75	83	57	206	128	110
Link Distance (ft)	330	330	330	291	291	291
Upstream Blk Time (%)				0		
Queuing Penalty (veh)				0		
Storage Bay Dist (ft)						
Storage Blk Time (%)						
Queuing Penalty (veh)						

Intersection: 21: Bogie Lake Road & WB Highland Road

Movement	WB	WB	WB	NB	SB	SB	SB
Directions Served	Т	Т	R	Т	Т	R	R
Maximum Queue (ft)	226	240	46	5	111	127	116
Average Queue (ft)	68	77	7	0	50	52	48
95th Queue (ft)	151	160	30	6	95	101	94
Link Distance (ft)	477	477	477	37	152	152	152
Upstream Blk Time (%)		0		1	0	0	0
Queuing Penalty (veh)		0		1	0	0	0
Storage Bay Dist (ft)							
Storage Blk Time (%)							
Queuing Penalty (veh)							

Intersection: 30: EB-to-WB X/O/Nordic Drive & WB Highland Road

	14/5	14/5			0.5
Movement	WB	WB	WB	NB	SB
Directions Served	Т	Т	R	LT	R
Maximum Queue (ft)	300	263	28	48	77
Average Queue (ft)	175	140	6	47	31
95th Queue (ft)	266	234	23	54	62
Link Distance (ft)	905	905		11	94
Upstream Blk Time (%)				54	0
Queuing Penalty (veh)				129	0
Storage Bay Dist (ft)			50		
Storage Blk Time (%)		15			
Queuing Penalty (veh)		6			
• • •					

Intersection: 31: EB Highland Road & EB-to-WB X/O

Movement	EB
Directions Served	L
Maximum Queue (ft)	250
Average Queue (ft)	112
95th Queue (ft)	214
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	300
Storage Blk Time (%)	0
Queuing Penalty (veh)	1

Intersection: 40: Bogie Lake Road & NB-to-SB X/O

Movement	WB	SB
	VVD	30
Directions Served	L	Т
Maximum Queue (ft)	34	35
Average Queue (ft)	2	4
95th Queue (ft)	15	22
Link Distance (ft)	28	192
Upstream Blk Time (%)	0	
Queuing Penalty (veh)	0	
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 41: Bogie Lake Road & NB-to-SB X/O

Movement	NB
Directions Served	L
Maximum Queue (ft)	11
Average Queue (ft)	1
95th Queue (ft)	10
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	300
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 50: W. Site Drive & EB Highland Road

Movement	
Directions Served	
Maximum Queue (ft)	
Average Queue (ft)	
95th Queue (ft)	
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 60: Bogie Lake Road & E. Site Drive

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)
Zone Summary

Zone wide Queuing Penalty: 184

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Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations		<u>††</u>			۲.			
Traffic Volume (vph)	0	1603	0	0	135	0		
Future Volume (vph)	0	1603	0	0	135	0		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)		6.1			5.9			
Lane Util. Factor		0.95			1.00			
Frt		1.00			1.00			
Flt Protected		1.00			0.95			
Satd. Flow (prot)		3471			1736			
Flt Permitted		1.00			0.95			
Satd. Flow (perm)		3471			1736			
Peak-hour factor, PHF	0.91	0.91	0.92	0.92	0.61	0.61		
Adj. Flow (vph)	0	1762	0	0	221	0		
RTOR Reduction (vph)	0	0	0	0	0	0		
Lane Group Flow (vph)	0	1762	0	0	221	0		
Heavy Vehicles (%)	4%	4%	2%	2%	4%	4%		
Turn Type		NA			Prot			
Protected Phases		2!			4 2!			
Permitted Phases								
Actuated Green, G (s)		56.9			90.0			
Effective Green, g (s)		56.9			83.9			
Actuated g/C Ratio		0.63			0.93			
Clearance Time (s)		6.1						
Vehicle Extension (s)		3.0						
Lane Grp Cap (vph)		2194			1618			
v/s Ratio Prot		c0.51			c0.13			
v/s Ratio Perm								
v/c Ratio		0.80			0.14			
Uniform Delay, d1		12.4			0.2			
Progression Factor		1.00			1.00			
Incremental Delay, d2		3.2			0.2			
Delay (s)		15.6			0.4			
Level of Service		В			А			
Approach Delay (s)		15.6	0.0		0.4			
Approach LOS		В	А		А			
Intersection Summary								
HCM 2000 Control Delay			13.9	H	CM 2000	Level of Service	В	
HCM 2000 Volume to Capacity	ratio		0.63					
Actuated Cycle Length (s)			90.0		um of lost		12.0	
Intersection Capacity Utilization			80.7%	IC	U Level o	of Service	D	
Analysis Period (min)			15					
Phase conflict between lane	groups							

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		<u></u>	1					•	11		•	
Traffic Volume (vph)	0	1234	504	0	0	0	0	103	296	0	45	0
Future Volume (vph)	0	1234	504	0	0	0	0	103	296	0	45	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.7	6.7					10.9	10.9		6.9	
Lane Util. Factor		0.95	1.00					1.00	0.88		1.00	
Frt		1.00	0.85					1.00	0.85		1.00	
Flt Protected		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (prot)		3471	1553					1827	2733		1681	
Flt Permitted		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (perm)		3471	1553					1827	2733		1681	
Peak-hour factor, PHF	0.89	0.89	0.89	0.92	0.92	0.92	0.87	0.87	0.87	0.95	0.95	0.95
Adj. Flow (vph)	0	1387	566	0	0	0	0	118	340	0	47	0
RTOR Reduction (vph)	0	0	231	0	0	0	0	0	65	0	0	0
Lane Group Flow (vph)	0	1387	335	0	0	0	0	118	275	0	47	0
Heavy Vehicles (%)	4%	4%	4%	2%	2%	2%	4%	4%	4%	13%	13%	13%
Turn Type		NA	Perm					NA	Perm		NA	
Protected Phases		2	_					4			8	
Permitted Phases			2					10.1	4		00.4	_
Actuated Green, G (s)		53.3	53.3					19.1	19.1		23.1	
Effective Green, g (s)		53.3	53.3					19.1	19.1		23.1	_
Actuated g/C Ratio		0.59	0.59					0.21	0.21		0.26	
Clearance Time (s)		6.7	6.7					10.9	10.9		6.9	
Vehicle Extension (s)		3.0	3.0					3.0	3.0		3.0	
Lane Grp Cap (vph)		2055	919					387	580		431	
v/s Ratio Prot		c0.40	0.00					0.06	-0.40		0.03	
v/s Ratio Perm		0.67	0.22					0.30	c0.10 0.47		0.11	
v/c Ratio Uniform Delay, d1		0.67 12.5	0.36 9.5					29.9	31.0		0.11 25.6	
Progression Factor		0.16	9.5 0.23					29.9	1.00		25.0	
Incremental Delay, d2		1.2	0.23					2.0	2.8		0.00	
Delay (s)		3.2	3.0					31.9	33.8		0.5	
Level of Service		3.2 A	3.0 A					01.9 C	00.0 C		0.5 A	
Approach Delay (s)		3.1	А		0.0			33.3	U		0.5	
Approach LOS		A			A			00.0 C			0.5 A	
Intersection Summary												
HCM 2000 Control Delay			8.7	Н	CM 2000	Level of S	Service		А			
HCM 2000 Volume to Capacity	ratio		0.62									
Actuated Cycle Length (s)			90.0	S	um of los	t time (s)			17.6			
Intersection Capacity Utilization	۱		59.1%			of Service			В			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					^	1		•			•	77
Traffic Volume (vph)	0	0	0	0	1078	44	0	103	0	0	45	69
Future Volume (vph)	0	0	0	0	1078	44	0	103	0	0	45	69
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.7	6.7		6.9			10.9	10.9
Lane Util. Factor					0.95	1.00		1.00			1.00	0.88
Frt					1.00	0.85		1.00			1.00	0.85
Flt Protected					1.00	1.00		1.00			1.00	1.00
Satd. Flow (prot)					3406	1524		1827			1681	2515
Flt Permitted					1.00	1.00		1.00			1.00	1.00
Satd. Flow (perm)					3406	1524		1827			1681	2515
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.87	0.87	0.87	0.95	0.95	0.95
Adj. Flow (vph)	0	0	0	0	1172	48	0	118	0	0	47	73
RTOR Reduction (vph)	0	0	0	0	0	20	0	0	0	0	0	58
Lane Group Flow (vph)	0	0	0	0	1172	28	0	118	0	0	47	15
Heavy Vehicles (%)	2%	2%	2%	6%	6%	6%	4%	4%	4%	13%	13%	13%
Turn Type					NA	Perm		NA			NA	Perm
Protected Phases					6			8			4	
Permitted Phases						6						4
Actuated Green, G (s)					53.3	53.3		23.1			19.1	19.1
Effective Green, g (s)					53.3	53.3		23.1			19.1	19.1
Actuated g/C Ratio					0.59	0.59		0.26			0.21	0.21
Clearance Time (s)					6.7	6.7		6.9			10.9	10.9
Vehicle Extension (s)					3.0	3.0		3.0			3.0	3.0
Lane Grp Cap (vph)					2017	902		468			356	533
v/s Ratio Prot					c0.34			c0.06			0.03	
v/s Ratio Perm						0.02						0.01
v/c Ratio					0.58	0.03		0.25			0.13	0.03
Uniform Delay, d1					11.4	7.6		26.6			28.7	28.1
Progression Factor					0.48	0.47		0.00			1.25	2.15
Incremental Delay, d2					1.1	0.1		1.3			0.8	0.1
Delay (s)					6.6	3.7		1.3			36.7	60.4
Level of Service					А	А		А			D	E
Approach Delay (s)		0.0			6.5			1.3			51.1	
Approach LOS		А			А			А			D	
Intersection Summary												
HCM 2000 Control Delay			9.8	Н	CM 2000	Level of S	Service		Α			
HCM 2000 Volume to Capacit	ty ratio		0.51									
Actuated Cycle Length (s)			90.0		um of losi				17.6			
Intersection Capacity Utilization	on		59.1%	IC	CU Level	of Service			В			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					† †	1		र्भ				1
Traffic Volume (vph)	0	0	0	0	996	7	120	9	0	0	0	6
Future Volume (vph)	0	0	0	0	996	7	120	9	0	0	0	6
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.1	6.1		5.9				5.9
Lane Util. Factor					0.95	1.00		1.00				1.00
Frt					1.00	0.85		1.00				0.86
Flt Protected					1.00	1.00		0.96				1.00
Satd. Flow (prot)					3406	1524		1763				1644
Flt Permitted					1.00	1.00		0.96				1.00
Satd. Flow (perm)					3406	1524		1763				1644
Peak-hour factor, PHF	0.92	0.92	0.92	0.95	0.95	0.95	0.78	0.78	0.78	0.75	0.75	0.75
Adj. Flow (vph)	0	0	0	0	1048	7	154	12	0	0	0	8
RTOR Reduction (vph)	0	0	0	0	0	3	0	93	0	0	0	6
Lane Group Flow (vph)	0	0	0	0	1048	4	0	73	0	0	0	2
Heavy Vehicles (%)	2%	2%	2%	6%	6%	6%	3%	3%	3%	0%	0%	0%
Turn Type					NA	Perm	custom	NA				Perm
Protected Phases					2!			4				
Permitted Phases						2	4 2!					4
Actuated Green, G (s)					56.9	56.9		21.1				21.1
Effective Green, g (s)					56.9	56.9		21.1				21.1
Actuated g/C Ratio					0.63	0.63		0.23				0.23
Clearance Time (s)					6.1	6.1		5.9				5.9
Vehicle Extension (s)					3.0	3.0		3.0				3.0
Lane Grp Cap (vph)					2153	963		413				385
v/s Ratio Prot					c0.31							
v/s Ratio Perm						0.00		0.04				0.00
v/c Ratio					0.49	0.00		0.18				0.00
Uniform Delay, d1					8.8	6.1		27.5				26.4
Progression Factor					1.00	1.00		1.28				1.00
Incremental Delay, d2					0.8	0.0		0.7				0.0
Delay (s)					9.6	6.1		36.0				26.4
Level of Service		0.0			A	А		D			00.4	С
Approach Delay (s)		0.0			9.6			36.0			26.4	
Approach LOS		A			A			D			С	
Intersection Summary												
HCM 2000 Control Delay			13.2	H	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capacity	/ ratio		0.40									
Actuated Cycle Length (s)			90.0		um of los				12.0			
Intersection Capacity Utilization	n		55.4%	IC	U Level	of Servic	е		В			
Analysis Period (min)			15									
Phase conflict between lane	e groups	•										

Movement WBL WBR NBT NBR SBL SBT Lane Configurations ↑ ↑↑ ↑↑ ↑↑ Traffic Volume (vph) 89 0 0 0 25 Ideal Flow (vphpl) 1900 1900 1900 1900 1900 1900 Total Lost time (s) 4.9 5.4
Traffic Volume (vph) 89 0 0 0 25 Future Volume (vph) 1900 1900 1900 1900 Total Lost time (s) 4.9 5.4 Lane Util. Factor 1.00 1.00 Fit 1.00 1.00 Stat. Flow (prot) 1556 3139 Peak-hour factor, PHF 0.82 0.92 0.91 Stat. Flow (prot) 100 0 0 Stat. Flow (prot) 109 0 0 0 Peak-hour factor, PHF 0.82 0.82 0.92 0.81 0.81 Adj. Flow (vph) 109 0 0 0 0 0 RTOR Reduction (vph) 0.9 0 0 0 0 0 Lane Group Flow (vph) 109 0 0 0 0 131 Heavy Vehicles (%) 16% 16% 2% 2% 15% 15% Turn Type Prot NA Protected Phases 4.21 21 21 Permitted Phases 4.21 21 21
Traffic Volume (vph) 89 0 0 0 25 Future Volume (vph) 1900 1900 1900 1900 Total Lost time (s) 4.9 5.4 Lane Util. Factor 1.00 1.00 Fit 1.00 1.00 Stat. Flow (prot) 1556 3139 Peak-hour factor, PHF 0.82 0.92 0.91 Stat. Flow (prot) 100 0 0 Stat. Flow (prot) 109 0 0 0 Peak-hour factor, PHF 0.82 0.82 0.92 0.81 0.81 Adj. Flow (vph) 109 0 0 0 0 1 Heavy Vehicles (%) 16% 16% 2% 2% 15% 1 Tum Type Prot NA Protected Phases 4 2! 2! 2! Peamitted Phases Actuated Green, G (s) 90.0 57.6 5.4 15% 1 Lane Group Flow (vph) 1462 2008 0.64 1 1 Clearance Time (s) 5.4 0.64
Future Volume (vph) 89 0 0 0 0 25 Ideal Flow (vphp) 1900 1900 1900 1900 1900 Total Lost time (s) 4.9 5.4 Lane Util, Factor 1.00 0.95 Frt 1.00 1.00 Statk. Flow (prot) 1556 3139 Fit Permitted 0.95 1.00 Satd. Flow (perm) 1556 3139 Peak-hour factor, PHF 0.82 0.82 0.92 0.81 0.81 Adj. Flow (perm) 109 0 0 0 0 1 Adj. Flow (vph) 109 0 0 0 0 1 Adj. Flow (vph) 109 0 0 0 0 1 Lane Group Flow (vph) 109 0 0 0 0 1 Turn Type Prot NA Protected Phases 4 2! 2! 2! Permitted Phases 4 2! 2! 2! 2! 1 1 Actuated Green, G (s) 90.0 57.6
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Frt 1.00 1.00 FIt Protected 0.95 1.00 Satd. Flow (prot) 1556 3139 FIt Permitted 0.95 1.00 Satd. Flow (perm) 1556 3139 Peak-hour factor, PHF 0.82 0.92 0.92 0.81 0.81 Adj. Flow (vph) 109 0 0 0 31 Peak-hour factor, PHF 0.82 0.82 0.92 0.81 0.81 Adj. Flow (vph) 109 0 0 0 31 RTOR Reduction (vph) 0 0 0 0 31 Heavy Vehicles (%) 16% 16% 2% 2% 15% Turn Type Prot NA Protected Phases 4 2! 2! Permitted Phases 4 2! 2! 2! 2! Permitted Phases 4 57.6 3.0 3.0 Lane Group (s) 84.6 57.6 3.0 3.0 Lane Grop Cap (vph) 1462 2008 v/s Ratio Prot 6.4 <td< td=""></td<>
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Satd. Flow (perm) 1556 3139 Peak-hour factor, PHF 0.82 0.92 0.92 0.81 0.81 Adj. Flow (vph) 109 0 0 0 31 RTOR Reduction (vph) 0 0 0 0 31 RTOR Reduction (vph) 0 0 0 0 31 Heavy Vehicles (%) 16% 16% 2% 15% 15% Turn Type Prot NA Protected Phases 42! 2! 2! Permitted Phases 42! 2! 2! 2! Permitted Phases Actuated Green, G (s) 90.0 57.6 57.6 Effective Green, g (s) 84.6 57.6 Effective Green, g (s) 84.6 57.6 5.4 Vehicle Extension (s) 3.0 Lane Grp Cap (vph) 1462 2008 5.4 Vehicle Extension (s) 3.0 Lane Grp Cap (vph) 1462 2008 5.9 1.00 1.00 Incremental Delay, d1 0.2
Peak-hour factor, PHF 0.82 0.82 0.92 0.81 0.81 Adj. Flow (vph) 109 0 0 0 31 RTOR Reduction (vph) 0 0 0 0 0 Lane Group Flow (vph) 109 0 0 0 0 0 Heavy Vehicles (%) 16% 16% 2% 2% 15% 15% Turn Type Prot NA Protected Phases 4 2! 2! Permitted Phases 4 2! 2! 2! Permitted Phases Actuated Green, G (s) 90.0 57.6 54 2! 2! Permitted Phases 5.4 Vehicle Extension (s) 3.0 1.04 Clearance Time (s) 5.4 2008 v/s Ratio Prot c0.07 0.01 v/s Ratio Prot c0.07 0.01 v/s Ratio Prot c0.07 0.02 Uniform Delay, d1 0.2 5.9 5.9 5.9 5.9 Progression Factor
Adj. Flow (vph) 109 0 0 0 31 RTOR Reduction (vph) 0 0 0 0 0 Lane Group Flow (vph) 109 0 0 0 31 Heavy Vehicles (%) 16% 16% 2% 2% 15% Turn Type Prot NA Protected Phases 4 2! 2! Permitted Phases
RTOR Reduction (vph) 0 0 0 0 0 0 0 10 10 0 0 0 10 0 0 0 10 0
RTOR Reduction (vph) 0 0 0 0 0 0 0 10 109 0 0 0 31 Heavy Vehicles (%) 16% 16% 2% 2% 15% 15% Turn Type Prot NA Protected Phases 42! 2! 2! Permitted Phases
Lane Group Flow (vph) 109 0 0 0 31 Heavy Vehicles (%) 16% 16% 2% 2% 15% Turn Type Prot NA Protected Phases 4 2! 2! Permitted Phases 57.6 Actuated Green, G (s) 90.0 57.6 Effective Green, g (s) 84.6 57.6 Actuated g/C Ratio 0.94 0.64 Clearance Time (s) 5.4 Vehicle Extension (s) 3.0 Lane Grp Cap (vph) 1462 2008 v/s Ratio Perm
Heavy Vehicles (%) 16% 16% 2% 2% 15% Turn Type Prot NA Protected Phases 4 2! 2! Permitted Phases 2 2! Actuated Green, G (s) 90.0 57.6 Effective Green, g (s) 84.6 57.6 Actuated g/C Ratio 0.94 0.64 Clearance Time (s) 5.4 Vehicle Extension (s) 3.0 Lane Grp Cap (vph) 1462 2008 v/s Ratio Prot c0.07 0.01 v/s Ratio Prot c0.07 0.01 v/c Ratio 0.07 0.02 Uniform Delay, d1 0.2 5.9 Progression Factor 1.00 1.00 Incremental Delay, d2 0.1 0.0 Delay (s) 0.3 5.9 Level of Service A A Approach Delay (s) 0.3 0.0 Approach LOS A A
Turn Type Prot NA Protected Phases 4 2! 2! Permitted Phases
Protected Phases 4 2! 2! Permitted Phases Actuated Green, G (s) 90.0 57.6 Actuated Green, g (s) 84.6 57.6 Actuated g/C Ratio 0.94 0.64 Clearance Time (s) 5.4 Vehicle Extension (s) 3.0 Lane Grp Cap (vph) 1462 2008 v/s Ratio Prot c0.07 0.01 v/s Ratio Prot c0.07 0.01 v/s Ratio Perm
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Clearance Time (s) 5.4 Vehicle Extension (s) 3.0 Lane Grp Cap (vph) 1462 2008 v/s Ratio Prot c0.07 0.01 v/s Ratio Perm
Lane Grp Cap (vph) 1462 2008 v/s Ratio Prot c0.07 0.01 v/s Ratio Perm v/c Ratio 0.07 0.02 Uniform Delay, d1 0.2 5.9 Progression Factor 1.00 1.00 Incremental Delay, d2 0.1 0.0 Delay (s) 0.3 5.9 Level of Service A A Approach Delay (s) 0.3 0.0 Approach LOS A A
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v/s Ratio Protc0.070.01v/s Ratio Perm0.070.02v/c Ratio0.070.02Uniform Delay, d10.25.9Progression Factor1.001.00Incremental Delay, d20.10.0Delay (s)0.35.9Level of ServiceAAApproach Delay (s)0.30.0Approach LOSAA
v/c Ratio0.070.02Uniform Delay, d10.25.9Progression Factor1.001.00Incremental Delay, d20.10.0Delay (s)0.35.9Level of ServiceAAApproach Delay (s)0.30.0Approach LOSAA
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Level of ServiceAAApproach Delay (s)0.30.05.9Approach LOSAAA
Approach LOS A A A A
Intersection Summary
HCM 2000 Control Delay 1.5 HCM 2000 Level of Service A
HCM 2000 Volume to Capacity ratio 0.08
Actuated Cycle Length (s)90.0Sum of lost time (s)10.3
Intersection Capacity Utilization 25.3% ICU Level of Service A
Analysis Period (min) 15
Phase conflict between lane groups.

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Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations		<u></u>			<u>۲</u>			
Traffic Volume (vph)	0	1421	0	0	214	0		
Future Volume (vph)	0	1421	0	0	214	0		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)		6.1			5.9			
Lane Util. Factor		0.95			1.00			
Frt		1.00			1.00			
Flt Protected		1.00			0.95			
Satd. Flow (prot)		3471			1787			
Flt Permitted		1.00			0.95			
Satd. Flow (perm)		3471			1787			
Peak-hour factor, PHF	0.94	0.94	0.92	0.92	0.88	0.88		
Adj. Flow (vph)	0.01	1512	0.02	0	243	0		
RTOR Reduction (vph)	Ũ	0	0	0	0	0		
Lane Group Flow (vph)	0	1512	0	0	243	0		
Heavy Vehicles (%)	4%	4%	2%	2%	1%	1%		
Turn Type		NA	_/*		Prot			
Protected Phases		2!			4 2!			
Permitted Phases		2.			1 21			
Actuated Green, G (s)		85.9			120.0			
Effective Green, g (s)		85.9			113.9			
Actuated g/C Ratio		0.72			0.95			
Clearance Time (s)		6.1			0.00			
Vehicle Extension (s)		3.0						
Lane Grp Cap (vph)		2484			1696			
v/s Ratio Prot		c0.44			c0.14			
v/s Ratio Perm		60.44			CO. 14			
v/c Ratio		0.61			0.14			
Uniform Delay, d1		8.6			0.14			
Progression Factor		1.00			1.00			
Incremental Delay, d2		1.1			0.1			
Delay (s)		9.7			0.1			
Level of Service		9.7 A			0.5 A			
Approach Delay (s)		9.7	0.0		0.3			
Approach LOS		9.7 A	A		0.5 A			
Intersection Summary								
HCM 2000 Control Delay			8.4	Н	CM 2000	Level of Service	А	
HCM 2000 Volume to Capacity	ratio		0.52					
Actuated Cycle Length (s)			120.0	S	um of lost	time (s)	12.0	
Intersection Capacity Utilization	1		96.2%			of Service	F	
Analysis Period (min)			15					
Phase conflict between lane	aroups							
	groupo	•						

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		<u></u>	1					†	77		•	
Traffic Volume (vph)	0	1301	334	0	0	0	0	188	348	0	66	0
Future Volume (vph)	0	1301	334	0	0	0	0	188	348	0	66	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.7	6.7					10.9	10.9		6.9	
Lane Util. Factor		0.95	1.00					1.00	0.88		1.00	
Frt		1.00	0.85					1.00	0.85		1.00	
Flt Protected		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (prot)		3505	1568					1863	2787		1827	
Flt Permitted		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (perm)		3505	1568					1863	2787		1827	
Peak-hour factor, PHF	0.95	0.95	0.95	0.92	0.92	0.92	0.93	0.93	0.93	0.92	0.92	0.92
Adj. Flow (vph)	0	1369	352	0	0	0	0	202	374	0	72	0
RTOR Reduction (vph)	0	0	108	0	0	0	0	0	117	0	0	0
Lane Group Flow (vph)	0	1369	244	0	0	0	0	202	257	0	72	0
Heavy Vehicles (%)	3%	3%	3%	2%	2%	2%	2%	2%	2%	4%	4%	4%
Turn Type		NA	Perm					NA	Perm		NA	
Protected Phases		2						4			8	
Permitted Phases			2						4			
Actuated Green, G (s)		83.3	83.3					19.1	19.1		23.1	
Effective Green, g (s)		83.3	83.3					19.1	19.1		23.1	
Actuated g/C Ratio		0.69	0.69					0.16	0.16		0.19	
Clearance Time (s)		6.7	6.7					10.9	10.9		6.9	
Vehicle Extension (s)		3.0	3.0					3.0	3.0		3.0	
Lane Grp Cap (vph)		2433	1088					296	443		351	
v/s Ratio Prot		c0.39						c0.11			0.04	
v/s Ratio Perm			0.16						0.09			
v/c Ratio		0.56	0.22					0.68	0.58		0.21	
Uniform Delay, d1		9.2	6.6					47.6	46.7		40.7	
Progression Factor		0.23	0.23					1.00	1.00		0.00	
Incremental Delay, d2		0.8	0.4					12.1	5.5		1.3	
Delay (s)		2.9	2.0					59.6	52.2		1.3	
Level of Service		A	A		0.0			E	D		A	_
Approach Delay (s)		2.7			0.0			54.8			1.3	
Approach LOS		A			A			D			A	
Intersection Summary												
HCM 2000 Control Delay			15.3	Н	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capacit	y ratio		0.58									
Actuated Cycle Length (s)			120.0		um of lost				17.6			_
Intersection Capacity Utilizatio	n		71.7%	IC	CU Level o	of Service	1		С			
Analysis Period (min)			15									_
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					- ††	1		↑			↑	11
Traffic Volume (vph)	0	0	0	0	1825	111	0	188	0	0	66	144
Future Volume (vph)	0	0	0	0	1825	111	0	188	0	0	66	144
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.7	6.7		6.9			10.9	10.9
Lane Util. Factor					0.95	1.00		1.00			1.00	0.88
Frpb, ped/bikes					1.00	0.99		1.00			1.00	0.98
Flpb, ped/bikes					1.00	1.00		1.00			1.00	1.00
Frt					1.00	0.85		1.00			1.00	0.85
Flt Protected					1.00	1.00		1.00			1.00	1.00
Satd. Flow (prot)					3539	1562		1863			1827	2670
Flt Permitted					1.00	1.00		1.00			1.00	1.00
Satd. Flow (perm)					3539	1562		1863			1827	2670
Peak-hour factor, PHF	0.92	0.92	0.92	0.90	0.90	0.90	0.93	0.93	0.93	0.92	0.92	0.92
Adj. Flow (vph)	0	0	0	0	2028	123	0	202	0	0	72	157
RTOR Reduction (vph)	0	0	0	0	0	38	0	0	0	0	0	30
Lane Group Flow (vph)	0	0	0	0	2028	85	0	202	0	0	72	127
Confl. Peds. (#/hr)						3						1
Heavy Vehicles (%)	2%	2%	2%	2%	2%	2%	2%	2%	2%	4%	4%	4%
Turn Type					NA	Perm		NA			NA	Perm
Protected Phases					6			8			4	
Permitted Phases						6						4
Actuated Green, G (s)					83.3	83.3		23.1			19.1	19.1
Effective Green, g (s)					83.3	83.3		23.1			19.1	19.1
Actuated g/C Ratio					0.69	0.69		0.19			0.16	0.16
Clearance Time (s)					6.7	6.7		6.9			10.9	10.9
Vehicle Extension (s)					3.0	3.0		3.0			3.0	3.0
Lane Grp Cap (vph)					2456	1084		358			290	424
v/s Ratio Prot					c0.57	1001		c0.11			0.04	
v/s Ratio Perm					00.01	0.05		00.111			0.01	0.05
v/c Ratio					0.83	0.08		0.56			0.25	0.30
Uniform Delay, d1					13.1	5.9		43.9			44.2	44.5
Progression Factor					0.91	0.33		0.00			1.34	1.44
Incremental Delay, d2					2.4	0.1		4.6			2.0	1.8
Delay (s)					14.4	2.0		4.7			61.0	66.1
Level of Service					В	Α		A			E	E
Approach Delay (s)		0.0			13.7	7.		4.7			64.5	_
Approach LOS		A			B			A			64.0 E	
Intersection Summary		,,									_	
HCM 2000 Control Delay			17.5		CM 2000	Level of S	Service		B			
HCM 2000 Volume to Capacity	v ratio		0.80	П		Level UI			D			
Actuated Cycle Length (s)	y Taulo		120.0	C	um of losi	t time (c)			17.6			
Intersection Capacity Utilizatio	n		71.7%			of Service			17.0 C			
Analysis Period (min)	11		15	iC.					U			
C Critical Lane Group			10									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					<u></u>	1		र्स				1
Traffic Volume (vph)	0	0	0	0	1671	38	205	34	0	0	0	60
Future Volume (vph)	0	0	0	0	1671	38	205	34	0	0	0	60
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.1	6.1		5.9				5.9
Lane Util. Factor					0.95	1.00		1.00				1.00
Frpb, ped/bikes					1.00	0.98		1.00				1.00
Flpb, ped/bikes					1.00	1.00		1.00				1.00
Frt					1.00	0.85		1.00				0.86
Flt Protected					1.00	1.00		0.96				1.00
Satd. Flow (prot)					3505	1536		1822				1644
Flt Permitted					1.00	1.00		0.96				1.00
Satd. Flow (perm)					3505	1536		1822				1644
Peak-hour factor, PHF	0.92	0.92	0.92	0.95	0.95	0.95	0.79	0.79	0.79	0.74	0.74	0.74
Adj. Flow (vph)	0	0	0	0	1759	40	259	43	0	0	0	81
RTOR Reduction (vph)	0	0	0	0	0	7	0	33	0	0	0	33
Lane Group Flow (vph)	0	0	0	0	1759	33	0	269	0	0	0	48
Confl. Peds. (#/hr)	•	•	•	•		1	Ţ		•	•	•	
Heavy Vehicles (%)	2%	2%	2%	3%	3%	3%	0%	0%	0%	0%	0%	0%
Turn Type			_//	•,•	NA	Perm	custom	NA		• / •	• , •	Perm
Protected Phases					2!	1 Chin	Custom	4				1 Chin
Permitted Phases					۷.	2	4 2!	Ŧ				4
Actuated Green, G (s)					85.9	85.9	7 2:	22.1				22.1
Effective Green, g (s)					85.9	85.9		22.1				22.1
Actuated g/C Ratio					0.72	0.72		0.18				0.18
Clearance Time (s)					6.1	6.1		5.9				5.9
Vehicle Extension (s)					3.0	3.0		3.0				3.0
Lane Grp Cap (vph)					2508	1099		335				302
v/s Ratio Prot					c0.50	1099		335				JUZ
v/s Ratio Perm					0.50	0.02		0.15				0.03
v/c Ratio					0.70	0.02		0.15				0.05
Uniform Delay, d1					9.7	5.0		46.9				41.1
Progression Factor					9.7	1.00		40.9				1.00
Incremental Delay, d2					1.00	0.1		15.7				1.1
Delay (s)					11.4	5.0		65.7				42.3
Level of Service					н.4 В	5.0 A		05.7 E				42.3 D
		0.0			11.3	A		⊑ 65.7			42.3	U
Approach Delay (s)		0.0 A						05.7 E			42.3 D	
Approach LOS		A			В			E			U	
Intersection Summary												
HCM 2000 Control Delay			19.9	Н	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capaci	ty ratio		0.72									
Actuated Cycle Length (s)	,		120.0	S	um of lost	t time (s)			12.0			
Intersection Capacity Utilization	on		80.1%		U Level o				D			
Analysis Period (min)			15									
! Phase conflict between lar	ne groups											
c Critical Lane Group												

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Movement	WBL	WBR	NBT	NBR	SBL	SBT			
Lane Configurations	۲					<u>††</u>			
Traffic Volume (vph)	187	0	0	0	0	23			
Future Volume (vph)	187	0	0	0	0	23			
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900			
Total Lost time (s)	4.9					5.4			
Lane Util. Factor	1.00					0.95			
Frt	1.00					1.00			
Flt Protected	0.95					1.00			
Satd. Flow (prot)	1752					3610			
Flt Permitted	0.95					1.00			
Satd. Flow (perm)	1752					3610			
Peak-hour factor, PHF	0.86	0.86	0.92	0.92	0.60	0.60			
Adj. Flow (vph)	217	0	0	0	0	38			
RTOR Reduction (vph)	0	0	0	0	0	0			
Lane Group Flow (vph)	217	0	0	0	0	38			
Heavy Vehicles (%)	3%	3%	2%	2%	0%	0%			
Turn Type	Prot					NA			
Protected Phases	4 2!					2!			
Permitted Phases									
Actuated Green, G (s)	120.0					86.6			
Effective Green, g (s)	114.6					86.6			
Actuated g/C Ratio	0.95					0.72			
Clearance Time (s)						5.4			
Vehicle Extension (s)						3.0			
Lane Grp Cap (vph)	1673					2605			
v/s Ratio Prot	c0.12					0.01			
v/s Ratio Perm									
v/c Ratio	0.13					0.01			
Uniform Delay, d1	0.1					4.7			
Progression Factor	1.00					1.00			
Incremental Delay, d2	0.2					0.0			
Delay (s)	0.3					4.7			
Level of Service	А					А			
Approach Delay (s)	0.3		0.0			4.7			
Approach LOS	А		А			А			
Intersection Summary									
HCM 2000 Control Delay			0.9	H	CM 2000	Level of Servic	e	А	
HCM 2000 Volume to Cap	acity ratio		0.14						
Actuated Cycle Length (s)			120.0	Sı	um of lost	t time (s)	1	0.3	
Intersection Capacity Utiliz			30.7%			of Service		А	
Analysis Period (min)			15						
! Phase conflict between	lane groups								
a Critical Lana Croup									

Intersection: 10: EB Highland Road & WB-to-EB X/O

Movement	EB	EB	SB
Directions Served	Т	Т	L
Maximum Queue (ft)	285	308	55
Average Queue (ft)	147	157	36
95th Queue (ft)	240	263	65
Link Distance (ft)	708	708	35
Upstream Blk Time (%)			12
Queuing Penalty (veh)			19
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 11: WB-to-EB X/O & WB Highland Road

Movement	WB
Directions Served	1
	100
Maximum Queue (ft)	108
Average Queue (ft)	15
95th Queue (ft)	59
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	325
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 20: Bogie Lake Road & EB Highland Road

Movement	EB	EB	EB	NB	NB	NB
Directions Served	Т	Т	R	Т	R	R
Maximum Queue (ft)	99	112	110	126	111	119
Average Queue (ft)	35	41	46	55	60	48
95th Queue (ft)	80	91	86	107	101	92
Link Distance (ft)	330	330	330	291	291	291
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)						
Storage Blk Time (%)						
Queuing Penalty (veh)						

Intersection: 21: Bogie Lake Road & WB Highland Road

Movement	WB	WB	WB	SB	SB	SB
Directions Served	Т	Т	R	Т	R	R
Maximum Queue (ft)	82	68	38	100	61	50
Average Queue (ft)	28	23	4	34	24	16
95th Queue (ft)	64	57	22	82	51	41
Link Distance (ft)	477	477	477	152	152	152
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)						
Storage Blk Time (%)						
Queuing Penalty (veh)						

Intersection: 30: EB-to-WB X/O/Nordic Drive & WB Highland Road

Movement	WB	WB	WB	NB	SB
Directions Served	Т	Т	R	LT	R
Maximum Queue (ft)	207	162	16	61	30
Average Queue (ft)	113	70	1	35	4
95th Queue (ft)	187	141	9	59	21
Link Distance (ft)	905	905		11	94
Upstream Blk Time (%)				16	
Queuing Penalty (veh)				21	
Storage Bay Dist (ft)			50		
Storage Blk Time (%)		9			
Queuing Penalty (veh)		1			

Intersection: 31: EB Highland Road & EB-to-WB X/O

Movement	EB
Directions Served	L
Maximum Queue (ft)	66
Average Queue (ft)	19
95th Queue (ft)	55
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	300
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 40: Bogie Lake Road & NB-to-SB X/O

Movement	WB	SB
Directions Served	L	Т
Maximum Queue (ft)	16	44
Average Queue (ft)	1	8
95th Queue (ft)	7	32
Link Distance (ft)	28	192
Upstream Blk Time (%)	0	
Queuing Penalty (veh)	0	
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 41: Bogie Lake Road & NB-to-SB X/O

Movement	NB
Directions Served	L
Maximum Queue (ft)	6
Average Queue (ft)	0
95th Queue (ft)	3
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	300
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 50: W. Site Drive & EB Highland Road

Movement		
Directions Served		
Maximum Queue (ft)		
Average Queue (ft)		
95th Queue (ft)		
Link Distance (ft)		
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 60: Bogie Lake Road & E. Site Drive

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)
Zone Summary

Zone wide Queuing Penalty: 41

Intersection: 10: EB Highland Road & WB-to-EB X/O

Movement	EB	EB	SB
Directions Served	Т	Т	L
Maximum Queue (ft)	269	252	60
Average Queue (ft)	153	125	45
95th Queue (ft)	238	216	65
Link Distance (ft)	708	708	35
Upstream Blk Time (%)			23
Queuing Penalty (veh)			49
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 11: WB-to-EB X/O & WB Highland Road

Movement	WB
Directions Served	L
Maximum Queue (ft)	135
Average Queue (ft)	32
95th Queue (ft)	91
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	325
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 20: Bogie Lake Road & EB Highland Road

Movement	EB	EB	EB	NB	NB	NB
Directions Served	Т	Т	R	Т	R	R
Maximum Queue (ft)	98	113	61	243	155	140
Average Queue (ft)	39	45	22	138	79	62
95th Queue (ft)	81	95	52	221	127	110
Link Distance (ft)	330	330	330	291	291	291
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)						
Storage Blk Time (%)						
Queuing Penalty (veh)						

Intersection: 21: Bogie Lake Road & WB Highland Road

Movement	WB	WB	WB	NB	SB	SB	SB
Directions Served	T	T	R	T	T	 R	 R
Maximum Queue (ft)	200	189	59	17	133	118	116
Average Queue (ft)	69	78	11	1	61	51	49
95th Queue (ft)	146	152	39	9	114	93	94
Link Distance (ft)	477	477	477	37	152	152	152
Upstream Blk Time (%)				1	0	0	0
Queuing Penalty (veh)				2	0	0	0
Storage Bay Dist (ft)							
Storage Blk Time (%)							
Queuing Penalty (veh)							

Intersection: 30: EB-to-WB X/O/Nordic Drive & WB Highland Road

	14/5	14/5			0.5
Movement	WB	WB	WB	NB	SB
Directions Served	Т	Т	R	LT	R
Maximum Queue (ft)	316	285	101	48	88
Average Queue (ft)	169	130	9	47	32
95th Queue (ft)	258	232	58	56	67
Link Distance (ft)	905	905		11	94
Upstream Blk Time (%)				54	0
Queuing Penalty (veh)				131	0
Storage Bay Dist (ft)			50		
Storage Blk Time (%)		14	0		
Queuing Penalty (veh)		5	0		
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Intersection: 31: EB Highland Road & EB-to-WB X/O

Movement	EB	ED
Movement	ED	EB
Directions Served	L	Т
Maximum Queue (ft)	324	198
Average Queue (ft)	121	4
95th Queue (ft)	240	65
Link Distance (ft)		518
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)	300	
Storage Blk Time (%)	1	
Queuing Penalty (veh)	9	

Intersection: 40: Bogie Lake Road & NB-to-SB X/O

Movement	WB	SB	SB
Directions Served	L	Т	Т
Maximum Queue (ft)	31	49	6
Average Queue (ft)	2	7	0
95th Queue (ft)	15	30	6
Link Distance (ft)	28	192	192
Upstream Blk Time (%)	0		
Queuing Penalty (veh)	0		
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 41: Bogie Lake Road & NB-to-SB X/O

Movement	NB
Directions Served	L
Maximum Queue (ft)	12
Average Queue (ft)	1
95th Queue (ft)	8
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	300
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 50: W. Site Drive & EB Highland Road

Movement	EB
Directions Served	TR
Maximum Queue (ft)	9
Average Queue (ft)	0
95th Queue (ft)	7
Link Distance (ft)	348
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 60: Bogie Lake Road & E. Site Drive

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)
Zone Summary

Zone wide Queuing Penalty: 198

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Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations		<u>††</u>			ľ			
Traffic Volume (vph)	0	1633	0	0	167	0		
Future Volume (vph)	0	1633	0	0	167	0		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)		6.1			5.9			
Lane Util. Factor		0.95			1.00			
Frt		1.00			1.00			
Flt Protected		1.00			0.95			
Satd. Flow (prot)		3471			1736			
Flt Permitted		1.00			0.95			
Satd. Flow (perm)		3471			1736			
Peak-hour factor, PHF	0.91	0.91	0.92	0.92	0.61	0.61		
Adj. Flow (vph)	0	1795	0	0	274	0		
RTOR Reduction (vph)	0	0	0	0	0	0		
Lane Group Flow (vph)	0	1795	0	0	274	0		
Heavy Vehicles (%)	4%	4%	2%	2%	4%	4%		
Turn Type		NA			Prot			
Protected Phases		2!			4 2!			
Permitted Phases								
Actuated Green, G (s)		56.9			90.0			
Effective Green, g (s)		56.9			83.9			
Actuated g/C Ratio		0.63			0.93			
Clearance Time (s)		6.1						
Vehicle Extension (s)		3.0						
Lane Grp Cap (vph)		2194			1618			
v/s Ratio Prot		c0.52			c0.16			
v/s Ratio Perm								
v/c Ratio		0.82			0.17			
Uniform Delay, d1		12.6			0.2			
Progression Factor		1.00			1.00			
Incremental Delay, d2		3.5			0.2			
Delay (s)		16.1			0.5			
Level of Service		В			А			
Approach Delay (s)		16.1	0.0		0.5			
Approach LOS		В	А		А			
Intersection Summary								
HCM 2000 Control Delay			14.1	H	CM 2000	Level of Service	В	
HCM 2000 Volume to Capacity	ratio		0.65					
Actuated Cycle Length (s)			90.0		um of lost		12.0	
Intersection Capacity Utilization	ı		82.3%	IC	U Level o	of Service	E	
Analysis Period (min)			15					
! Phase conflict between lane	groups							
 Oritical Lana Oracin 								

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		<u>††</u>	1					•	11		•	
Traffic Volume (vph)	0	1292	504	0	0	0	0	103	296	0	45	0
Future Volume (vph)	0	1292	504	0	0	0	0	103	296	0	45	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.7	6.7					10.9	10.9		6.9	
Lane Util. Factor		0.95	1.00					1.00	0.88		1.00	
Frt		1.00	0.85					1.00	0.85		1.00	
Flt Protected		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (prot)		3471	1553					1827	2733		1681	
Flt Permitted		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (perm)		3471	1553					1827	2733		1681	
Peak-hour factor, PHF	0.89	0.89	0.89	0.92	0.92	0.92	0.87	0.87	0.87	0.95	0.95	0.95
Adj. Flow (vph)	0	1452	566	0	0	0	0	118	340	0	47	0
RTOR Reduction (vph)	0	0	231	0	0	0	0	0	56	0	0	0
Lane Group Flow (vph)	0	1452	335	0	0	0	0	118	284	0	47	0
Heavy Vehicles (%)	4%	4%	4%	2%	2%	2%	4%	4%	4%	13%	13%	13%
Turn Type		NA	Perm					NA	Perm		NA	
Protected Phases		2						4			8	
Permitted Phases			2						4			
Actuated Green, G (s)		53.3	53.3					19.1	19.1		23.1	
Effective Green, g (s)		53.3	53.3					19.1	19.1		23.1	
Actuated g/C Ratio		0.59	0.59					0.21	0.21		0.26	
Clearance Time (s)		6.7	6.7					10.9	10.9		6.9	_
Vehicle Extension (s)		3.0	3.0					3.0	3.0		3.0	
Lane Grp Cap (vph)		2055	919					387	580		431	_
v/s Ratio Prot		c0.42	0.00					0.06	0.40		0.03	
v/s Ratio Perm		0.74	0.22					0.00	c0.10		0.44	_
v/c Ratio		0.71	0.36					0.30	0.49		0.11	
Uniform Delay, d1		12.9	9.5					29.9	31.2		25.6	
Progression Factor		0.20	0.18					1.00	1.00		0.00	
Incremental Delay, d2		1.5	0.8					2.0	2.9		0.5	
Delay (s) Level of Service		4.1 A	2.5					31.9 C	34.1 C		0.5	
Approach Delay (s)		3.7	А		0.0			33.5	U		A 0.5	
Approach LOS		3.7 A			0.0 A			33.5 C			0.5 A	
		A			~			0			A	
Intersection Summary			9.0		CM 2000	Level of S	Convioo		A			
HCM 2000 Control Delay HCM 2000 Volume to Capacity	ratio		9.0 0.65	п		Level of	Service		A			
Actuated Cycle Length (s)	Tallo		90.0	c	um of loo	t time (a)			17.6			
Intersection Capacity Utilization			90.0 60.7%		um of lost	of Service			17.0 B			
Analysis Period (min)			15						D			
c Critical Lane Group			10									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					<u></u>	1		•			↑	77
Traffic Volume (vph)	0	0	0	0	1138	44	0	103	0	0	45	69
Future Volume (vph)	0	0	0	0	1138	44	0	103	0	0	45	69
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.7	6.7		6.9			10.9	10.9
Lane Util. Factor					0.95	1.00		1.00			1.00	0.88
Frt					1.00	0.85		1.00			1.00	0.85
Flt Protected					1.00	1.00		1.00			1.00	1.00
Satd. Flow (prot)					3406	1524		1827			1681	2515
Flt Permitted					1.00	1.00		1.00			1.00	1.00
Satd. Flow (perm)					3406	1524		1827			1681	2515
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.87	0.87	0.87	0.95	0.95	0.95
Adj. Flow (vph)	0	0	0	0	1237	48	0	118	0	0	47	73
RTOR Reduction (vph)	0	0	0	0	0	20	0	0	0	0	0	58
Lane Group Flow (vph)	0	0	0	0	1237	28	0	118	0	0	47	15
Heavy Vehicles (%)	2%	2%	2%	6%	6%	6%	4%	4%	4%	13%	13%	13%
Turn Type					NA	Perm		NA			NA	Perm
Protected Phases					6			8			4	
Permitted Phases						6		00.4			40.4	4
Actuated Green, G (s)					53.3	53.3		23.1			19.1	19.1
Effective Green, g (s)					53.3	53.3		23.1			19.1	19.1
Actuated g/C Ratio					0.59	0.59		0.26			0.21	0.21
Clearance Time (s)					6.7	6.7		6.9			10.9	10.9
Vehicle Extension (s)					3.0	3.0		3.0			3.0	3.0
Lane Grp Cap (vph)					2017	902		468			356	533
v/s Ratio Prot					c0.36	0.00		c0.06			0.03	0.04
v/s Ratio Perm					0.04	0.02		0.05			0.40	0.01
v/c Ratio					0.61	0.03		0.25			0.13	0.03
Uniform Delay, d1					11.8	7.6		26.6			28.7	28.1
Progression Factor					0.60	0.42		0.00 1.3			1.24	2.16
Incremental Delay, d2					1.3 8.3	0.1 3.3		1.3			0.8 36.4	0.1 60.7
Delay (s) Level of Service					0.3 A	3.3 A		1.5 A			30.4 D	60.7 E
Approach Delay (s)		0.0			8.1	A		1.3			51.2	E
Approach LOS		0.0 A			0.1 A			1.5 A			51.Z D	
Intersection Summary											_	
HCM 2000 Control Delay			11.0	Н	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capacit	v ratio		0.53		2000				D			
Actuated Cycle Length (s)	., 1010		90.0	S	um of losi	t time (s)			17.6			
Intersection Capacity Utilization	n		60.7%			of Service			В			
Analysis Period (min)			15						U			
c Critical Lane Group			10									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					<u></u>	1		र्च				1
Traffic Volume (vph)	0	0	0	0	1015	7	161	9	0	0	0	6
Future Volume (vph)	0	0	0	0	1015	7	161	9	0	0	0	6
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.1	6.1		5.9				5.9
Lane Util. Factor					0.95	1.00		1.00				1.00
Frt					1.00	0.85		1.00				0.86
Flt Protected					1.00	1.00		0.95				1.00
Satd. Flow (prot)					3406	1524		1761				1644
Flt Permitted					1.00	1.00		0.95				1.00
Satd. Flow (perm)					3406	1524		1761				1644
Peak-hour factor, PHF	0.92	0.92	0.92	0.95	0.95	0.95	0.78	0.78	0.78	0.75	0.75	0.75
Adj. Flow (vph)	0	0	0	0	1068	7	206	12	0	0	0	8
RTOR Reduction (vph)	0	0	0	0	0	3	0	90	0	0	0	6
Lane Group Flow (vph)	0	0	0	0	1068	4	0	128	0	0	0	2
Heavy Vehicles (%)	2%	2%	2%	6%	6%	6%	3%	3%	3%	0%	0%	0%
Turn Type					NA	Perm	custom	NA				Perm
Protected Phases					2!	_		4				
Permitted Phases						2	4 2!					4
Actuated Green, G (s)					56.9	56.9		21.1				21.1
Effective Green, g (s)					56.9	56.9		21.1				21.1
Actuated g/C Ratio					0.63	0.63		0.23				0.23
Clearance Time (s)					6.1	6.1		5.9				5.9
Vehicle Extension (s)					3.0	3.0		3.0				3.0
Lane Grp Cap (vph)					2153	963		412				385
v/s Ratio Prot					c0.31							
v/s Ratio Perm					0 - 0	0.00		0.07				0.00
v/c Ratio					0.50	0.00		0.31				0.00
Uniform Delay, d1					8.9	6.1		28.5				26.4
Progression Factor					1.00	1.00		1.10				1.00
Incremental Delay, d2					0.8	0.0		1.4				0.0
Delay (s) Level of Service					9.7	6.1		32.6 C				26.4
		0.0			A 9.7	A		32.6			26.4	С
Approach Delay (s) Approach LOS		0.0 A			9.7 A			32.0 C			20.4 C	
Intersection Summary								0			0	
HCM 2000 Control Delay			13.6	Н	CM 2000		Service		В			
HCM 2000 Volume to Capacit	v ratio		0.45	11	0101 2000	Level O	OCIVICE		D			
Actuated Cycle Length (s)	yrallo		90.0	S	um of losi	time (s)			12.0			
Intersection Capacity Utilization	n		58.2%		CU Level				12.0 B			
Analysis Period (min)			15				•		U			
Phase conflict between lan	e arouns		10									
	is groups	•										

	4	*	1	۲	5	Ļ		
Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	<u> </u>					<u></u>		
Traffic Volume (vph)	89	0	0	0	0	25		
Future Volume (vph)	89	0	0	0	0	25		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)	4.9					5.4		
Lane Util. Factor	1.00					0.95		
Frt	1.00					1.00		
Flt Protected	0.95					1.00		
Satd. Flow (prot)	1556					3139		
Flt Permitted	0.95					1.00		
Satd. Flow (perm)	1556					3139		
Peak-hour factor, PHF	0.82	0.82	0.92	0.92	0.81	0.81		
Adj. Flow (vph)	109	0	0	0	0	31		
RTOR Reduction (vph)	0	0	0	0	0	0		
Lane Group Flow (vph)	109	0	0	0	0	31		
Heavy Vehicles (%)	16%	16%	2%	2%	15%	15%		
Turn Type	Prot					NA		
Protected Phases	4 2!					2!		
Permitted Phases								
Actuated Green, G (s)	90.0					57.6		
Effective Green, g (s)	84.6					57.6		
Actuated g/C Ratio	0.94					0.64		
Clearance Time (s)						5.4		
Vehicle Extension (s)						3.0		
Lane Grp Cap (vph)	1462					2008		
v/s Ratio Prot	c0.07					0.01		
v/s Ratio Perm								
v/c Ratio	0.07					0.02		
Uniform Delay, d1	0.2					5.9		
Progression Factor	1.00					1.00		
Incremental Delay, d2	0.1					0.0		
Delay (s)	0.3					5.9		
Level of Service	А					А		
Approach Delay (s)	0.3		0.0			5.9		
Approach LOS	А		А			А		
Intersection Summary								
HCM 2000 Control Delay			1.5	H	CM 2000	Level of Servic	e A	
HCM 2000 Volume to Capa	acity ratio		0.08					
Actuated Cycle Length (s)	-		90.0	Si	um of lost	t time (s)	10.3	
Intersection Capacity Utiliza	ation		25.3%			of Service	A	
Analysis Period (min)			15					
Phase conflict between	lane groups							
o Critical Lano Group								

Intersection

Int Delay, s/veh	0.6			
Movement	EBT	EBR	WBL	WBT

Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	Åî≽					1
Traffic Vol, veh/h	1715	85	0	0	0	81
Future Vol, veh/h	1715	85	0	0	0	81
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Stop	Stop	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	-	0
Veh in Median Storage	e, # 0	-	10815	77472	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	89	89	92	92	92	92
Heavy Vehicles, %	4	4	2	2	2	2
Mvmt Flow	1927	96	0	0	0	88

Major/Minor	Major1			Mi	nor1					
Conflicting Flow All	0	0			-	1012				
Stage 1	-	-			-	-				
Stage 2	-	-			-	-				
Critical Hdwy	-	-			-	6.94				
Critical Hdwy Stg 1	-	-			-	-				
Critical Hdwy Stg 2	-	-			-	-				
Follow-up Hdwy	-	-			-	3.32				
Pot Cap-1 Maneuver	-	-			0	*441				
Stage 1	-	-			0	-				
Stage 2	-	-			0	-				
Platoon blocked, %	-	-				1				
Mov Cap-1 Maneuver		-			-	*441				
Mov Cap-2 Maneuver	-	-			-	-				
Stage 1	-	-			-	-				
Stage 2	-	-			-	-				
Approach	EB				NB					
HCM Control Delay, s	0				15.2					
HCM LOS					С					
Minor Lane/Major Mvn	nt N	VBLn1	EBT	EBR						
· · · · · ·	nt r	441								
Capacity (veh/h) HCM Lane V/C Ratio		44 I 0.2	-	-						
HCM Control Delay (s	1	0.2 15.2	-	-						
HCM Lane LOS)	15.2 C	-							
	.)	0.7	-	-						
HCM 95th %tile Q(veh	1)	0.7	-	-						
Notes										
~: Volume exceeds ca	pacity	\$: De	lay exc	eeds 300	s	+: Comp	outation Not	Defined	*: All major volume in platoon	

Intersection

Int Delay, s/veh	0.4					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	Y			ب	4	
Traffic Vol, veh/h	5	15	13	394	541	8
Future Vol, veh/h	5	15	13	394	541	8
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	,# 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	87	87	92	92
Heavy Vehicles, %	2	2	4	4	2	2
Mvmt Flow	5	16	15	453	588	9

Major/Minor	Minor2	1	Major1	Ν	/lajor2			
Conflicting Flow All	1076	593	597	0	-	0		
Stage 1	593	-	-	-	-	-		
Stage 2	483	-	-	-	-	-		
Critical Hdwy	6.42	6.22	4.14	-	-	-		
Critical Hdwy Stg 1	5.42	-	-	-	-	-		
Critical Hdwy Stg 2	5.42	-	-	-	-	-		
Follow-up Hdwy	3.518	3.318		-	-	-		
Pot Cap-1 Maneuver		*634	*942	-	-	-		
Stage 1	*598	-	-	-	-	-		
Stage 2	*620	-	-	-	-	-		
Platoon blocked, %	1	1	1	-	-	-		
Mov Cap-1 Maneuver		*634	*942	-	-	-		
Mov Cap-2 Maneuver		-	-	-	-	-		
Stage 1	*586	-	-	-	-	-		
Stage 2	*620	-	-	-	-	-		
Approach	EB		NB		SB			
HCM Control Delay, s	s 14		0.3		0			
HCM LOS	В							
Minor Lane/Major Mv	mt	NBL	NBT E	EBLn1	SBT	SBR		
Capacity (veh/h)		* 942	-	421	-	-		
HCM Lane V/C Ratio		0.016	-	0.052	-	-		
HCM Control Delay (s		8.9	0	14	-	-		
HCM Lane LOS	,	A	A	В	-	-		
HCM 95th %tile Q(ve	h)	0	-	0.2	-	-		
Notes								
~: Volume exceeds ca	apacity	\$: De	elay exc	eeds 30)0s	+: Comp	outation Not Defined	*: All major volume in platoon

	≯	-	+	×	1	4		
Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations		<u>††</u>			۳.			
Traffic Volume (vph)	0	1444	0	0	266	0		
Future Volume (vph)	0	1444	0	0	266	0		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)		6.1			5.9			
Lane Util. Factor		0.95			1.00			
Frt		1.00			1.00			
Flt Protected		1.00			0.95			
Satd. Flow (prot)		3471			1787			
Flt Permitted		1.00			0.95			
Satd. Flow (perm)		3471			1787			
Peak-hour factor, PHF	0.94	0.94	0.92	0.92	0.88	0.88		
Adj. Flow (vph)	0	1536	0	0	302	0		
RTOR Reduction (vph)	0	0	0	0	0	0		
Lane Group Flow (vph)	0	1536	0	0	302	0		
Heavy Vehicles (%)	4%	4%	2%	2%	1%	1%		
Turn Type		NA			Prot			
Protected Phases		2!			4 2!			
Permitted Phases								
Actuated Green, G (s)		85.9			120.0			
Effective Green, g (s)		85.9			113.9			
Actuated g/C Ratio		0.72			0.95			
Clearance Time (s)		6.1						
Vehicle Extension (s)		3.0						
Lane Grp Cap (vph)		2484			1696			
v/s Ratio Prot		c0.44			c0.17			
v/s Ratio Perm								
v/c Ratio		0.62			0.18			
Uniform Delay, d1		8.7			0.2			
Progression Factor		1.00			1.00			
Incremental Delay, d2		1.2			0.1			
Delay (s)		9.9			0.3			
Level of Service		А			А			
Approach Delay (s)		9.9	0.0		0.3			
Approach LOS		А	А		А			
Intersection Summary								
HCM 2000 Control Delay			8.3	H	CM 2000	Level of Service	А	
HCM 2000 Volume to Capacity	ratio		0.53					
Actuated Cycle Length (s)			120.0		um of lost		12.0	
Intersection Capacity Utilization	۱		97.4%	IC	U Level o	of Service	F	
Analysis Period (min)			15					
! Phase conflict between lane	groups	i.						
 Outline II and Outline 								

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		<u></u>	1					•	11		•	
Traffic Volume (vph)	0	1370	334	0	0	0	0	188	348	0	66	0
Future Volume (vph)	0	1370	334	0	0	0	0	188	348	0	66	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.7	6.7					10.9	10.9		6.9	
Lane Util. Factor		0.95	1.00					1.00	0.88		1.00	
Frt		1.00	0.85					1.00	0.85		1.00	
Flt Protected		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (prot)		3505	1568					1863	2787		1827	
Flt Permitted		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (perm)		3505	1568					1863	2787		1827	
Peak-hour factor, PHF	0.95	0.95	0.95	0.92	0.92	0.92	0.93	0.93	0.93	0.92	0.92	0.92
Adj. Flow (vph)	0	1442	352	0	0	0	0	202	374	0	72	0
RTOR Reduction (vph)	0	0	108	0	0	0	0	0	101	0	0	0
Lane Group Flow (vph)	0	1442	244	0	0	0	0	202	273	0	72	0
Heavy Vehicles (%)	3%	3%	3%	2%	2%	2%	2%	2%	2%	4%	4%	4%
Turn Type		NA	Perm					NA	Perm		NA	
Protected Phases		2						4			8	
Permitted Phases			2						4			
Actuated Green, G (s)		83.3	83.3					19.1	19.1		23.1	
Effective Green, g (s)		83.3	83.3					19.1	19.1		23.1	
Actuated g/C Ratio		0.69	0.69					0.16	0.16		0.19	
Clearance Time (s)		6.7	6.7					10.9	10.9		6.9	
Vehicle Extension (s)		3.0	3.0					3.0	3.0		3.0	
Lane Grp Cap (vph)		2433	1088					296	443		351	
v/s Ratio Prot		c0.41						c0.11			0.04	
v/s Ratio Perm			0.16						0.10			
v/c Ratio		0.59	0.22					0.68	0.62		0.21	
Uniform Delay, d1		9.5	6.6					47.6	47.0		40.7	
Progression Factor		0.30	0.20					1.00	1.00		0.00	
Incremental Delay, d2		0.9	0.4					12.1	6.3		1.3	
Delay (s)		3.8	1.7					59.6	53.3		1.3	
Level of Service		A	A		0.0			E	D		A	_
Approach Delay (s)		3.4			0.0			55.5			1.3	
Approach LOS		A			A			E			A	
Intersection Summary			45.0		014 0000	1						
HCM 2000 Control Delay			15.6	Н	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capacity	ratio		0.61	^					47.0			
Actuated Cycle Length (s)			120.0		um of los				17.6			
Intersection Capacity Utilization	1		73.7%	IC	U Level (of Service			D			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					- ††	1		↑			↑	77
Traffic Volume (vph)	0	0	0	0	1897	111	0	188	0	0	66	144
Future Volume (vph)	0	0	0	0	1897	111	0	188	0	0	66	144
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.7	6.7		6.9			10.9	10.9
Lane Util. Factor					0.95	1.00		1.00			1.00	0.88
Frpb, ped/bikes					1.00	0.99		1.00			1.00	0.98
Flpb, ped/bikes					1.00	1.00		1.00			1.00	1.00
Frt					1.00	0.85		1.00			1.00	0.85
Flt Protected					1.00	1.00		1.00			1.00	1.00
Satd. Flow (prot)					3539	1562		1863			1827	2670
Flt Permitted					1.00	1.00		1.00			1.00	1.00
Satd. Flow (perm)					3539	1562		1863			1827	2670
Peak-hour factor, PHF	0.92	0.92	0.92	0.90	0.90	0.90	0.93	0.93	0.93	0.92	0.92	0.92
Adj. Flow (vph)	0	0	0	0	2108	123	0	202	0	0	72	157
RTOR Reduction (vph)	0	0	0	0	0	37	0	0	0	0	0	29
Lane Group Flow (vph)	0	0	0	0	2108	86	0	202	0	0	72	128
Confl. Peds. (#/hr)						3						1
Heavy Vehicles (%)	2%	2%	2%	2%	2%	2%	2%	2%	2%	4%	4%	4%
Turn Type					NA	Perm		NA			NA	Perm
Protected Phases					6			8			4	
Permitted Phases						6						4
Actuated Green, G (s)					83.3	83.3		23.1			19.1	19.1
Effective Green, g (s)					83.3	83.3		23.1			19.1	19.1
Actuated g/C Ratio					0.69	0.69		0.19			0.16	0.16
Clearance Time (s)					6.7	6.7		6.9			10.9	10.9
Vehicle Extension (s)					3.0	3.0		3.0			3.0	3.0
Lane Grp Cap (vph)					2456	1084		358			290	424
v/s Ratio Prot					c0.60			c0.11			0.04	
v/s Ratio Perm						0.06						0.05
v/c Ratio					0.86	0.08		0.56			0.25	0.30
Uniform Delay, d1					13.9	5.9		43.9			44.2	44.6
Progression Factor					0.99	0.48		0.00			1.34	1.44
Incremental Delay, d2					2.9	0.1		4.6			2.0	1.8
Delay (s)					16.6	3.0		4.7			61.2	66.0
Level of Service					В	А		А			E	E
Approach Delay (s)		0.0			15.9			4.7			64.5	
Approach LOS		А			В			А			E	
Intersection Summary												
HCM 2000 Control Delay			19.2	H	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capacity	y ratio		0.83									
Actuated Cycle Length (s)	-		120.0	S	um of los	t time (s)			17.6			
Intersection Capacity Utilizatio	n		73.7%			of Service			D			
Analysis Period (min)			15									
c Critical Lane Group												

Movement EBI EBI EBI EBI WBI WBI WBI NBI NBI NBR SBI SBI SBR S		≯	-	\mathbf{F}	∢	-	•	1	Ť	1	1	ţ	~
Traffic Volume (vph) 0 0 0 1688 38 250 34 0 0 0 6 Ideal Flow (vph) 1900 1000 100	Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Traffic Volume (vph) 0 0 0 1688 38 250 34 0 0 0 6 Ideal Flow (vph) 1900 1000 100	Lane Configurations					^	1		र्स				1
Ideal Flow (vphp) 1900 <td>Traffic Volume (vph)</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td></td> <td>38</td> <td>250</td> <td></td> <td>0</td> <td>0</td> <td>0</td> <td></td>	Traffic Volume (vph)	0	0	0	0		38	250		0	0	0	
Total Lost time (s) 6.1 6.1 5.9 5.9 Lane Util. Factor 0.95 1.00 1.00 1.00 Fibp. pedi/bikes 1.00 0.98 1.00 1.00 Fibp. pedi/bikes 1.00 0.98 1.00 1.00 Fibp. pedi/bikes 1.00 1.00 0.96 1.00 Fibr. pedi/bikes 1.00 1.00 0.96 1.00 Stdt. Flow (prot) 3505 1536 1820 1644 Peak-hour factor, PHF 0.92 0.92 0.95 0.95 0.79 0.79 0.74 0.74 0.74 Peak-hour factor, PHF 0.92 0.92 0.95 0.95 0.79 0.79 0.74 0.74 0.74 0.74 Lane Group Flow (ph) 0	Future Volume (vph)	0	0	0	0	1698	38	250	34	0	0	0	60
Total Lost time (c) 6.1 6.1 5.9 5.9 Lane Util. Factor 0.95 1.00 1.00 1.00 Fibp. ped/bikes 1.00 0.98 1.00 1.00 Fibp. ped/bikes 1.00 0.98 1.00 1.00 Fibr. Ped/bikes 1.00 1.00 1.00 1.00 Fibr. ped/bikes 1.00 1.00 0.96 1.00 Stat. Flow (prot) 3505 1536 1820 1644 Peak-hour factor, PHF 0.92 0.92 0.95 0.95 0.79 0.79 0.74 0.74 0.74 Peak-hour factor, PHF 0.92 0.92 0.95 0.95 0.79 0.79 0.74 0.74 0.74 Peak-hour factor, PHF 0.92 0.92 0.95 0.95 0.79 0.79 0.79 0.74 0.74 0.74 0.74 Lane Group Flow (oph) 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(1)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Uhi, Factor 0.95 1.00 1.00 1.00 Frpb, ped/bikes 1.00 0.98 1.00 1.00 Frbb, ped/bikes 1.00 1.00 1.00 1.00 Frt 1.00 0.85 1.00 0.98 1.00 Frt 1.00 0.85 1.00 0.98 1.00 Frt 1.00 1.00 0.96 1.00 1.00 Stdt. Flow (ptrot) 3505 1536 1820 1644 Peak-hour factor, PHF 0.92 0.92 0.95 0.95 0.79 0.79 0.74 0.74 0.74 Adj. Flow (vph) 0 0 0 0 7 0 31 0 <						6.1	6.1		5.9				
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Phase conflict between lane groups.													
		e groups											
c Childai Lane Group	c Critical Lane Group												

	4	*	Ť	1	1	Ļ			
Movement	WBL	WBR	NBT	NBR	SBL	SBT			
Lane Configurations	٦					<u>††</u>			
Traffic Volume (vph)	187	0	0	0	0	23			
Future Volume (vph)	187	0	0	0	0	23			
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900			
Total Lost time (s)	4.9					5.4			
Lane Util. Factor	1.00					0.95			
Frt	1.00					1.00			
Flt Protected	0.95					1.00			
Satd. Flow (prot)	1752					3610			
Flt Permitted	0.95					1.00			
Satd. Flow (perm)	1752					3610			
Peak-hour factor, PHF	0.86	0.86	0.92	0.92	0.60	0.60			
Adj. Flow (vph)	217	0.00	0.02	0.02	0.00	38			
RTOR Reduction (vph)	0	0	0	0	0 0	0			
Lane Group Flow (vph)	217	0	0	0	0	38			
Heavy Vehicles (%)	3%	3%	2%	2%	0%	0%			
Turn Type	Prot					NA			
Protected Phases	4 2!					2!			
Permitted Phases									
Actuated Green, G (s)	120.0					86.6			
Effective Green, g (s)	114.6					86.6			
Actuated g/C Ratio	0.95					0.72			
Clearance Time (s)						5.4			
Vehicle Extension (s)						3.0			
Lane Grp Cap (vph)	1673					2605			
v/s Ratio Prot	c0.12					0.01			
v/s Ratio Perm									
v/c Ratio	0.13					0.01			
Uniform Delay, d1	0.1					4.7			
Progression Factor	1.00					1.00			
Incremental Delay, d2	0.2					0.0			
Delay (s)	0.3					4.7			
Level of Service	A					А			
Approach Delay (s)	0.3		0.0			4.7			
Approach LOS	А		А			А			
Intersection Summary									
HCM 2000 Control Delay			0.9	H	CM 2000	Level of Servic	e	А	
HCM 2000 Volume to Capa	acity ratio		0.14						
Actuated Cycle Length (s)			120.0	Si	um of lost	t time (s)		10.3	
Intersection Capacity Utilization	ation		30.7%	IC	U Level o	of Service		А	
Analysis Period (min)			15						
Phase conflict between	lane groups								
 Critical Lana Group 									

Intersection							
Int Delay, s/veh	0.8						
Movement	EBT	EBR	WBL	WBT	NBL	NBR	
		LDIX	VVDL		NDL		
Lane Configurations	_ ≜ î≽					r	
Traffic Vol, veh/h	1612	98	0	0	0	92	
Future Vol, veh/h	1612	98	0	0	0	92	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Stop	Stop	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	-	-	-	-	-	0	
Veh in Median Storage	e, # 0	-	10815	77472	0	-	
Grade, %	0	-	-	0	0	-	
Peak Hour Factor	95	95	92	92	92	92	
Heavy Vehicles, %	3	3	2	2	2	2	
Mvmt Flow	1697	103	0	0	0	100	

Major/Minor M	ajor1		Minor1			
Conflicting Flow All	0 0		-	900		
Stage 1			-	-		
Stage 2			-	-		
Critical Hdwy			-	6.94		
Critical Hdwy Stg 1			-	-		
Critical Hdwy Stg 2			-	-		
Follow-up Hdwy			-	3.32		
Pot Cap-1 Maneuver			0	*458		
Stage 1			0	-		
Stage 2			0	-		
Platoon blocked, %				1		
Mov Cap-1 Maneuver			-	*458		
Mov Cap-2 Maneuver			-	-		
Stage 1			-	-		
Stage 2			-	-		
Approach	EB		NB			
HCM Control Delay, s	0		15			
HCM LOS			С			
Minor Lane/Major Mvmt	NBLn1	EBT	EBR			
Capacity (veh/h)	458	-	-			
HCM Lane V/C Ratio	0.218	-	-			
HCM Control Delay (s)	15	-	-			
HCM Lane LOS	С	-	-			
HCM 95th %tile Q(veh)	0.8	-	-			
Notes						
~: Volume exceeds capa	acity \$: D	elay exce	eds 300s	+: Com	putation Not Defined	*: All major volume in platoon

Intersection

Int Delay, s/veh	0.4						
Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations	Y			र्भ	el el		
Traffic Vol, veh/h	7	14	16	529	394	6	
Future Vol, veh/h	7	14	16	529	394	6	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Stop	Stop	Free	Free	Free	Free	
RT Channelized	-	None	-	None	-	None	
Storage Length	0	-	-	-	-	-	
Veh in Median Storage	,# 0	-	-	0	0	-	
Grade, %	0	-	-	0	0	-	
Peak Hour Factor	92	92	93	93	92	92	
Heavy Vehicles, %	2	2	2	2	2	2	
Mvmt Flow	8	15	17	569	428	7	'

Major/Minor	Minor2		Major1	Ma	jor2	
Conflicting Flow All	1035	432	435	0	-	0
Stage 1	432	-	-	-	-	-
Stage 2	603	-	-	-	-	-
Critical Hdwy	6.42	6.22	4.12	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.218	-	-	-
Pot Cap-1 Maneuver	237	772	1151	-	-	-
Stage 1	728	-	-	-	-	-
Stage 2	546	-	-	-	-	-
Platoon blocked, %	1	1	1	-	-	-
Mov Cap-1 Maneuver	231	772	1151	-	-	-
Mov Cap-2 Maneuver	231	-	-	-	-	-
Stage 1	712	-	-	-	-	-
Stage 2	546	-	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	13.8	0.2	0
HCM LOS	В		

Minor Lane/Major Mvmt	NBL	NBTI	EBLn1	SBT	SBR
Capacity (veh/h)	1151	-	434	-	-
HCM Lane V/C Ratio	0.015	-	0.053	-	-
HCM Control Delay (s)	8.2	0	13.8	-	-
HCM Lane LOS	А	А	В	-	-
HCM 95th %tile Q(veh)	0	-	0.2	-	-

Intersection: 10: EB Highland Road & WB-to-EB X/O

Movement	EB	EB	SB
Directions Served	Т	Т	L
Maximum Queue (ft)	300	305	69
Average Queue (ft)	153	159	41
95th Queue (ft)	241	255	68
Link Distance (ft)	708	708	35
Upstream Blk Time (%)			15
Queuing Penalty (veh)			30
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 11: WB-to-EB X/O & WB Highland Road

Movement	WB
Directions Served	L
Maximum Queue (ft)	140
Average Queue (ft)	32
95th Queue (ft)	101
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	325
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 20: Bogie Lake Road & EB Highland Road

Movement	EB	EB	EB	NB	NB	NB
Directions Served	Т	Т	R	Т	R	R
Maximum Queue (ft)	129	144	109	119	120	123
Average Queue (ft)	56	70	46	55	64	49
95th Queue (ft)	110	125	84	104	107	97
Link Distance (ft)	330	330	330	291	291	291
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)						
Storage Blk Time (%)						
Queuing Penalty (veh)						

Intersection: 21: Bogie Lake Road & WB Highland Road

	14/5	14/5	14/5	0.0	0.5	0.5
Movement	WB	WB	WB	SB	SB	SB
Directions Served	Т	Т	R	Т	R	R
Maximum Queue (ft)	102	102	39	92	70	52
Average Queue (ft)	40	36	4	31	29	16
95th Queue (ft)	83	83	20	71	62	44
Link Distance (ft)	477	477	477	152	152	152
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)						
Storage Blk Time (%)						
Queuing Penalty (veh)						

Intersection: 30: EB-to-WB X/O/Nordic Drive & WB Highland Road

M				ND	00
Movement	WB	WB	WB	NB	SB
Directions Served	Т	Т	R	LT	R
Maximum Queue (ft)	203	161	11	52	30
Average Queue (ft)	115	65	1	39	5
95th Queue (ft)	180	137	9	59	23
Link Distance (ft)	905	905		11	94
Upstream Blk Time (%)				22	
Queuing Penalty (veh)				39	
Storage Bay Dist (ft)			50		
Storage Blk Time (%)		9			
Queuing Penalty (veh)		1			
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Intersection: 31: EB Highland Road & EB-to-WB X/O

Movement	EB
Directions Served	L
Maximum Queue (ft)	120
Average Queue (ft)	31
95th Queue (ft)	88
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	300
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 40: Bogie Lake Road & NB-to-SB X/O

Movement	WB	SB
Directions Served	L	Т
Maximum Queue (ft)	5	62
Average Queue (ft)	0	11
95th Queue (ft)	6	40
Link Distance (ft)	28	192
Upstream Blk Time (%)	0	
Queuing Penalty (veh)	0	
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 41: Bogie Lake Road & NB-to-SB X/O

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)

Intersection: 50: W. Site Drive & EB Highland Road

Movement	EB	NB
Directions Served	TR	R
Maximum Queue (ft)	21	96
Average Queue (ft)	1	42
95th Queue (ft)	11	76
Link Distance (ft)	348	334
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 60: Bogie Lake Road & E. Site Drive

Movement	EB	NB
Directions Served	LR	LT
Maximum Queue (ft)	40	46
Average Queue (ft)	17	3
95th Queue (ft)	43	21
Link Distance (ft)	294	343
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Zone Summary

Zone wide Queuing Penalty: 70

Intersection: 10: EB Highland Road & WB-to-EB X/O

Movement	EB	EB	SB
Directions Served	Т	Т	L
Maximum Queue (ft)	238	236	68
Average Queue (ft)	138	123	48
95th Queue (ft)	218	210	63
Link Distance (ft)	708	708	35
Upstream Blk Time (%)			26
Queuing Penalty (veh)			70
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 11: WB-to-EB X/O & WB Highland Road

Movement	WB
Directions Served	L
Maximum Queue (ft)	185
Average Queue (ft)	51
95th Queue (ft)	137
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	325
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 20: Bogie Lake Road & EB Highland Road

Movement	EB	EB	EB	NB	NB	NB
Directions Served	Т	Т	R	Т	R	R
Maximum Queue (ft)	144	151	69	261	157	140
Average Queue (ft)	58	68	28	125	82	66
95th Queue (ft)	117	128	57	224	135	115
Link Distance (ft)	330	330	330	291	291	291
Upstream Blk Time (%)				0		
Queuing Penalty (veh)				0		
Storage Bay Dist (ft)						
Storage Blk Time (%)						
Queuing Penalty (veh)						

Intersection: 21: Bogie Lake Road & WB Highland Road

Movement	WB	WB	WB	NB	SB	SB	SB
Directions Served	Т	Т	R	Т	Т	R	R
Maximum Queue (ft)	239	237	43	15	110	120	117
Average Queue (ft)	78	89	9	1	49	52	46
95th Queue (ft)	144	156	32	11	95	99	94
Link Distance (ft)	477	477	477	37	152	152	152
Upstream Blk Time (%)				2	0		0
Queuing Penalty (veh)				4	0		0
Storage Bay Dist (ft)							
Storage Blk Time (%)							
Queuing Penalty (veh)							

Intersection: 30: EB-to-WB X/O/Nordic Drive & WB Highland Road

N					00
Movement	WB	WB	WB	NB	SB
Directions Served	Т	Т	R	LT	R
Maximum Queue (ft)	303	277	95	48	82
Average Queue (ft)	172	126	8	47	31
95th Queue (ft)	265	229	48	52	65
Link Distance (ft)	905	905		11	94
Upstream Blk Time (%)				57	0
Queuing Penalty (veh)				164	0
Storage Bay Dist (ft)			50		
Storage Blk Time (%)		14	0		
Queuing Penalty (veh)		5	0		
0, ()					

Intersection: 31: EB Highland Road & EB-to-WB X/O

Movement	EB	EB
	ED	ED
Directions Served	L	Т
Maximum Queue (ft)	268	121
Average Queue (ft)	136	4
95th Queue (ft)	252	65
Link Distance (ft)		518
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)	300	
Storage Blk Time (%)	1	
Queuing Penalty (veh)	4	

Intersection: 40: Bogie Lake Road & NB-to-SB X/O

Movement	WB	SB
Directions Served	L	Т
Maximum Queue (ft)	25	40
Average Queue (ft)	1	7
95th Queue (ft)	12	29
Link Distance (ft)	28	192
Upstream Blk Time (%)	0	
Queuing Penalty (veh)	0	
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 41: Bogie Lake Road & NB-to-SB X/O

vement
ections Served
ximum Queue (ft)
erage Queue (ft)
h Queue (ft)
k Distance (ft)
stream Blk Time (%)
euing Penalty (veh)
rage Bay Dist (ft)
rage Blk Time (%)
euing Penalty (veh)

Intersection: 50: W. Site Drive & EB Highland Road

Movement	NB
Directions Served	R
Maximum Queue (ft)	108
Average Queue (ft)	43
95th Queue (ft)	83
Link Distance (ft)	334
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 60: Bogie Lake Road & E. Site Drive

Movement	EB	NB
Directions Served	LR	LT
Maximum Queue (ft)	45	48
Average Queue (ft)	15	5
95th Queue (ft)	43	25
Link Distance (ft)	294	343
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Zone Summary

Zone wide Queuing Penalty: 248

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Movement EE	BL EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	<u>^</u>	1					†	77		†	
Traffic Volume (vph)	0 1292		0	0	0	0	103	296	0	45	0
Future Volume (vph)	0 1292	504	0	0	0	0	103	296	0	45	0
Ideal Flow (vphpl) 190			1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.7						10.9	10.9		6.9	
Lane Util. Factor	0.95						1.00	0.88		1.00	
Frt	1.00						1.00	0.85		1.00	
Flt Protected	1.00						1.00	1.00		1.00	
Satd. Flow (prot)	3471						1827	2733		1681	
Flt Permitted	1.00						1.00	1.00		1.00	
Satd. Flow (perm)	3471						1827	2733		1681	
Peak-hour factor, PHF 0.8			0.92	0.92	0.92	0.87	0.87	0.87	0.95	0.95	0.95
Adj. Flow (vph)	0 1452		0	0	0	0	118	340	0	47	0
RTOR Reduction (vph)	0 0		0	0	0	0	0	31	0	0	0
Lane Group Flow (vph)	0 1452		0	0	0	0	118	309	0	47	0
	% 4%		2%	2%	2%	4%	4%	4%	13%	13%	13%
Turn Type	NA						NA	Perm		NA	
Protected Phases	2						4			8	
Permitted Phases		2						4			
Actuated Green, G (s)	45.3						27.1	27.1		31.1	
Effective Green, g (s)	45.3						27.1	27.1		31.1	_
Actuated g/C Ratio	0.50						0.30	0.30		0.35	
Clearance Time (s)	6.7						10.9	10.9		6.9	_
Vehicle Extension (s)	3.0						3.0	3.0		3.0	
Lane Grp Cap (vph)	1747						550	822		580	_
v/s Ratio Prot	c0.42						0.06	0.44		0.03	
v/s Ratio Perm	0.00	0.18					0.04	c0.11		0.00	
v/c Ratio	0.83						0.21	0.38		0.08	
Uniform Delay, d1	19.1						23.5	24.8		19.8	
Progression Factor Incremental Delay, d2	0.43 3.4						1.00 0.9	1.00 1.3		0.00 0.3	
Delay (s)	5.4 11.5						24.4	26.1		0.3	
Level of Service	E						24.4 C	20.1 C		0.3 A	
Approach Delay (s)	9.4			0.0			25.7	U		0.3	
Approach LOS	9.4 A			A O.U			23.1 C			0.5 A	
Intersection Summary	,	,		Λ			Ū			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	
HCM 2000 Control Delay		12.2	H	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capacity ratio	2	0.66		2000	_0.0101			5			
Actuated Cycle Length (s)		90.0	S	um of los	t time (s)			17.6			
Intersection Capacity Utilization		60.7%			of Service			В			
Analysis Period (min)		15		20101				-			
c Critical Lane Group											

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					† †	1		†			•	77
Traffic Volume (vph)	0	0	0	0	1138	44	0	103	0	0	45	69
Future Volume (vph)	0	0	0	0	1138	44	0	103	0	0	45	69
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.7	6.7		6.9			10.9	10.9
Lane Util. Factor					0.95	1.00		1.00			1.00	0.88
Frt					1.00	0.85		1.00			1.00	0.85
Flt Protected					1.00	1.00		1.00			1.00	1.00
Satd. Flow (prot)					3406	1524		1827			1681	2515
Flt Permitted					1.00	1.00		1.00			1.00	1.00
Satd. Flow (perm)					3406	1524		1827			1681	2515
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.87	0.87	0.87	0.95	0.95	0.95
Adj. Flow (vph)	0	0	0	0	1237	48	0	118	0	0	47	73
RTOR Reduction (vph)	0	0	0	0	0	24	0	0	0	0	0	49
Lane Group Flow (vph)	0	0	0	0	1237	24	0	118	0	0	47	24
Heavy Vehicles (%)	2%	2%	2%	6%	6%	6%	4%	4%	4%	13%	13%	13%
Turn Type					NA	Perm		NA			NA	Perm
Protected Phases					6	<u>^</u>		8			4	
Permitted Phases					45.0	6		04.4			07.4	4
Actuated Green, G (s)					45.3	45.3		31.1			27.1	27.1
Effective Green, g (s)					45.3	45.3		31.1			27.1	27.1
Actuated g/C Ratio					0.50 6.7	0.50 6.7		0.35 6.9			0.30 10.9	0.30
Clearance Time (s) Vehicle Extension (s)					6.7 3.0	0.7 3.0		6.9 3.0			3.0	10.9
												3.0
Lane Grp Cap (vph)					1714 c0.36	767		631			506 0.03	757
v/s Ratio Prot v/s Ratio Perm					0.30	0.02		c0.06			0.05	0.01
v/c Ratio					0.72	0.02		0.19			0.09	0.01
Uniform Delay, d1					17.4	11.3		20.6			22.6	22.2
Progression Factor					0.71	0.27		0.00			1.39	2.38
Incremental Delay, d2					2.4	0.27		0.00			0.4	0.1
Delay (s)					14.7	3.1		0.0			31.8	52.9
Level of Service					В	A		A			C	02.0 D
Approach Delay (s)		0.0			14.3	7.		0.7			44.6	2
Approach LOS		A			В			A			D	
Intersection Summary												
HCM 2000 Control Delay			15.6	H	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capacity	y ratio		0.53									
Actuated Cycle Length (s)			90.0		um of los				17.6			
Intersection Capacity Utilizatio	n		60.7%	IC	CU Level	of Service			В			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		<u>††</u>	1					•	11		•	
Traffic Volume (vph)	0	1370	334	0	0	0	0	188	348	0	66	0
Future Volume (vph)	0	1370	334	0	0	0	0	188	348	0	66	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.7	6.7					10.9	10.9		6.9	
Lane Util. Factor		0.95	1.00					1.00	0.88		1.00	
Frt		1.00	0.85					1.00	0.85		1.00	
Flt Protected		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (prot)		3505	1568					1863	2787		1827	
Flt Permitted		1.00	1.00					1.00	1.00		1.00	
Satd. Flow (perm)		3505	1568					1863	2787		1827	
Peak-hour factor, PHF	0.95	0.95	0.95	0.92	0.92	0.92	0.93	0.93	0.93	0.92	0.92	0.92
Adj. Flow (vph)	0	1442	352	0	0	0	0	202	374	0	72	0
RTOR Reduction (vph)	0	0	137	0	0	0	0	0	61	0	0	0
Lane Group Flow (vph)	0	1442	215	0	0	0	0	202	313	0	72	0
Heavy Vehicles (%)	3%	3%	3%	2%	2%	2%	2%	2%	2%	4%	4%	4%
Turn Type		NA	Perm					NA	Perm		NA	
Protected Phases		2						4			8	
Permitted Phases			2					00.4	4		00.4	_
Actuated Green, G (s)		73.3	73.3					29.1	29.1		33.1	
Effective Green, g (s)		73.3	73.3					29.1	29.1		33.1	_
Actuated g/C Ratio		0.61	0.61					0.24	0.24		0.28	
Clearance Time (s)		6.7	6.7					10.9	10.9		6.9	
Vehicle Extension (s)		3.0	3.0					3.0	3.0		3.0	
Lane Grp Cap (vph)		2140	957					451	675		503	
v/s Ratio Prot		c0.41	0.4.4					0.11	-0.11		0.04	
v/s Ratio Perm		0.67	0.14 0.22					0.45	c0.11		0.14	
v/c Ratio Uniform Delay, d1		0.67 15.4	0.22 10.5					0.45 38.6	0.46 38.8		0.14 32.8	
Progression Factor		0.52	0.17					30.0 1.00	30.0 1.00		52.0 0.00	
Incremental Delay, d2		1.5	0.17					3.2	2.3		0.00	
Delay (s)		9.5	2.2					41.8	41.1		0.0	
Level of Service		9.5 A	2.2 A					41.0 D	41.1 D		0.0 A	
Approach Delay (s)		8.1	Л		0.0			41.3	D		0.6	
Approach LOS		A			A			D			A	
Intersection Summary												
HCM 2000 Control Delay			15.7	Н	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capacity	ratio		0.61									
Actuated Cycle Length (s)			120.0	S	um of los	t time (s)			17.6			
Intersection Capacity Utilization	۱		73.7%			of Service			D			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					- ††	1		↑			↑	11
Traffic Volume (vph)	0	0	0	0	1897	111	0	188	0	0	66	144
Future Volume (vph)	0	0	0	0	1897	111	0	188	0	0	66	144
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)					6.7	6.7		6.9			10.9	10.9
Lane Util. Factor					0.95	1.00		1.00			1.00	0.88
Frpb, ped/bikes					1.00	0.99		1.00			1.00	0.98
Flpb, ped/bikes					1.00	1.00		1.00			1.00	1.00
Frt					1.00	0.85		1.00			1.00	0.85
Flt Protected					1.00	1.00		1.00			1.00	1.00
Satd. Flow (prot)					3539	1562		1863			1827	2673
Flt Permitted					1.00	1.00		1.00			1.00	1.00
Satd. Flow (perm)					3539	1562		1863			1827	2673
Peak-hour factor, PHF	0.92	0.92	0.92	0.90	0.90	0.90	0.93	0.93	0.93	0.92	0.92	0.92
Adj. Flow (vph)	0	0	0	0	2108	123	0	202	0	0	72	157
RTOR Reduction (vph)	0	0	0	0	0	37	0	0	0	0	0	26
Lane Group Flow (vph)	0	0	0	0	2108	86	0	202	0	0	72	131
Confl. Peds. (#/hr)						3						1
Heavy Vehicles (%)	2%	2%	2%	2%	2%	2%	2%	2%	2%	4%	4%	4%
Turn Type					NA	Perm		NA			NA	Perm
Protected Phases					6			8			4	
Permitted Phases					•	6		•			•	4
Actuated Green, G (s)					73.3	73.3		33.1			29.1	29.1
Effective Green, g (s)					73.3	73.3		33.1			29.1	29.1
Actuated g/C Ratio					0.61	0.61		0.28			0.24	0.24
Clearance Time (s)					6.7	6.7		6.9			10.9	10.9
Vehicle Extension (s)					3.0	3.0		3.0			3.0	3.0
Lane Grp Cap (vph)					2161	954		513			443	648
v/s Ratio Prot					c0.60	504		c0.11			0.04	040
v/s Ratio Perm					00.00	0.06		00.11			0.04	0.05
v/c Ratio					0.98	0.00		0.39			0.16	0.00
Uniform Delay, d1					22.5	9.6		35.3			35.8	36.2
Progression Factor					0.60	1.04		0.00			1.46	1.59
Incremental Delay, d2					10.0	0.1		2.1			0.8	0.7
Delay (s)					23.5	10.1		2.1			53.3	58.2
Level of Service					23.3 C	B		2.1 A			55.5 D	50.2 E
Approach Delay (s)		0.0			22.8	D		2.1			56.6	L
Approach LOS		0.0 A			22.0 C			2.1 A			50.0 E	
		A			U			A			E	
Intersection Summary												
HCM 2000 Control Delay			24.1	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capacit	y ratio		0.83									
Actuated Cycle Length (s)			120.0		um of los				17.6			
Intersection Capacity Utilization	on		73.7%	IC	CU Level	of Service			D			
Analysis Period (min)			15									
c Critical Lane Group												

Movement EBI EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR Lane Configurations		۶	-	\mathbf{F}	∢	←	•	1	Ť	۲	1	Ļ	~
Traffic Volume (vph) 0 0 0 1688 38 250 34 0 0 0 60 Future Volume (vph) 1900 100	Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Traffic Volume (vph) 0 0 0 1688 38 250 34 0 0 0 60 Future Volume (vph) 1900 100	Lane Configurations					^	1		ا				1
Ideal Flow (pph) 1900 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 10	Traffic Volume (vph)	0	0	0	0		38	250		0	0	0	60
Total Lost time (s) 6.1 6.1 5.9 5.9 Lane Util, Factor 0.95 1.00 1.00 1.00 Fipb, ped/bikes 1.00 0.08 1.00 1.00 Fipb, ped/bikes 1.00 0.08 1.00 1.00 Fit 1.00 1.00 0.96 1.00 Fith Protected 1.00 1.00 0.96 1.00 Satd, Flow (part) 3505 1535 1820 1644 Peak-hour factor, PHF 0.92 0.92 0.95 0.95 0.79 0.79 0.74 0.74 0.74 Peak-hour factor, PHF 0.92 0.92 0.95 0.95 0.79 0.79 0.74 0.74 0.74 Peak-hour factor, PHF 0.92 0.92 0.95 0.95 0.79 0.79 0.79 0.74<	Future Volume (vph)	0	0	0	0	1698	38	250	34	0	0	0	60
Lane Util, Factor 0.95 1.00 1.00 1.00 Frpb, pedbikes 1.00 0.98 1.00 1.00 Fib, pedbikes 1.00 1.00 1.00 1.00 Fit 1.00 0.85 1.00 1.00 Fit 1.00 0.85 1.00 1.00 Fit Protected 1.00 1.00 0.96 1.00 Std. Flow (prot) 3505 1535 1820 1644 Peak-hour factor, PHF 0.92 0.92 0.95 0.95 0.79 0.79 0.74 0.74 0.74 RTOR Reductor (vph) 0 0 0 11 0 0 0 0 19 Lane Group Flow (vph) 0 0 0 1787 29 340 0 0 62 Contil. Peds. (#hr) - - 1 - - - - - - - - - - - - - -	Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Frpb, ped/bikes 1.00 0.98 1.00 1.00 Flpb, ped/bikes 1.00 1.00 1.00 1.00 Flt 1.00 0.85 1.00 0.86 Flt Protected 1.00 1.00 0.96 1.00 Stdt. Flow (port) 3505 1535 1820 1644 Flt Premitted 1.00 1.00 0.96 1.00 Stdt. Flow (port) 3505 1535 1820 1644 Flt Premitted 0.92 0.92 0.95 0.95 0.79 0.79 0.74 <td>Total Lost time (s)</td> <td></td> <td></td> <td></td> <td></td> <td>6.1</td> <td>6.1</td> <td></td> <td>5.9</td> <td></td> <td></td> <td></td> <td>5.9</td>	Total Lost time (s)					6.1	6.1		5.9				5.9
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Fri 1.00 0.85 1.00 0.86 FIt Protected 1.00 1.00 0.96 1.00 Std. Flow (prot) 3505 1535 1820 1644 Fit Protected 1.00 0.05 0.79 0.79 0.74 0.74 0.74 Std. Flow (prot) 0 0 0 1.00 0.96 1.00 1.04 Std. Flow (prot) 0 0.92 0.92 0.95 0.95 0.79 0.79 0.79 0.74 0.74 0.74 Adj. Flow (prh) 0 0 0 1.10 19 0 0 0 181 Lan Group Flow (ph) 0 0 0 1.787 40 316 43 0	Frpb, ped/bikes					1.00	0.98		1.00				1.00
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Fit Permitted 1.00 1.00 0.96 1.00 Satd. Flow (perm) 3505 1535 1820 1644 Peak-hour factor, PHF 0.92 0.92 0.95 0.95 0.79 0.79 0.74 0.74 0.74 Adj. Flow (vph) 0 0 0 1787 40 316 43 0 0 0 88 Adj. Flow (vph) 0 0 0 0 11 0 19 0 0 0 19 Lane Group Flow (vph) 0 0 0 0 1787 29 0 340 0 0 0 19 Lane Group Flow (vph) 0 0 0 0 1787 29 0 340 0 0 0 69 Confl. Peds. (#/hr)	Flt Protected					1.00	1.00		0.96				1.00
Fit Permitted 1.00 1.00 0.96 1.00 Satd. Flow (perm) 3505 1535 1820 1644 Peak-hour factor, PHF 0.92 0.92 0.92 0.95 <t< td=""><td>Satd. Flow (prot)</td><td></td><td></td><td></td><td></td><td>3505</td><td>1535</td><td></td><td>1820</td><td></td><td></td><td></td><td>1644</td></t<>	Satd. Flow (prot)					3505	1535		1820				1644
Peak-hour factor, PHF 0.92 0.92 0.92 0.95 0.95 0.79 0.79 0.74						1.00	1.00		0.96				1.00
Peak-hour factor, PHF 0.92 0.92 0.92 0.95 0.95 0.79 0.79 0.74	Satd. Flow (perm)					3505	1535		1820				1644
Adj. Flow (vph) 0 0 0 1787 40 316 43 0 0 0 11 RTOR Reduction (vph) 0 0 0 11 0 19 0 0 0 19 Lane Group Flow (vph) 0 0 0 1787 29 0 340 0 0 0 622 Confl. Peds. (#hr) 1 <td< td=""><td></td><td>0.92</td><td>0.92</td><td>0.92</td><td>0.95</td><td>0.95</td><td>0.95</td><td>0.79</td><td>0.79</td><td>0.79</td><td>0.74</td><td>0.74</td><td>0.74</td></td<>		0.92	0.92	0.92	0.95	0.95	0.95	0.79	0.79	0.79	0.74	0.74	0.74
RTOR Reduction (vph) 0 0 0 0 1 0 19 0 0 0 62 Confi. Peds. (#hr) 1													
Lane Group Flow (vph) 0 0 0 1787 29 0 340 0 0 0 62 Confl. Peds. (#/hr) 1 1 1 1 1 1 1 Heavy Vehicles (%) 2% 2% 2% 3% 3% 0%	2 (1)												
Confl. Peds. (#/hn) 1 Heavy Vehicles (%) 2% 2% 3% 3% 0%													
Heavy Vehicles (%) 2% 2% 3% 3% 3% 0%	,												
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Protected Phases 2! 4 Permitted Phases 2 4 21 4 Actuated Green, G (s) 68.9 68.9 39.1 39.1 Effective Green, g (s) 68.9 68.9 39.1 39.1 Actuated g/C Ratio 0.57 0.33 0.33 Clearance Time (s) 6.1 6.1 5.9 5.9 Vehicle Extension (s) 3.0 3.0 3.0 3.0 3.0 Lane Grp Cap (vph) 2012 881 593 535 v/s Ratio Prot c0.51 v/s Ratio Perm 0.02 0.19 0.04 v/c Ratio 0.89 0.03 0.57 0.12 Uniform Delay, d1 22.2 11.1 33.5 28.3 Progression Factor 1.00 1.00 1.48 1.00 Incremental Delay, d2 6.3 0.1 3.2 0.4 Delay (s) 28.5 11.2 53.0 28.8 Level of Service C B D C Approach LOS A C D C Intersec	· · · · ·												
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Actuated Green, G (s) 68.9 68.9 39.1 39.1 Effective Green, g (s) 68.9 68.9 39.1 39.1 Actuated g/C Ratio 0.57 0.57 0.33 0.33 Clearance Time (s) 6.1 6.1 5.9 5.9 Vehicle Extension (s) 3.0 3.0 3.0 3.0 Lane Grp Cap (vph) 2012 881 593 535 v/s Ratio Port c0.51						۲.	2	4 21	•				4
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Intersection Capacity Utilization 83.3% ICU Level of Service E Analysis Period (min) 15 ! Phase conflict between lane groups.	HCM 2000 Volume to Capacit	y ratio		0.77									
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				15									
c Critical Lane Group	! Phase conflict between lan	e groups											
	c Critical Lane Group												

Intersection: 10: EB Highland Road & WB-to-EB X/O

Movement	EB	EB	SB
Directions Served	Т	Т	L
Maximum Queue (ft)	298	363	61
Average Queue (ft)	157	169	42
95th Queue (ft)	254	287	66
Link Distance (ft)	708	708	35
Upstream Blk Time (%)			15
Queuing Penalty (veh)			29
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 11: WB-to-EB X/O & WB Highland Road

Movement	WB
Directions Served	L
Maximum Queue (ft)	109
Average Queue (ft)	26
95th Queue (ft)	83
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	325
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 20: Bogie Lake Road & EB Highland Road

Movement	EB	EB	EB	NB	NB	NB	SB
Directions Served	Т	Т	R	Т	R	R	Т
Maximum Queue (ft)	245	260	148	122	123	111	7
Average Queue (ft)	110	116	70	50	64	51	0
95th Queue (ft)	193	201	118	100	108	95	5
Link Distance (ft)	330	330	330	291	291	291	37
Upstream Blk Time (%)							0
Queuing Penalty (veh)							0
Storage Bay Dist (ft)							
Storage Blk Time (%)							
Queuing Penalty (veh)							

Intersection: 21: Bogie Lake Road & WB Highland Road

Movement	WB	WB	WB	SB	SB	SB
	т Т					
Directions Served			R		R	R
Maximum Queue (ft)	157	158	35	76	74	78
Average Queue (ft)	79	77	9	26	27	18
95th Queue (ft)	133	139	30	62	62	50
Link Distance (ft)	477	477	477	152	152	152
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)						
Storage Blk Time (%)						
Queuing Penalty (veh)						

Intersection: 30: EB-to-WB X/O/Nordic Drive & WB Highland Road

Management				ND	00
Movement	WB	WB	WB	NB	SB
Directions Served	Т	Т	R	LT	R
Maximum Queue (ft)	213	165	24	55	30
Average Queue (ft)	112	62	1	37	3
95th Queue (ft)	183	126	9	60	17
Link Distance (ft)	905	905		11	94
Upstream Blk Time (%)				17	
Queuing Penalty (veh)				30	
Storage Bay Dist (ft)			50		
Storage Blk Time (%)		8			
Queuing Penalty (veh)		1			
J I I					

Intersection: 31: EB Highland Road & EB-to-WB X/O

Movement	EB
Directions Served	L
Maximum Queue (ft)	113
Average Queue (ft)	31
95th Queue (ft)	85
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	300
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 40: Bogie Lake Road & NB-to-SB X/O

Movement	WB	SB
Directions Served	L	Т
Maximum Queue (ft)	20	52
Average Queue (ft)	1	7
95th Queue (ft)	10	32
Link Distance (ft)	28	192
Upstream Blk Time (%)	0	
Queuing Penalty (veh)	0	
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 41: Bogie Lake Road & NB-to-SB X/O

Movement	NB
Directions Served	L
Maximum Queue (ft)	6
Average Queue (ft)	0
95th Queue (ft)	4
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	300
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 50: W. Site Drive & EB Highland Road

Movement	NB
Directions Served	R
Maximum Queue (ft)	98
Average Queue (ft)	38
95th Queue (ft)	70
Link Distance (ft)	334
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 60: Bogie Lake Road & E. Site Drive

Movement	EB	NB
Directions Served	LR	LT
Maximum Queue (ft)	60	38
Average Queue (ft)	18	4
95th Queue (ft)	47	23
Link Distance (ft)	294	343
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Zone Summary

Zone wide Queuing Penalty: 60

Intersection: 10: EB Highland Road & WB-to-EB X/O

Movement	EB	EB	SB
Directions Served	Т	Т	L
Maximum Queue (ft)	258	265	63
Average Queue (ft)	147	130	48
95th Queue (ft)	232	234	63
Link Distance (ft)	708	708	35
Upstream Blk Time (%)			25
Queuing Penalty (veh)			67
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 11: WB-to-EB X/O & WB Highland Road

Movement	WB
	VVD
Directions Served	L
Maximum Queue (ft)	156
Average Queue (ft)	45
95th Queue (ft)	122
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	325
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 20: Bogie Lake Road & EB Highland Road

Movement	EB	EB	EB	NB	NB	NB	SB
Directions Served	Т	Т	R	Т	R	R	Т
Maximum Queue (ft)	210	217	78	219	171	146	5
Average Queue (ft)	110	112	38	109	78	58	0
95th Queue (ft)	178	185	67	185	130	104	4
Link Distance (ft)	330	330	330	291	291	291	37
Upstream Blk Time (%)	0	0					0
Queuing Penalty (veh)	0	0					0
Storage Bay Dist (ft)							
Storage Blk Time (%)							
Queuing Penalty (veh)							

Intersection: 21: Bogie Lake Road & WB Highland Road

Movement	WB	WB	WB	SB	SB	SB
Directions Served	Т	Т	R	Т	R	R
Maximum Queue (ft)	488	475	134	105	100	101
Average Queue (ft)	313	308	28	41	46	41
95th Queue (ft)	457	449	85	89	88	83
Link Distance (ft)	477	477	477	152	152	152
Upstream Blk Time (%)	1	0		0		
Queuing Penalty (veh)	4	2		0		
Storage Bay Dist (ft)						
Storage Blk Time (%)						
Queuing Penalty (veh)						

Intersection: 30: EB-to-WB X/O/Nordic Drive & WB Highland Road

Movement	WB	WB	WB	NB	SB
Directions Served	Т	Т	R	LT	R
Maximum Queue (ft)	572	527	200	48	76
Average Queue (ft)	346	309	26	47	28
95th Queue (ft)	494	463	117	53	65
Link Distance (ft)	905	905		11	94
Upstream Blk Time (%)				54	0
Queuing Penalty (veh)				154	0
Storage Bay Dist (ft)			50		
Storage Blk Time (%)		32	0		
Queuing Penalty (veh)		12	0		

Intersection: 31: EB Highland Road & EB-to-WB X/O

Movement	EB	EB
	ED	ED
Directions Served	L	Т
Maximum Queue (ft)	296	85
Average Queue (ft)	167	3
95th Queue (ft)	260	61
Link Distance (ft)		518
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)	300	
Storage Blk Time (%)	0	
Queuing Penalty (veh)	3	

Intersection: 40: Bogie Lake Road & NB-to-SB X/O

Movement	WB	SB	SB
Directions Served	1	<u>т</u>	<u>т</u>
	L	1	1
Maximum Queue (ft)	22	44	6
Average Queue (ft)	2	7	0
95th Queue (ft)	12	30	4
Link Distance (ft)	28	192	192
Upstream Blk Time (%)	0		
Queuing Penalty (veh)	0		
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 41: Bogie Lake Road & NB-to-SB X/O

Movement	NB
Directions Served	L
Maximum Queue (ft)	6
Average Queue (ft)	0
95th Queue (ft)	4
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	300
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 50: W. Site Drive & EB Highland Road

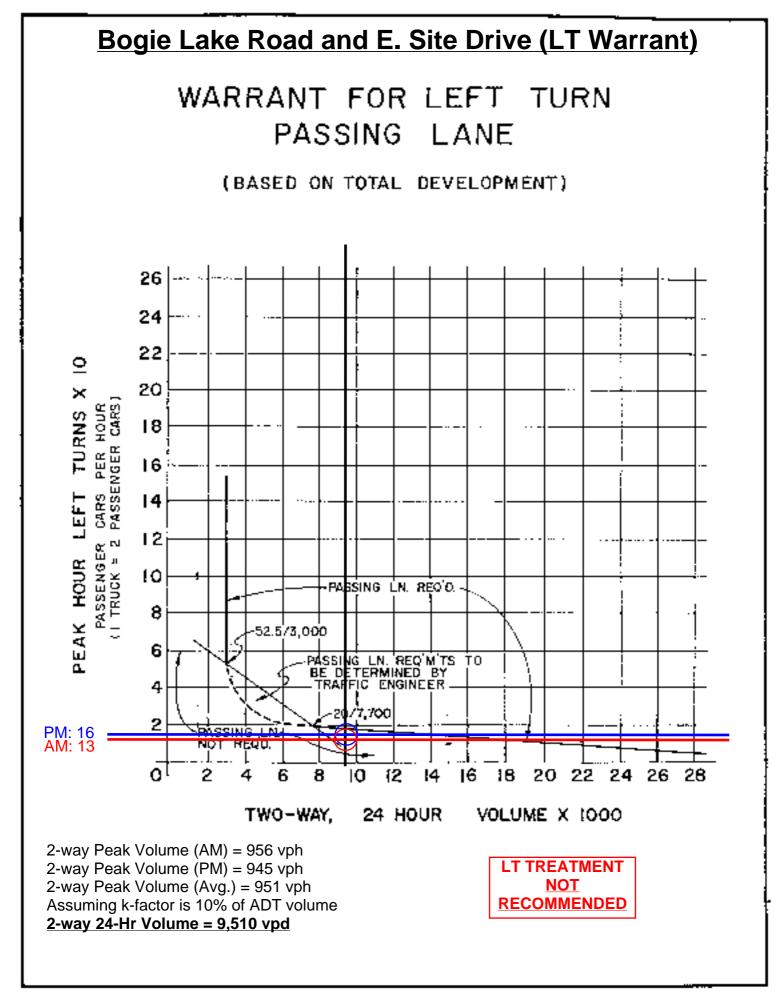
Movement	EB	EB	NB
Directions Served	Т	TR	R
Maximum Queue (ft)	21	6	96
Average Queue (ft)	1	0	39
95th Queue (ft)	11	4	72
Link Distance (ft)	348	348	334
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 60: Bogie Lake Road & E. Site Drive

LR	LT
44	68
16	9
43	42
294	343
	44 16 43

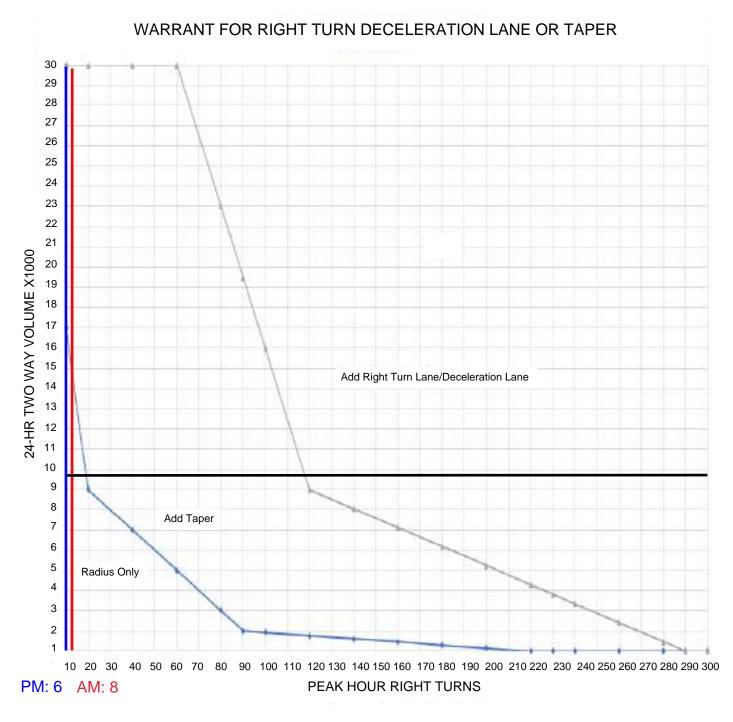
Zone Summary

Zone wide Queuing Penalty: 242



Bogie Lake Road and E. Site Drive (RT Warrant)

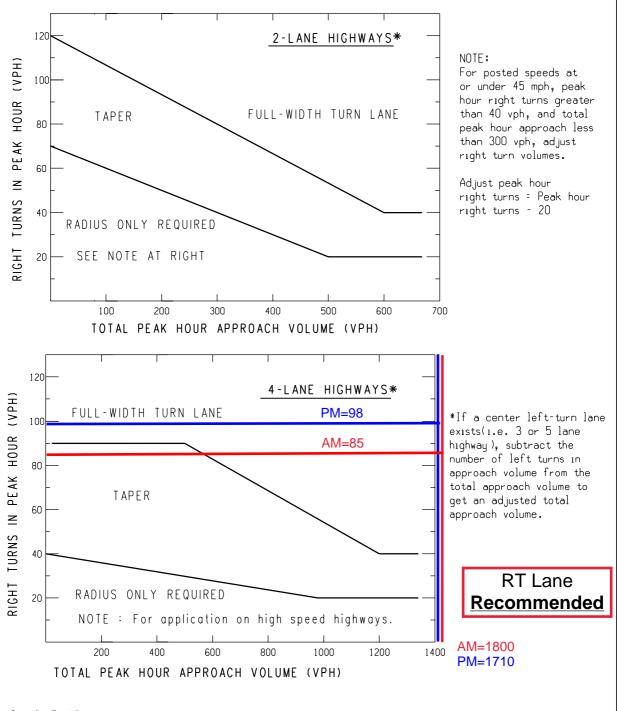
FIGURE 6-3



2-way Peak Volume (AM) = 956 vph 2-way Peak Volume (PM) = 945 vph 2-way Peak Volume (Avg.) = 951 vph Assuming k-factor is 10% of ADT volume **2-way 24-Hr Volume = 9,510 vpd**

RT TREATMENT <u>NOT</u> <u>RECOMMENDED</u>

Highland Road (M-59) and W. Site Drive (RT Warrant)



Sample Problem:

The Design Speed is 55 mph. The Peak Hour Approach Volume is 300 vph. The Number of Right Turns in the Peak Hour is 100 vph. Determine if a right turn lane is recommended.

<u>Solution</u>:

Figure indicates that the intersection of 300 vph and 100 vph is located above the upper trend line; thus, a right-turn lane may be recommended.

Michigan Department of Transportation					
TRAFFIC AND SAFETY					

TRAFFIC VOLUME GUIDELINES FOR RIGHT-TURN LANES AND TAPERS

NOTE			
DRAWN BY: MTS	08/05/2004	C04A	SHEET
CHECKED BY: JAT	PLAN DATE:	604A	2 OF 2
FILE: K:/DGN/ts notes/N	REV.08/05/2004		

Coffee Shop Drive Through Lane

Volume =

service rate =

95th Percentile Probability - Drive Through Queue Length (# of Vehicles)

70 vph

60 veh/hr

		$\lambda =$ 1.166667									
		1	2	3	4	5	6	7	8	9	
λ ^ x		No Veh in Cycle X		X!	$P = (e^{(-\lambda)})(\lambda^{x})/X!$	ΣΡ	P* # Cycle containing Volume in 1	Σ Cycles in 6	Volume in Cycle (1*6)	Σ volume	Poisson Queue
	1.0000	0	0	1	31.14%	31.14%	19	19	0	0	NO
	1.1667	1	1	1	36.33%	67.47%	22	40	22	22	NO
	1.3611	2	2	2	21.19%	88.66%	13	11	25	47	NO
	1.5880	3	3	6	8.24%	96.91%	5	16	15	62	NO
	1.8526	4	4	24	2.40%	99.31%	1	17	6	68	NO
	2.1614	5	5	120	0.56%	99.87%	0	18	2	70	MET
	2.5216	6	6	720	0.11%	99.98%	0	18	0	70	MET
	2.9419	7	7	5040	0.02%	100.00%	0	18	0	70	MET
	3.4322	8	8	40320	0.00%	100.00%	0	18	0	70	MET
	4.0042	9	9	362880	0.00%	100.00%	0	18	0	70	MET
	4.6716	10	10	3628800	0.00%	100.00%	0	18	0	70	MET
	5.4502	11	11	39916800	0.00%	100.00%	0	18	0	70	MET

Fast-Food Restaurant Drive Through Lane

Volume =

service rate =

95th Percentile Probability - Drive Through Queue Length (# of Vehicles)

49 vph

90 veh/hr

	$\lambda = 0.544444$									
	1	2	3	4	5	6	7	8	9	
λ ^ x	No Veh in Cycle		X!	$P = (e^{(-\lambda)})(\lambda^{x})/X!$	ΣΡ	P* # Cycle containing Volume in 1	Σ Cycles in 6	Volume ir Cycle (1*6)	η Σ volume	Poisson Queue
1.0000	0 0	0	1	58.02%	58.02%	52	52	0	0	NO
0.5444	4 1	1	1	31.59%	89.60%	28	81	28	28	NO
0.2964	4 2	2	2	8.60%	98.20%	8	11	15	44	NO
0.1614	4 3	3	6	1.56%	99.76%	1	12	4	48	NO
0.0879	9 4	4	24	0.21%	99.97%	0	13	1	49	MET
0.0478	85	5	120	0.02%	100.00%	0	13	0	49	MET
0.0260	D 6	6	720	0.00%	100.00%	0	13	0	49	MET
0.0142	2 7	7	5040	0.00%	100.00%	0	13	0	49	MET
0.0077	7 8	8	40320	0.00%	100.00%	0	13	0	49	MET
0.0042	2 9	9	362880	0.00%	100.00%	0	13	0	49	MET
0.0023	3 10	10	3628800	0.00%	100.00%	0	13	0	49	MET
0.0012	2 11	11	39916800	0.00%	100.00%	0	13	0	49	MET

PROPERTY DESCRIPTION:

DESCRIPTION OF COMBINED PARCEL, AS SURVEYED BY KIEFT ENGINEERING, INC., JOB NO. KE 2012.247, DATED 1-30-13, AS SHOWN ON SURVEY BY ALPINE ENGINEERING, INC., JOB NO. 15-113, DATED 2-10-15:

PART OF THE NORTH 1/2 OF THE SOUTHEAST 1/4 OF SECTION 20. T3N-R8E. WHITE OAKLAND CÓUNTY, MICHIGAN, DESCRIBED AS BEGINNING AT A POINT ON THE SOUTH RIGHT-OF-WAY LINE OF HIGHLAND ROAD (M-59, 70 FOOT HALF WIDTH) LOCATED S88'58'48"E 1032.50 FEET AND S01°25'12"W 70.00 FEET FROM THE CENTER OF SECTION 20. T3N-R8E: THEN S88'58'48"F 480.35 FEFT TO A POINT ON THE WESTERLY RIGHT-OF-WAY LINE OF BOGIE LAKE ROA THENCE ALONG SAID WESTERLY RIGHT-OF-WAY LINE ON A CURVE TO THE RIGHT 119.37 FEE CURVE HAVING A RADIUS OF 356.47 FEET. A DELTA OF 19°11'09" AND A LONG CHORD OF S18*14'12"W 118.81 FEET; THENCE S27*49'46"W 242.55 FEET; THENCE ALONG ON A CURVE T LEFT 127.93 FEFT, SAID CURVE HAVING A RADIUS OF 1060.72 FEFT, A DELTA OF 06'54'37" AND A LONG CHORD OF S23*39'55"W 127.85 FEET; S01*58'42"W 203.96 FEET: THENCE N88*58'48"W 287.74 FEET; THENCE N01°25'12"E 652.00 FEET TO THE POINT OF BEGINNING. SUBJECT TO THE RIGHTS OF THE PUBLIC IN BOGIE LAKE ROAD. CONTAINING 5.36 ACRES.

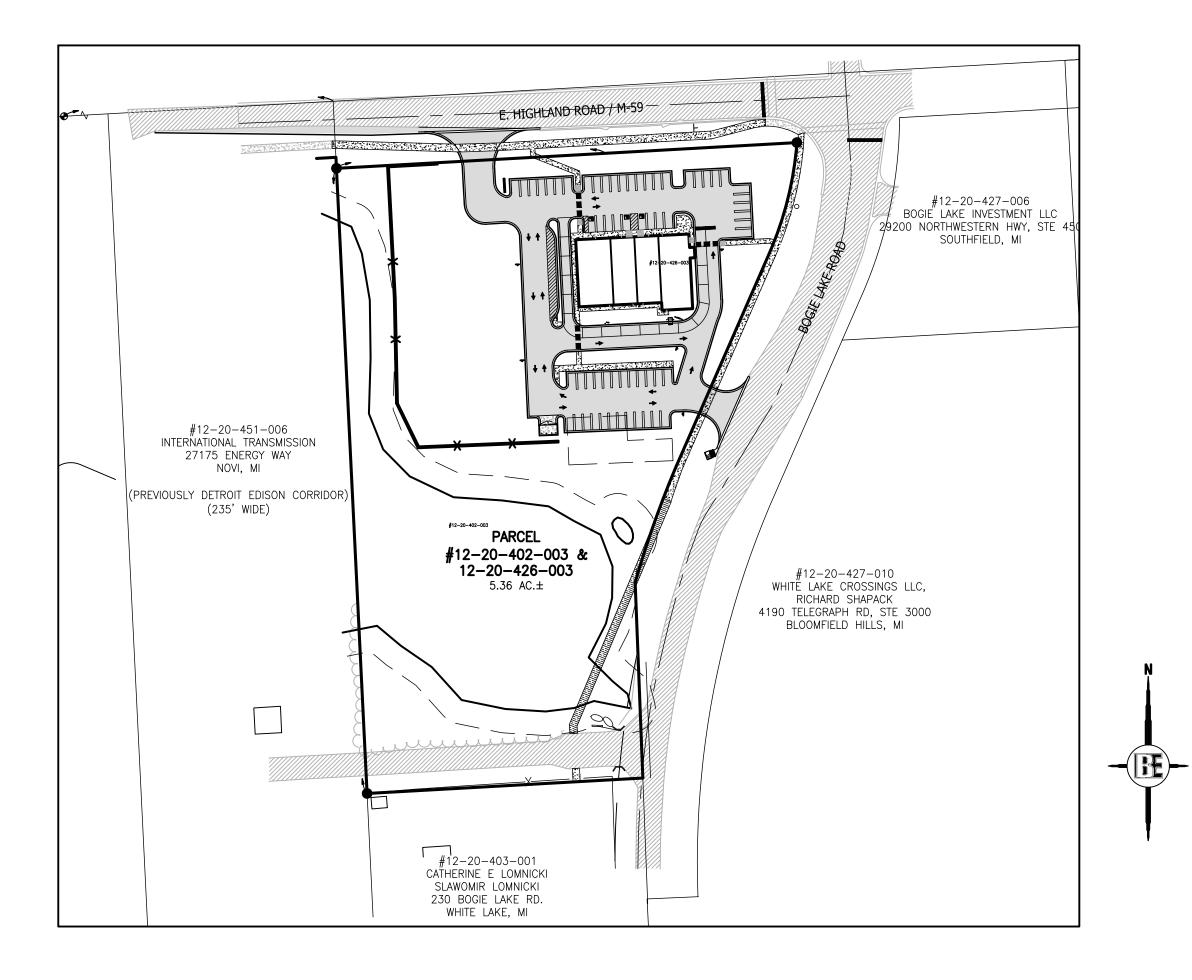
CONSTRUCTION NOTES

- THE CONTRACTOR SHALL COMPLY WITH THE FOLLOWING NOTES AND ANY WORK INVOLVED SHALL BE CONSIDERED INCIDENTAL TO THE CONTRACT 1. THE CONTRACTOR SHALL HOLD HARMLESS THE DESIGN PROFESSIONAL, MUNICIPALITY, COUNTY, STATE AND ALL OF ITS SUB CONSULTANTS, PUBLIC AND PRIVATE UTILITY COMPANIES, AND LANDOWNERS FOR DAMAGES TO INDIVIDUALS AND PROPERTY, REAL OR OTHERWISE, DUE TO THE OPERATIONS
- OF THE CONTRACTOR AND/OR THEIR SUBCONTRACTORS. 2. A GRADING PERMIT FOR SOIL EROSION-SEDIMENTATION CONTROL SHALL BE OBTAINED FROM THE GOVERNING AGENCY PRIOR TO THE START OF CONSTRUCTION.
- 3. IF DUST PROBLEM OCCURS DURING CONSTRUCTION, CONTROL WILL BE PROVIDED BY AN APPLICATION OF WATER, EITHER BY SPRINKLER OR TANK TRUCK
- 4. ALL CONSTRUCTION AND MATERIALS SHALL BE IN ACCORDANCE WITH LOCAL MUNICIPAL STANDARDS AND SPECIFICATIONS.
- 5. THE CONTRACTOR IS RESPONSIBLE FOR OBTAINING ALL REQUIRED TOWNSHIP, COUNTY, AND STATE OF MICHIGAN PERMITS 6. PAVED SURFACES, WALKWAYS, SIGNS, LIGHTING AND OTHER STRUCTURES SHALL BE MAINTAINED IN A SAFE, ATTRACTIVE CONDITION AS ORIGINALLY DESIGNED AND CONSTRUCTED
- 7. ALL BARRIER-FREE FEATURES SHALL BE CONSTRUCTED TO MEET ALL LOCAL, STATE AND A.D.A. REQUIREMENTS. 8. ANY DISCREPANCY IN THIS PLAN AND ACTUAL FIELD CONDITIONS SHALL BE REPORTED TO THE DESIGN ENGINEER PRIOR TO THE START OF
- CONSTRUCTION. CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFICATION OF ALL SETBACKS, EASEMENTS AND DIMENSIONS SHOWN HEREON BEFORE BEGINNING CONSTRUCTION. THE CONTRACTOR SHALL CONTACT ALL OWNERS OF EASEMENTS, UTILITIES AND RIGHTS-OF-WAY, PUBLIC OR PRIVATE, PRIOR TO THE START OF
- CONSTRUCTION. 10. THE CONTRACTOR SHALL COORDINATE WITH ALL OWNERS TO DETERMINE THE LOCATION OF EXISTING LANDSCAPING, IRRIGATION LINES & PRIVATE
- UTILITY LINES. THE CONTRACTOR IS RESPONSIBLE FOR ANY DAMAGE TO EXISTING LANDSCAPING, IRRIGATION LINES, AND PRIVATE UTILITY LINES. 11. THE CONTRACTOR SHALL REMOVE ALL TRASH AND DEBRIS FROM THE SITE UPON COMPLETION OF THE PROJECT. 12. THE CONTRACTOR SHALL MAINTAIN THE SITE IN A MANNER SO THAT WORKMEN AND PUBLIC SHALL BE PROTECTED FROM INJURY, AND ADJOINING PROPERTY PROTECTED FROM DAMAGE.
- 13. THE CONTRACTOR SHALL KEEP THE AREA OUTSIDE THE "CONSTRUCTION LIMITS" BROOM CLEAN AT ALL TIMES.
- 14. THE CONTRACTOR SHALL CALL MISS DIG A MINIMUM OF 72 HOURS PRIOR TO THE START OF CONSTRUCTION 15. ALL EXCAVATION UNDER OR WITHIN 3 FEET OF PUBLIC PAVEMENT, EXISTING OR PROPOSED SHALL BE BACKFILLED AND COMPACTED WITH SAND (MDOT CLASS II)
- 16. ALL PAVEMENT REPLACEMENT AND OTHER WORKS COVERED BY THESE PLANS SHALL BE DONE IN ACCORDANCE WITH THE REQUIREMENTS OF THE TOWNSHIP, INCLUDING THE LATEST MICHIGAN DEPARTMENT OF TRANSPORTATION (MDOT) SPECIFICATIONS FOR HIGHWAY CONSTRUCTION. 17. THE CONTRACTOR IS RESPONSIBLE FOR ALL DAMAGE TO EXISTING UTILITIES.
- 18. NO ADDITIONAL COMPENSATION WILL BE PAID TO THE CONTRACTOR FOR ANY DELAY OR INCONVENIENCE DUE TO THE MATERIAL SHORTAGES OR RESPONSIBLE DELAYS DUE TO THE OPERATIONS OF SUCH OTHER PARTIES DOING WORK INDICATED OR SHOWN ON THE PLANS OR IN THE SPECIFICATION OR FOR ANY REASONABLE DELAYS IN CONSTRUCTION DUE TO THE ENCOUNTERING OR EXISTING UTILITIES THAT MAY OR MAY NOT BE SHOWN ON THE PLANS.
- 19. DURING THE CONSTRUCTION OPERATIONS, THE CONTRACTOR SHALL NOT PERFORM WORK BY PRIVATE AGREEMENT WITH PROPERTY OWNERS ADJACENT TO THE PROJECT.
- 20. IF WORK EXTENDS BEYOND NOVEMBER 15, NO COMPENSATION WILL BE DUE TO THE CONTRACTOR FOR ANY WINTER PROTECTION MEASURES THAT MAY BE REQUIRED BY THE ENGINEER.
- 21. NO TREES ARE TO BE REMOVED UNTIL MARKED IN THE FIELD BY THE ENGINEER.
- 22. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY DAMAGE TO THE PROPERTY BEYOND THE CONSTRUCTION LIMITS INCLUDING BUT NOT LIMITED TO EXISTING FENCE, LAWN, TREES AND SHRUBBERY. 23. ALL AREAS DISTURBED BY THE CONTRACTOR BEYOND THE NORMAL CONSTRUCTION LIMITS OF THE PROJECT SHALL BE SODDED OR SEEDED AS
- SPECIFIED OR DIRECTED BY THE ENGINEER. 24. ALL ROOTS, STUMPS AND OTHER OBJECTIONABLE MATERIALS SHALL BE REMOVED AND THE HOLE BACKFILLED WITH SUITABLE MATERIAL. WHERE
- GRADE CORRECTION IS REQUIRED, THE SUBGRADE SHALL BE CUT TO CONFORM TO THE CROSS-SECTION AS SHOWN IN THE PLANS. 25. TRAFFIC SHALL BE MAINTAINED DURING CONSTRUCTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROVIDING ALL SIGNS AND TRAFFIC CONTROL DEVICES. FLAG PERSONS SHALL BE PROVIDED BY THE CONTRACTOR IF DETERMINED NECESSARY BY THE ENGINEER. ALL SIGNS SHALL CONFORM TO THE MICHIGAN MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES AT NO COST TO THE TOWNSHIP. NO WORK SHALL BE DONE UNLESS THE APPROPRIATE TRAFFIC CONTROL DEVICES ARE IN PLACE.
- 26. ALL DEMOLISHED MATERIALS AND SOIL SPOILS SHALL BE REMOVED FROM THE SITE AT NO ADDITIONAL COST, AND DISPOSED OF IN ACCORDANCE WITH LOCAL, STATE AND FEDERAL REGULATIONS.
- 27. AFTER REMOVAL OF TOPSOIL, THE SUBGRADE SHALL BE COMPACTED TO 95% OF ITS UNIT WEIGHT. 28. ALL GRADING IN THE PLANS SHALL BE DONE AS PART OF THIS CONTRACT. ALL DELETERIOUS MATERIAL SHALL BE REMOVED FROM THE SUBGRADE PRIOR TO COMPACTING
- 29. NO SEEDING SHALL BE DONE AFTER OCTOBER 15 WITHOUT APPROVAL OF THE ENGINEER. 30. ANY EXISTING APPURTENANCES SUCH AS MANHOLES, GATE VALVES, ETC. SHALL BE ADJUSTED TO THE PROPOSED GRADE AND SHALL BE
- CONSIDERED INCIDENTAL TO THE CONTRACT. 31. SOIL EROSION MEASURES SHALL BE MAINTAINED BY THE CONTRACTOR UNTIL VEGETATION HAS BEEN RE-ESTABLISHED.
- 32. ALL PERMANENT SIGNS AND PAVEMENT MARKINGS SHALL BE INSTALLED IN ACCORDANCE WITH THE LATEST REVISION OF THE MICHIGAN MUTCD MANUAL AND SHALL BE INCIDENTAL TO THE CONTRACT.

INDEMNIFICATION STATEMENT

THE CONTRACTOR SHALL HOLD HARMLESS THE DESIGN PROFESSIONAL, MUNICIPALITY, COUNTY, STATE AND ALL OF ITS SUB CONSULTANTS, PUBLIC AND PRIVATE UTILITY COMPANIES, AND LANDOWNERS FOR DAMAGES TO INDIVIDUALS AND PROPERTY, REAL OR OTHERWISE, DUE TO THE OPERATIONS OF THE CONTRACTOR AND/OR THEIR SUBCONTRACTORS.

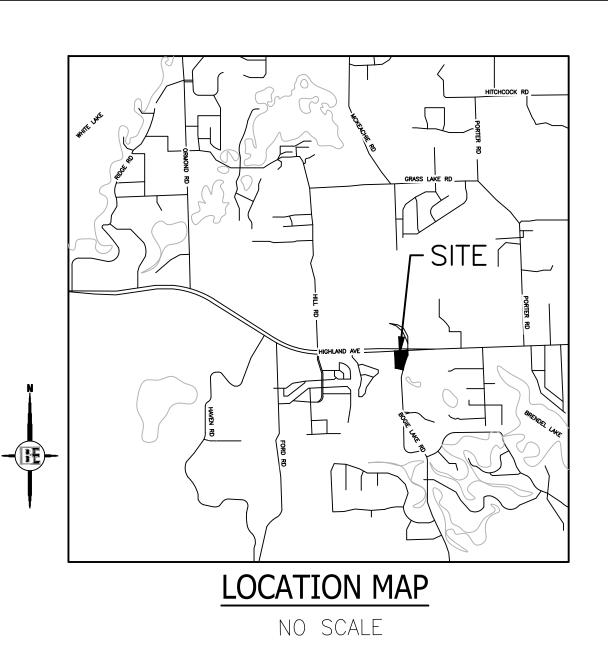
PRELIMINARY SITE PLAN FOR GATEWAY CROSSING PART OF NORTHEAST QUARTER OF SOUTHEAST QUARTER, SECTION 20 WHITE LAKE TOWNSHIP, OAKLAND COUNTY, MICHIGAN



OVERALL	SITE	MAP

1" = 100'

PERMITS & APPROVALS		
AGENCY	DATE SUBMITTED	DATE APPROVED
TOWNSHIP ENGINEERING APPROVAL	_	-
• RCOC	_	_
• SESC	—	—
• MDEGLE ACT 399	—	—
MDEGLE PART 41	—	—
 MDEGLE WETLANDS 	—	—



	SHEET INDEX
SHEET NO.	DESCRIPTION
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	COVER GENERAL NOTES & LEGEND EXISTING CONDITIONS & DEMOLITION PLAN SITE PLAN UTILITY PLAN GRADING PLAN DRAINAGE PLAN SESC PLAN DETENTION BASIN DETAILS CONTECH UNDERGROUND DETAILS CONSTRUCTION DETAILS TOWNSHIP STORM SEWER DETAILS TOWNSHIP SANITARY DETAILS TOWNSHIP WATERMAIN DETAILS WRC SESC DETAILS
SHEET NO.	DRAWINGS BY DETROIT ARCHITECTURAL GROUP
PP-4 PP-4.1	MULTI–TENANT BUILDING PRELIMINARY FLOOR PLAN & DETAILS MULTI–TENANT BUILDING PRELIMINARY ELEVATIONS

PREPARED FOR:

PREPARED BY:

GATEWAY CROSSING, LLC 600 N. OLD WOODWARD, SUITE 101 BIRMINGHAM, MI 48009 **BRIAN NAJOR** 248.433.7000 BRIAN@NAJORCOMPANIES.COM

Engineering

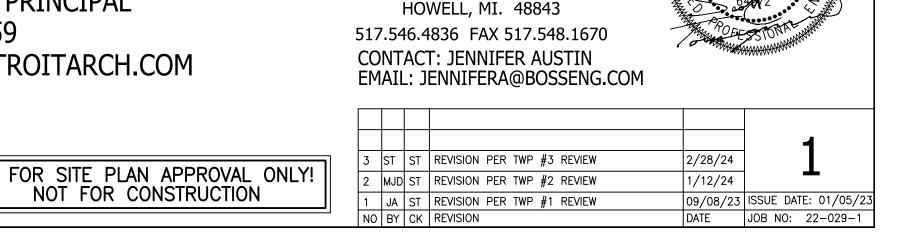
Engineers Surveyors Planners Landscape Architects

3121 E. GRAND RIVER AVE.

ARCHITECT:

DETROIT ARCHITECTURAL GROUP 1644 FORD AVENUE WYANDOTTE, MI 48192 JAKE ROOT, PRINCIPAL 734-556-3259 JROOT@DETROITARCH.COM

NOT FOR CONSTRUCTION



SCOTT T TOUSIGNANT

ENGINEER

GENERAL NOTES

- 1. THE CONTRACTOR IS RESPONSIBLE FOR OBTAINING ALL REQUIRED TOWNSHIP, COUNTY, AND STATE OF MICHIGAN PERMITS.
- 2. A GRADING PERMIT FOR SOIL EROSION-SEDIMENTATION CONTROL SHALL BE OBTAINED FROM THE GOVERNING AGENCY PRIOR TO THE START OF CONSTRUCTION.
- 3. IF DUST PROBLEM OCCURS DURING CONSTRUCTION, CONTROL WILL BE PROVIDED BY AN APPLICATION OF WATER, EITHER BY SPRINKLER OR TANK TRUCK.
- 4. ALL CONSTRUCTION AND MATERIALS SHALL BE IN ACCORDANCE WITH LOCAL MUNICIPAL STANDARDS AND SPECIFICATIONS.
- 5. PAVED SURFACES, WALKWAYS, SIGNS, LIGHTING AND OTHER STRUCTURES SHALL BE MAINTAINED IN A SAFE, ATTRACTIVE CONDITION AS ORIGINALLY DESIGNED AND CONSTRUCTED.
- 6. ALL BARRIER-FREE FEATURES SHALL BE CONSTRUCTED TO MEET ALL LOCAL, STATE AND A.D.A. REQUIREMENTS. WHERE EXISTING CONDITIONS AND/OR THE REQUIREMENTS OF THE PLANS WILL RESULT IN FINISHED CONDITIONS THAT DO NOT MEET ADA REQUIREMENTS, THE CONTRACTOR SHALL NOTIFY THE DESIGN ENGINEER PRIOR TO WORK COMMENCING.
- 7. ANY DISCREPANCY IN THIS PLAN AND ACTUAL FIELD CONDITIONS SHALL BE REPORTED TO THE DESIGN ENGINEER PRIOR TO THE START OF CONSTRUCTION. CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFICATION OF ALL SETBACKS, EASEMENTS AND DIMENSIONS SHOWN HEREON PRIOR TO BEGINNING CONSTRUCTION.
- 8. THE CONTRACTOR SHALL CONTACT ALL OWNERS OF EASEMENTS, UTILITIES AND RIGHT-OF-WAY, PUBLIC OR PRIVATE, PRIOR TO THE START OF CONSTRUCTION.
- 9. THE CONTRACTOR SHALL COORDINATE WITH ALL OWNERS TO DETERMINE THE LOCATION OF EXISTING LANDSCAPING, IRRIGATION LINES & PRIVATE UTILITY LINES. THE CONTRACTOR IS RESPONSIBLE FOR ANY DAMAGE TO EXISTING LANDSCAPING, IRRIGATION LINES, AND PRIVATE UTILITY LINES.
- 10. THE CONTRACTOR SHALL REMOVE ALL TRASH AND DEBRIS FROM THE SITE UPON COMPLETION OF THE PROJECT. 11. THE CONTRACTOR SHALL MAINTAIN THE SITE IN A MANNER SO THAT WORKMEN AND PUBLIC SHALL BE PROTECTED FROM INJURY, AND ADJOINING PROPERTY PROTECTED FROM DAMAGE.
- 12. THE CONTRACTOR SHALL KEEP THE AREA OUTSIDE THE "CONSTRUCTION LIMITS" BROOM CLEAN AT ALL TIMES.
- 13. THE CONTRACTOR SHALL CALL MISS DIG A MINIMUM OF 72 HOURS PRIOR TO THE START OF CONSTRUCTION.
- 14. ALL PAVEMENT REPLACEMENT AND OTHER WORKS COVERED BY THESE PLANS SHALL BE DONE IN ACCORDANCE WITH THE REQUIREMENTS OF THE TOWNSHIP, INCLUDING THE LATEST MICHIGAN DEPARTMENT OF TRANSPORTATION (MDOT) SPECIFICATIONS FOR HIGHWAY CONSTRUCTION.
- 15. THE CONTRACTOR IS RESPONSIBLE FOR ALL DAMAGE TO EXISTING UTILITIES.
- 16. NO ADDITIONAL COMPENSATION WILL BE PAID TO THE CONTRACTOR FOR ANY DELAY OR INCONVENIENCE DUE TO THE MATERIAL SHORTAGES OR RESPONSIBLE DELAYS DUE TO THE OPERATIONS OF SUCH OTHER PARTIES DOING WORK INDICATED OR SHOWN ON THE PLANS OR IN THE SPECIFICATION OR FOR ANY REASONABLE DELAYS IN CONSTRUCTION DUE TO THE ENCOUNTERING OR EXISTING UTILITIES THAT MAY OR MAY NOT BE SHOWN ON THE PLANS.
- 17. DURING THE CONSTRUCTION OPERATIONS, THE CONTRACTOR SHALL NOT PERFORM WORK BY PRIVATE AGREEMENT WITH PROPERTY OWNERS ADJACENT TO THE PROJECT.
- 18. IF WORK EXTENDS BEYOND NOVEMBER 15, NO COMPENSATION WILL BE DUE TO THE CONTRACTOR FOR ANY WINTER PROTECTION MEASURES THAT MAY BE REQUIRED BY THE ENGINEER.
- 19. NO TREES ARE TO BE REMOVED UNTIL MARKED IN THE FIELD BY THE ENGINEER.
- 20. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY DAMAGE TO THE PROPERTY BEYOND THE CONSTRUCTION LIMITS INCLUDING BUT NOT LIMITED TO EXISTING FENCE, LAWN, TREES AND SHRUBBERY.
- 21. TRAFFIC SHALL BE MAINTAINED DURING CONSTRUCTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROVIDING ALL SIGNS AND TRAFFIC CONTROL DEVICES. FLAG PERSONS SHALL BE PROVIDED BY THE CONTRACTOR IF DETERMINED NECESSARY BY THE ENGINEER. ALL SIGNS SHALL CONFORM TO THE MICHIGAN MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES AT NO COST TO THE TOWNSHIP. NO WORK SHALL BE DONE UNLESS THE APPROPRIATE TRAFFIC CONTROL DEVICES ARE IN PLACE.
- 22. ALL DEMOLISHED MATERIALS AND SOIL SPOILS SHALL BE REMOVED FROM THE SITE AT NO ADDITIONAL COST, AND DISPOSED OF IN ACCORDANCE WITH LOCAL, STATE AND FEDERAL REGULATIONS.
- 23. ANY EXISTING APPURTENANCES SUCH AS MANHOLES, GATE VALVES, ETC. SHALL BE ADJUSTED TO THE PROPOSED GRADE AND SHALL BE CONSIDERED INCIDENTAL TO THE CONTRACT.
- 24. ALL PERMANENT SIGNS AND PAVEMENT MARKINGS SHALL BE INSTALLED IN ACCORDANCE WITH THE LATEST REVISION OF THE MICHIGAN MUTCD MANUAL AND SHALL BE INCIDENTAL TO THE CONTRACT.
- 25. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO ENSURE THAT ALL ITEMS REQUIRED FOR CONSTRUCTION OF THE PROJECT ARE INCLUDED IN THE CONTRACT. ANY ITEMS NOT SPECIFICALLY DESIGNATED IN THE PLANS SHALL BE ONSIDERED INCIDENTAL TO THE CONTRACT
- 26. THE CONTRACTOR IS RESPONSIBLE FOR HAVING A SET OF APPROVED CONSTRUCTION PLANS, WITH THE LATEST REVISION DATE, ON SITE PRIOR TO THE START OF CONSTRUCTION, IN THE EVENT OF ANY QUESTIONS PERTAINING TO THE INTENT OF THE CONSTRUCTION PLANS OR SPECIFICATIONS, THE CONTRACTOR SHALL CONTACT THE DESIGN ENGINEER FOR A FINAL DETERMINATION FROM THE DESIGN ENGINEER.
- 27. THE CONTRACTOR, NOT THE OWNER OR THE ENGINEER, ARE RESPONSIBLE FOR THE MEANS, METHODS, AND SEQUENCE OF CONSTRUCTION. THE CONTRACTOR IS RESPONSIBLE FOR SAFE EXECUTION OF THE PROJECT SCOPE IN ACCORDANCE WITH THE APPROVED CONSTRUCTION PLANS.
- 28. THE CONTRACTOR IS RESPONSIBLE FOR PRESERVING CONSTRUCTION STAKING AS NECESSARY, CONTRACTOR TO NOTIFY CONSTRUCTION SURVEYOR OF REPLACEMENT STAKES NEEDED WHICH SHALL BE AT THE CONTRACTORS EXPENSE.
- 29. THE OWNER AND/OR CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATING FRANCHISE UTILITY SERVICES (CABLE, ELECTRIC, GAS, ETC.) OWNER AND/OR CONTRACTOR SHALL WORK WITH UTILITY COMPANIES ON FURNISHING SITE UTILITY LAYOUTS AND PROVIDING CONDUIT CROSSINGS AS REQUIRED.
- 30. DAMAGE TO ANY EXISTING UTILITIES OR INFRASTRUCTURE (INCLUDING PAVEMENT, CURB, SIDEWALK, ETC.) SHALL PROMPTLY BE REPLACED IN KIND AND SHALL BE AT THE CONTRACTORS EXPENSE.
- 31. COORDINATION OF TESTING SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR AND PER ALL CITY/TOWNSHIP/COUNTY REQUIREMENTS. COPIES OF ALL TEST REPORTS SHALL BE FURNISHED TO THE DESIGN ENGINEER.
- 32. PRIOR TO THE START OF CONSTRUCTION, PROTECTION FENCING SHALL BE ERECTED AROUND THE TREE DRIPLINE OF ANY TREES INDICATED TO BE SAVED WITHIN THE LIMITS OF DISTURBANCE.
- 33. THE CONTRACTOR SHALL MAINTAIN DRAINAGE OF THE PROJECT AREA AND ADJACENT AREAS. WHERE EXISTING DRAINAGE FACILITIES ARE IMPACTED/DISTURBED DUE TO CONSTRUCTION, THE CONTRACTOR SHALL PROVIDE ANY NECESSARY TEMPORARY DRAINAGE PROVISIONS.
- 34. SOIL BORING LOGS ARE REPRESENTATIVE OF SPECIFIC POINTS ON THE PROJECT SITE, AND IF PROVIDED TO THE CONTRACTOR ARE FOR INFORMATIONAL PURPOSES ONLY.
- 35. WHERE CITY/TOWNSHIP STANDARD CONSTRUCTION DETAILS/SPECIFICATIONS ARE PROVIDED AND ARE IN CONFLICT WITH NOTES AND SPECIFICATIONS HEREIN, THE CITY/TOWNSHIP STANDARD SHALL GOVERN.

INDEMNIFICATION STATEMENT

THE CONTRACTOR SHALL HOLD HARMLESS THE DESIGN PROFESSIONAL, MUNICIPALITY, COUNTY, STATE, AND ALL OF ITS SUB CONSULTANTS, PUBLIC AND PRIVATE UTILITY COMPANIES, AND LANDOWNERS FOR DAMAGES TO INDIVIDUALS AND PROPERTY, REAL OR OTHERWISE, DUE TO THE OPERATIONS OF THE CONTRACTOR AND/OR THEIR SUBCONTRACTORS.

CONTRACTOR TO FOLLOW MANUFACTURER SPECS/RECOMMENDATIONS THAT SUPERCEDE PLANS

GENERAL GRADING & SESC NOTES

- SCOPE OF WORK
- ALTERNATIVE SESC MEASURES BE UTILIZED.
- MATERIALS, DEBRIS, ETC ARE CONTAINED ON-SITE.
- LINE.
- ESTABLISHED WITH ACCEPTABLE AMOUNT OF VEGETATIVE GROUND COVER.
- SODDED OR SEEDED AS SPECIFIED OR DIRECTED BY THE ENGINEER.

FROM THE SUBGRADE PRIOR TO COMPACTING.

- AS SHOWN IN THE PLANS.
- COMPACTED WITH SAND (MDOT CLASS II).

GENERAL LANDSCAPE NOTES

- PLANT MATERIAL SHALL BE SUBJECT TO THE APPROVAL OF THE LANDSCAPE ARCHITECT.

- INGREDIENTS SHALL BE THOROUGHLY BLENDED FOR UNIFORM CONSISTENCY.
- CIRCLE OF MULCH AND CONIFER TREES 8-FT (PLANTED CROWN OF TREE) UNLESS OTHERWISE NOTED.
- APPLICATION.
- 9. THE CONTRACTOR SHALL GUARANTEE ALL PLANT MATERIALS FOR A PERIOD OF 1 YEAR FROM THE DATE THE WORK IS SHALL CONFORM TO THE ORIGINAL SPECIFICATIONS.
- IN STRAIGHT LINES OR SMOOTH CURVES WITHOUT IRREGULARITIES.
- 36-HOURS AFTER CUTTING.

IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO ESTABLISH A DENSE LAWN OF PERMANENT GRASSES, FREE OF LUMPS AND DEPRESSIONS. ALL SODDED AREAS THAT BROWN-OUT OR HAVE NOT FIRMLY KNITTED TO THE SOIL BASE WITHIN A PERIOD OF 1 MONTH SHALL BE REPLACED BY THE CONTRACTOR, AT NO COST TO THE OWNER.

LANDSCAPED, OR SODDED SHALL BE SEEDED AND MULCHED.

SEED MIXTURE SHALL BE AS FOLLOWS: KENTUCKY BLUEGRASS (CHOOSE 3 VARIETIES -ADELPHI, RUGBY, GLADE, OR PARADE) RUBY RED OR DAWSON RED FINE FESCUE ATLANTA RED FESCUE PENNFINE PERENNIAL RYE

THE ABOVE SEED MIXTURE SHALL BE SOWN AT A RATE OF 250 LBS PER ACRE. PRIOR TO SEEDING, THE TOPSOIL SHALL BE FERTILIZED WITH A COMMERCIAL FERTILIZER WITH A 10-0-10 ANALYSIS:

10% NITROGEN - MIN 25% FROM A UREA FORMALDEHYDE SOURCE 0 % PHOSPHATE 10% POTASH - SOURCE POTASSIUM SULFATE OR POTASSIUM NITRATE

THE FIRST FERTILIZER APPLICATION SHALL BE AT A RATE OF 10 LBS PER 1000 SQ FT OF BULK FERTILIZER.

IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO ESTABLISH A DENSE LAWN OF PERMANENT GRASSES, FREE OF LUMPS AND DEPRESSIONS. ANY PART OF THE AREA THAT FAILS TO SHOW A UNIFORM GERMINATION SHALL BE RE-SEEDED AND SUCH RE-SEEDING SHALL CONTINUE UNTIL A DENSE LAWN IS ESTABLISHED. DAMAGE TO SEEDED AREAS RESULTING FROM EROSION SHALL BE REPAIRED BY THE CONTRACTOR.

- ARCHITECT OF ANY CONFLICTS PRIOR TO COMMENCING LANDSCAPING.

GENERAL UTILITY NOTES

- MDOT CLASS II GRANULAR MATERIAL ONLY FOR WATERMAIN.

- THICKNESS. COMPACTION SHALL BE 95% AS DETERMINED BY AASHTO T99.
- SANITARY/STORM SEWER TO THE MAXIMUM EXTENT POSSIBLE.

1. THE CONTRACTOR SHALL HAVE IN PLACE ALL REQUIRED EROSION CONTROL METHODS AS INDICATED ON THE CONSTRUCTION PLANS AND AS REQUIRED BY GENERAL PRACTICE, SPECIFIC MEANS, METHODS AND SEQUENCES OF CONSTRUCTION MAY DICTATE ADDITIONAL SOIL EROSION CONTROL MEASURES BE NEEDED. THE CONTRACTOR SHALL COORDINATE WITH THE DESIGN ENGINEER ON THESE ANTICIPATED METHODS. ADDITIONAL SOIL EROSION CONTROL METHODS SHALL BE INCIDENTAL TO THE

2. ACTUAL FIELD CONDITIONS MAY DICTATE ADDITIONAL OR ALTERNATE SOIL EROSION CONTROL MEASURES BE UTILIZED. THE CONTRACTOR SHALL NOTIFY THE ENGINEER OF ANY DEFICIENCIES OR FIELD CONDITIONS THAT WARRANT ADDITIONAL AND/OR

3. AT THE CLOSE OF EACH DAY, THE CONTRACTOR SHALL BE RESPONSIBLE FOR ENSURING ALL CONSTRUCTION OPERATIONS,

4. AT THE CLOSE OF EACH WORKING DAY, ALL DRAINAGE STRUCTURES SHALL BE FREE OF DIRT AND DEBRIS AT THE FLOW

5. ALL SOIL EROSION CONTROL MEASURES SHALL BE INSTALLED IN ACCORDANCE PER MDEGLE REGULATIONS AND BEST PRACTICES, ALL SOIL EROSION CONTROL MEASURES SHALL BE MAINTAINED BY THE CONTRACTOR.

6. THE SOIL EROSION CONTROL MEASURES SHALL BE KEPT IN PLACE UNTIL SUCH A TIME THAT THE SITE IS DETERMINED TO BE

7. ALL AREAS DISTURBED BY THE CONTRACTOR BEYOND THE NORMAL CONSTRUCTION LIMITS OF THE PROJECT SHALL BE

8. AFTER REMOVAL OF TOPSOIL, THE SUBGRADE SHALL BE COMPACTED TO 95% OF ITS UNIT WEIGHT.

9. ALL GRADING IN THE PLANS SHALL BE DONE AS PART OF THIS CONTRACT. ALL DELETERIOUS MATERIAL SHALL BE REMOVED

10. ALL ROOTS, STUMPS AND OTHER OBJECTIONABLE MATERIALS SHALL BE REMOVED AND THE HOLE BACKFILLED WITH SUITABLE MATERIAL. WHERE GRADE CORRECTION IS REQUIRED, THE SUBGRADE SHALL BE CUT TO CONFORM TO THE CROSS-SECTION

11. ALL EXCAVATION UNDER OR WITHIN 3 FEET OF PUBLIC PAVEMENT, EXISTING OR PROPOSED SHALL BE BACKFILLED AND

1. ALL PLANT MATERIAL SHALL CONFORM TO THE REQUIREMENTS AND SPECIFICATIONS OF THE GOVERNING MUNICIPALITY. ALL STOCK SHALL BE NURSERY GROWN, CONFORMING TO ANSI Z60.1 "AMERICAN STANDARD FOR NURSERY STOCK", AND IN ACCORDANCE WITH GOOD HORTICULTURAL PRACTICE. STOCK SHALL EXHIBIT NORMAL GROWTH HABIT AND BE FREE OF DISEASE, INSECTS, EGGS, LARVAE, & DEFECTS SUCH AS KNOTS, SUN-SCALD, INJURIES, ABRASIONS, OR DISFIGUREMENT. ALL

2. ALL PLANT MATERIALS SHALL BE BALLED AND BURLAPPED OR CONTAINER STOCK. NO BARE ROOT STOCK IS PERMITTED. ALL PLANT BALLS SHALL BE FIRM, INTACT, AND SECURELY WRAPPED AND BOUND.

3. ALL PLANT BED MATERIALS SHALL BE EXCAVATED OF ALL BUILDING MATERIALS, OTHER EXTRANEOUS OBJECTS, AND POOR SOILS TO A MINIMUM DEPTH OF 12-INCHES AND BACKFILLED TO GRADE WITH SPECIFIED PLANTING MIX (SEE BELOW).

4. PLANTING MIXTURE SHALL CONSIST OF 5 PARTS TOPSOIL FROM ON-SITE (AS APPROVED), 4 PARTS COARSE SAND, 1 PART SPHAGNUM PEAT MOSS (OR APPROVED COMPOST), AND 5 LBS OF SUPERPHOSPHATE FERTILIZER PER CU. YD. OF MIX.

5. ALL PLANT BEDS AND INDIVIDUAL PLANTS, NOT OTHERWISE NOTED SHALL BE MULCHED WITH A 4-INCH LAYER OF SHREDDED BARK MULCH. EDGE OF MULCH BEDS AS SHOWN. DECIDUOUS TREES IN LAWN AREAS SHALL RECEIVE A 5-FT DIAMETER

6. LANDSCAPE STONE SHALL BE INSTALLED WHERE NOTED OR INDICATED (HATCHED). STONE SHALL BE 3/4"-1-1/4" WASHED RIVER GRAVEL OR AS SELECTED AND SHALL BE INSTALLED TO A MINIMUM DEPTH OF 3-INCHES.

ALL LANDSCAPE BEDS, UNLESS OTHERWISE NOTED SHALL BE INSTALLED OVER WEED BARRIER FABRIC - WATER PERMEABLE FILTRATION FABRIC OF NON-WOVEN POLYPROPYLENE OR POLYESTER FABRIC. FABRIC SHALL BE OF SUITABLE THICKNESS FOR

8. ALL PLANTS AND PLANT BEDS SHALL BE THOROUGHLY WATERED UPON COMPLETION OF PLANTING AND STAKING OPERATIONS.

ACCEPTED, IN WRITING, BY THE LANDSCAPE ARCHITECT. THE CONTRACTOR SHALL REPLACE, WITHOUT COST TO THE OWNER, WITHIN A SPECIFIED PERIOD OF TIME, ALL DEAD PLANTS, AND ALL PLANTS NOT IN A VIGOROUS, THRIVING CONDITION, AS DETERMINED BY THE LANDSCAPE ARCHITECT, DURING AND AT THE END OF THE GUARANTEE PERIOD. REPLACEMENT STOCK

10. EDGING SHALL BE PROVIDED FOR ALL LANDSCAPE BEDS NOT ADJACENT TO CONCRETE PAVEMENT. EDGING SHALL BE BLACK ALUMINUM EDGING, 3/16-INCH X 4-INCH. INSTALL PER MANUFACTURER'S INSTRUCTIONS, ALL EDGING SHALL BE INSTALLED

11. SOD SHALL BE DENSE, WELL ROOTED TURF, FREE OF WEEDS. IT SHALL BE COMPRISED OF A BLEND OF AT LEAST TWO KENTUCKY BLUE GRASSES AND ONE FESCUE. IT SHALL HAVE A UNIFORM THICKNESS OF 3/4-INCH AT TIME OF PLANTING, AND CUT IN UNIFORM STRIPS NOT LESS THAN 10-INCHES BY 18-INCHES. SOD SHALL BE KEPT MOIST AND LAID WITHIN

12. ALL AREAS OF THE SITE THAT BECOME DISTURBED DURING CONSTRUCTION AND ARE NOT TO BE PAVED, STONED,



13. ALL AREAS OF THE SITE SCHEDULED FOR SEEDING OR SODDING SHALL FIRST RECEIVE A 6-INCH LAYER OF CLEAN, FRIABLE TOPSOIL. THE SOIL SHALL BE DISCED AND SHALL BE GRADED IN CONFORMANCE WITH THE GRADING PLAN.

14. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THE LOCATION OF ALL UTILITIES AND TO INFORM THE LANDSCAPE

BEDDING SHALL EXTEND A MINIMUM OF 4" BELOW THE PIPE, UNLESS OTHERWISE NOTED ON THE PLANS. BEDDING SHALL BE OF UNIFORM GRADATION MDOT 6AA STONE OR MDOT CLASS II GRANULAR MATERIAL FOR SANITARY AND STORM PIPE AND

2. WHERE UNSTABLE GROUND CONDITIONS ARE ENCOUNTERED, STONE BEDDING SHALL BE USED AS DIRECTED BY THE ENGINEER. 3. BACKFILL SHALL BE OF A SUITABLE MATERIAL AND SHALL BE FREE OF ANY ORGANIC MATERIALS AND ROCKS.

4. BACKFILL ABOVE THE PIPE SHALL BE OF GRANULAR MATERIAL MDOT CLASS II TO A POINT 12" ABOVE THE TOP OF THE PIPE. WHERE THE TRENCH IS NOT WITHIN THE INFLUENCE OF THE ROAD, SUITABLE SITE MATERIAL MAY BE COMPACTED AND UTILIZED FROM A POINT 12" ABOVE THE PIPE TO GRADE. WHERE THE TRENCH IS WITHIN A 1:1 INFLUENCE OF THE ROAD, GRANULAR MATERIAL, MDOT CLASS II OR III, IS TO BE PLACED AND COMPACTED IN LAYERS NOT EXCEEDING 12" IN

5. 18" MINIMUM VERTICAL SEPARATION AND 10' HORIZONTAL SEPARATION IS TO BE MAINTAINED BETWEEN WATERMAIN AND

GENERAL STORM NOTES

1. ALL STORM PIPE LENGTHS ARE SHOWN FROM C/L TO C/L OF STRUCTURE OR FROM C/L OF STRUCTURE TO DISCHARGE END OF FLARED END SECTION.

2. STORM PIPE MATERIALS SHALL BE AS FOLLOWS:

- RCP(REINFORCED CONCRETE PIPE): SHALL MEET THE REQUIREMENTS OF ASTM C76 WITH MODIFIED GROOVED 2.1. TONGUE AND RUBBER GASKETS MEETING THE REQUIREMENTS OF ASTM C443. RCP TO BE EITHER CLASS IV OR V
- AS CALLED OUT ON THE PLANS. 2.2. HDPE(HIGH DENSITY POLYETHYLENE): SHALL MEET THE REQUIREMENTS OF ASTM F2648
- 2.3. PP(POLYPROPYLENE): SHALL MEET THE REQUIREMENTS OF ASTM F2881. 2.4. PVC(POLYVINYL CHLORIDE): SHALL MEET THE REQUIREMENTS OF ASTM D3034.
- 3. STORM PIPE JOINTS SHALL MEET THE REQUIREMENTS OF ASTM D3212. HDPE AND PP PIPE GASKETS SHALL MEET THE REQUIREMENTS OF ASTM F477.
- 4. ALL STORM PIPE TO HAVE WATERTIGHT PREMIUM JOINTS, UNLESS OTHERWISE NOTED ON THE PLANS.
- 5. STORM DRAINAGE STRUCTURES SHALL BE FURNISHED WITH STEPS WHICH SHALL BE STEEL ENCASED WITH POLYPROPYLENE PLASTIC OR EQUIVALENT. STEPS SHALL BE SET AT 16" CENTER TO CENTER.
- 6. ALL FLARED END SECTIONS 15" AND LARGER SHALL BE FURNISHED WITH AN ANIMAL GRATE.
- 7. FLARED END SECTIONS DISCHARGING STORM WATER SHALL RECEIVE A MINIMUM OF 10 SQ YDS OF PLAIN COBBLESTONE RIP RAP WITH A MINIMUM STONE SIZE OF 6" AND SHALL BE PLACED ON A GEOTEXTILE FABRIC WRAP.
- 8. ALL CATCH BASINS WITHIN THE ROADWAY SHALL INCLUDE INSTALLATION OF 6" DIAMETER PERFORATED PIPE SUBDRAIN.
- 9. STORM DRAINAGE STRUCTURE COVERS SHALL BE OF THE FOLLOWING (OR APPROVED EQUAL):

COVER	USE	FRAME	GRATE/BACK
'A'	MANHOLE	1040	TYPE 'B'
'В'	TYPE B2 CURB	7085	TYPE 'M1'
'C'	VALLEY CURB	7065	7045 TYPE 'M1' GRATE/7060 TYPE 'T1' BACK
'D'	PARKING LOTS	1040/5100	TYPE 'M1' GRATE OR 5105 TYPE 'M1' GRATE
Έ'	LAWN	1040	TYPE '02' GRATE
'K'	TYPE C & F CURB	7045	TYPE 'M1' GRATE/7050 TYPE 'T1' BACK

GENERAL SANITARY NOTES

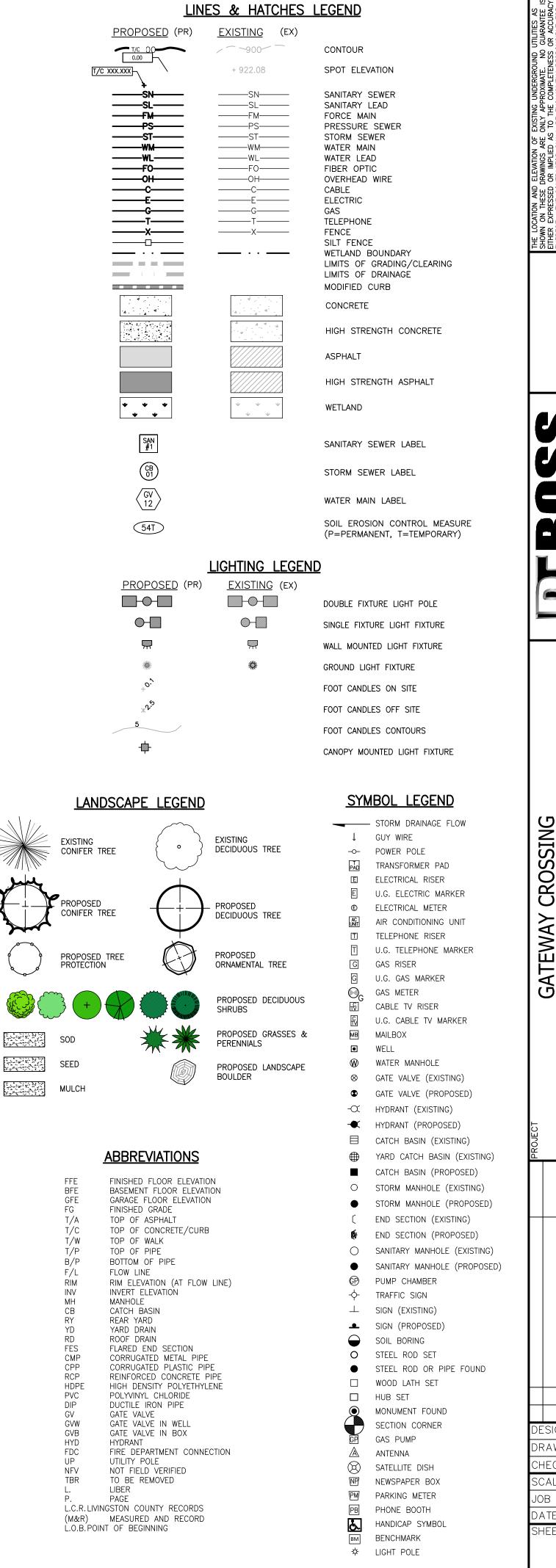
- 1. ALL SANITARY PIPE LENGTHS ARE SHOWN FROM C/L OF STRUCTURE TO C/L OF STRUCTURE
- 2. SANITARY PIPE MATERIALS SHALL BE AS FOLLOWS:

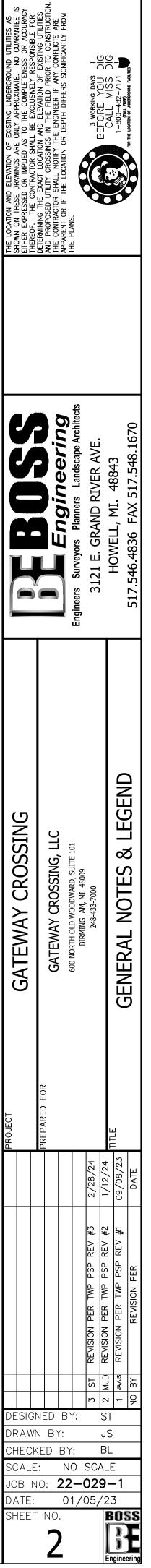
2.1. PVC SDR-26 (SANITARY MAIN) 2.2. PVC SDR-23.5 (SANITARY LEADS)

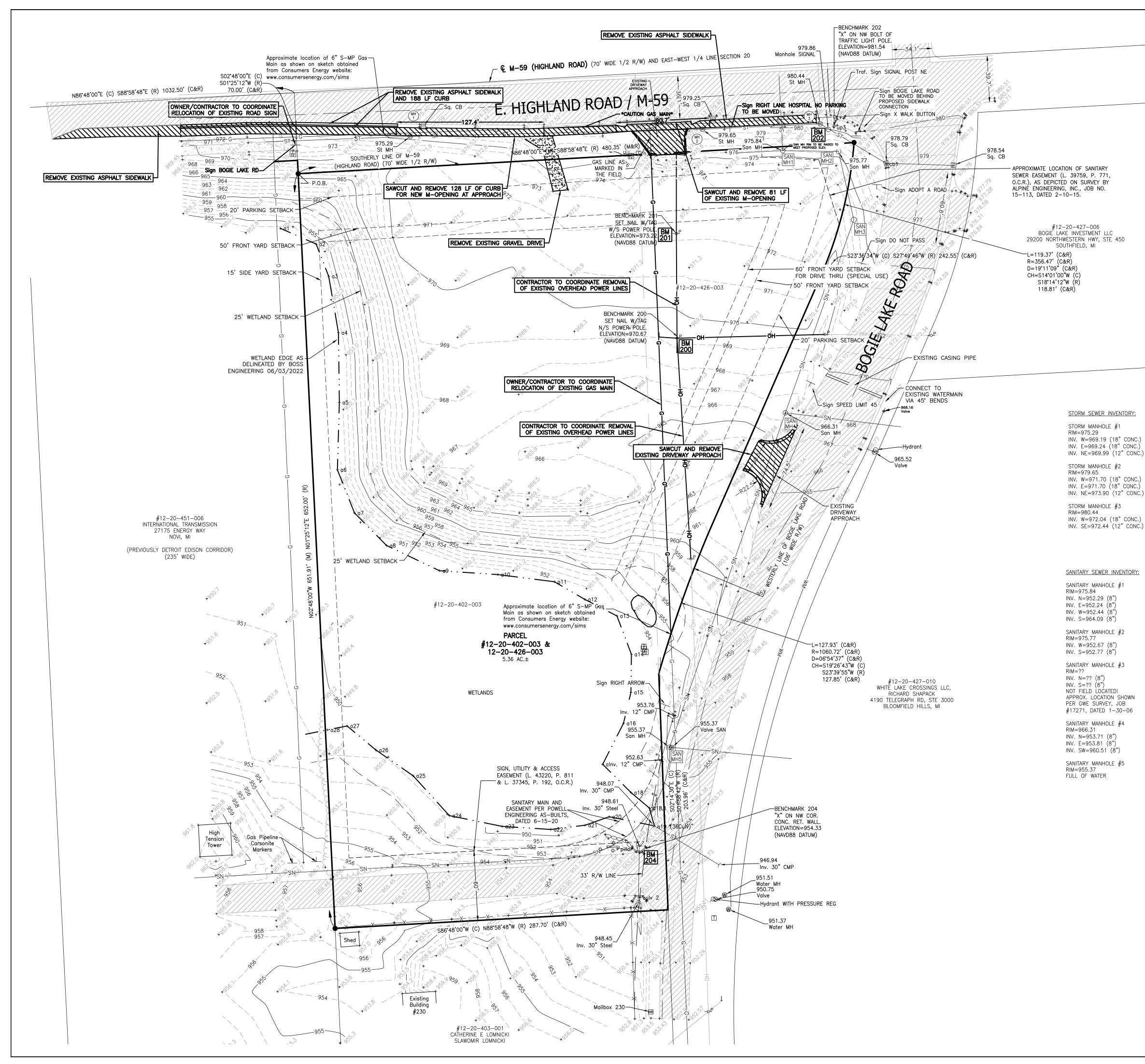
- 2.3. HDPE DR-11 (SANITARY FORCEMAIN)
- 3. ALL PVC SDR SANITARY SEWER PIPE SHALL MEET THE REQUIREMENTS OF ASTM D3034 AND D2241. PVC SCHD 40 PIPE SHALL MEET THE REQUIREMENTS OF ASTM D1785. GASKET JOINTS FOR SANITARY PIPE SHALL MEET THE REQUIREMENTS OF ASTM D3139 AND D3212.
- 4. SANITARY STRUCTURES SHALL BE FURNISHED WITH STEPS WHICH SHALL BE STEEL ENCASED WITH POLYPROPYLENE PLASTIC OR EQUIVALENT. STEPS SHALL BE SET AT 16" CENTER TO CENTER.
- 5. ALL NEW MANHOLES SHALL BE MINIMUM 4' DIAMETER, PRECAST MANHOLE SECTIONS AND AN ECCENTRIC CONE. PRECAST MANHOLE JOINTS SHALL BE INSTALLED WITH BUTYL ROPE MEETING THE REQUIREMENTS OF ASTM C990. 6.
- MANHOLES SHALL BE CONSTRUCTED WITH FLOW CHANNEL WALLS THAT ARE FORMER, AT A MINIMUM, TO THE SPRINGLINE OF THE PIPE. 7. ALL NEW MANHOLES SHALL HAVE AN APPROVED FLEXIBLE, WATERTIGHT SEALS WHERE PIPES PASS THROUGH MANHOLE
- WALLS. 8. WHEREVER AN EXISTING MANHOLE IS TO BE TAPPED, THE STRUCTURE SHALL BE CORED AND A KOR-N-SEAL BOOT UTILIZED FOR THE PIPE CONNECTION.
- 9. ALL MANHOLES SHALL BE PROVIDED WITH WATERTIGHT COVERS. COVERS TO BE EJCO 1040 TYPE 'A' SOLID COVER.
- 10. A MAXIMUM OF 12" OF GRADE ADJUSTMENT RINGS SHALL BE USED TO ADJUST THE FRAME ELEVATION. BUTYL ROPE
- SHALL BE USED BETWEEN EACH ADJUSTMENT RING.
- 11. SANITARY SEWER LATERALS SHALL HAVE A MINIMUM SLOPE OF 1.0%.
- 12. CLEANOUTS SHALL BE INSTALLED EVERY 100', AT ALL BENDS AND STUBS.
- 13. PUBLIC SANITARY SEWER SHALL BE CENTERED WITHIN A XX FOOT WIDE SANITARY SEWER EASEMENT

GENERAL WATERMAIN NOTES

- 1. WATERMAIN PIPE MATERIALS SHALL BE AS FOLLOWS:
- 1.1. D.I.P. CL.52 (WATERMAIN) 1.2. TYPE 'K' COPPER (WATER LATERAL – MAIN TO CURB STOP)
- 1.3. HDPE DR-9 (WATER LATERAL CURB STOP TO STUB)
- 2. WATERMAIN FITTINGS SHALL BE OF DUCTILE IRON WITH CEMENT MORTAR LINING AND MECHANICAL JOINTS CONFORMING TO AWWA C110.
- WATERMAINS SHALL BE DISINFECTED IN ACCORDANCE WITH AWWA C651. BAC-T SAMPLES SHALL BE TAKEN IN ACCORDANCE WITH R235.11110 OF THE ADMINISTRATIVE RULES PROMULGATED UNDER MICHIGAN SAFE DRINKING WATER ACT, 1976 PA 399, AS AMENDED.
- 4. ALLOWABLE LEAKAGE OR HYDROSTATIC PRESSURE TESTING SHALL BE IN ACCORDANCE WITH AWWA C600 AND C605.
- MAXIMUM DEFLECTION AT PIPE JOINTS SHALL BE IN ACCORDANCE WITH PIPE MANUFACTURERS CURRENT RECOMMENDATIONS AND AWWA SPECIFICATIONS
- 6. A FULL STICK OF PIPE SHALL BE LAID CENTERED AT A PIPE CROSSING IN ORDER TO MAINTAIN THE MAXIMUM SEPARATION OF WATERMAIN JOINT TO THE CROSSING PIPE.
- 7. WATERMAIN SHALL BE INSTALLED WITH A MINIMUM OF 5.5' OF COVER FROM FINISHED GRADE TO TOP OF PIPE AND NO MORE THAN 8' OF COVER, UNLESS SPECIAL CONDITIONS WARRANT.
- 8. WATERMAIN VALVES SHALL BE IRON BODY RESILIENT WEDGE GATE VALVES, NON-RISING STEMS, COUNTERCLOCKWISE OPEN, AWWA C509
- 9. FIRE HYDRANTS SHALL BE INSTALLED WITH AN AUXILIARY VALVE WITH CAST IRON VALVE BOX. THE HYDRANT PUMPER HOSE CONNECTION SHALL FACE THE ROADWAY.
- 10. THE BREAKAWAY FLANGE AND ALL BELOW GRADE FITTINGS SHALL HAVE STAINLESS STEEL NUTS AND BOLTS.
- 11. PUBLIC WATERMAIN SHALL BE CENTERED WITHIN A XX FOOT WIDE WATERMAIN EASEMENT.







<u>LEGEND</u> OM CTION. CTION. <u>EXISTING</u> (EX) <u>PROPOSED</u> (PR) -900-CONTOUR T/C SPOT ELEVATION + 922.08 XXX.XX FINISHED FLOOR ELEVATION FINISHED GRADE ELEVATION T/A T/A TOP OF ASPHALT T/C TOP OF CURB / CONCRETE T∕W T/W TOP OF WALK F/L FLOW LINE T/F T/P TOP OF PIPE B/P BOTTOM OF PIPE RIM ELEVATION INVERT ELEVATION MANHOLE STRUCTURE INLET STRUCTURE CATCHBASIN STRUCTURE REARYARD STRUCTURE END-SECTION GATEVALVE STRUCTURE HYDRANT UTILITY POLE SANITARY SEWER SANITARY LEAD SCALE: 1 INCH = 40 FEET FORCE MAIN ------PS------PRESSURE SEWER _____ST_____ STORM SEWER _____WM_____ WATER MAIN _____WI _____ WATER LEAD ——___FO_____ FIBER OPTIC OVERHEAD WIRE ____OH____ ____C____ CABLE ELECTRIC _____ GAS TELEPHONE _____T____ _____X_____ ____X____ FENCE _____O_____ SILT FENCE ___ · · · ___ WETLAND BOUNDARY LIMITS OF GRADING/CLEARING MANHOLE INLET / CATCHBASIN FLARED END-SECTION GATE VALVE **HYDRANT** UTILITY POLE NOT FIELD VERIFIED NFV TBR TO BE REMOVED SAN #1 SANITARY SEWER LABEL (CB 01 STORM SEWER LABEL $\left< \begin{array}{c} GV\\ 12 \end{array} \right>$ WATER MAIN LABEL SOIL EROSION CONTROL MEASURE 54T (P=PERMANENT, T=TEMPORARY) CONCRETE . 4 ASPHALT ____ MODIFIED CURB **GENERAL SURVEY NOTES:** BEARINGS ARE BASED ON MICHIGAN STATE PLANE COORDINATE SYSTEM, SOUTH SUBSURFACE UTILITIES NOT LOCATED FOR THIS SURVEY MAY EXIST. IT IS THE RESPONSIBILITY OF THE OWNER OF THE RESPECTIVE UTILITY TO ACCURATELY LOCATE SUCH UTILITIES. 3. EASEMENTS OR RESTRICTIONS OF RECORD NOT DEPICTED ON THIS DRAWING MAY FXIST 4. ELEVATIONS WERE ESTABLISHED WITH GPS USING OPUS GPS POST-PROCESSING. (NAVD88 DATUM) 5. CONTOURS ARE SHOWN AT 1 FOOT INTERVALS. 6. THE LOCATIONS OF UNDERGROUND UTILITIES, AS SHOWN ON THIS DRAWING ARE APPROXIMATE. THE LOCATIONS ARE BASED ON PHYSICAL FIELD LOCATIONS O STRUCTURES ALONG WITH MISS DIG MARKINGS AND DRAWINGS SUPPLIED BY WHITE LAKE TOWNSHIP. 7. ALL WORK SHALL BE IN ACCORDANCE WITH THE STANDARDS AND SPECIFICATIONS OF THE MUNICIPALITY, THE COUNTY, AND THE STATE OF MICHIGAN. 8. ALLOW THREE WORKING DAYS BEFORE YOU DIG, CALL MISS DIG TOLL FREE 1-800-482-7171. DESCRIPTION OF COMBINED PARCEL, AS SURVEYED BY KIEFT ENGINEERING, INC., JOB NO. KE 2012.247, DATED 1-30-13, AS SHOWN ON SURVEY BY ALPINE ENGINEERING, INC., JOB NO. 15–113, DATED 2–10–15: PART OF THE NORTH 1/2 OF THE SOUTHEAST 1/4 OF SECTION 20, T3N-R8E, WHITE LAKE TOWNSHIP, OAKLAND COUNTY, MICHIGAN, DESCRIBED AS BEGINNING AT A POINT ON THE SOUTH RIGHT-OF-WAY LINE OF HIGHLAND ROAD (M-59, 70 FOOT HALF WIDTH) LOCATED S88'58'48"E 1032.50 FEET AND S01°25'12"W 70.00 FEET FROM THE CENTER OF SECTION 20. T3N-R8E: THENCE S88*58'48"E 480.35 FEET TO A POINT ON THE WESTERLY RIGHT-OF-WAY LINE OF BOGIE LAKE ROAD; THENCE ALONG SAID WESTERLY RIGHT-OF-WAY LINE ON A CURVE TO THE RIGHT 119.37 FEET, SAID CURVE HAVING A RADIUS OF 356.47 FEET, A DELTA OF 19°11'09" AND A LONG CHORD OF S18*14'12"W 118.81 FEET: THENCE S27*49'46"W 242.55 FEET: THENCE ALONG ON A CURVE TO THE LEFT 127.93 FEET, SAID CURVE HAVING A RADIUS OF 1060.72 FEET, A DELTA OF 06'54'37" AND A LONG CHORD OF \$23*39'55"W 127.85 FEET; \$01*58'42"W 203.96 FEET: THENCE N88*58'48"W 287.70 FEET; THENCE NO1"25'12"E 652.00 FEET TO THE POINT OF BEGINNING. SUBJECT TO THE RIGHTS OF THE PUBLIC IN BOGIE LAKE ROAD. CONTAINING 5.36 ACRES.

SITE BENCHMARKS (NAVD88 DATUM): -BM #200 = SET NAIL WITH TAG N/S POWER POLE. ELEV.=970.67 -BM #201 = SET NAIL WITH TAG W/S POWER POLE. ELEV.=973.22 -BM #202 = "X" ON NW BOLT OF TRAFFIC LIGHT POLE. ELEV.=981.54

-BM #204 = "X" ON NW CORNER CONCRETE RETAINING WALL. ELEV.=954.33

WETLAND DELINEATION

A WETLAND DELINEATION WAS CONDUCTED ON 6-03-2022 IN ACCORDANCE WITH THE 1987 USCOE WETLAND DELINEATION MANUAL AND THE REGIONAL SUPPLEMENT FOR THE MIDWEST REGION AUGUST, 2010 AND/OR THE REGIONAL SUPPLEMENT FOR THE NORTHCENTRAL AND NORTHEAST REGION JANUARY, 2012.

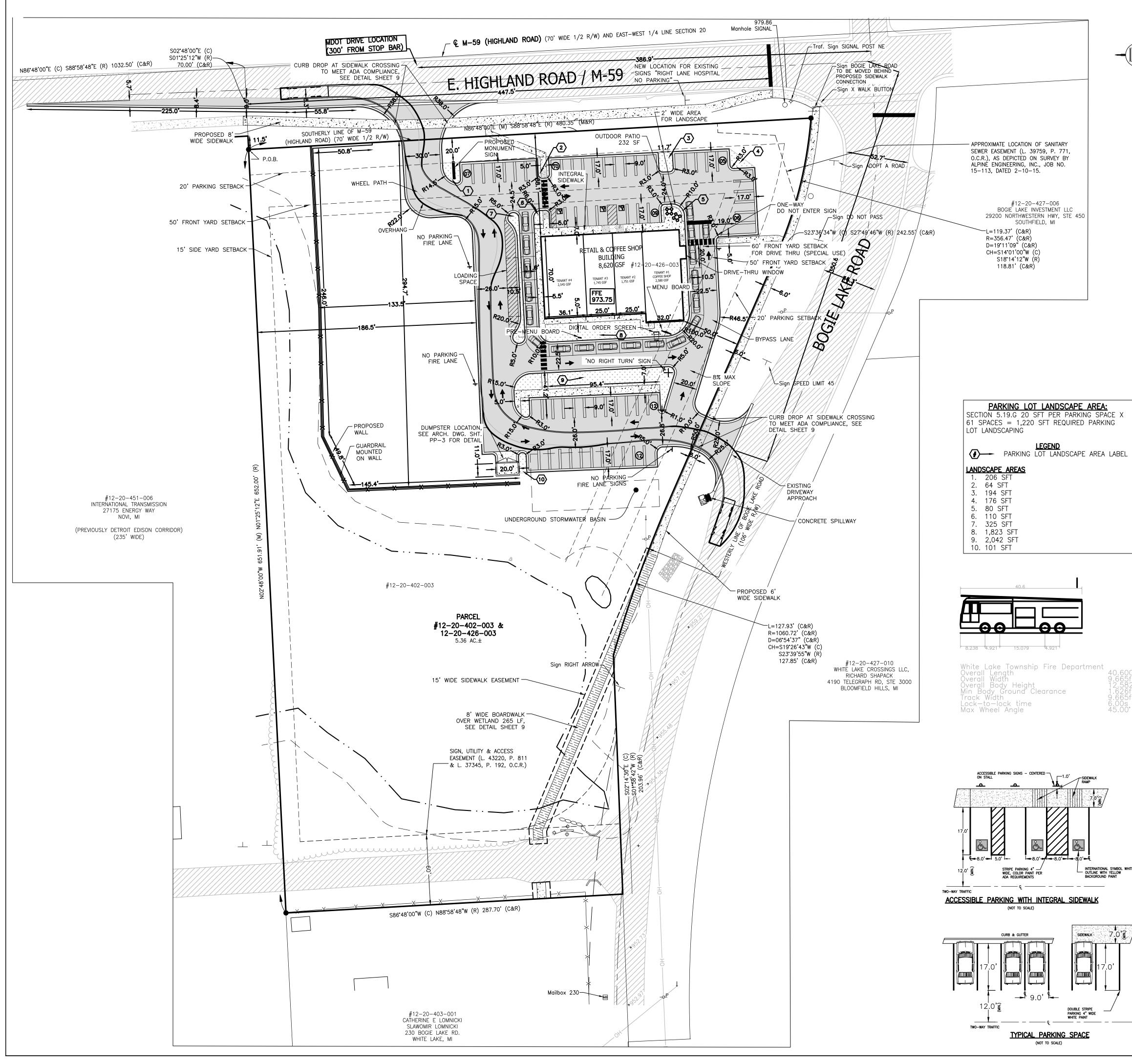
REFERENCES UTILIZED INCLUDED: NATIONAL WETLAND INVENTORY (NWI) MAP, USDA NRCS WEB SOIL SURVEY, COUNTY SOIL SURVEY, AND THE USCOE STATE OF MICHIGAN WETLAND PLANT LIST 2018.

A ROUTINE METHODOLOGY WAS USED. WETLAND TRANSECTS, WETLAND DETERMINATION DATA FORMS (DATA SHEETS) WERE COMPLETED AND BOUNDARY SURVEYED AS PART OF THE OVERALL INVESTIGATION.

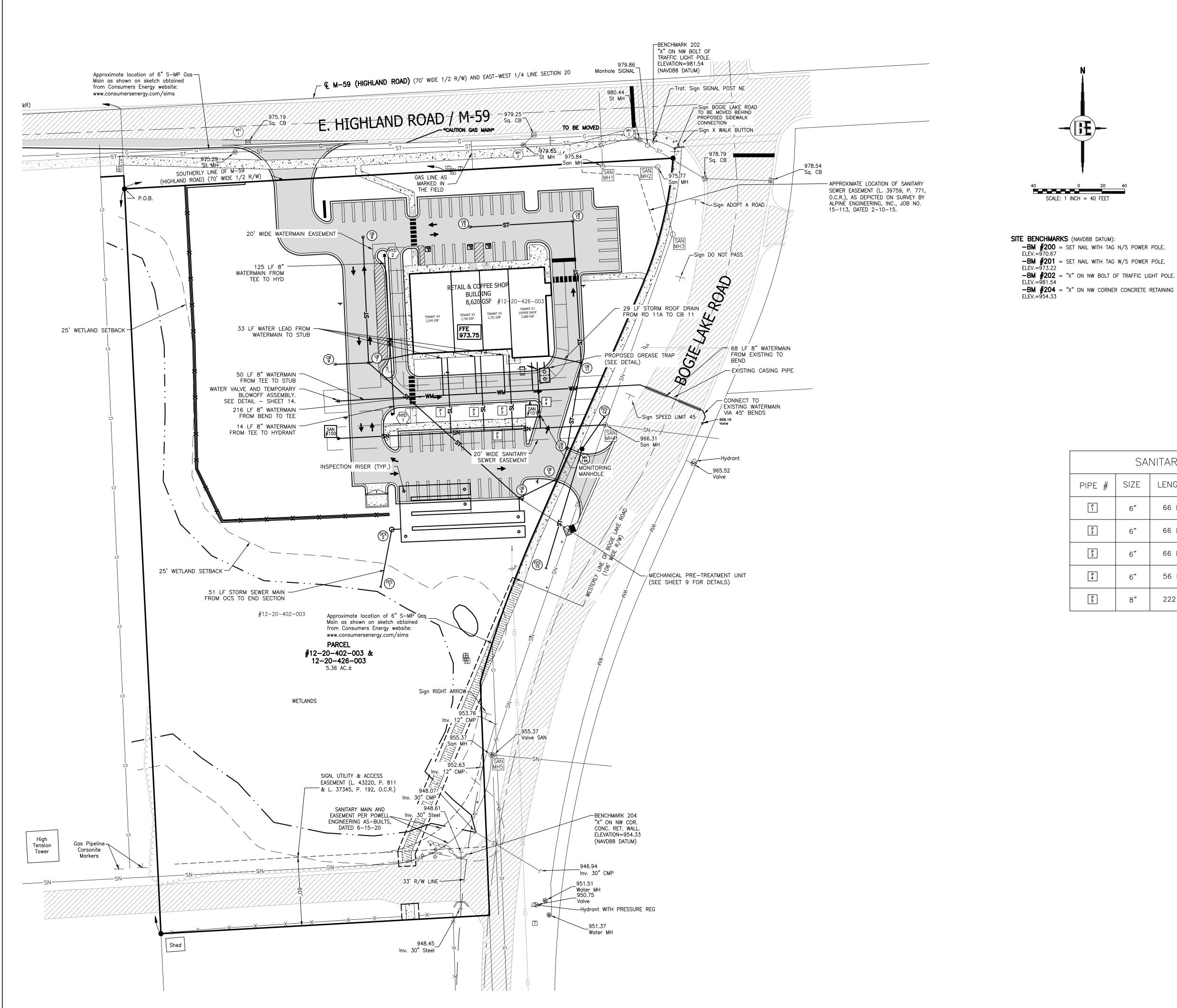
THIS DELINEATION WAS COMPLETED BASED ON OUR EXPERIENCE AND QUALIFICATIONS. IT REPRESENTS OUR BEST JUDGEMENT AS EXPERIENCED AND QUALIFIED PROFESSIONALS. IT SHOULD BE RECOGNIZED THAT THE ULTIMATE DETERMINATION AUTHORITY IS THE MICHIGAN DEPARTMENT OF ENVIRONMENT, GREAT LAKES, AND ENERGY (MEGLE) AND/OR THE U.S. ARMY CORPS OF ENGINEERS (USACE).

THE LOCATION AND ELEVATION OF EXISTING UNDERGROUND UTILITIES A SHOWN ON THESE DRAWINGS ARE ONLY APPROXIMATE. NO GUARANTEI EITHER EXPRESSED OR IMPLIED AS TO THE COMPLETENESS OR ACCUR THEREOF. THE CONTRACTOR SHALL BE EXCLUSIVELY RESPONSIBLE FO	DETERMINING THE EXACT LOCATION AND ELEVATION OF EXISTING UTILITI AND PROPOSED UTILITY CROSSINGS IN THE FIELD PRIOR TO CONSTRUC THE CONTRACTOR SHALL NOTIFY THE ENGINEER IF ANY CONFLICTS ARE APPARENT OR IF THE LOCATION OR DEPTH DIFFERS SIGNIFICANTLY FRO THE PLANS.	BEFORE YOU DIG	CALL MISS DIG 1-800-482-7171	
	Engineers Surveyors Planners Landscape Architects	3121 E. GRAND RIVER AVE.	HOWELL, MI. 48843	517.546.4836 FAX 517.548.1670
PROJECT GATEWAY CROSSING	PREPARED FOR GATEWAY CROSSING, LLC 600 NORTH OLD WOODWARD, SUITE 101 BIRMINGHAM MI 48009	248-433-7000	TITLE EXISTING CONDITIONS & DEMOLITION PLAN	
		2/28/24 1/12/24		DATE
		ST REVISION PER TWP PSP REV #3 MIN REVISION PER TWP PSP REV #2	REVISION PER TWP PSP REV #1	Y REVISION PER
DESIG	NED BY:	β		NO BY
-	KED BY:		/CZ	
	: 1" 0: 22 - 01/		-1	
DATE: SHEET		00/2	20 BOS	ŝS

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40 0 20 A	40 40 40 40 40 40 40 40 40 40	LEGEND EXISTING (EX) 900 + 922.08 FF FG T/A T/C T/W F/L T/P B/P RIM INV MH IN CB RY ES GV HY UP SN SL FM PS ST WM WL FO OH C E G	CONTOUR SPOT ELEVATION FINISHED FLOOR ELEVATION FINISHED GRADE ELEVATION TOP OF ASPHALT TOP OF CURB / CONCRETE TOP OF WALK FLOW LINE TOP OF PIPE BOTTOM OF PIPE RIM ELEVATION INVERT ELEVATION MANHOLE STRUCTURE INLET STRUCTURE CATCHBASIN STRUCTURE REARYARD STRUCTURE END-SECTION GATEVALVE STRUCTURE HYDRANT UTILITY POLE SANITARY SEWER SANITARY LEAD FORCE MAIN PRESSURE SEWER STORM SEWER WATER MAIN WATER LEAD FIBER OPTIC OVERHEAD WIRE CABLE ELECTRIC GAS	THE LOCATION AND ELEVATION OF EXISTING UNDERGROUND UTILITIES AS SHOWN ON THESE DRAWINGS ARE ONLY APPROXIMATE. NO GUARANTEE IS EITHER EXPRESSED OR IMPLIED AS TO THE COMPLETENESS OR ACCUAGCY THEREOF. THE CONTRACTOR SHALL BE EXCLUSIVELY RESPONSIBLE FOR		CALL MISS DIG 1-800-482-7171
WHITE LAKE TOWNSHIP COMBINED PARCELS # 4712–20 HIGHLAND ROAD WHITE LAKE, MI 48383	TBR TBR TBR SITE DATA 0-402-003 AND # 47		TELEPHONE FENCE SILT FENCE WETLAND BOUNDARY LIMITS OF GRADING/CLEARIN MANHOLE INLET / CATCHBASIN FLARED END-SECTION GATE VALVE HYDRANT UTILITY POLE SIGN NOT FIELD VERIFIED TO BE REMOVED CONCRETE ASPHALT PARKING LOT LANDSCAPING			HOWELL, MI. 4884 546.4836 FAX 517.5
AND NEAREST INTERSECTION	DING WITH ADDITIONAL E EMAIN UNDER SINGLE (ZONING: 1 ACRE G, 85% IMPERVIOUS <u>PROPOSED SE</u> FRONT (NORTH FRONT (EAST): REAR (SOUTH: SIDE (WEST): CORIVE-THROUGH) SS FLOOR AREA PACES ~ 34 SPACES PI G SPACES ~ 9 SPACES 3 SPACES ~ 9 SPACES 45 SPACES ~ 9 SPACES 45 SPACES ~ 9 SPACES 45 SPACES ~ 25 SPACES 45 SPACES ~ 25 SPACES MG 3 ADA SPACES, PLU <u>SITE PLAN NC</u> QUESTED: PROPOSED LOCATION OF L AKE ROAD INTERSECTION IN SHALL NOT BE LESS TO	DEVELOPABLE SPA DWNER AT THIS TI TBACKS 1): 88.1 FT 50.0 FT 487.6 FT 245.2 FT LUS 8 STACKING CES S AND 8 STACKING S CES S AND 8 STACKING DTES HIGHLAND ROAD DR (MIN. DISTANCE BE	CE ON THE WEST SIDE ME. SPACES	PROJECT GATEWAY CROSSING	PREPARED FOR GATEWAY CROSSING, LLC 600 NORTH OLD WOODWARD, SUITE 101 BIRMINGHAM, MI 48009 248-433-7000 33	ITTE PLAN
THAN OR EQUAL TO 50 MF B. VARIANCE FOR PARKING DE PROPOSED 61 SPACES WIT	EFICIENCY – 77 SPACES . TH 16 STACKING SPACES.				• • • • • • •	1/12/24 1 09/08/23 DATE
C. VARIANCE FROM ACCESS M ENTRANCE AND INTERSECTION CURRENT PROPOSED DISTA	ON WITH BOGIE LAKE ROA NCE IS 300 FEET.	AD CANNOT BE LESS	3 THAN 455 FEET.		#3	/ #2 / #1
D. (SPECIAL USE) DRIVE—THRU						PSP REV PSP REV PER
R.O.W. THE DRIVE—THRU CORNER OF THE BUILDING APPEALS MAKES AN INTERF THE 60—FOOT FRONT YARE	IS THE BUILDING IS 50 PRETATION ALLOWING THE D SETBACK. FOR HIGHLAND ROAD DRIVI ICT TO THE WEST.	FEET WAY. REQUES SETBACK AS PROPO EWAY LOCATED LESS	T ZONING BOARD OF DSED BEING CONFORMING TO THAN 200 FEET FROM THE		PER TWP	PER TWP PER TWP REVISION
R.O.W. THE DRIVE-THRU CORNER OF THE BUILDING APPEALS MAKES AN INTERF THE 60-FOOT FRONT YARE E. (SPECIAL USE) VARIANCE F RESIDENTIAL ZONING DISTRI	IS THE BUILDING IS 50 I PRETATION ALLOWING THE D SETBACK. FOR HIGHLAND ROAD DRIVING ICT TO THE WEST. IN GLASS FACADE ON EA OVERAGE. BE DESIGNED AND MA	FEET WAY. REQUES SETBACK AS PROP EWAY LOCATED LESS ST ELEVATION. REQU	T ZONING BOARD OF DSED BEING CONFORMING TO THAN 200 FEET FROM THE JIRED 30% GLASS COVERAGE PPORT THE IMPOSED		REVISION PER TWP	MJD REVISION PER TWP MJJS REVISION PER TWP BY REVISION
 R.O.W. THE DRIVE-THRU V CORNER OF THE BUILDING APPEALS MAKES AN INTERF THE 60-FOOT FRONT YARE E. (SPECIAL USE) VARIANCE F RESIDENTIAL ZONING DISTRI F. VARIANCE FOR REDUCTION PROVIDED 9.27% GLASS CO 2. ACCESS DRIVE SHALL E LOADS OF FIRE APPARATUS A ALL-WEATHER DRIVING CAPAI 3. THE OUTDOOR DINING I M-TH: 8:00A FRIDAY: 8:00 SATURDAY: 1 	IS THE BUILDING IS 50 I PRETATION ALLOWING THE D SETBACK. FOR HIGHLAND ROAD DRIVINI IN GLASS FACADE ON EA OVERAGE. BE DESIGNED AND MA AND SHALL BE SURF BILITIES.	FEET WAY. REQUES SETBACK AS PROPO EWAY LOCATED LESS ST ELEVATION. REQU NINTAINED TO SU ACED SO AS TO DURING THE FO NIGHT),	T ZONING BOARD OF DSED BEING CONFORMING TO THAN 200 FEET FROM THE JIRED 30% GLASS COVERAGE PPORT THE IMPOSED PROVIDE	DESIGI DRAWI CHECK SCALE	N BY: KED B	D P D Z MJD REVISION PER TWP 1 JAVJS REVISION PER TWP NO BY REVISION



<u>LEGEND</u>

+ 922.08

FF

T/A

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F/L T/P

B/P

RIM

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UP

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------PS------

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<u>PROPOSED</u> (PR) <u>EXISTING</u> (EX) **____**900**___** - -900- -

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T/C

T/W

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TBR

SAN #1

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54T

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CONTOUR SPOT ELEVATION

FINISHED FLOOR ELEVATION

FINISHED GRADE ELEVATION

FINISHED GRADE ELEVATION
TOP OF ASPHALT
TOP OF ASPHALT TOP OF CURB / CONCRETE
TOP OF WALK
FLOW LINE
TOP OF PIPE
BOTTOM OF PIPE
RIM ELEVATION
INVERT ELEVATION
MANHOLE STRUCTURE
INLET STRUCTURE
CATCHBASIN STRUCTURE
REARYARD STRUCTURE
END-SECTION
GATEVALVE STRUCTURE
HYDRANT
UTILITY POLE
SANITARY SEWER SANITARY LEAD
FORCE MAIN
PRESSURE SEWER
STORM SEWER
WATER MAIN
WATER LEAD
FIBER OPTIC
OVERHEAD WIRE
CABLE
ELECTRIC
GAS
TELEPHONE
FENCE
SILT FENCE
WETLAND BOUNDARY
LIMITS OF GRADING/CLEARING
MANHOLE
INLET / CATCHBASIN FLARED END—SECTION
GATE VALVE
HYDRANT
UTILITY POLE
UTILITY PULE

SIGN NOT FIELD VERIFIED TO BE REMOVED

SANITARY SEWER LABEL

STORM SEWER LABEL

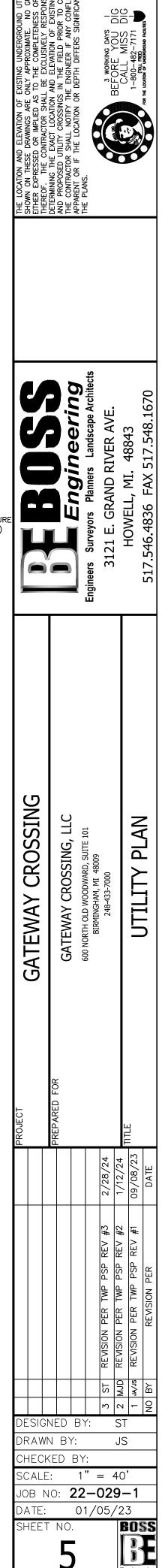
WATER MAIN LABEL SOIL EROSION CONTROL MEASURE (P=PERMANENT, T=TEMPORARY) CONCRETE ASPHALT

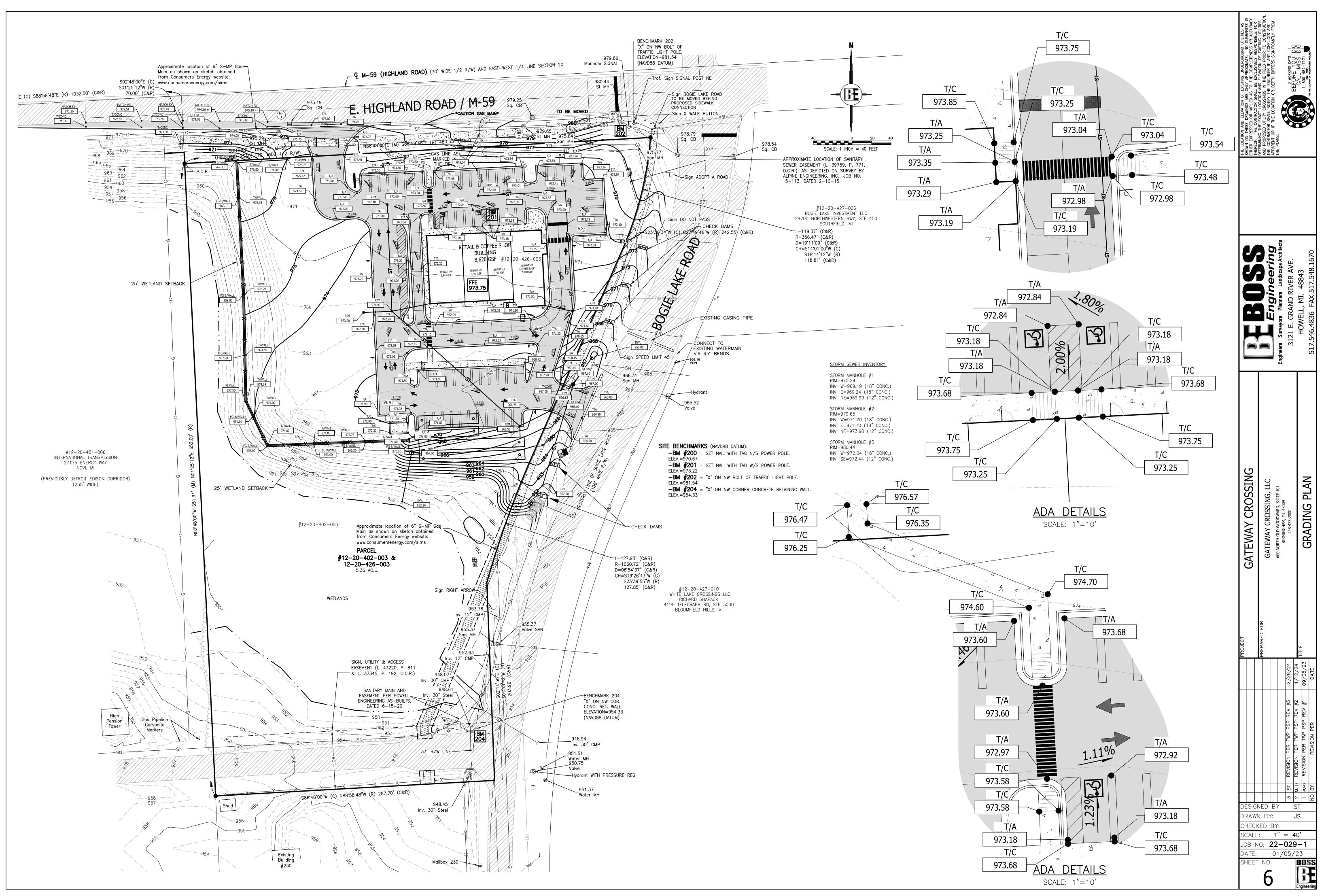
MODIFIED CURB

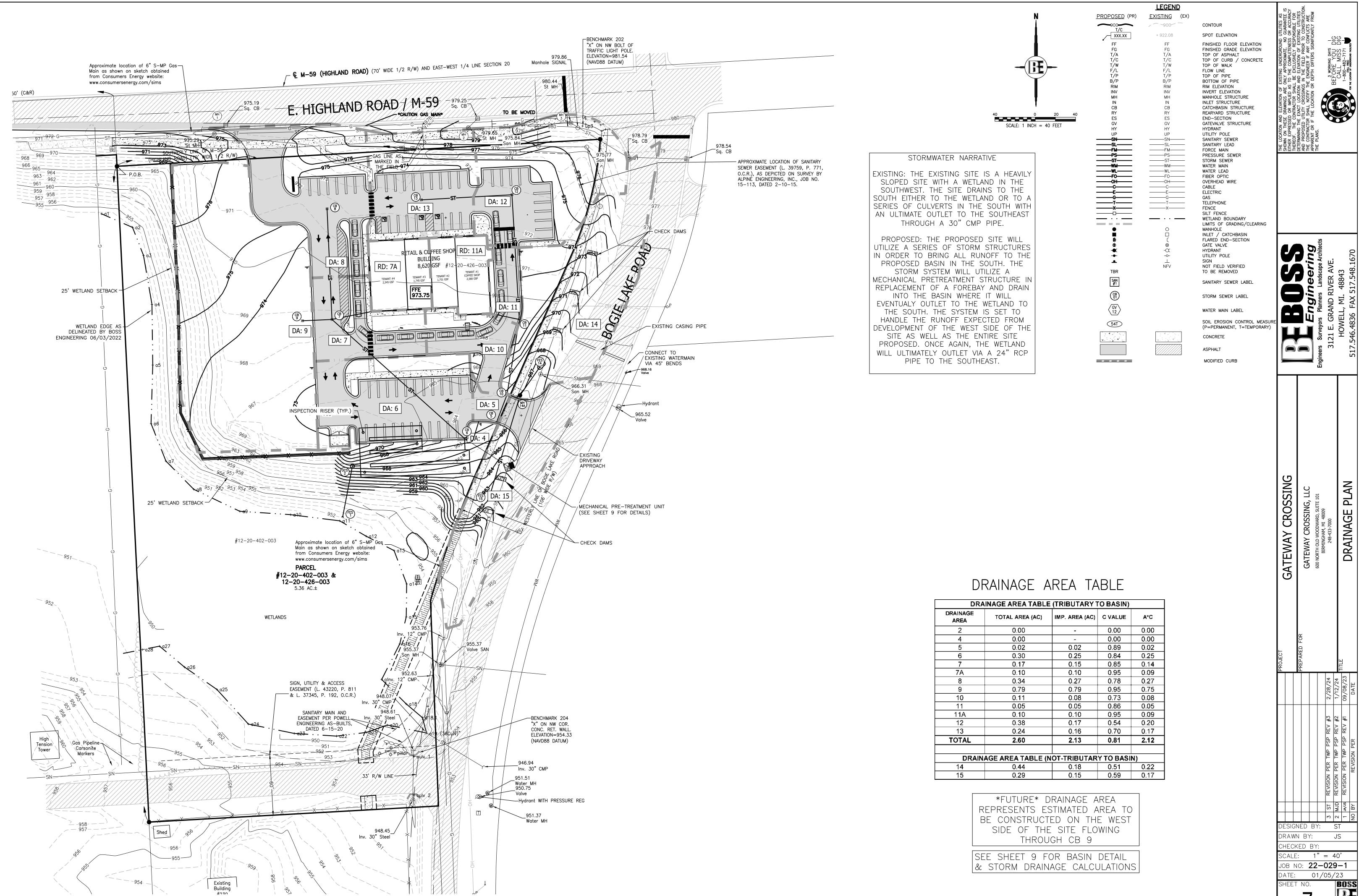
20	40		
FEET			
DATUM):			

-BM #204 = "X" ON NW CORNER CONCRETE RETAINING WALL.

	SA	NITARY F	PIPE SCH	HEDULE
= #	SIZE	LENGTH	MATERIAL	DESCRIPTION
]	6"	66 LF	SDR 23.5	SANITARY LEAD FROM RETAIL #1 TO SANITARY MAIN
]	6"	66 LF	SDR 23.5	SANITARY LEAD FROM RETAIL #2 TO SANITARY MAIN
]	6"	66 LF	SDR 23.5	SANITARY LEAD FROM RETAIL #3 TO SANITARY MAIN
]	6"	56 LF	SDR 23.5	SANITARY LEAD FROM COFFEE SHOP TO SANITARY MAIN
	8"	222 LF	SDR 26	SANITARY MAIN FROM MH #100 TO EX MH 4

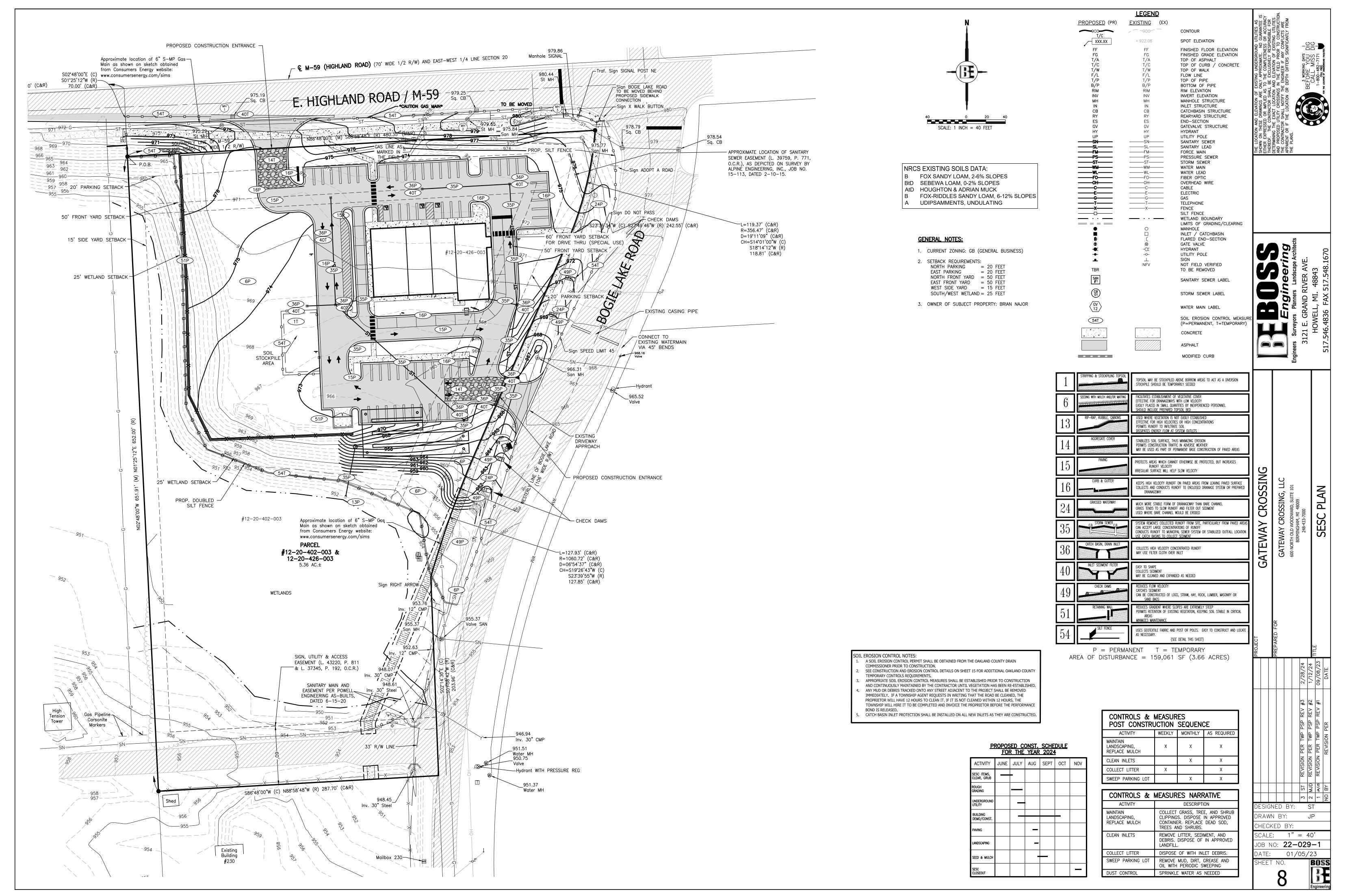






	DRA	INAGE AREA TABLE	(TRIBUTARY T	OBASIN)	
NAGE REA	I	TOTAL AREA (AC)	IMP. AREA (AC)	C VALUE	A*C
2		0.00	-	0.00	0.00
4		0.00	-	0.00	0.00
5		0.02	0.02	0.89	0.02
6		0.30	0.25	0.84	0.25
7		0.17	0.15	0.85	0.1 4
Ά		0.10	0.10	0.95	0.09
8		0.34	0.27	0.78	0.27
9		0.79	0.79	0.95	0.75
0		0.11	0.08	0.73	0.08
1		0.05	0.05	0.86	0.05
1A		0.10	0.10	0.95	0.09
2		0.38	0.17	0.54	0.20
3		0.24	0.16	0.70	0.17
TAL		2.60	2.13	0.81	2.12
DR	AIN/	AGE AREA TABLE (N	OT-TRIBUTAR	Y TO BASI	N)
4		0.44	0.18	0.51	0.22
5		0.29	0.15	0.59	0.17
	E	E CONSTRUCTE SIDE OF THE THROUG	TIMATED A ED ON THI SITE FLO GH CB 9	REA TC E WEST WING	

THE LOCATION AND ELEVATION OF EXIST	EITHER EXPESSED OR IMPLIED AS TO T	DETERMINING THE EXACT LOCATION AND	AND PROPOSED UTILITY CROSSINGS THE CONTRACTOR SHALL NOTIFY THE	APPARENT OR IF THE LOCATION OR					FOR THE LOOM
					Engineers Surveyors Planners Landscape Architects	3121 F GRAND RIVER AVE		HOWELL, MI. 48843	517.546.4836 FAX 517.548.1670
	GAI EWAY CKUSSING		GATEWAY CROSSING. LLC		BURNINGHAM, MI 48009	248-433-7000		DDATNAGE DI AN	
PROJECT		PREPAREN FOR				/24			Ш
DF CH SC JC	RAV HEC DB	VN KE E: NC	B` D : :	r: BY 1 22 0'	: " =	2 "3 ST REVISION PER TWP PSP REV #3	6 6 6 2 MJD REVISION PER TWP PSP REV #2	L , 1 JAVIS REVISION PER TWP PSP REV #1	NO BY REVISION PER DATE
		DESIC DESIC DESIC DESIC DESIC DESIC DESIC DESIC DESIC DESIC	BREVEN CROSSING DESIGNE DESIGNE DESIGNE DESIGNE DESIGNE DESIGNE	BREPARD CROSSING. LC CHECKED DATE: DATE:		PROJECT JOUNCE PREPARED FOR GATEWAY CROSSING PREPARED FOR GATEWAY CROSSING DESIGNED BI: DESIGNED BI: DESIGN	PROJECT DE LA CROSSING PREPARED FOR CATEWAY CROSSING PREPARED FOR CATEWAY CROSSING PREPARED FOR CATEWAY CROSSING CATEWAY CROSSING	PROJECT PRO	PROJECT PROJECT PROJECT PREPARED FOR GATEWAY CROSSING ACTIONAL SULF ACTIONAL SULF ACTIONA



JRIFICE DE	SIGN SUMN	<u>IARY</u>										/EEN PRECAST			
ELEVATIO		# OF HOLES	DI/	AMETER OF I								FLOW RESTRICTOR ASE WITH BUTYL R			NCRETE FLOW
952.50		1.0		1 -INC							WALL & D	ASE WITH DUTLE N		RESTRICTOR	WALL
957.70		2.0		2 -INC	ЭН								<u>SECTION A-</u>	۵	
		<u>Y SUMMARY</u>													
VIDTH OF O	VERFLOW	SPILLWAY :	=	6 FT										FLOW RE	STRICTOR W
													-		(NOT TO SCA
				RUNOFF	EQUIV.		TIME OF		RUNOFF	PIPE	PIPE	VELOCITY	HYDRAULIC	ACTUAL	•
FROM	то	DRAIN	ACRES	COEFF	AREA	INTEN-SITY	CONC.	RUNOFF	(CFS)	LENGTH	DIA.	FLOWING	GRADIENT	SLOPE	MANNING
		AREA	A	C	A * C	I	T _C	Q	Q	(LF)	(IN)	FULL (FPS)	SLOPE %	USED	COEFFICIENT
8	7	8	0.34	0.78	0.27	4.38	15.00		1.18	110	15	2.61	0.24%	0.50%	0.013
7	6	7	0.17	0.85	0.14	4.32	15.49	3.68	5.47	177	18	4.70	0.62%	0.75%	0.013
6	BASIN	6	0.30	0.84	0.25	4.26	16.06	2.65	9.19	6	18	6.93	1.35%	1.50%	0.013
9	7	9	0.79	0.95	0.75	4.38	15.00		3.27	29	15	3.55	0.45%	0.50%	0.013
7A	7	7A	0.10	0.95	0.09	4.38	15.00		0.40	40	8	2.69	0.60%	1.00%	0.013
13	12	13	0.24	0.70	0.17	4.38	15.00		0.74	90	12	1.99	0.19%	0.32%	0.013
12	11	12	0.38	0.54	0.20	4.31	15.58		1.62	124	12	2.55	0.31%	0.32%	0.013
11	10	11	0.05	0.86	0.05	4.23	16.39	0.42	2.23	76	15	4.89	0.86%	1.75%	0.013
10	5	10	0.11	0.73	0.08	4.21	16.57		2.56	30	15	2.56	0.24%	0.24%	0.013
5	6	5	0.02	0.89	0.02	4.19	16.76		2.65	35	15	2.84	0.29%	0.24%	0.013
11A	11	11A	0.10	0.95	0.09	4.38	15.00		0.42	29	8	2.69	0.60%	1.00%	0.013
14	14A	14	0.44	0.51	0.22	4.38	15.00		0.98	34	12	5.79	1.62%	4.50%	0.013
14A	13	-	-	-	-	-	15.06		0.98	109	12	2.57	0.32%	0.50%	0.013
BASIN	2	ALL	_ 1	-	-	-	15.00	9.19	9.19	8	24	4.22	0.34%	0.40%	0.013
2	1	-	-	-	-	-	15.03		9.19	51	24	4.22	0.34%	0.40%	0.013
		100-Y	EAR PIF		V CALCUI		OROCS]							
BASIN "	2	ALL	2.60	0.81	2.117188	5.96	16.76	٦	12.62	8	24	5.48	0.58%	0.40%	0.013
2	1	-	-	-	-	-	16.79		12.62	51	24	5.48	0.58%	0.40%	0.013

BASIN DESIGN S	UMMARY		
BASIN SIZE REQU	JIRED =	27,334	FT ³
BASIN SIZE PROV	/IDED =	27,646	FT ³
ORIFICE DESIGN	SUMMARY		
ELEVATION	# OF HOLES	DIAMETER	OF HOLES
ELEVATION 952.50	# OF HOLES 1.0		OF HOLES
		1	
952.50 957.70	1.0	1	-INCH

Width of Spillway:	L _{WEIR} =	Q _{100IN} /3.33H _{WEI}	R ^{~**=}			
BASIN DESIGN S	UMMARY					
BASIN SIZE REQU	JIRED =	27,334	FT³			
BASIN SIZE PROV	/IDED =	27,646	FT ³			
ORIFICE DESIGN	SUMMARY					
ELEVATION	# OF HOLES	DIAMETER OF HOLES				
952.50	1.0	1	-INCH			
957.70	2.0	2	-INCH			
OVER OW SRUL WAY SUMMARY						

OVERFLOW SPILLWAY I	DESIGN				
Design Flow Rate:	Q _{100IN} =	12.56	CFS		
Depth of Spillway:	H _{WEIR} =	9	INCHES		
Width of Spillway:	$L_{WEIR} = Q$	_{100IN} /3.33⊢	WEIR 3' 2=	5.8	FT
BASIN DESIGN SUMMARY					
BASIN SIZE REQUIRED =		27,3	34 FT ³		
BASIN SIZE PROVIDED =		27,6	46 FT ³		

$Q_{ED-ACTUAL} = (A_{ED})(0.62 \times (2 \times 32))$	2.2 x h) ^{0.5})	=	0.077 (CFS	
		0.446	050		
$Q_{100-ACTUAL} = Q_{100P} - Q_{ED-ACTUAL}$			CFS		
$A_{100} = Q_{100-ACTUAL} / (0.62 * (2*3))$	2.2 * (ELE	V _{DHWL} - ELEV _E	_D)) ^{0.5}) =	0.053	FT ²
AREA OF 2		INCH DIAMETE	ER ORIFICE =	0.022	FT ²
# ORIFICES = A100 / 0.005 =		2.0	ORIFICES		
OVERFLOW SPILLWAY DES	SIGN				
Design Flow Rate:	Q _{100IN} =	12.56	CFS		

			-1		
959.5	9.5201		3,351	20,670	
958.5	9.9329		3,496	17,319	
957.5	9.9329		3,496	13,823	
956.5	9.5201		3,351	10,327	
955.5	8.6345		3,039	6,976	
954.5	7.0949		2,497	3,936	
953.5	4.0875		1,439	1,439	
952.5	0.0000				BOTTOM OF STORAGE
PROVIDED FOOTF	PRINT OF BASIN B	OTTOM AREA	4108	FT ²	
OUTLET CONTRO	L STRUCTURE				
Q _{ED} ACTUAL					
H _{ED} =	1	(1" HOLES)			
A _{ED} =	0.0055	FT ²			

R =	⁷ 0.20615(ln(Q ₁₀	00P/Q100I	J) =		0.6
V _{100D} =	[™] V _{100R} *R-V _{CP-P} =				27
Is $V_{100D} \ge V_{ED}$?	YES	•	٩		
V _{100D} =	٦	27,334	FT ³		
BASIN STORAG	E PROVIDED				
LINEAL FOOTA		352 LF	Г		

INCREMENTAL

VOLUME / LFT

4.0875

7.0949

8.6345

	PROTECTION RATE CONTROL	(EXTEN	IDED DE	TENTION VOL	UME)	
V _{ED} =	6,897(C)(A) =	14525 F	T ³			
	DETENTION OUTLET RATE					
Q _{ED} =	V _{ED} /(48hr) =	0.084 C	FS			
H _{ED} =	V _{ED} /4,666 (H) ^{1/2} =	1.0	1" HOLE	S		
Н=	8.00 FT					
ELEV _{ED} =	957.70					
	LLOWABLE OUTLET RATE	_		-		
Q _{DRAIN} =	Restricted Drain Rate =		0.2	CFS/ACRE		
Q _{VRR} =	1.1055 - 0.206LN(A) =		0.909	CFS/ACRE		
Q _{100P} =	(LESSER OF Q _{DRAIN} & Q _{VRR})*A =	=	0.520	CFS		
					VARIABLE RE	LEASE RATE
100-YEAR D	ETENTION VOLUME				1 CFS/ACRE	< 2 ACRES
V _{100R} =	18985 (C)(A) =		39982	FT ³	0.15 CFS/ACRE	> 100 ACRES
	N					

Basin Footrpint Infiltration Area Required =NO INFILTRATIO о^р гт³ V_{CP-P} =

(C)(A)30.2/(T_c+9.17)⁸¹ = 4.55 CFS Q_{WQ}= CHANNEL PROTECTION VOLUME CONTROL - REQUIRED **4**,719(C)(A) = $V_{CP-R} =$ 9938 FT³ CHANNEL PROTECTION VOLUME CONTROL - PROVIDED In-Situ Infiltration rate = IN/HR 0 Are upstream infiltration BMP's provided? NO

WATER QUALITY RATE FOR MECHANICAL STRUCTURE $T_{\rm C}$ = MAX TIME OF CONCENTRATION = - 16.76 MIN

7645 FT³ 3,630(C)(A) = 0.15(V_{wa}) = 1147 FT³

WATER QUALITY VOLUME Vwo

OAKLAND COUNTY DETENTION BASIN CALCULATIONS

AREA (ACRES) IMPERVIOUS FACTOR IMPERVIOUS

0.95

0.7

0.2

2.13

0.00

0.47

COMPOUND C:

 $Q_{100|N} =$

ELEVATION

962.5

961.5

960.5

TOTAL DRAINAGE AREA:

.

٦

V_E=

V_{WQ}=

ACRE

2.02

0.00

0.09

0.81

2.60 ACRES

12.56 CFS 6836

$(C)(A)83.3/(T_c+9.17)^{0.81} =$ 27334 FT³

VOLUME TOTAL VOLUME

(FT³)

27,646

26,207

23,710

DHWL

1. THIS TYPE OF FLOW RESTRICTOR TO BE USED ONLY WITH

2. THE PRECAST REINFORCED FLOW RESTRICTOR STRUCTURE

SHALL BE MANUFACTURED PER ASTM C-478 SPECIFICATIONS.

MDOT FRAME &

COVER TYPE "A"

UNDERGROUND DETENTION SYSTEMS.

RIM ELEVATION

FLOOD CONTROL DESIGN WATER

BANKFULL FLOOD

INVERT =

_952.46 ____

<u>ELEVATION = 962.50</u>

 $\underline{\mathsf{ELEVATION}} = 957.70$

FLOW

24" SUMP (MIN.) -

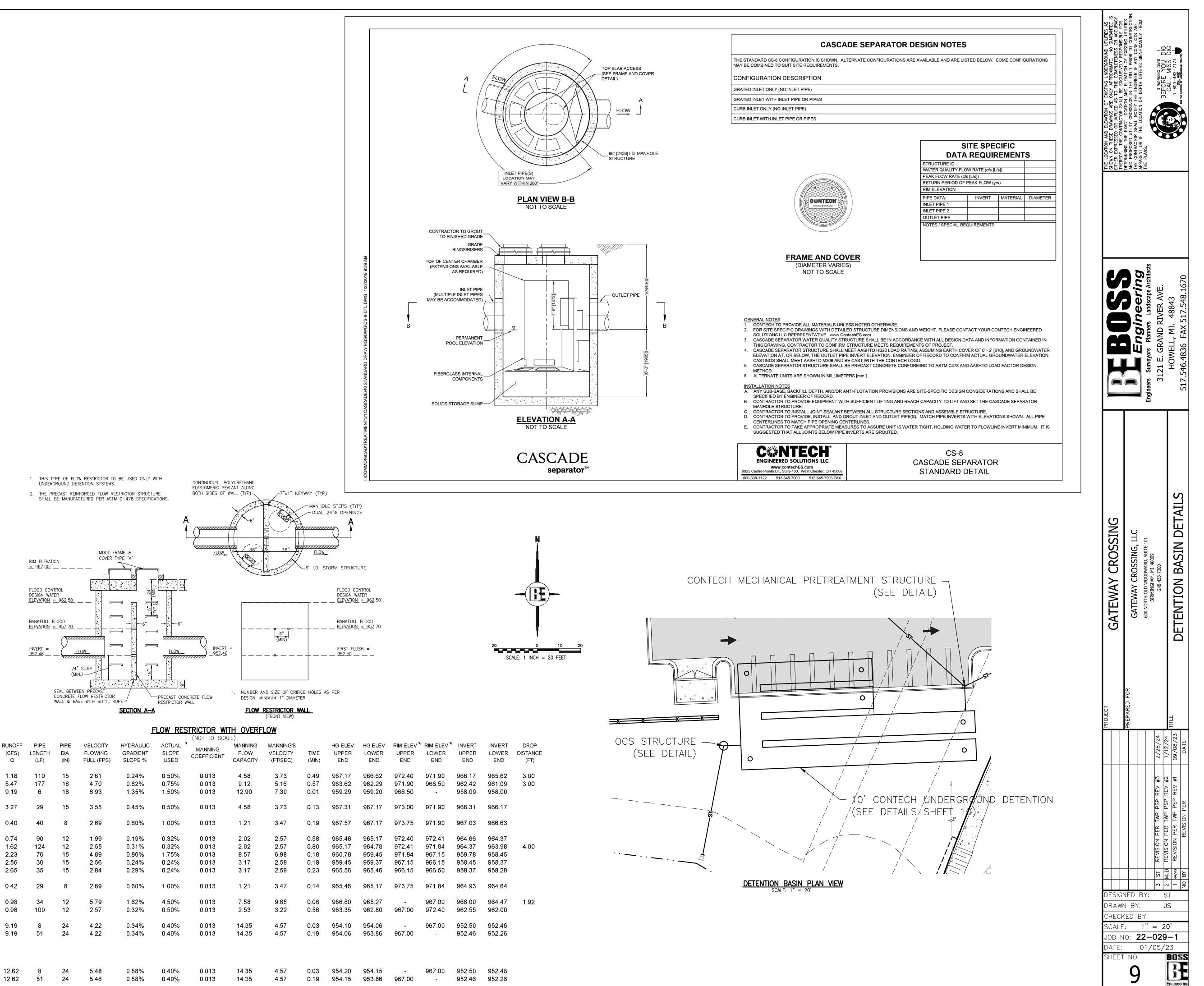
SEAL BETWEEN PRECAST

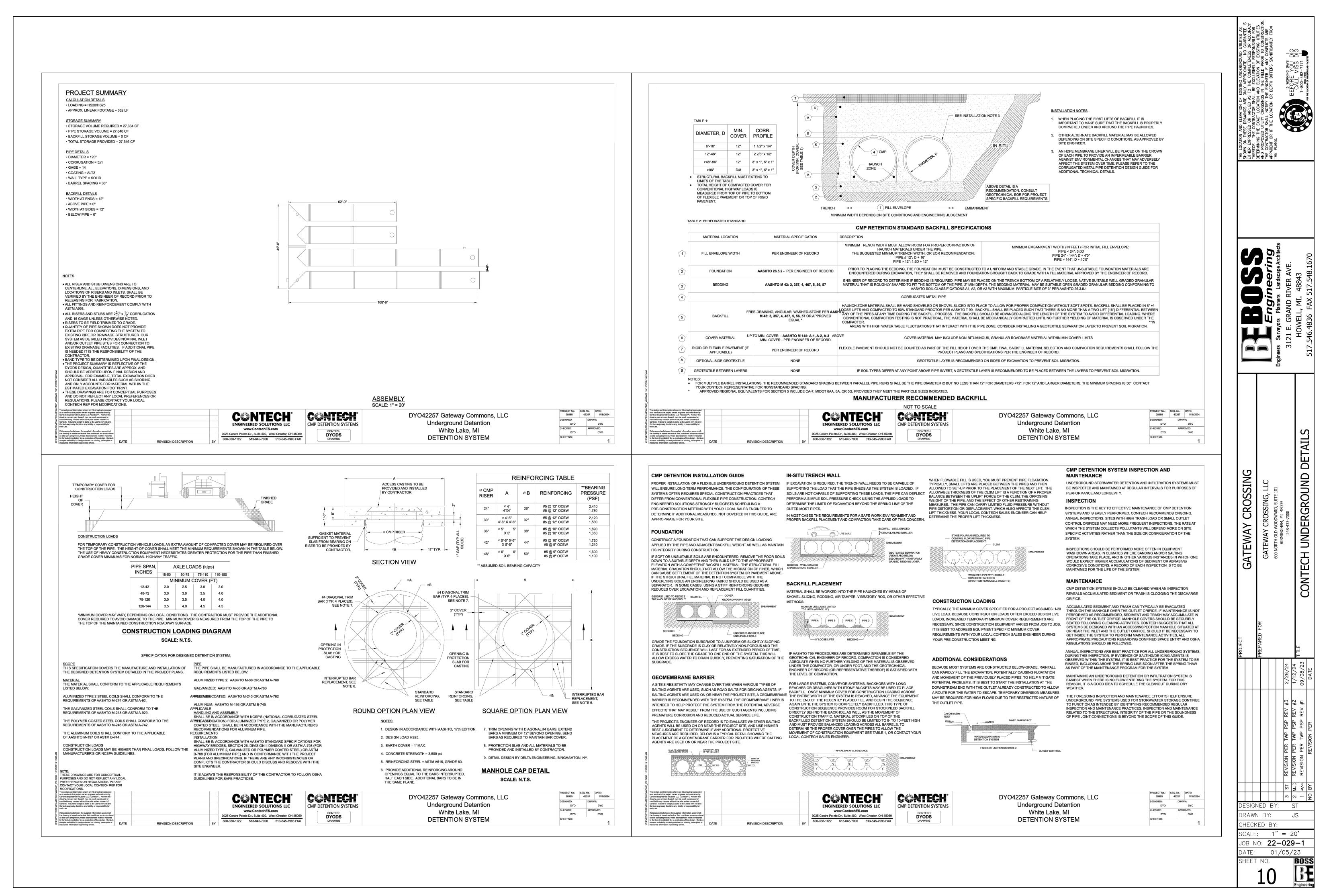
(FT³)

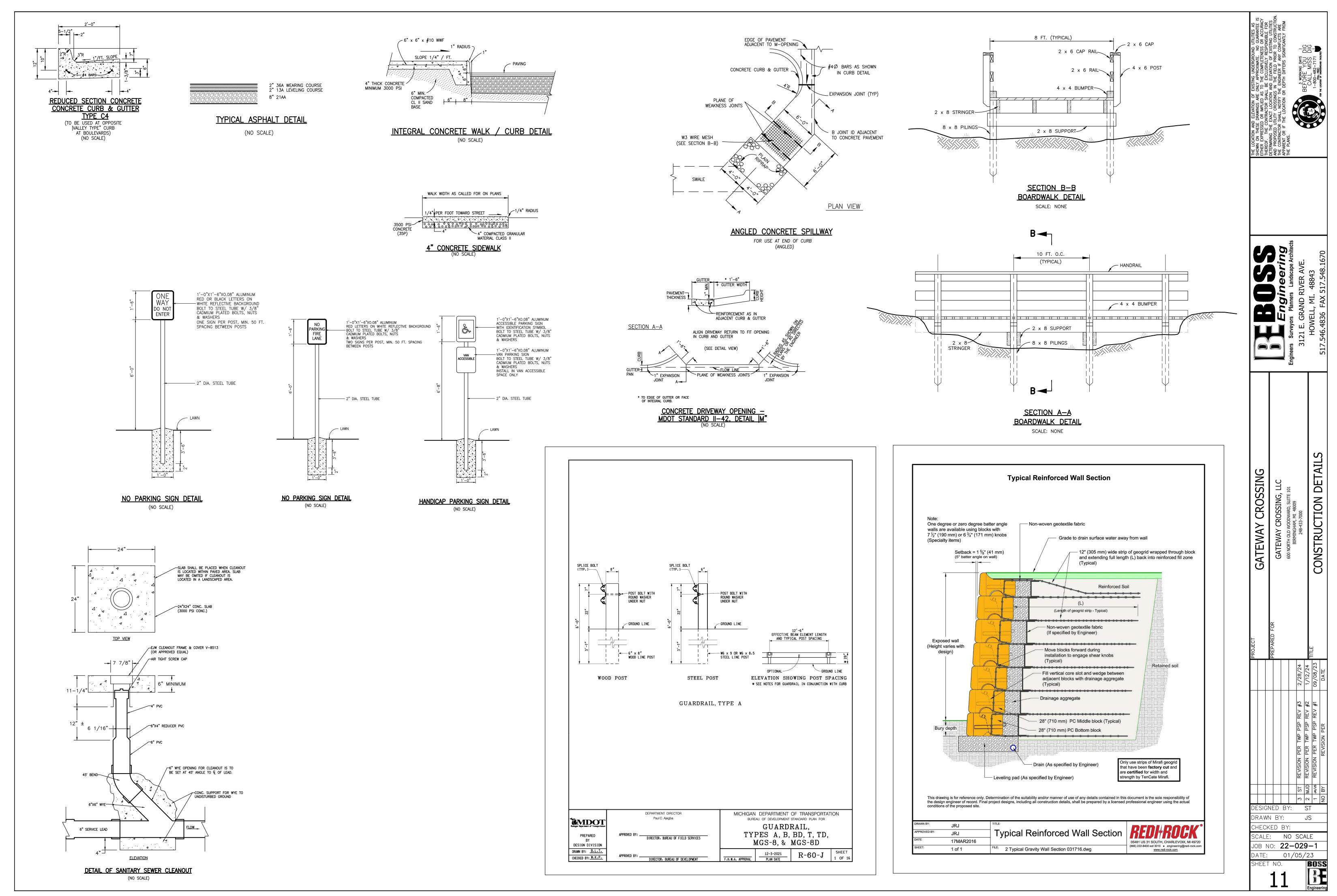
1,439

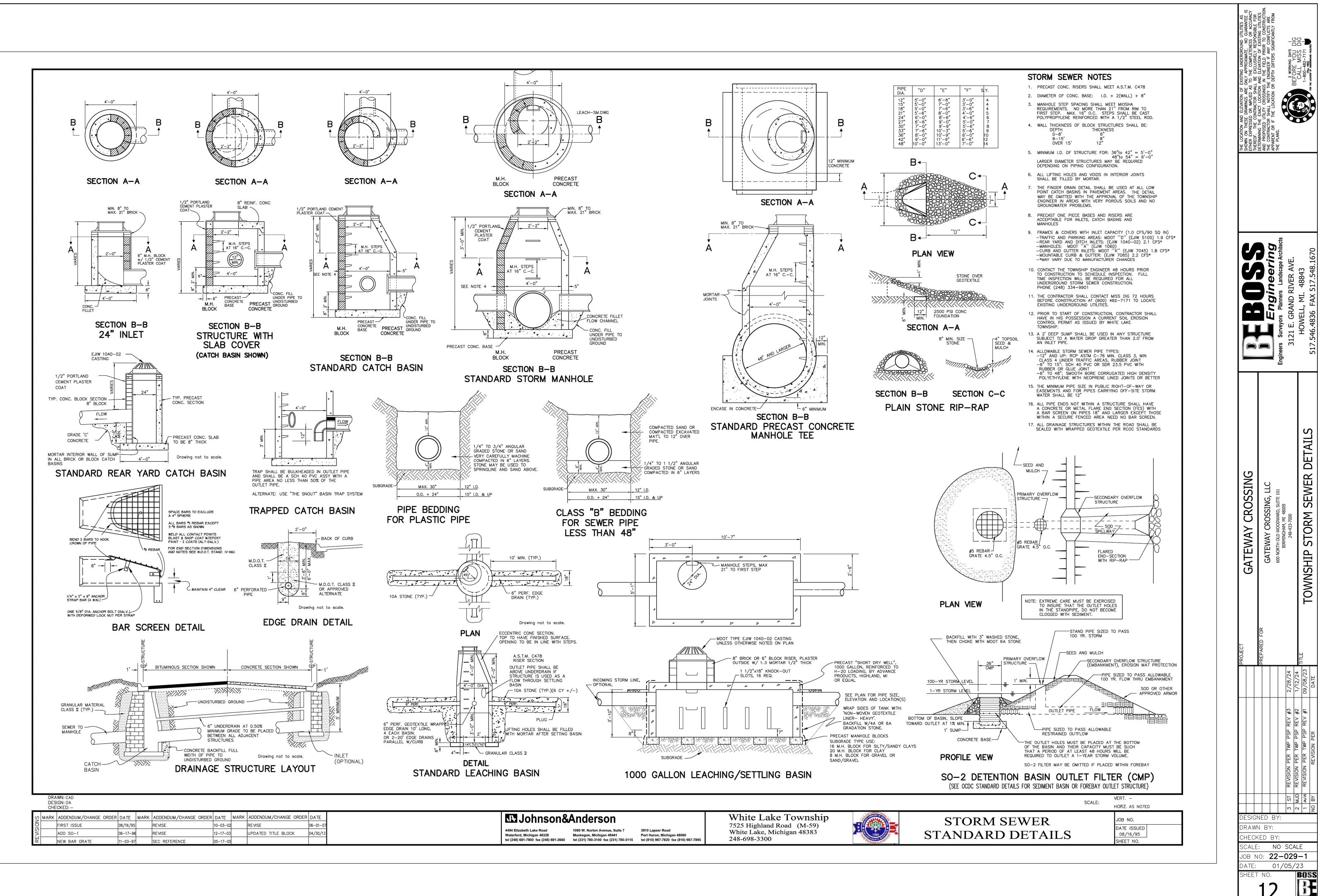
2,497

3,039

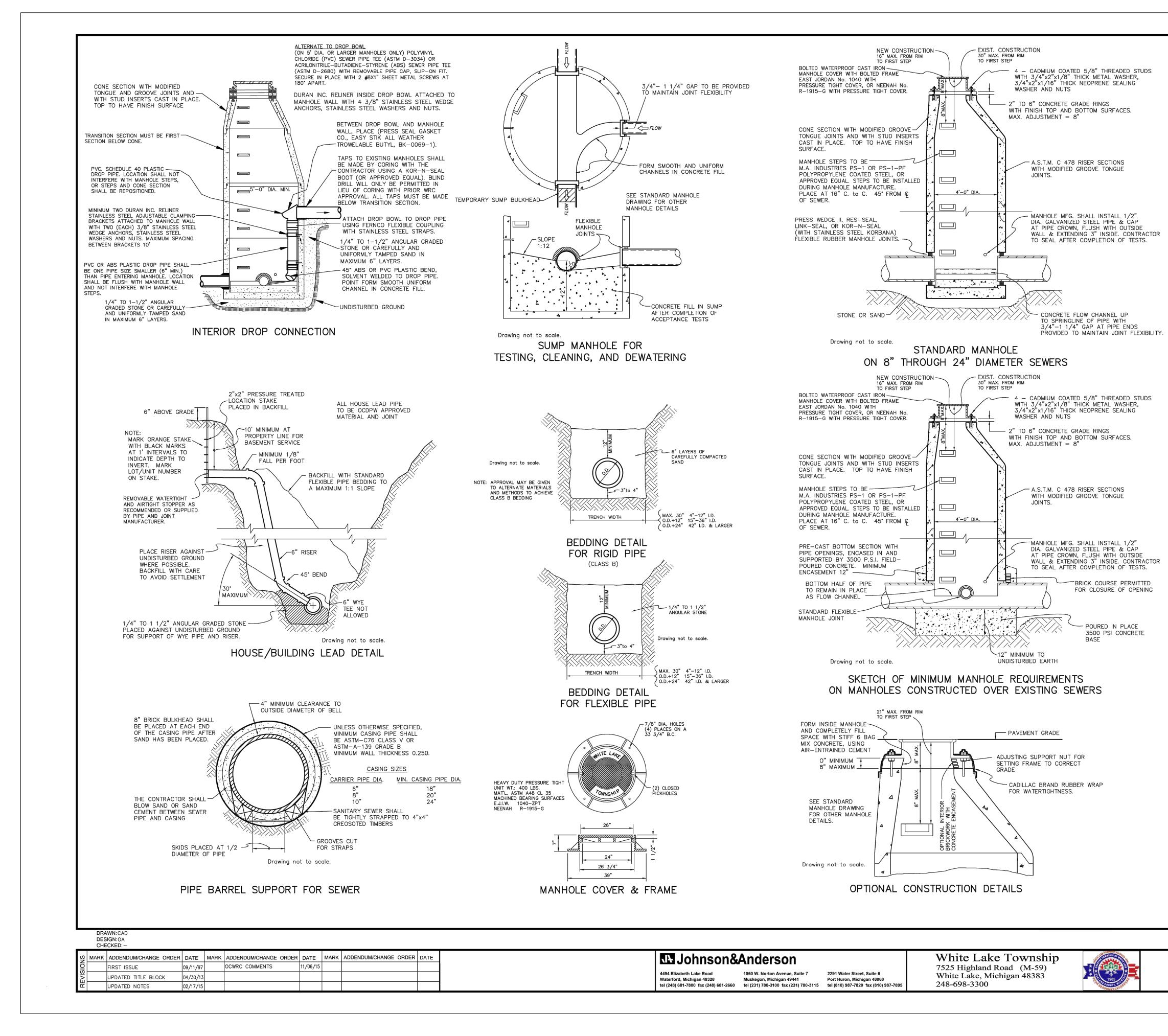




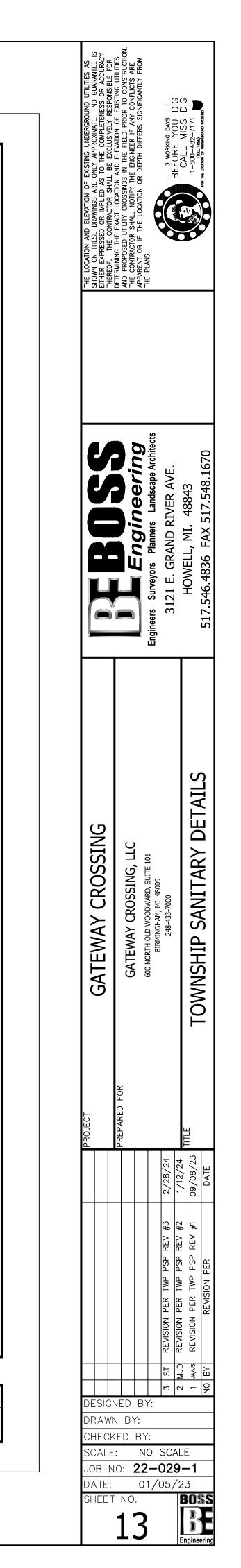




Johnson&	Anderson	White Lake Township 7525 Highland Road (M-59)		
4494 Elizabeth Lake Road Waterford, Michigan 48328 tel (248) 681-7800 fax (248) 681-2660	1060 W. Norton Avenue, Suite 7 Muskegon, Michigan 49441 tel (231) 780-3100 fax (231) 780-3115	3910 Lapeer Road Port Huron, Michigan 48060 tel (810) 987-7820 fax (810) 987-7895	White Lake, Michigan 48383 248-698-3300	



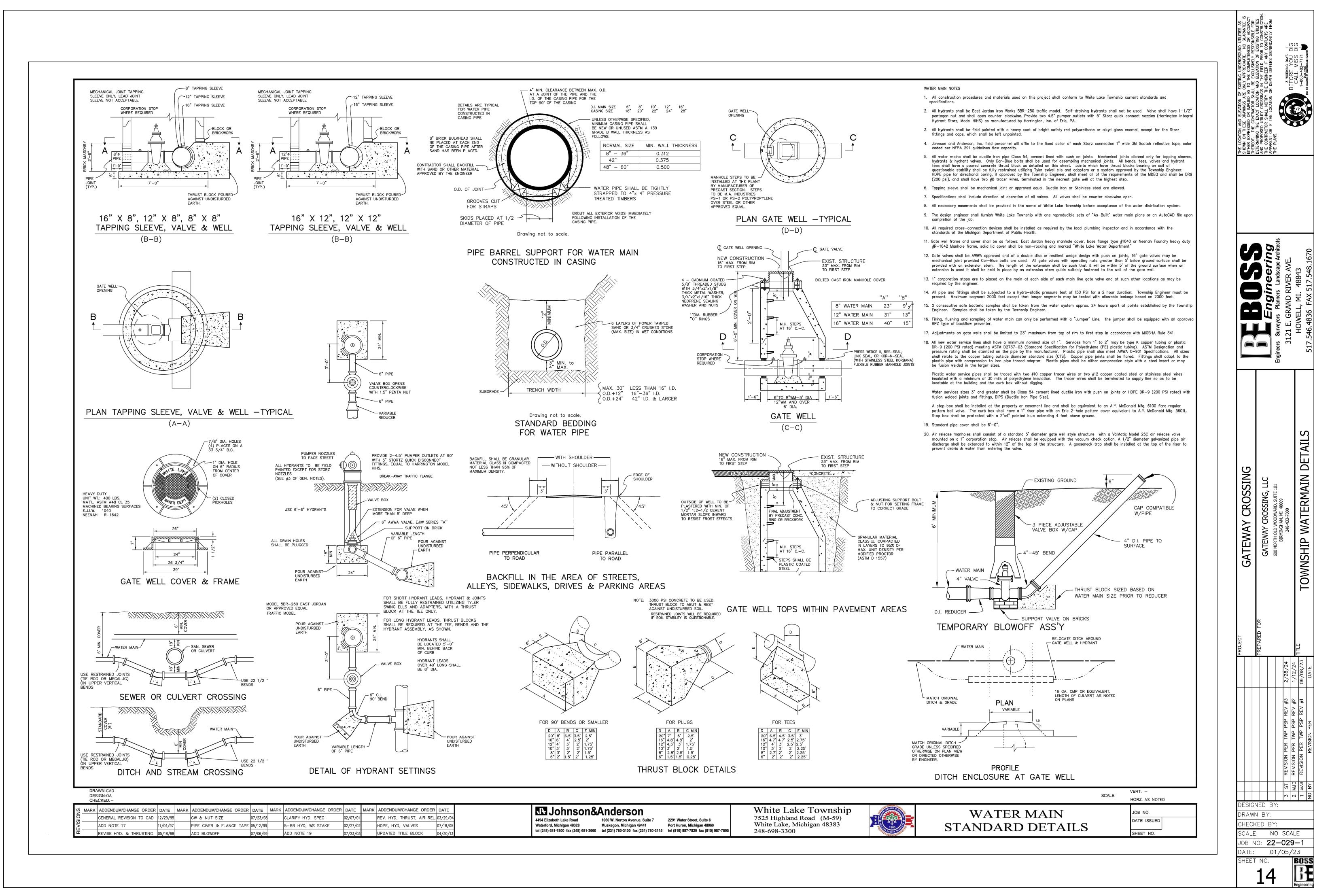
N Johnson&	Anderson		White Lake Township	
4494 Elizabeth Lake Road Waterford, Michigan 48328 tel (248) 681-7800 fax (248) 681-2660	1060 W. Norton Avenue, Suite 7 Muskegon, Michigan 49441 tel (231) 780-3100 fax (231) 780-3115	2291 Water Street, Suite 6 Port Huron, Michigan 48060 tel (810) 987-7820 fax (810) 987-7895	7525 Highland Road (M-59) White Lake, Michigan 48383 248-698-3300	



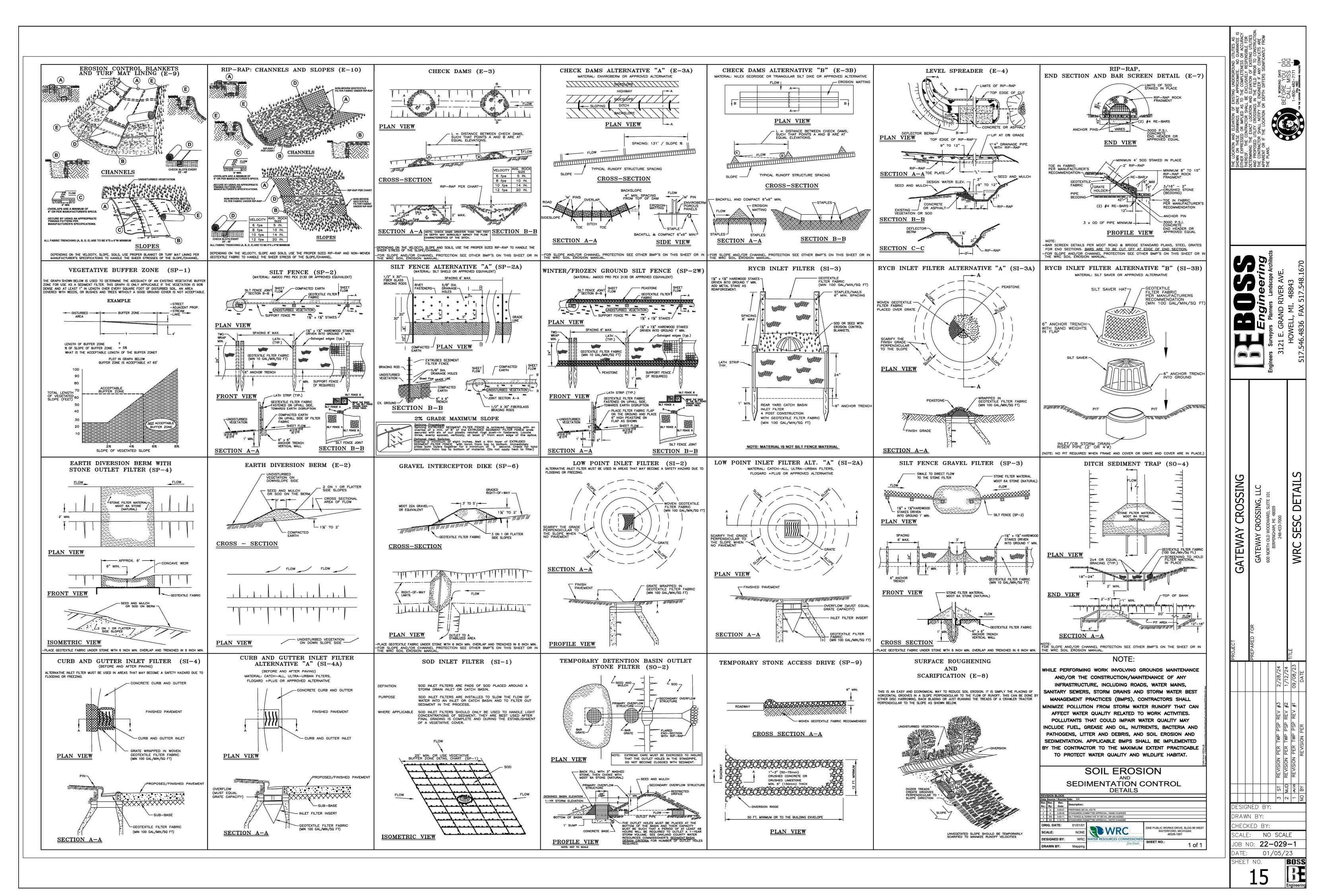
SANITARY SEWER CONSTRUCTION NOTES

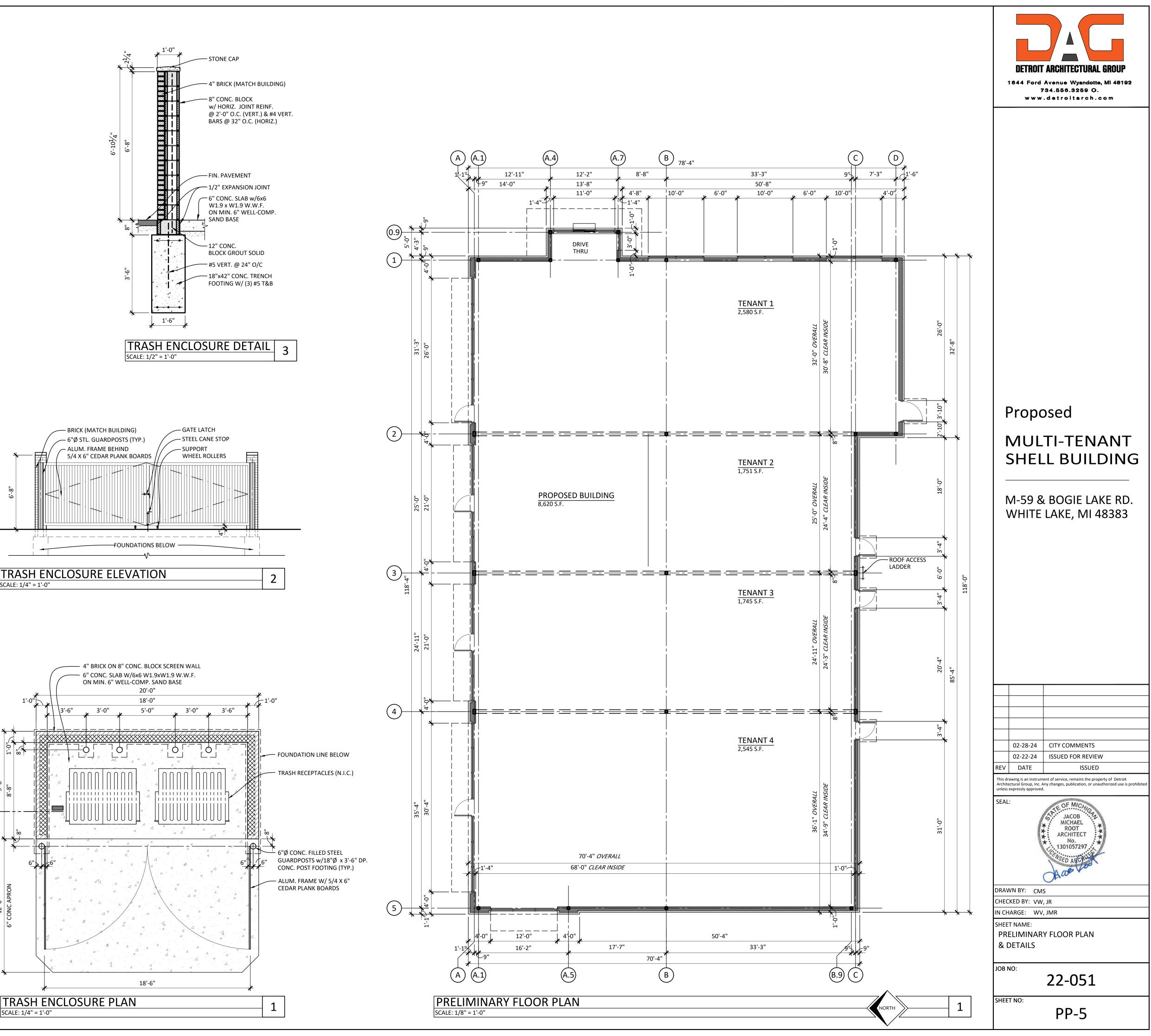
- 1. All construction shall conform to the current standards and specifications of the local unit of government and the Oakland County Water Resources Commissioner (OCWRC). All sanitary sewer construction shall have full time inspection supervised by a professional engineer provided by or caused to be provided by the local unit of government.
- 2. At all connections to Oakland County Water Resources Commissioner's sewers or extensions, and before start of construction, the Contractor must obtain a Sewer Inspection Permit issued by the OCWRC. Gravity sewer permit charges are \$250.00 for each connection plus \$25.00 for each manhole constructed. Pressure sewer permit charges are \$250.00 per 2460 L.F. of force main with a minimum permit fee of \$250.00. Failure to pass any test segment will result in an additional charge to the Contractor for each retest, in accordance with the above price schedule. The Contractor shall also have posted with the OCWRC a \$5,000.00 surety bond and \$500.00 cash deposit. The Contractor shall notify the local unit of government and the OCWRC (248-858-1110) 24 hours prior to the beginning of any construction. Final acceptance tests must be witnessed by County personnel and must be scheduled by Municipality or It's consultant in advance with 24 hour notice at 248-858-1110.
- 3. No sewer installation shall have an infiltration or exfiltration exceeding 100 gallons per inch diameter per mile of pipe in a 24 hour period, and no single run of sewer between manholes shall exceed 100 gallons per inch diameter per mile. Air tests in lieu of infiltration tests shall be as specified in the OCWRC "Acceptance Tests", dated September, 1972. Only pipe and pipe joints approved by the Oakland County Water Resources Commissioner may be used for sanitary sewer construction.
- 4. Located in the first manhole upstream from the point of all connections to an existing OCWRC sewer, or extension thereto, a temporary 12-inch deep sump shall be provided in the first manhole above the connection which will be filled in after such successful completion of any acceptance test up to the standard fillet provided for the flow channel. A watertight bulkhead shall be provided on the downstream of the sump manhole.
- 5. All building leads and risers shall be 6-inch S.D.R. 23.5 ABS OR PVC pipe with chemically fused joints, or an approved equal pipe and joint. Sewer pipe wye shall contain factory installed premium joint material of an approved type compatible with that of the building lead pipe used. Building leads to be furnished with removable air tight and water-tight stoppers.
- 6. All rigid sewer pipe shall be installed in Class "B" bedding or better. All flexible, semi-flexible or composite sewer pipe shall be installed in conformance to the Oakland County Water Resources Commissioner specifications.
- 7. All new manholes shall have Oakland County Water Resources Commissioner approved flexible, water-tight seals where pipes pass through walls. Manholes shall be of precast sections with modified groove tongue and rubber gasket type joints. Precast manhole cone sections shall be Öakland County Water Resources Commissioner approved modified eccentric cone type. All manholes shall be provided with bolted, water-tight covers.
- 8. At all connections to manholes on Oakland County Water Resources Commissioner's sewers or extensions thereto drop connections will be required when the difference in invert elevations exceeds 18-inches. Outside drop connections only will be approved.
- 9. Taps to existing manholes shall be made by coring. The Contractor shall place a KOR-N-SEAL boot (or OCWRC approved equal) after coring is completed. Blind drilling will not be permitted in lieu of coring.
- 10. New manholes constructed directly on Oakland County Water Resources Commissioner's sewers shall be provided with covers reading "Oakland County - Sanitary" in raised letters. New manholes built over an existing sanitary sewer shall have monolithic poured bottoms.
- 11. No ground water, storm water, construction water, downspout drainage or weep tile drainage shall be allowed to enter any sanitary sewer installation.
- 12. Prior to excavation, the Contractor shall telephone MISS DIG (647-7344) for the location of underground pipeline and cable facilities, and shall also notify representatives of other utilities located in the vicinity of the work.
- 13. 18" minimum vertical separation and 10' minimum horizontal separation must be maintained between sanitary sewer and water main.
- 14. Manhole frame and cover shall be as follows: East Jordan heavy manhole cover, base flange type #1040 or Neenah Foundry heavy duty #R-1642 manhole frame. Solid lid cover shall be non-rocking and marked "WHITE LAKE TOWNSHIP SEWER DEPARTMENT."

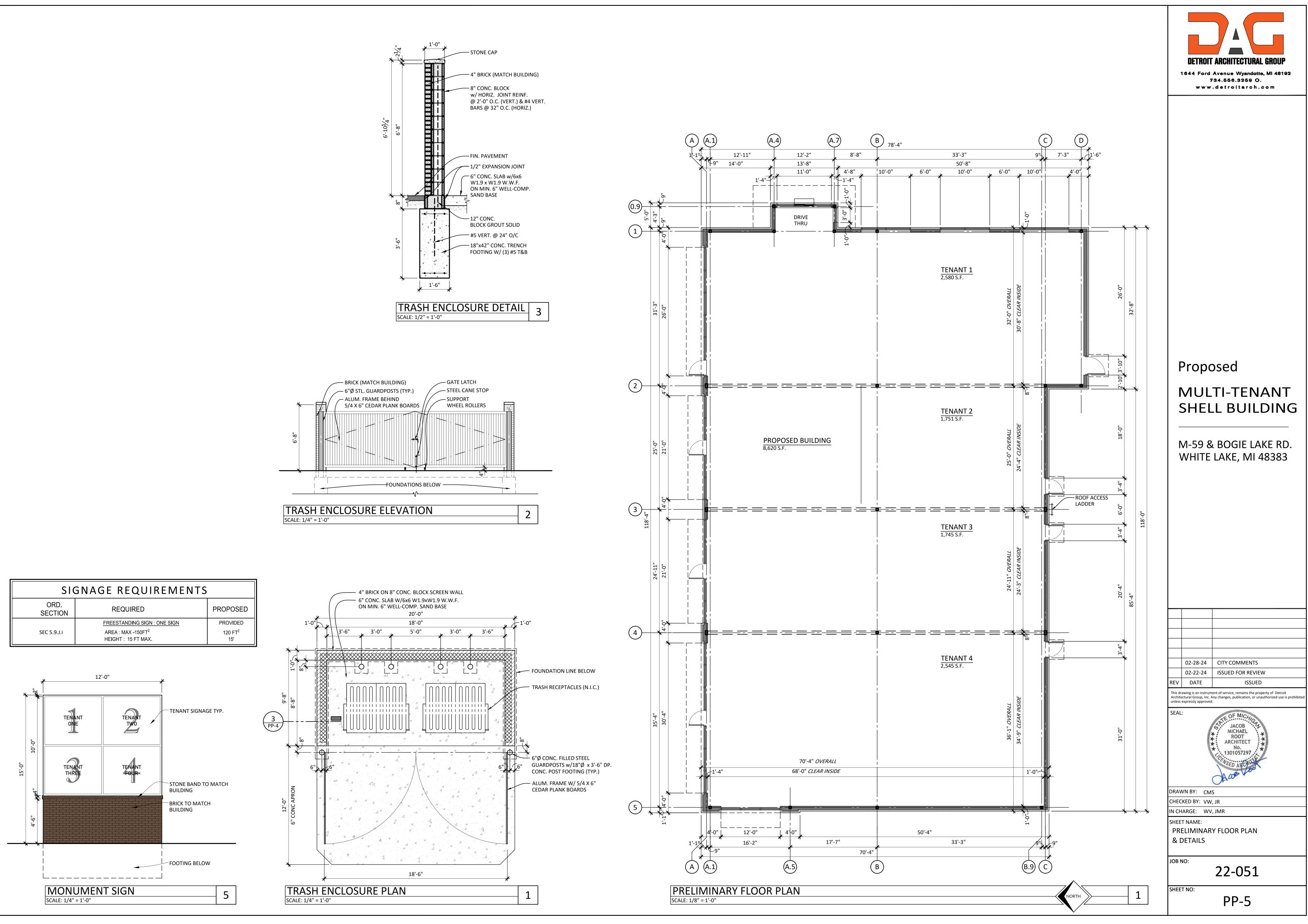
	SCALE:	VERT. – HORZ. AS NOTED
SANITARY SEWER		JOB NO.
STANDARD DETAILS		DATE ISSUED 09/11/97
STINDING DETINES		SHEET NO.



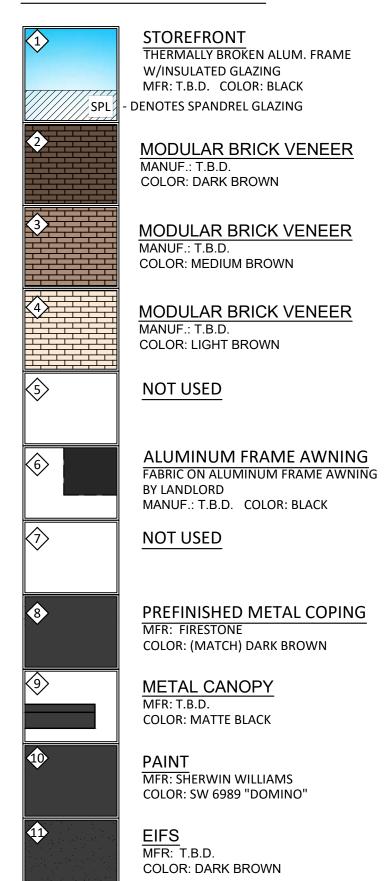
DATE	IN Johnson&/	Anderson		White Lake Township	SUCTOR SHIP OF THE
03/29/04		1060 W. Norton Avenue, Suite 7	2291 Water Street, Suite 6	7525 Highland Road (M-59)	
07/18/05	Waterford, Michigan 48328	Muskegon, Michigan 49441	Port Huron, Michigan 48060	White Lake, Michigan 48383	* 2 1985
04/30/13	tel (248) 681-7800 fax (248) 681-2660	tel (231) 780-3100 fax (231) 780-3115	tel (810) 987-7820 fax (810) 987-7895	248-698-3300	Sons PLASO







EXTERIOR FINISH KEY



GLASS CALCULATION

ELEVATION AREA: 2,631 SF GLASS AREA: 983 SF GLASS RATIO: 983/2,631 = 37.36 %

NOTES: 1. PROVIDE 5/8" FRT PLYWOOD SUBSTRATE AS REQUIRED AS REQUIRED FOR ALL SIGN BOXES, SCONCES, UTILITIES, AWNINGS.

2. ALL GLAZING SHALL BE TEMPERED AS REQUIRED ADJACENT TO DOORS AND FINISHED FLOOR

