Traffic Impact Analysis

Warrenton Village Center

Town of Warrenton, Virginia

June 30, 2023 Revised February 13, 2024



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Executive Summary

This report presents the findings of a Traffic Impact Analysis (TIA) conducted for the proposed Warrenton Village Center development (the Site / the Development / the Property) situated in the Town of Warrenton, Virginia.

This study was developed in accordance with the Virginia Department of Transportation (VDOT) and the Town of Warrenton (the Town) transportation impact analysis guidelines. The document was prepared in accordance with best professional practices and standards that assess the impact of a proposed development on the transportation system. Traffic operational analyses, as presented in this TIA, involve the evaluation of anticipated roadway conditions with and without the proposed development. The analysis assists public officials and developers to balance the interrelations between efficient traffic movements with necessary lane access. This revised TIA is based on review comments provided by VDOT and the Town.

Site Location and Study Area

The proposed development will be located primarily along the southern frontage of Oak Springs Drive (Town Route 3), east of Broadview Avenue (US Route 17 Business) and west of Branch Drive (Town Route 4) in the Town of Warrenton, Virginia. The vehicular study area includes ten existing intersections along Broadview Avenue, Lee Highway, Branch Drive, and Oak Springs Drive.

Description of Proposed Development

The development will be situated on a single parcel of vacant land (approximately 6.46 acres) and a portion of an adjacent developed parcel of land, which can be identified on Fauquier County Tax Maps with the following GPIN #s: 6985-20-7247-000, and 6984-29-6753-000, respectively. The property is currently zoned as C (Commercial District) with a Future Land Use of Mixed Use as part of the New Town Warrenton Character District (Lee Highway Urban Development Area [UDA]).

The Applicant is proposing to apply for a Special Use Permit (SUP) in order to construct approximately 386 multifamily residential dwelling units (320 multifamily apartments, 36 2-over-2 units, and 30 townhomes) and a parking deck. The site has an anticipated build-out date of 2027.

Access to the site will be provided via one full movement parking deck entry along Oak Springs Drive (Town Route 3) forming the fourth leg of the High School Driveway, one full movement driveway along Oak Springs Drive forming the fourth leg to the existing full-movement intersection of Hastings Lane, and via the existing shopping center accesses to the south.

This report analyzes the trips generated by the Warrenton Village Center Development and its impact on traffic operations on the surrounding road network.

Principal Findings and Conclusions

Discussions regarding the study assumptions and relevant background information were held with VDOT, County, and Town staff during January 2023. The scope details the study assumptions and relevant background information discussed. A copy of the scoping document is included in Appendix A.

The analysis contained herein presents the 2023 Existing Conditions, 2027 Future Conditions without Development, and 2027 Future Conditions with Development:

The analysis presented in this report supports the following assumptions and major findings:

Analysis Components

- 2023 existing volumes were derived via turning movement counts collected at intersections within the study area in February 2023.
- As determined based on review comments from VDOT and the Town, an inherent regional growth of 1.0% per year was applied to the Lee Highway mainline through movements at the intersection of Lee Highway at Broadview Avenue (US

Route 17 Business). The growth volumes were balanced along the road network by increasing the mainline through movements at subsequent study intersections along the road network where applicable for the period between 2023 and 2027 to account for 2027 conditions.

- The trip generation associated with the Site was based on the ITE <u>Trip Generation Manual</u>, 11th Edition publication. The Site in total is expected to generate approximately 154 new trips during the AM peak hour, 197 new trips during the PM peak hour, and 2,602 new daily trips on a typical weekday.
- Intersection capacity and queuing analyses were performed for all analysis scenarios at the study area intersections during
 the weekday morning (AM) and weekday afternoon (PM) peak hours. Synchro, version 11, was used to analyze the study
 intersections with results based on the Transportation Research Board's (TRB) Highway Capacity Manual (HCM)
 methodology and analysis guidelines provided in VDOT's Traffic Operations and Safety Analysis Manual (TOSAM) (version
 2). The analysis herein includes level of service (LOS), delay, and queue length comparisons for the turning movements
 analyzed.
- The analysis also considers an assessment of historical crash data at all existing study intersections.
- The analysis also includes preliminary access management assessment and turn lane warrant assessments for the Site
 access points along Oak Springs Drive.

Analysis Results

2023 Existing Conditions

- Based on the capacity analysis of Existing Conditions, the two signalized study intersections operate at an overall level of service D or better during both the AM and PM peak hours.
- Based on the capacity analysis of Existing Conditions, three study intersections have at least one approach that operates
 at levels of service (LOS E or F) for at least one peak hour. The remaining intersection approaches operate at acceptable
 levels of service during both peak hours.
- Based on the analysis of the Synchro 95th percentile queue lengths, all turning movements have queue lengths that can
 be accommodated within the available storage length of the turn bays, except the southbound left turn movement at Study
 Intersection 1 (Broadview Avenue / Lee Highway at Winchester Street).

2027 Future Conditions without Development

- Based on the capacity analysis of 2027 Future Conditions with Development, the signalized study intersection would
 operate at an overall level of service D or better during both the AM and PM peak hours.
- The planned roundabout is expected to operate at an overall LOS B or better with all approaches operating at LOS D or better during the AM and PM peak hours.
- Based on the capacity analysis of 2027 Future Conditions without Development, two study intersections have at least one approach that would operate at levels of service (LOS E or F) for at least one peak hour. The remaining intersection approaches would operate at acceptable levels of service during both peak hours.
- Based on the analysis of the Synchro 95th percentile queue lengths, all turning movements have queue lengths that could be accommodated within the available storage length of the turn bays.

2027 Future Conditions with Development

 The Site is expected to generate approximately 154 new total trips during the AM peak hour, 197 new trips during the PM peak hour and 2,602 new trips during a typical weekday.

- Based on the capacity analysis of 2027 Future Conditions with Development, the signalized study intersection would
 operate at an overall level of service D or better during both the AM and PM peak hours.
- The planned roundabout is expected to operate at an overall LOS B with all approaches operating at LOS D or better during the AM and PM peak hours.
- Based on the capacity analysis of the 2027 Future Conditions with Development, two study intersections have at least
 one approach that would operate at levels of service (LOS E or F) for at least one peak hour (similar to 2027 Future
 Conditions without Development) during the AM and PM peak hours. The remaining intersection approaches would
 operate at acceptable levels of service during both peak hours.
- Based on the queuing analysis performed for the 2027 Future Conditions with Development, all turning movements have queue lengths that could be accommodated within the available storage length of the turn bays.

Overall Conclusion

Based on the capacity and queueing analysis results, the proposed Development will not have a substantial impact to the surrounding transportation and roadway network, assuming that the site is constructed as depicted on the concept plan. No improvements are warranted or recommend to accommodate the proposed Development.

Introduction

This report presents the findings of a Traffic Impact Analysis (TIA) conducted for the proposed Warrenton Village Center (the Site / the Development / the Property) along the southern frontage of Oak Springs Drive (Town Route 3), east of Broadview Avenue (US Route 17 Business) and west of Branch Drive (Town Route 4) in the Town of Warrenton, Virginia

The development will be situated on a single parcel of vacant land (approximately 6.46 acres) and a portion of an adjacent developed parcel of land, which can be identified on Fauquier County Tax Maps with the following GPIN #s: 6985-20-7247-000, and 6984-29-6753-000, respectively. The property is currently zoned as C (Commercial District) with a Future Land Use of Mixed Use as part of the New Town Warrenton Character District (Lee Highway Urban Development Area [UDA]).

The Applicant is proposing to apply for a Special Use Permit (SUP) in order to construct approximately 386 multifamily residential dwelling units (320 multifamily apartments, 36 2-over-2 units, and 30 townhomes) and a parking deck. The site has an anticipated build-out date of 2027.

Access to the site will be provided via one full movement parking deck entry along Oak Springs Drive (Town Route 3) forming the fourth leg of the High School Driveway, one full movement driveway along Oak Springs Drive forming the fourth leg to the existing full-movement intersection of Hastings Lane, and via the existing shopping center accesses to the south.

The following tasks were completed as part of this study effort:

- A scoping meeting was held on January 3, 2023 with the Virginia Department of Transportation (VDOT), Fauquier County
 (the County), and the Town of Warrenton (Town) staff to discuss the parameters of this study as well as any relevant
 background information. A copy of the scoping document is included in Appendix A.
- Review comments of the first TIA submission were provided and addressed in this study submission.
- Existing conditions were observed in the field to verify roadway geometry, pedestrian and bicycle infrastructure, and traffic flow characteristics.
- Signal timings were acquired from VDOT and are provided in Appendix E.
- In order to determine the weekday morning and afternoon peak hour turning movement traffic volumes, traffic counts were conducted in February 2023.
- The 2027 Future Conditions without Development scenario was projected based on the existing traffic volumes, an
 inherent growth to account for regional growth on the roadway network, two approved background developments, and
 roadway improvements.
- Proposed site traffic volumes were derived based on the methodology outlined in ITE's <u>Trip Generation Manual</u>, 11th
 Edition, publication and were assigned to the road network based on the agreed-upon direction of approach discussed during the aforementioned scoping meeting.
- The 2027 Future Conditions with Development scenario was projected based on the existing traffic volumes, regional
 growth, and the projected trips generated by the proposed development.
- Intersection capacity and queueing analyses were performed for the identified study intersections for the 2023 Existing
 Conditions, 2027 Future Conditions without Development, and 2027 Future Conditions with Development scenarios
 during the weekday morning (AM), and weekday afternoon (PM) peak hours.
- Intersection capacity and queuing analyses were performed using Synchro, version 11, with LOS and delay results based
 on the Transportation Research Board's (TRB) <u>Highway Capacity Manual</u> (HCM) 6 methodology and in following VDOT's
 <u>Traffic Operations and Safety Manual</u> (TOSAM) (version 2).
- The analysis also considers an assessment of historical crash data at all study intersections.

- The analysis also includes preliminary access management assessment and turn lane warrant assessments for the Site
 access points along Oak Springs Drive.
- The study also includes preliminary discussions on the pedestrian facilities in the study area.

Sources of data for this study include the Institute of Transportation Engineers (ITE), VDOT, the County, the Town and the office files and field reconnaissance efforts of Gorove Slade.

Background Information: Proposed Development (Site & Nearby)

Description of the Existing Site

Site Location

The proposed Development will be located primarily along the southern frontage of Oak Springs Drive (Town Route 3), east of Broadview Avenue (US Route 17 Business) and west of Branch Drive (Town Route 4) in the Town of Warrenton, Virginia. A description of the proposed Development is provided in the *Introduction* section of this report.

Location within Jurisdiction and Region

The Site is located generally on the northern portion of Warrenton approximately 0.5 miles from the north Town line an approximately 1 mile west of the US 17 and US 29 Business interchange. A regional aerial of the Site is provided in **Figure 1**.

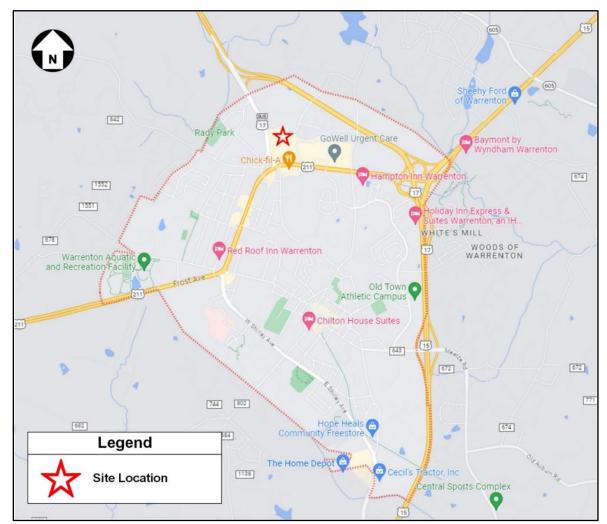


Figure 1: Regional Location

Description of the Parcel

The development will be situated on a single parcel of vacant land (approximately 6.46 acres) and a portion of an adjacent developed parcel of land, which can be identified on Fauquier County Tax Maps with the following GPIN #s: 6985-20-7247-000, and 6984-29-6753-000 as illustrated in **Figure 2.**



Figure 2: Parcel Map

(Source: https://fauquiergis.maps.arcgis.com/)

Existing Zoning and Future Land-Use

The property is currently zoned as C (Commercial District) with a Future Land Use of Mixed Use as part of the New Town Warrenton Character District (Lee Highway Urban Development Area [UDA]).

The existing zoning is presented in Error! Reference source not found.; the Town of Warrenton 2040 Comp Plan future land use is presented in **Figure 4**.

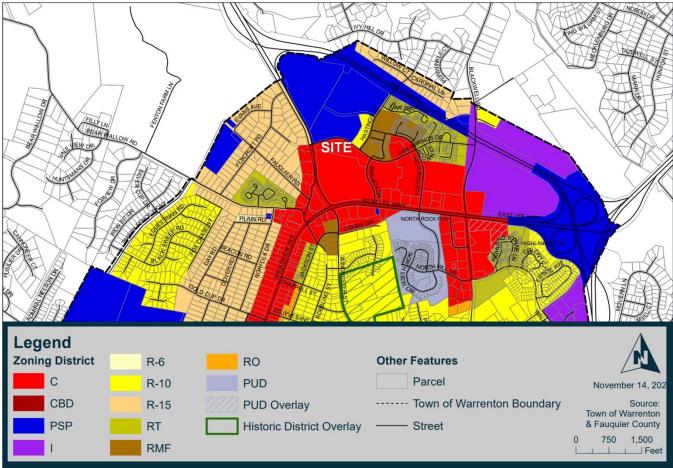


Figure 3: Town of Warrenton Zoning Map

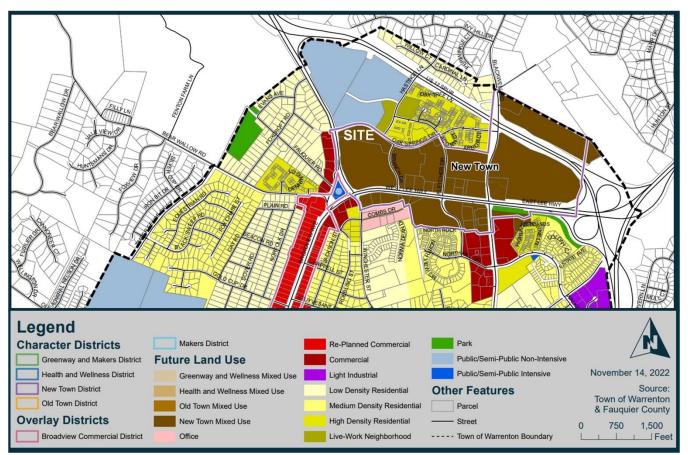


Figure 4: Town of Warrenton Future Land Use Map

Descriptions of Geographic Scope of Study and Limits of the Study Area

The geographic scope of the study area was developed in accordance with VDOT and County guidance. The vehicular study area includes ten existing study intersections. At build out of the Site, the proposed site driveways will form the fourth leg of two existing intersections.

The existing study intersections are as follows:

- Intersection 1: Broadview Avenue (US Route 17) / Lee Highway at Broadview Avenue / Winchester Street [existing full-movement, signalized],

 Intersection 2: Lee Highway (US Route 17) at Warrenton Village Center Driveway at Chick-fil-a Driveway [existing full-movement, unsignalized],
- Intersection 3: Lee Highway (US Route 17) at Branch Drive (Town Route 4) [existing full-movement, signalized],
- Intersection 4: Branch Drive (Town Route 4) at Warrenton Village Driveway / Safeway Driveway [existing full-movement, unsignalized],
- Intersection 5: Oak Springs Drive (Town Route 3) at Branch Drive (Town Route 4) / Cedar Crest Drive [existing full-movement, unsignalized],
- Intersection 6: Oak Springs Drive (Town Route 3) at Hastings Lane / Future Access [existing full-movement, unsignalized, future fourth leg],

Intersection 7: Oak Springs Drive (Town Route 3) at Highland School Driveway / Future Garage Access [existing full-movement, unsignalized, future fourth leg],

Intersection 8: Broadview Avenue (US Route 17 Business) at Oak Springs Drive (Town Route 3) [existing full-movement, unsignalized],

Intersection 9: Broadview Avenue (US Route 17 Business) at Warrenton Village Center South Driveway [existing full-movement, unsignalized],

Intersection 10: Broadview Avenue (US Route 17 Business) at Warrenton Village Center North Driveway [existing full-movement, unsignalized].

An aerial of the study intersections is provided in Figure 5.



Figure 5: Aerial of Study Boundaries (Study Intersections)

Existing Roadway Network

A description of the major roadways within the immediate vicinity of the Site is presented below in Error! Reference source not found.

Table 1: Summary of Existing Road Network

Roadway	RTE#	VDOT Classification	Legal/Design Speed Limit (mph)	Lanes	AADT (vpd)	Road Segment Between:		k-factor
Broadview Avenue	US 17 Bus	Other Principal Arterial	35	4 Div	11,000	Bus US 29 Lee Hwy	NCL Warrenton	9.7%
Oak Springs Drive	Town 3	Major Collector	25	2 Undiv	3,100	Broadview Ave	Branch Dr	10.3%
Branch Drive	Town 4	Major Collector	25	4 Undiv	4,300	Lee Highway	Oak Springs Drive	11.1%
Lee Highway	US 211/29 Bus	Other Principal Arterial	40	4 Div	26,000	US 17 Broadview	US 15 Blackwell	7.7%

<u>Lee Highway (US Route 211/US Route 29 Business)</u> is generally a four-lane divided Principal Arterial with a posted speed limit of 40 mph within the vicinity of the Site. The 2021 VDOT ADT on Lee Highway is 26,000 vehicles per day (vpd). For the purposes of this analysis, Lee Highway is assumed to be an east-west roadway.

<u>Broadview Avenue (US 17 Business)</u> is a four-lane divided Principal Arterial with a posted speed limit of 35 mph and a 2021 VDOT ADT of approximately 11,000 vpd. For the purposes of this study, Broadview Avenue is assumed to be a north-south roadway.

<u>Branch Drive (Town Route 4)</u> is a four-lane, undivided Major Collector with a posted speed limit of 25 mph and a 2021 VDOT ADT of approximately 4,300 vpd. For the purposes of this study, Branch Drive is assumed to be a north-south roadway.

<u>Oak Springs Drive (Town Route 3)</u> is a two-lane, undivided Major Collector with a posted speed limit of 25 mph and a 2021 VDOT ADT of approximately 3,100 vpd. For the purposes of this study, Oak Springs Drive is assumed to be an east-west roadway.

Analysis of 2023 Existing Conditions

Existing Roadway Safety Assessment

As agreed upon in the aforementioned scoping meeting, existing crash reports for all existing study intersections over a five-year period between May 2018 and May 2023 were provided by VDOT's Crash Analysis Tool. These reports are summarized in **Table 2** and **Table 3**.

During the five-year period, a total of 88 crashes were recorded at the ten existing study intersections as illustrated in Error! Reference source not found. Of the 88 recorded crashes, 58 were classified as "Property Damage Only (PDO)," 30 were classified as "Injury Collision (IC), and zero fatalities occurred during the five-year period.

An aerial of the recorded crash locations is provided in **Figure 6**. The crash data by study intersection is provided in Appendix B.

The intersection crash rate was computed for the existing study intersections using the following formula and was calculated as crashes per one million entering vehicles (MEV). The approach average daily traffic volumes (ADT_{approach}) were derived from calculations based on the existing link ADTs.

$$Rate_{intersection} = \frac{1,000,000* \# of Crashes}{\# of Years*365 \left(\frac{days}{year}\right)* ADT_{approach}}$$

It should be noted that according to the Institute of Transportation Engineers' (ITE) <u>Transportation Impact Analysis for Site Development</u>, a crash rate of 1.0 MEV or higher is an indication that further study may be required. A rate over 1.0 MEV does not necessarily mean there is a significant problem at an intersection, but rather it is a threshold used to identify which intersections may have an elevated crash rate due to operational, geometric, or other deficiencies. Based on the crash rates, none of the existing study intersections were considered high crash locations.

The following tables provide detailed reported crash data for all study intersections.

Table 2: Historical Crash Data Summary (May 2018 - May 2023)

Inte	rsection	Approximate ADT	PDO	IC	Fatality	Total	Crash Rate (Per MEV)
1	Lee Highway (US 211/US 29 BUS) at Broadview Avenue	29,125	28	12	0	40	0.75
2	Lee Highway (US 211/US 29 BUS) at Warrenton Village /	21,375	3	2	0	5	0.13
3	Lee Highway (US 211/US 29 BUS) at Branch Drive	23035	14	5	0	19	0.45
4	Branch Drive at Warrenton Village / Safeway	4485	1	1	0	2	0.24
5	Branch Drive at Oak Springs Drive	4000	2	0	0	2	0.27
6	Oak Springs Drive at Hastings Lane	No Crashes	0	0	0	0	0.00
7	Oak Springs Drive at Highland School Entrance	No Crashes	0	0	0	0	0.00
8	Broadview Avenue at Oak Springs Drive	12010	2	1	0	3	0.14
9	Broadview Avenue at Warrenton Village North	10425	2	2	0	4	0.21
10	Broadview Avenue at Warrenton Village South	13165	6	7	0	13	0.54
Tota	l Reported Crashes Analyzed		58	30	0	88	-
Perc	entages		65.9%	34.1%	0.0%	100.0%	-

Based on the crash rates, none of the existing study intersections were considered high crash locations, however, Study Intersections 1 and 10 are on the Culpepper District top 100 PSI list. A pipeline study has been conducted and these locations have been identified for construction of roundabouts.

Table 3: VDOT Crash Data Summary by Type of Collision (May 2018 - May 2023)

		Fixed Object/Single		Sideswipe (Same	Sideswipe (Opposite							
Inte	rsection	Vehicle	Head-on	Direction)	Direction)	Rear End	Angle	Backing	Pedestrian	Animal	Other	Total
1	Lee Highway (US 211/US 29 BUS) at Broadview Avenue	0	0	3	0	24	11	0	0	0	2	40
2	Lee Highway (US 211/US 29 BUS) at Warrenton Village /	2	0	0	0	1	2	0	0	0	0	5
3	Lee Highway (US 211/US 29 BUS) at Branch Drive	1	0	1	1	6	8	1	0	0	1	19
4	Branch Drive at Warrenton Village / Safeway	0	0	0	0	0	2	0	0	0	0	2
5	Branch Drive at Oak Springs Drive	0	0	0	0	0	2	0	0	0	0	2
6	Oak Springs Drive at Hastings Lane	0	0	0	0	0	0	0	0	0	0	0
7	Oak Springs Drive at Highland School Entrance	0	0	0	0	0	0	0	0	0	0	0
8	Broadview Avenue at Oak Springs Drive	0	0	0	0	0	3	0	0	0	0	3
9	Broadview Avenue at Warrenton Village North	0	0	0	0	0	3	0	0	1	0	4
10	Broadview Avenue at Warrenton Village South	0	3	1	0	1	7	0	0	0	1	13
Tota	I Reported Crashes Analyzed	3	3	5	1	32	38	1	0	1	4	88
Perc	centages	3.4%	3.4%	5.7%	1.1%	36.4%	43.2%	1.1%	0.0%	1.1%	4.5%	100.0%

Approximately 43% of the crashes that occurred were classified as angle collisions and approximately 36% were classified as rear end collisions. Rear end and angle collisions are common at congested signalized intersections. Study Intersection 1 has been identified as a location for a potential roundabout.

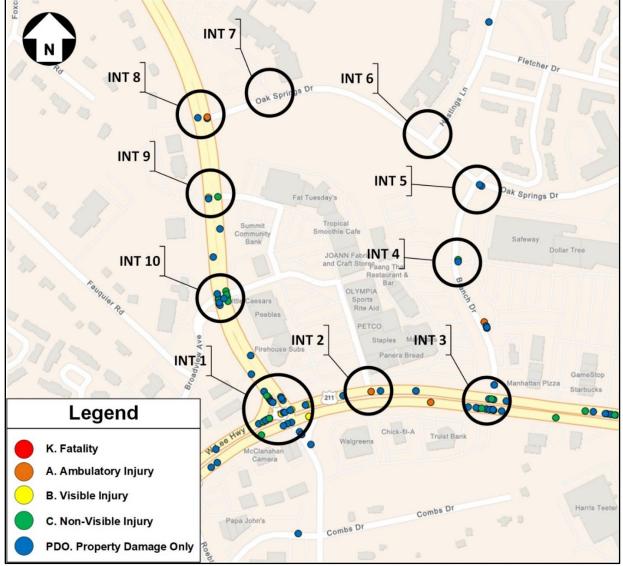


Figure 6: Recorded Crash Location Map

2023 Existing Traffic Volumes

In order to determine the weekday morning (AM) and weekday afternoon (PM) peak hour turning movement traffic volumes, turning movement counts (TMC) were collected at the study intersections in February 2023. The referenced weekday turning movement counts were collected from the hours of 6:00 AM to 9:00 AM and 4:00 PM to 7:00 PM:

- Study Intersection 1: Lee Highway (US 211/US 29 BUS) at Broadview Avenue (US 17 BUS)
- o Study Intersection 2: Lee Highway (US 211/US 29 BUS) at Warrenton Village / Chick-fil-a Driveway
- Study Intersection 3: Lee Highway (US 211/US 29 BUS) at Branch Drive
- o Study Intersection 4: Branch Drive at Warrenton Village / Safeway
- Study Intersection 5: Branch Drive at Oak Springs Drive
- Study Intersection 6: Oak Springs Drive at Hastings Lane
- o Study Intersection 7: Oak Springs Drive at Highland School Entrance
- Study Intersection 8: Broadview Avenue at Oak Springs Drive
- Study Intersection 9: Broadview Avenue at Warrenton Village North
- Study Intersection 10: Broadview Avenue at Warrenton Village South
- From the turning movement counts, the following system peak hours were determined.

AM Peak Hour: 7:30 AM to 8:30 AM

PM Peak Hour: 4:00 PM to 5:00 PM

The 2023 existing road network configuration is presented in **Figure 7**. The existing AM and PM peak hour traffic volumes for the existing study intersections are shown in **Figure 8**. The ADT volumes, depicted in **Figure 8** and in subsequent volume graphics, were calculated based on VDOT published k-factors from 2021, if available, or assumed k-factors per approach of 0.10 and the PM peak hour volumes. The raw existing traffic count data is provided in Appendix C.

In addition to turning movement volumes, pedestrians crossing data was collected at all study intersections. The peak hour pedestrian crossing data is presented in **Figure 9**.

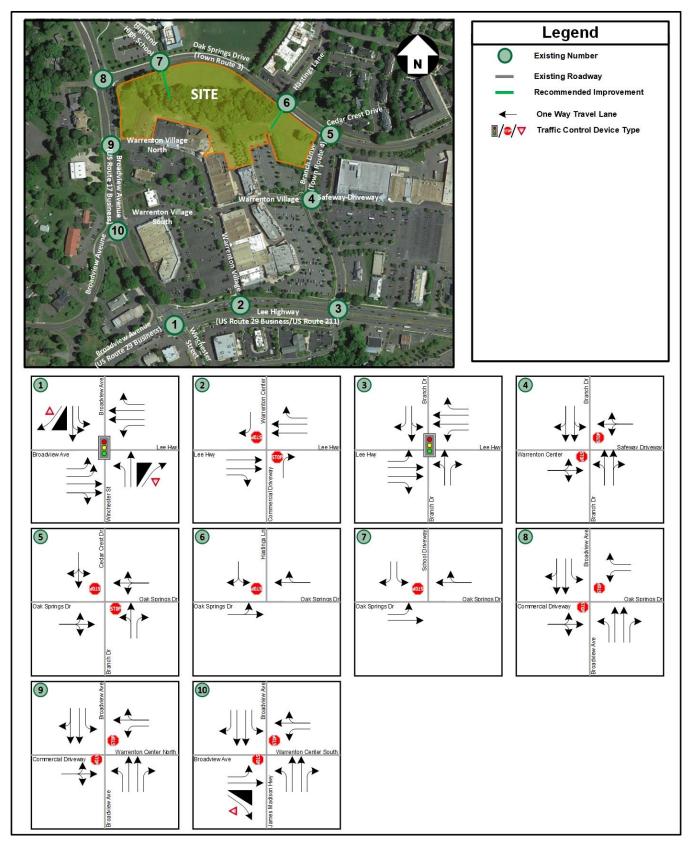


Figure 7: 2023 Existing Conditions – Roadway Network Geometric Configuration and Traffic Control Devices

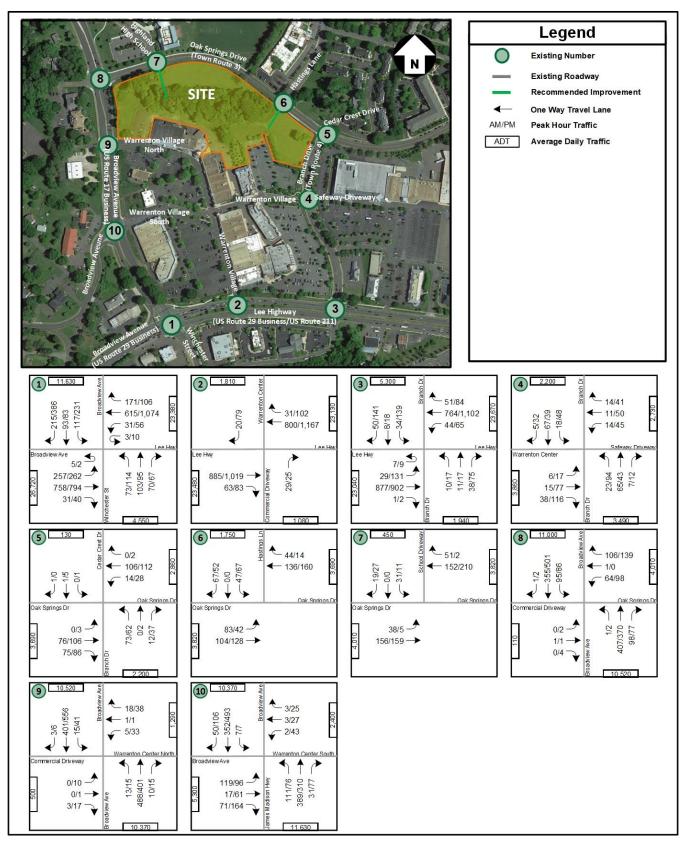


Figure 8: 2023 Existing Conditions – Vehicular Traffic Volumes

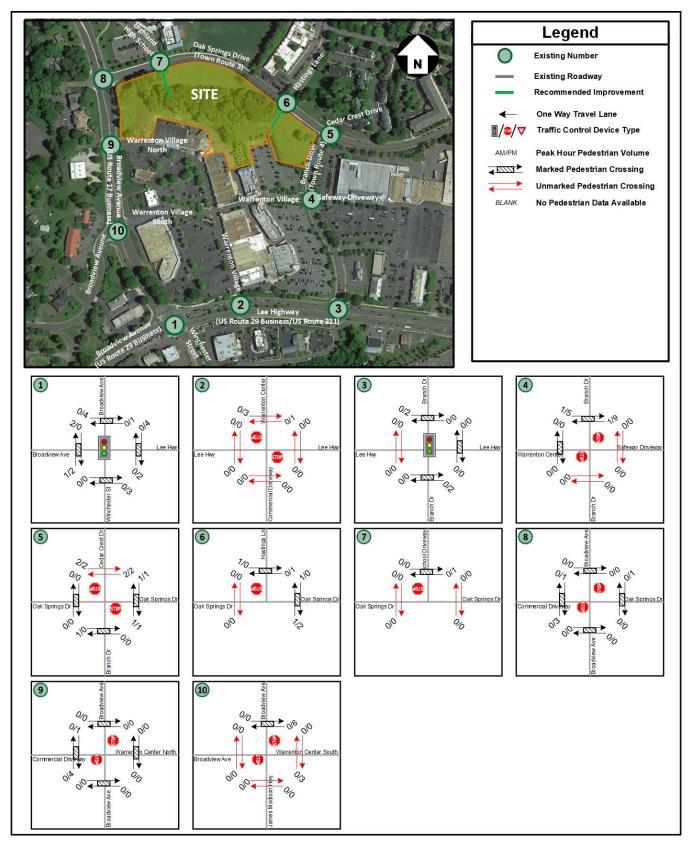


Figure 9: 2023 Existing Conditions - Pedestrian Volumes

Existing Intersection Capacity and Queueing Analysis

Intersection capacity and queuing analyses were performed for the 2023 Existing Conditions scenario at the study area intersections during AM and PM peak hours, in accordance with VDOT's *TOSAM* (version 2) guidelines. *Synchro*, version 11, was used to analyze the study intersections with results based on the Transportation Research Board's (TRB) <u>Highway Capacity Manual</u> (HCM) 6th edition methodology¹ and include level of service (LOS), delay, and queue length comparisons for the turning movements analyzed. Lane configurations at study intersections along the road network were field-verified, and the existing traffic volumes discussed in the aforementioned section as well as other relevant data were entered into the analysis models.

Signal timings were obtained from VDOT and were utilized as a base for the analysis models. Traffic operation conditions as well as lane configurations were field verified. The existing traffic volumes discussed in the aforementioned section as well as other relevant data were entered into the analysis models. For the purposes of this analysis, the existing peak hour factors (PHF) utilized in the analysis of existing conditions were based on the 2023 existing volumes and were modeled in the *Synchro* network on a by-intersection basis. PHF in the range of 0.85 to 1.00 were used for the existing scenario, as agreed to in the scoping document. The heavy vehicle percentages (HV%) utilized per movement were based on the existing traffic counts collected. Pedestrian crossing data utilized per crossing were based on the existing traffic counts collected. Based on *Synchro* guidance and pedestrian count data, all pedestrian calls at both signalized intersections were set to five calls per hour. Note that for analysis purposes, all turning movement counts were coded with a minimum volume of one vehicle in *Synchro*.

Per the scoping meeting with VDOT and Town staff, it would be considered acceptable and/or desirable to achieve an approach LOS D or better for traffic operations using HCM methodology. The results of the intersection capacity and queuing analyses from *Synchro* are presented in **Table 4** and graphically in **Figure 10**. The results are expressed in LOS and delay (seconds per vehicle) for overall signalized/all-way stop control intersections and per approach and lane group for all study intersections. Any overall signalized intersection or approach that operates at LOS E or F is displayed in red.

The queue lengths were reported as the 95th percentile queues from *Synchro* and are expressed in feet. The lane groups where the queue lengths exceeded the available effective storage capacity of existing turn lanes are displayed in red.

The description of different LOS and delay are included in Appendix D. The signal timing data provided by VDOT is included in Appendix E. The detailed analysis worksheets of 2023 Existing Conditions are contained in Appendix F.

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¹ It should be noted that HCM 2000 methodology was used in lieu of HCM 6th if the HCM 6th methodology was not applicable. HCM 6th could not be applicable in such cases as nonstandard National Electrical Manufacturers Association (NEMA) configurations, shared lane configurations, placement of loop detectors, U-turns, etc.

Table 4: 2023 Existing Conditions - Intersection Capacity Analysis Results

				AM Peak Ho			PM Peak Hour		
No.	Intersection (Movement)	Effective Storage Length (ft.)	LOS	Delay (sec/veh)	95th % Queue (ft.) ^[2]	LOS	Delay (sec/veh)	95th % Queue [2]	
				Synchro			Synchro		
1	Broadview Ave (E/W) at Winchester St (N/S)								
	Overall Intersection (Signalized)		D	36.4		D	39.4		
	Eastbound Approach		<u>Б</u>	34.2		<u>Б</u> D	40.6		
	Eastbound Left	250	E	64.9	186	E	72.0	193	
	Eastbound Thru/Right	200	C	24.0	428	C	30.6	428	
	Westbound Approach		C	25.5	i -	C	25.9		
	Westbound Left	130	F	89.7	78	F	93.8	m119	
	Westbound Thru		В	19.8	143	С	22.7	192	
	Westbound Right	200	С	33.6	46	В	16.8	m15	
	Northbound Approach		E	60.3		E	66.6		
	Northbound Left	250	Е	61.7	126	Е	74.8	188	
	Northbound Thru		Е	66.5	166	Е	67.3	160	
	Northbound Right	125	D	49.9	0	D	51.7	17	
	Southbound Approach		D	49.2		D	50.9		
	Southbound Left	215	Е	63.1	167	Е	59.2	251	
	Southbound Left/Thru		Е	62.0	171	Е	59.0	257	
	Southbound Right		D	36.1	95	D	44.2	417	
2	Broadview Ave (E/W) at Warrenton Village Center Dwy (Chipotle)/Walgreens Dwy (N/S) Overall Intersection (TWSC)								
	Northbound Approach	······································	В	12.6		В	13.4		
	Northbound Right		В	12.6	5	В	13.4	5	
	Southbound Approach		В	10.7	<u>-</u>	В	13.3		
	Southbound Right		В	10.7	3	В	13.3	15	
3	Broadview Ave (E/W) at Branch Dr (N/S)								
	Overall Intersection (Signalized)		В	16.2		С	31.6		
	Eastbound Approach		A	9.0		C	20.9		
	Eastbound Left	240	F	81.5	m80	F	80.8	225	
	Eastbound Thru		A	6.0	133	В	11.6	226	
	Eastbound Right	330	Α	9.9	m0	В	13.4	m0	
	Westbound Approach		В	15.8		С	28.5		
	Westbound Left	150	Е	67.4	88	Е	78.5	123	
	Westbound Thru		В	13.2	394	С	26.4	610	
	Westbound Right	150	Α	9.8	0	В	17.3	0	
	Northbound Approach		E	60.3		E	67.0		
	Northbound Left/Thru		Е	61.0	43	Е	68.6	73	
	Northbound Right	60	E	59.9	0	E	66.2	0	
	Southbound Approach		E	64.7		E	69.4		
	Southbound Left/Thru		E	67.2	86	E	78.8	249	
	Southbound Right		Е	62.7	0	Е	59.0	53	
4	Warrenton Village Center Dwy/Shopping								
	Center Dwy (E/W) at Branch Dr (N/S)								
	Overall Intersection (TWSC)								
	Eastbound Approach		A	9.4	_	В	11.8	2.0	
	Eastbound Left/Thru/Right		A	9.4	8	В	11.8	30	
	Westbound Approach		В	10.1	ا	В	14.2		
	Westbound Left/Thru/Right		В	10.1	5	В	14.2	28	
	Northbound Approach			- .			7.5	_	
	Northbound Approach		Α	7.4	3	Α	7.5	5	
	Southbound Approach			7.4			7.4	^	
5	Southbound Left Oak Springs Dr (E/W) at Branch Dr (N/S)		A	7.4	0	A	7.4	3	
•									
	Overall Intersection (TWSC)								
	Eastbound Approach		_		_	_		_	
	Eastbound Left		A	7.5	0	Α	7.5	0	
	Westbound Approach								
	Westbound Left		Α	7.7	0	Α	7.7	3	
	Northbound Approach		В	11.2		В	11.4		
	Northbound Left/Thru		В	11.6	13	В	12.6	13	
	Northbound Right		Α	9.0	0	Α	9.4	5	
	Southbound Approach		В	10.0		В	10.9		
	Southbound Left/Thru/Right		В	10.0	0	В	10.9	0	

Table 4 (Continued): 2023 Existing Conditions - Intersection Capacity Analysis Results

				AM Peak Hou			PM Peak Ho	
No.	Intersection (Movement)	Effective Storage Length (ft.)	LOS	Delay (sec/veh)	95th % Queue (ft.) ^[2]	LOS	Delay (sec/veh)	95th % Queue [2]
6	Oak Springs Dr (E/W) at Hastings Ln /			Synchro			Synchro	
О	Future Access (N/S)							
	Overall Intersection (TWSC)							
	Eastbound Approach							
	Eastbound Left		Α	7.9	5	Α	7.7	3
	Southbound Approach		В	7.9 11.5	5	<u>А</u> В	11.3	s
	Southbound Left/Thru/Right		В	11.5 11.5	10	В	11.3 11.3	18
7	Oak Springs Dr (E/W) at Highland School			11.5	18	В	11.3	10
•	Dwy / Future Garage Access (N/S)							
	Overall Intersection (TWSC)							
	Eastbound Approach				_	_		
	Eastbound Left	75	Α	7.8	3	A	7.7	0
	Southbound Approach		В	11.2		В	10.2	
	Southbound Left/Thru		В	12.3	5	В	11.5	3
	Southbound Right	ļ	Α	9.4	3	A	9.7	3
8	Oak Springs Dr (E/W) at Broadview Ave (N/S)							
	Overall Intersection (TWSC)							
	Eastbound Approach		D	25.2		С	16.8	
	Eastbound Left/Thru/Right		D	25.2	0	C	16.8	3
	Westbound Approach		С	23.0		D	27.5	
	Westbound Left/Thru	125	Е	42.8	53	F	51.1	83
	Westbound Right		В	10.8	15	В	10.8	18
	Northbound Approach							
	Northbound Left	90	Α	8.1	0	Α	8.6	0
	Southbound Approach							
	Southbound Left	225	Α	9.3	10	Α	8.7	8
9	Warrenton Village North Dwy (E/W) at Broadview Ave (N/S) Overall Intersection (TWSC)							
	Eastbound Approach		Α	9.9		С	20.3	
	Eastbound Left/Thru/Right		A	9.9	0	C	20.3	10
	Westbound Approach		 B	13.8	············	C	18.5	
	Westbound Left		C	22.9	3	D	27.8	18
	Westbound Thru/Right		В	11.4	3	В	10.6	5
	Northbound Approach			11.4			10.0	
	Northbound Left	150	Α	8.3	0	Α	8.8	3
	Southbound Approach	130	Д	0.3	U	^	0.0	<u></u>
	Southbound Left	110	Α	8.7	3	Α	8.4	3
10	Warrenton Village South Dwy/Broadview	110	Α	0.7	3	Α	0.4	3
	Ave (E/W) at Broadview Ave/Winchester St							
	(N/S)							
	Overall Intersection (TWSC)							
	Eastbound Approach		E	38.8		D	28.4	
	Eastbound Left		F	57.3	110	F	52.1	83
	Eastbound Thru		D.	29.6	10	E	36.7	40
	Eastbound Right		В	10.1	8	В	11.5	25
	Westbound Approach		С	21.4		D	33.0	
	Westbound Left		D	28.0	0	E	47.2	38
	Westbound Thru/Right		С	19.2	3	C	21.3	20
	Northbound Approach	·····		10.4		<u>-</u>		20
	Northbound Left	160	Α	8.7	10	Α	9.2	8
	Southbound Approach	100	^	0.1	IU	^	3.∠	Ö
	Southbound Left	160	Α	8.4	0	Α	8.2	0

NOTES:

 ^[1] Effective storage length is based on the storage length plus one-half of the taper length per TOSAM guidelines.
 [2] m: 95th percentile volume and queues (reported from Synchro) are metered by upstream signal.

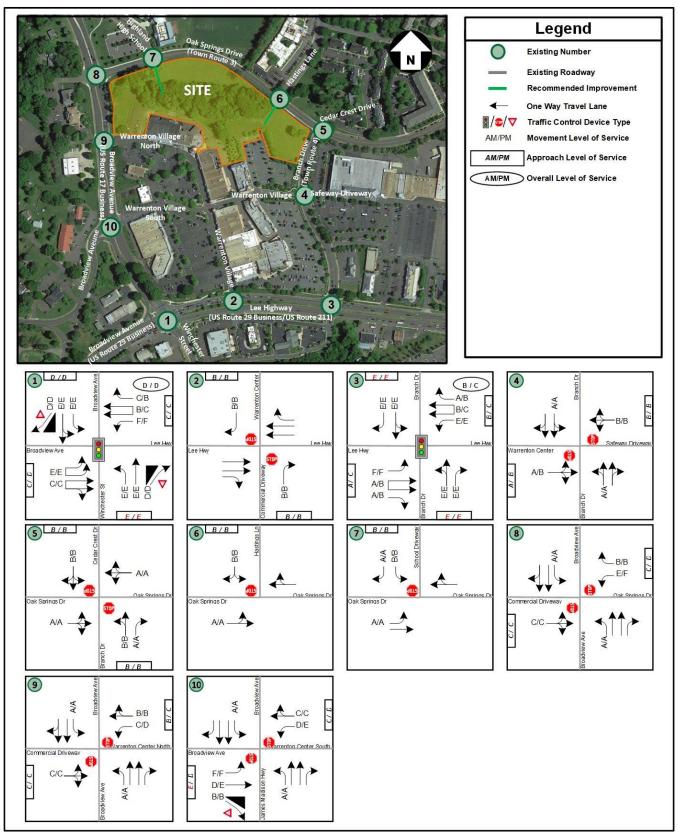


Figure 10: 2023 Existing Conditions – Level of Service Results

Based on the capacity analysis of existing conditions, the two signalized study intersections operate at overall levels of service of D or better during both the AM and PM peak hours.

Based on the capacity analysis of existing conditions, the approaches of all study intersections operate at approach levels of service of D or better during both the AM and PM peak hours, except for the following study intersections that have at least one approach that operates at levels of service E or F during at least one peak hour:

- Study Intersection 1: Lee Highway (US 211/US 29 BUS) at Broadview Avenue / Winchester Street
- Study Intersection 3: Lee Highway (US 211/US 29 BUS) at Branch Drive
- Study Intersection 10: Broadview Avenue at Warrenton Village South

Based on the queuing analysis performed for existing conditions, all turning movements at the study intersections have maximum queue lengths that are accommodated within the available storage lengths of the turn bays except for the southbound left turn movement at Study Intersection 1 (Lee Highway at Broadview Avenue / Winchester Street).

Analysis of 2027 Future Conditions Without Development

For the purposes of this study, the Development is anticipated to be constructed by 2027; this scenario analyzes the future without development conditions for the year 2027.

Future without Development Traffic Volumes

The derivation of future without development traffic volumes was based on assumptions and parameters discussed with VDOT and the County during the scoping process for this study. The future conditions include anticipated inherent regional growth, the inclusion of any potential background developments in the pipeline around the vicinity of the Site, and any anticipated roadway improvements.

Inherent Regional Growth

The Development is anticipated to be complete in 2027. In order to account for increased demand on the traffic network between 2023 and 2027, an inherent growth rate was applied to the future scenarios. This "inherent" growth was anticipated to account for regional development within the at-large area, which would ultimately result in increased roadway demand. Furthermore, the inherent growth was anticipated to account for any potential background developments unaccounted for within the vicinity of the study area.

To account for 2027 future conditions, an inherent growth rate of 1.0%, (compounded annually) over a four-year period, between 2023 to 2027 (and totaling 4.06% growth of the existing volumes) was applied to the Lee Highway mainline through movements at the intersection of Lee Highway at Broadview Avenue / Winchester Street. The growth volumes were balanced along the road network by increasing the mainline through movements at subsequent study intersections along the road network where applicable.

The inherent regional growth volumes (for the period between 2023 and 2027) are illustrated in Figure 11.

Potential Background Development(s)

In addition to the applied inherent regional growth reflecting increased regional traffic demand, a total of two "background" developments within the vicinity of the Site, with their locations depicted in **Figure 12**, were identified in the meeting with VDOT and Town staff for inclusion in this study. The background developments included are as follows:

- 1. Waterloo Junction
 - Located in the southeast quadrant of Bear Wallow Road and Norfolk Drive, the Waterloo Junction development is anticipated to include 47 townhomes, 6 apartments, and 3,600 square feet of retail space.
- 2. Patrick Ryan Way Homes
 - Located along Winchester Street at Patrick Ryan Way, this development is expected to consist of 60 single family homes. This development was partially built out at the time the turning movement counts were collected.
 For the purposes of this study, it was assumed that 40 of the 60 homes are built and occupied.

The assignment of the total combined background trips to the road network is depicted in **Figure 13**. Additional information, including the trips generated and the assignment of trips for each individual background development are included in Appendix G.

Potential Roadway Improvement(s)

As discussed during the scoping meeting, there is one roadway improvement within the vicinity of the site that is either fully funded or would be completely constructed by 2027.

• Smartscale project to construct a roundabout at the intersection of Lee Highway at Winchester Street / Broadview Avenue (Study Intersection 1)

There is one roadway improvement within the vicinity of the site that was previously identified for construction but was not selected for funding and therefore not included in the analysis:

• Smartscale project to construct a six-leg roundabout at the intersection of Broadview Avenue at Warrenton Village South (Study Intersection 10)

Relevant Smartscale excerpts and information are included in Appendix G.

The anticipated 2027 future road network (without the development) is illustrated in Figure 14.

Future without Development Traffic Volumes

In order to forecast future roadway traffic volumes for the year 2027, the 2023 existing traffic volumes were combined with the inherent regional growth traffic volumes and the combined background development trips. The 2027 future conditions without Development traffic volumes are illustrated in **Figure 15**.

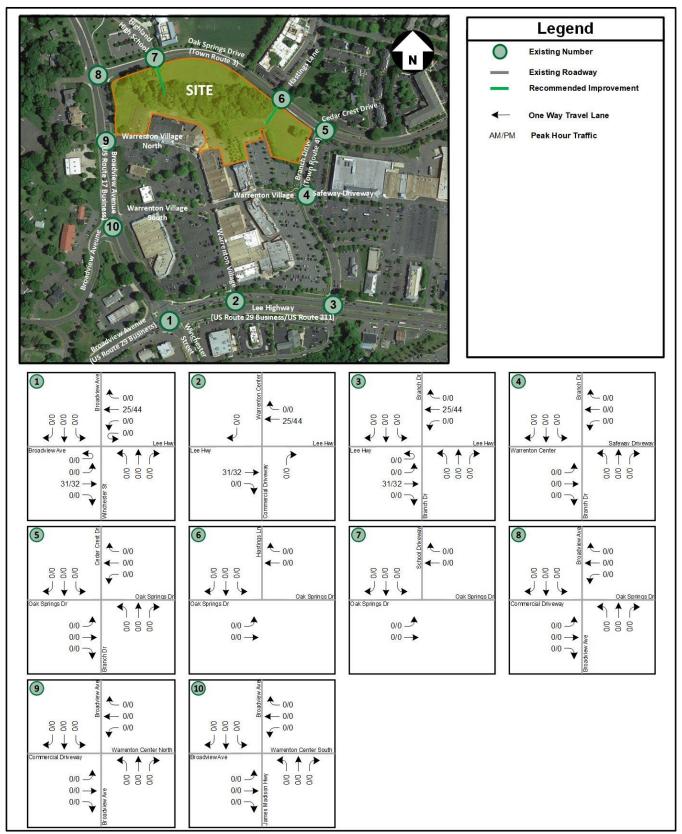


Figure 11: Projected Inherent Regional Growth Traffic Volumes (2023 to 2027)

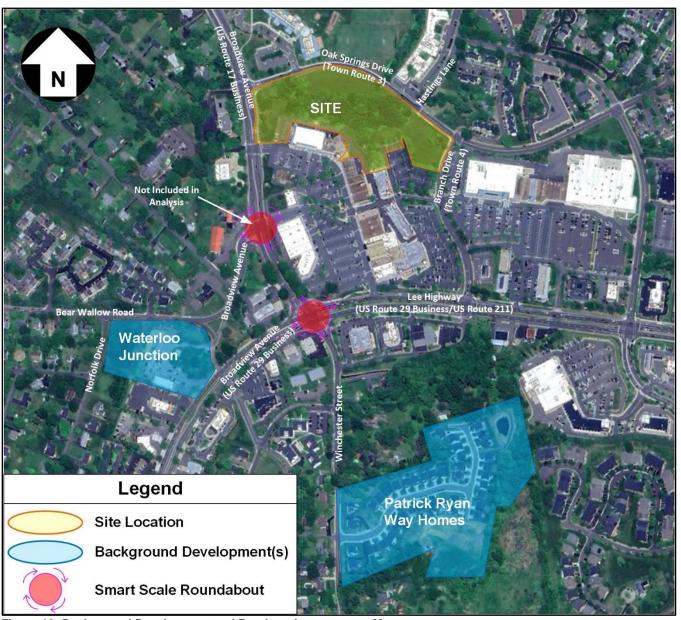


Figure 12: Background Development and Roadway Improvement Map

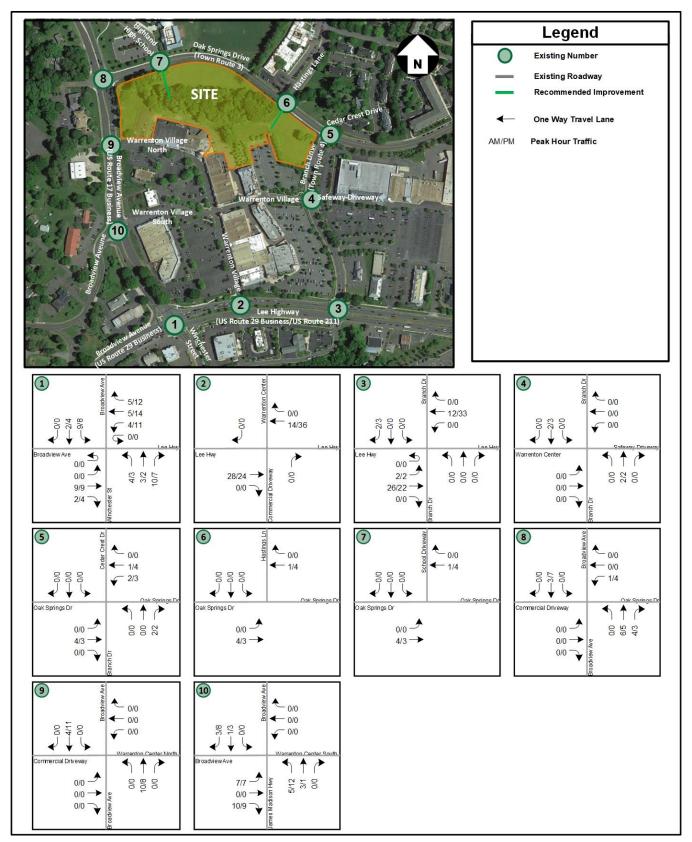


Figure 13: Total Combined Background Development Trips

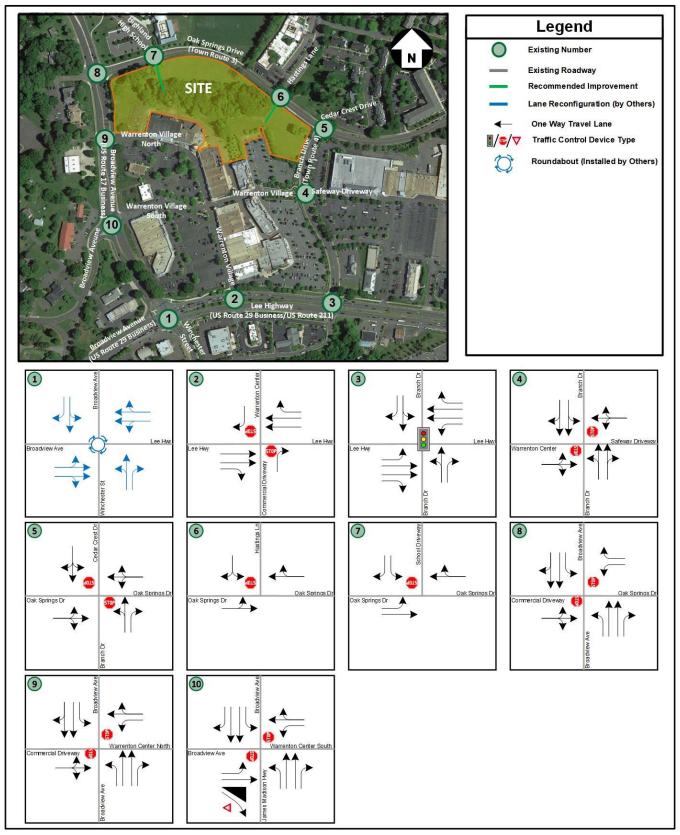


Figure 14: 2027 Future Conditions without Development – Roadway Network Geometric Configuration and Traffic Control Devices

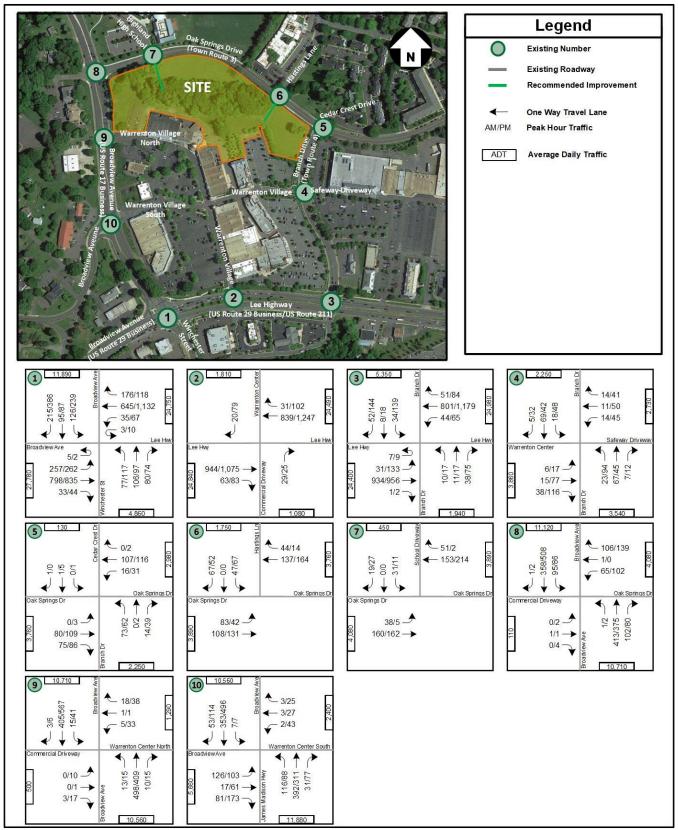


Figure 15: 2027 Future Conditions without Development - Vehicular Traffic Volumes

Future without Development Intersection Capacity and Queuing Analysis

Intersection capacity and queueing analyses were performed for the 2027 Future Conditions without Development scenario at the study area intersections during the AM and PM peak hours, in accordance with VDOT's *TOSAM* (version 2) guidelines. *Synchro*, version 11, was used to analyze the study intersections with results based on TRB's HCM 6th methodology and include LOS, delay, and queue length comparisons for the turning movements analyzed. The roundabout was analyzed using *Sidra*, version 9.

For the purposes of this analysis, the intersection PHF utilized in the analysis of future conditions was determined based on the existing traffic counts, with a minimum of 0.92 as agreed to in the scoping document. The HV% were based on the existing conditions scenario. Note that for analysis purposes, all turning movement counts were coded with a minimum volume of one vehicle in *Synchro*.

Per the scoping meeting with VDOT and County staff, it would be considered acceptable and/or desirable to achieve an approach LOS D or better for traffic operations using HCM methodology. The results of the intersection capacity and queuing analyses from *Synchro* are presented in **Table 5** and graphically in **Figure 16**. The results are expressed in LOS and delay (seconds per vehicle) for overall signalized intersections and per approach and lane group for all study intersections. Any overall signalized intersection or approach that operates at LOS E or F is displayed in red.

The queue lengths were reported as the 95th percentile queues determined from *Synchro* and are expressed in feet. The lane groups where the queue lengths exceeded the available effective storage capacity of existing turn lanes are displayed in red.

The detailed analysis worksheets of the 2027 Future Conditions without Development are contained in Appendix H.

Table 5: 2027 Future Conditions without Development - Intersection Capacity Analysis Results

				AM Peak Ho			ur	
No.	Intersection (Movement)	Effective Storage Length (ft.)	LOS	Delay (sec/veh)	95th % Queue (ft.)	LOS	Delay (sec/veh)	95th % Queue
1				Synchro			Synchro	
1	Broadview Ave (E/W) at Winchester St (N/S)							
	Overall Intersection (Roundabout)		۸	8.1		В	17.6	
	Eastbound Approach	·····	А А	7.6		В	11.1	
	Eastbound Left/Thru		A	8.0	80	В	11.9	158
	Eastbound Thru/Right		A	7.2	83	В	10.4	158
	Westbound Approach	······································		7.6		В	15.0	
	Westbound Left/Thru		A	8.0	78	В	16.2	252
	Westbound Thru/Right		A	7.2	81	В	14.0	268
	Northbound Approach		A	9.5		В	12.4	
	Northbound Left/Thru		A	9.2	36	В	12.2	56
	Northbound Right		В	10.2	19	В	13.0	22
	Southbound Approach		A	9.1		С	34.7	
	Southbound Left/Thru		Α	8.6	39	D	35.1	161
	Southbound Right		Α	9.7	43	С	34.4	191
2	Broadview Ave (E/W) at Warrenton Village				•			
	Center Dwy (Chipotle)/Walgreens Dwy (N/S)							
	Overall Intersection (TWSC)							
	Northbound Approach		В	13.0		В	13.9	
	Northbound Right		В	13.0	5	В	13.9	5
	Southbound Approach		В	10.8		В	13.9	
	Southbound Right		В	10.8	3	В	13.9	15
3	Broadview Ave (E/W) at Branch Dr (N/S)							
	Overall Intersection (Signalized)		В	19.7		С	34.0	
	Eastbound Approach		В	16.4		С	26.4	
	Eastbound Left	240	Е	67.0	80	Е	75.4	224
	Eastbound Thru		В	14.3	485	В	19.1	441
	Eastbound Right	330	A	9.7	0	В	13.4	0
	Westbound Approach		В	15.7		С	29.6	
	Westbound Left	150	Е	67.4	88	Е	78.5	123
	Westbound Thru		В	13.3	400	С	27.8	675
	Westbound Right	150	A	9.7	0	В	17.3	0
	Northbound Approach		E	60.8		E	67.0	
	Northbound Left/Thru		E	61.5	44	E	68.6	73
	Northbound Right	60	E	60.4	0	E	66.2	0
	Southbound Approach		E	64.7		E	69.3	
	Southbound Left/Thru		E	67.2	86	E	78.8	249
4	Southbound Right		E	62.7	0	Е	59.1	58
4	Warrenton Village Center Dwy/Shopping Center Dwy (E/W) at Branch Dr (N/S) Overall Intersection (TWSC)							
	Eastbound Approach		Α	9.3		В	11.8	
	Eastbound Left/Thru/Right		Α	9.3	5	В	11.8	30
	Westbound Approach		В	10.0		В	14.3	
	Westbound Left/Thru/Right		В	10.0	5	В	14.3	28
	Northbound Approach							
	Northbound Left		Α	7.4	3	Α	7.5	5
	Southbound Approach							
	Southbound Left		Α	7.4	0	Α	7.4	3
5	Oak Springs Dr (E/W) at Branch Dr (N/S)							
	Overall Intersection (TWSC)					<u> </u>		
	Eastbound Approach							
	Eastbound Left		A	7.4	0	A	7.5	0
	Westbound Approach							
	Westbound Left		A	7.6	0	A	7.7	3
	Northbound Approach		В	11.0		В	11.4	
	Northbound Left/Thru		В	11.4	10	В	12.6	10
	Northbound Right		Α	9.0	3	A	9.4	5
	Southbound Approach		Α	9.9		В	11.0	
	Southbound Left/Thru/Right		Α	9.9	0	В	11.0	0

Table 5 (Continued): 2027 Future Conditions without Development – Intersection Capacity Analysis Results

				AM Peak Ho		PM Peak Hour			
lo.	Intersection (Movement)	Effective Storage Length (ft.)	LOS	Delay (sec/veh)	95th % Queue (ft.)	LOS	Delay (sec/veh)	95th % Queue	
				Synchro			Synchro		
6	Oak Springs Dr (E/W) at Hastings Ln /								
	Future Access (N/S)								
	Overall Intersection (TWSC)								
	Eastbound Approach								
	Eastbound Left		A	7.9	5	A	7.7	3	
	Southbound Approach		В	11.1		В	11.0		
	Southbound Left/Right		В	11.1	15	В	11.0	15	
7	Oak Springs Dr (E/W) at Highland School Dwy / Future Garage Access (N/S) Overall Intersection (TWSC)								
	Eastbound Approach								
	Eastbound Left	75	A	7.7	3	A	7.7	0	
	Southbound Approach		В	10.9	-	В	10.1	_	
	Southbound Left		В	11.9	5	В	11.2	3	
8	Southbound Right		A	9.3	3	Α	9.6	3	
0	Oak Springs Dr (E/W) at Broadview Ave (N/S) Overall Intersection (TWSC)								
	Eastbound Approach		С	17.8		С	16.6		
	Eastbound Left/Thru/Right		C	17.8	0	C	16.6	3	
	Westbound Approach		<u>Ö</u>	19.7		D	27.9		
	Westbound Left/Thru	125	D	34.3	40	F	51.0	85	
	Westbound Right	-	В	10.6	13	В	10.7	18	
	Northbound Approach					1			
	Northbound Left	90	Α	8.1	0	Α	8.5	0	
	Southbound Approach								
	Southbound Left	225	Α	9.1	8	Α	8.7	8	
9	Warrenton Village North Dwy (E/W) at Broadview Ave (N/S) Overall Intersection (TWSC)								
	Eastbound Approach		С	15.6		С	20.0		
	Eastbound Left/Thru/Right		С	15.6	0	С	20.0	10	
	Westbound Approach		В	13.2		С	18.3		
	Westbound Left		С	21.2	3	D	27.3	15	
	Westbound Thru/Right		В	11.1	3	В	10.6	5	
	Northbound Approach								
	Northbound Left	150	A	8.2	0	A	8.8	3	
	Southbound Approach								
10	Southbound Left	110	Α	8.6	0	Α	8.4	3	
10	Warrenton Village South Dwy/Broadview Ave (E/W) at Broadview Ave/Winchester St (N/S) Overall Intersection (TWSC)								
	Eastbound Approach		D	30.7		D	31.9		
	Eastbound Left		Е	44.6	90	F	62.0	98	
	Eastbound Thru		D	26.5	8	E	38.5	43	
	Eastbound Right		В	10.0	10	В	11.6	25	
	Westbound Approach	T	С	19.7		E	35.5		
	Westbound Left		D	25.4	0	F	51.8	40	
	Westbound Thru/Right		С	17.8	3	С	22.1	20	
	Northbound Approach								
	Northbound Left	160	Α	8.6	10	A	9.3	8	
	Southbound Approach								
	Southbound Left	160	Α	8.3	0	Α	8.2	0	

NOTES:

^[1] Effective storage length is based on the storage length plus one-half of the taper length per TOSAM guidelines.

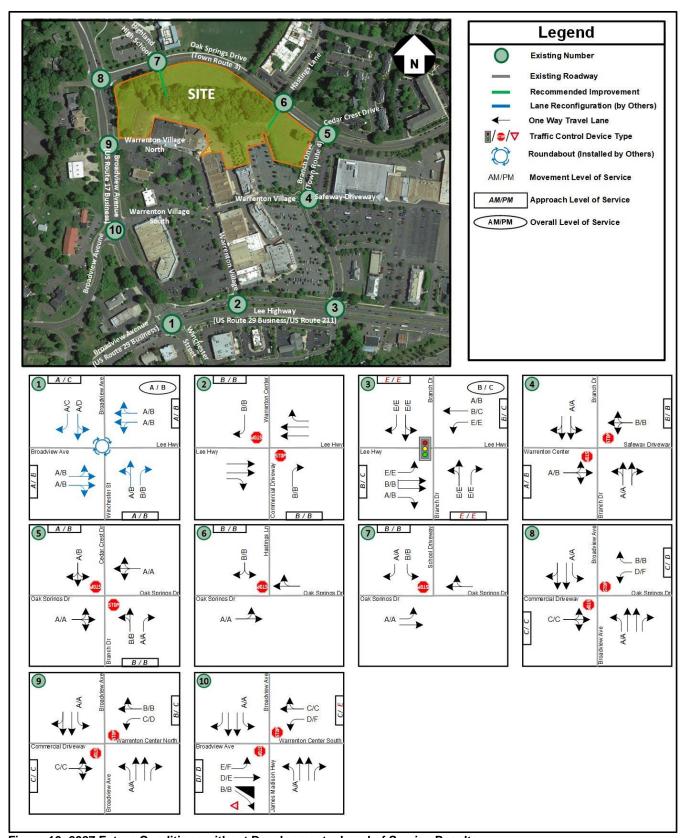


Figure 16: 2027 Future Conditions without Development – Level of Service Results

Study Intersection 1 (Lee Highway at Winchester Street / Broadview Avenue) was approved for a roundabout and received SmartScale funding. As such, this intersection was converted from a signalized intersection to a roundabout in all future conditions.

Based on the capacity analysis of 2027 Future Conditions without Development, the planned roundabout is expected to operate at overall levels of service of B or better during both the AM and PM peak hours.

Based on the capacity analysis of 2027 Future Conditions without Development, the signalized study intersection is expected to operate at overall levels of service of C or better during both the AM and PM peak hours.

Based on the capacity analysis of 2027 Future Conditions without Development, the approaches of all study intersections continue to operate at approach levels of service of D or better during both the AM and PM peak hours, except for the following study intersections that have at least one approach that would operates at level of service E of F during at least one peak hour:

- Study Intersection 3: Lee Highway (US 211/US 29 BUS) at Branch Drive
- Study Intersection 10: Broadview Avenue at Warrenton Village South

Based on the queuing analysis performed for 2027 Future Conditions without Development, all turning movements at the study intersections have maximum queue lengths that are accommodated within the available storage lengths of the turn bays.

Analysis of 2027 Future Conditions with Development

For the purposes of this study, the Development is anticipated to be constructed by 2027; this scenario analyzes the future with development conditions for the year 2027.

Site Description

The development will be situated on a single parcel of vacant land (approximately 6.46 acres) and a portion of an adjacent developed parcel of land, which can be identified on Fauquier County Tax Maps with the following GPIN #s: 6985-20-7247-000, and 6984-29-6753-000, respectively. The property is currently zoned as C (Commercial District) with a Future Land Use of Mixed Use as part of the New Town Warrenton Character District (Lee Highway Urban Development Area [UDA]).

The Applicant is proposing to apply for a Special Use Permit (SUP) in order to construct approximately 386 multifamily residential dwelling units (320 multifamily apartments, 362-over-2 units, and 30 townhomes) and a parking deck. The site has an anticipated build-out date of 2027.

A conceptual plan for the Site is illustrated in Figure 17

Traffic Impact Analysis – Warrenton Village Center
February 9, 2024

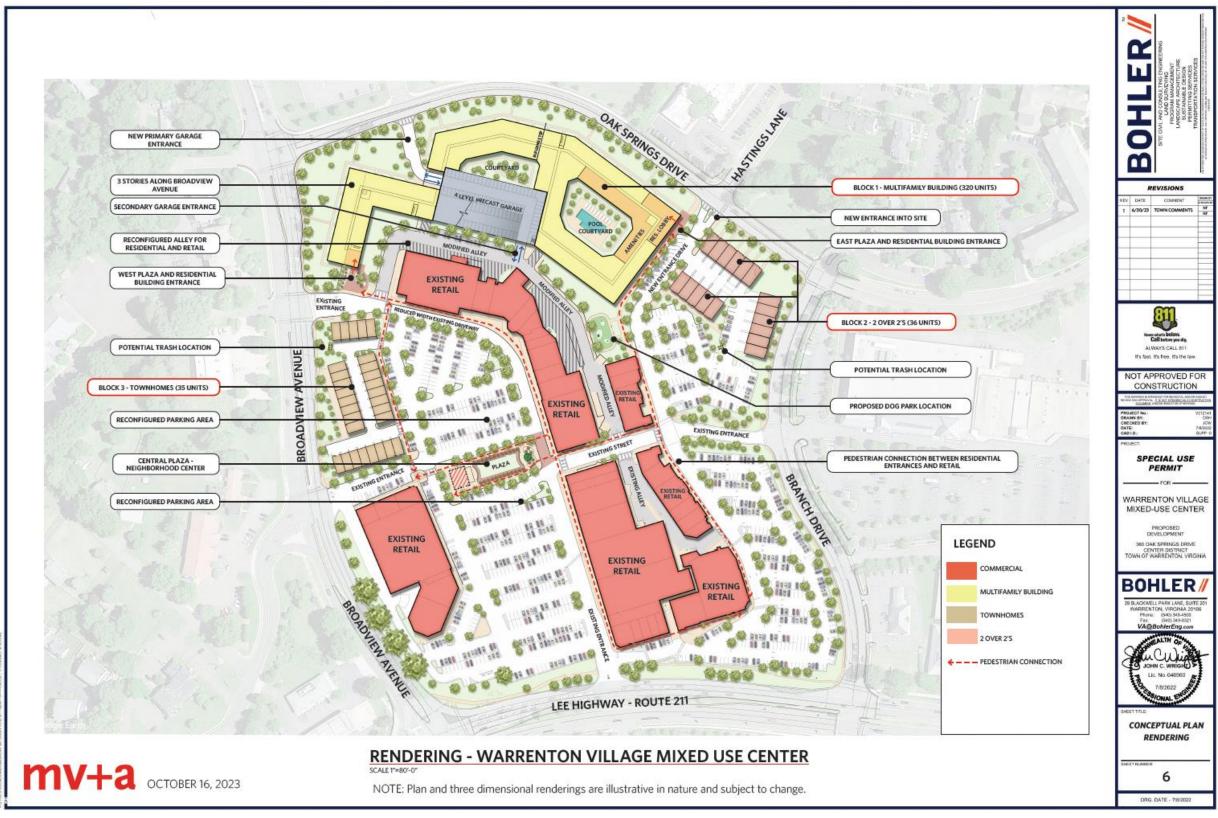


Figure 17: Conceptual Development Plan
Note: Plan provided by Bohler and is for conceptual purposes only.

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Proposed Site Access

Access to the site will be provided via one full movement parking deck entry along Oak Springs Drive (Town Route 3) forming the fourth leg of the High School Driveway, one full movement driveway along Oak Springs Drive forming the fourth leg to the existing full-movement intersection of Hastings Lane, and via the existing shopping center accesses to the south.

Projected Site Trip Generation

In order to calculate the trips generated by the proposed Development, the Institute of Transportation Engineers' (ITE) <u>Trip Generation Manual</u>, 11th Edition, publication was used to determine the total trips going into and out of the subject study site during the AM and PM peak hours as well as the typical number of weekday daily trips. The projected trip generation for the proposed Development is depicted in **Table 6**Table 6. Of note, as agreed to in the scoping document, no internal capture or pass-by trip reductions were assumed with respect to the proposed Development, and therefore are not assumed within the table.

Table 6: Site Trip Generation (Peak Hour of the Adjacent Street; ITE 11th Ed.)

				Weekday						
Land Use	ITE Code	Size	AM Peak Hour PM Peak Hou		Hour	Daily				
			In	Out	Total	In	Out	Total	Total	
Multifamily Housing	220	386 DU	37	117	154	124	73	197	2,602	

As illustrated in the table above, the Site is expected to generate approximately 154 new trips during the AM peak hour, 197 new trips during the PM peak hour, and 2,602 new daily trips on a typical weekday.

Distribution and Assignment of Site Traffic

The distribution and assignment of the site generated trips were based on the existing traffic patterns, engineering judgement, the nature of the proposed Development, and with the guidance and input from the VDOT and the Town staff. The site direction of approach and trip distribution are illustrated in **Figure 18**.



Figure 18: Global Vehicular Direction of Approach (Site Trip Distribution)

Future with Development Traffic Volumes

In order to project future traffic volumes on the roadways in the vicinity of the Development, trips generated from the Development were assigned to the road network based on the previously mentioned direction of approach. The site traffic assignment is illustrated for the AM and PM peak hours in **Figure 19**.

The future with development traffic volumes for were determined by adding the assigned site generated traffic volumes to the 2027 Future Conditions without Development traffic volumes. The 2027 Future Conditions with Development traffic volumes are depicted in **Figure 20.**

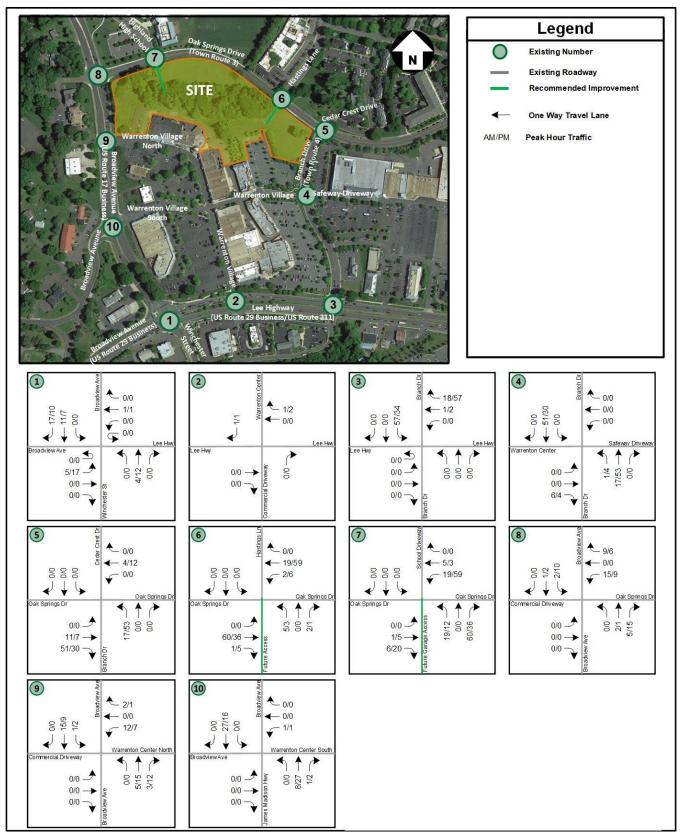


Figure 19: Site Generated Trip Assignment

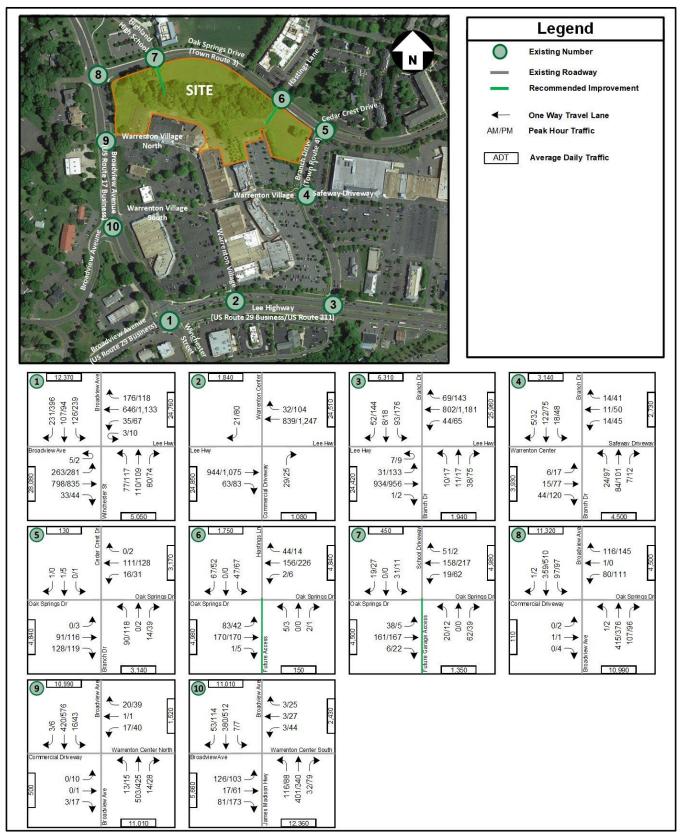


Figure 20: 2027 Future Conditions with Development

Future with Development Intersection Capacity and Queuing Analysis

Intersection capacity and queueing analyses were performed for the 2027 Future Conditions without Development scenario at the study area intersections during the AM and PM peak hours, in accordance with VDOT's *TOSAM* (version 2) guidelines. *Synchro*, version 11, was used to analyze the study intersections with results based on TRB's HCM 6th methodology and include LOS, delay, and queue length comparisons for the turning movements analyzed. Roundabouts were analyzed using *Sidra*, version 9.

For the purposes of this analysis, the intersection PHF utilized in the analysis of future conditions was determined based on the existing traffic counts, with a minimum of 0.92 as agreed to in the scoping document. The HV% were based on the existing conditions scenario, with any new approaches utilizing a default *Synchro* value of 2.0% per movement. Note that for analysis purposes, all turning movement counts were coded with a minimum volume of one vehicle in *Synchro*.

Per the scoping meeting with VDOT and the Town staff, it would be considered acceptable and/or desirable to achieve an approach LOS of D or better for traffic operations using the HCM methodology. The results of the intersection capacity and queuing analyses from *Synchro* are presented in **Table 7** and graphically in **Figure 21.** The results are expressed in LOS and delay (seconds per vehicle) for overall signalized intersections and per approach and lane group for all study intersections. The overall signalized intersections and any approaches that operate at LOS E or F are displayed in red.

The queue lengths were reported as the 95th percentile queues determined from *Synchro* and are expressed in feet. The lane groups where the queue lengths exceeded the available effective storage capacity of existing turn lanes are displayed in red.

The detailed analysis worksheets of the 2027 Future Conditions with Development scenario are contained in Appendix I.

Table 7: 2027 Future Conditions without Development - Intersection Capacity Analysis Results

				AM Peak Ho			PM Peak Ho	
No.	Intersection (Movement)	Effective Storage Length (ft.)	LOS	Delay (sec/veh)	95th % Queue (ft.) ^[2]	LOS	Delay (sec/veh)	95th % Queue [2]
				Synchro			Synchro	
1	Broadview Ave (E/W) at Winchester St							
	(N/S)		_			_		
	Overall Intersection (Roundabout)		В	10.1		В	19.3	
	Eastbound Approach		Α	9.4		В	11.5	
	Eastbound Left/Thru		Α	10.0	111	В	12.4	170
	Eastbound Thru/Right		Α	8.9	116	В	10.8	172
	Westbound Approach		В	10.5		В	16.3	
	Westbound Left/Thru		Α	11.4	116	В	17.7	272
	Westbound Thru/Right		В	9.8	117	В	15.3	291
	Northbound Approach		В	11.9		В	13.3	
	Northbound Left/Thru		В	11.5	47	В	13.2	62
	Northbound Right		В	12.7	23	В	13.7	23
	Southbound Approach		В	10.1		D	39.6	
	Southbound Left/Thru		Α	9.5	47	D	39.5	170
	Southbound Right		В	10.8	53	D	39.7	172
2	Broadview Ave (E/W) at Warrenton							
	Village Center Dwy							
	(Chipotle)/Walgreens Dwy (N/S)							
	Overall Intersection (TWSC)	<u> </u>						
	Northbound Approach		В	13.0		В	13.9	
	Northbound Right		В	13.0	5	В	13.9	5
	Southbound Approach	-	В	10.8		В	13.9	
	Southbound Right		В	10.8	3	В	13.9	15
3	Broadview Ave (E/W) at Branch Dr (N/S)							-
	Overall Intersection (Signalized)		С	23.0		D	35.8	
	Eastbound Approach		В	19.0		С	28.1	
	Eastbound Left	240	E	67.0	80	E	75.4	224
	Eastbound Thru	240						
	Eastbound Right	000	В	17.0	485	С	21.1	441
		330	В	11.6	0	В	14.7	0
	Westbound Approach		В	18.0		С	31.6	
	Westbound Left	150	Е	67.4	88	E	78.5	123
	Westbound Thru		В	15.8	400	С	30.4	675
	Westbound Right	150	В	11.6	0	В	19.3	26
	Northbound Approach		E	62.1		E	67.0	
	Northbound Left/Thru		Е	63.0	47	E	68.6	73
	Northbound Right	60	E	61.6	0	E	66.2	0
	Southbound Approach		E	63.4		E	68.7	
	Southbound Left/Thru		Е	66.7	162	E	78.1	#338
	Southbound Right		Е	57.2	0	E	56.4	58
4	Warrenton Village Center Dwy/Shopping Center Dwy (E/W) at Branch Dr (N/S) Overall Intersection (TWSC)							
	Eastbound Approach		Α	9.5		В	12.5	
	Eastbound Left/Thru/Right		A	9.5	8	В	12.5	35
	Westbound Approach		<i>B</i>	10.4	.	С	16.0	
	Westbound Left/Thru/Right		В	10.4	5	C	16.0	33
	Northbound Approach		<u>.</u>			† <u>V</u>		
	Northbound Left		Α	7.5	3	А	7.6	5
	Southbound Approach		Λ	1.0	<u></u>	·····	1.0	
	Southbound Left		^	7.4	0		7.5	2
5	Oak Springs Dr (E/W) at Branch Dr (N/S)		A	7.4	0	A	7.5	3
•	Overall Intersection (TWSC)							
	L							
	Eastbound Approach				_	_		
	Eastbound Left		Α	0.0	0	A	7.5	0
	Westbound Approach							
	Westbound Left		Α	7.8	0	A	7.8	3
	Northbound Approach		В	11.8		В	13.1	
	Northbound Left/Thru		В	12.2	15	В	14.3	25
	Northbound Right	<u> </u>	Α	9.2	3	Α	9.5	5
	Southbound Approach		В	10.1		В	11.3	
	Southbound Left/Thru/Right		В	10.1	0	В	11.3	0

Table 7 (Continued): 2027 Future Conditions without Development - Intersection Capacity Analysis Results

				AM Peak Ho			PM Peak Ho	
No.	Intersection (Movement)	Effective Storage Length (ft.)	LOS	Delay (sec/veh)	95th % Queue (ft.) ^[2]	LOS	Delay (sec/veh)	95th % Queue [2]
				Synchro			Synchro	
6	Oak Springs Dr (E/W) at Hastings Ln / Future Access (N/S) Overall Intersection (TWSC)							
	Eastbound Approach Eastbound Left		Α	7.9	5	А	7.9	3
	Westbound Approach Westbound Left		Α	7.6	0	A	7.6	0
	Northbound Approach		В	13.6		В	13.1	
	Northbound Left/Thru/Right Southbound Approach		В В	13.6 12.1	3	В В	13.1 12.5	0
	Southbound Left/Thru/Right		В	12.1	18	В	12.5	20
7	Oak Springs Dr (E/W) at Highland School Dwy / Future Garage Access (N/S) Overall Intersection (TWSC)							
	Eastbound Left	75	Α	7.7	3	А	7.7	0
	Westbound Approach Westbound Left		Α	7.6	0	А	7.8	3
	Northbound Approach		В	10.8		В	11.0	
	Northbound Left/Thru/Right Southbound Approach		В В	10.8 12.6	10	В В	11.0 11.1	8
	Southbound Left/Thru Southbound Right		B A	14.6 9.4	8 3	B A	14.7 9.6	3 3
8	Oak Springs Dr (E/W) at Broadview Ave (N/S) Overall Intersection (TWSC)		A	9.4	3	A	9.0	<u> </u>
	Eastbound Approach		С	18.1		С	17.1	
	Eastbound Left/Thru/Right Westbound Approach		<u>с</u>	18.1 22.4	0	C D	17.1 32.9	3
	Westbound Left/Thru	125	Е	39.0	55	F	61.8	103
	Westbound Right Northbound Approach		В	10.7	15	В	10.8	20
	Northbound Left	90	Α	8.1	0	A	8.5	0
	Southbound Approach Southbound Left	225	Α	9.1	10	Α	8.8	8
9	Warrenton Village North Dwy (E/W) at Broadview Ave (N/S) Overall Intersection (TWSC)							
	Eastbound Approach		С	16.0		С	20.7	
	Eastbound Left/Thru/Right Westbound Approach		С С	16.0 16.3	3	С С	20.7 20.3	10
	Westbound Left		С	22.8	8	D	30.0	23
	Westbound Thru/Right Northbound Approach		В	11.1	3	В	10.7	5
	Northbound Left	150	Α	8.3	0	A	8.8	3
	Southbound Approach Southbound Left	110	Α	8.6	3	Α	8.5	3
10	Warrenton Village South Dwy/Broadview Ave (E/W) at Broadview Ave/Winchester St (N/S) Overall Intersection (TWSC)	-		-			-	-
	Eastbound Approach		D	34.4		E	35.6	
	Eastbound Left Eastbound Thru		F D	51.0 27.8	100 8	F E	71.7 42.2	108 45
	Eastbound Right		В	10.1	10	В	11.7	45 25
	Westbound Approach Westbound Left		С D	21.2 26.6	3	<i>E</i> F	40.2 60.0	45
	Westbound Thru/Right		С	26.6 18.5	3	C	60.0 23.5	45 20
	Northbound Approach Northbound Left	160	Α	8.7	10	А	9.4	8
	Southbound Approach							••••••••••••
TES.	Southbound Left	160	Α	8.3	0	Α	8.3	0

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^[1] Effective storage length is based on the storage length plus one-half of the taper length per TOSAM guidelines.

^{[2] #: 95}th percentile queues (reported from Synchro) exceed capacity; actual queues may be longer. Queues shown are based on the maximum after two cycles.

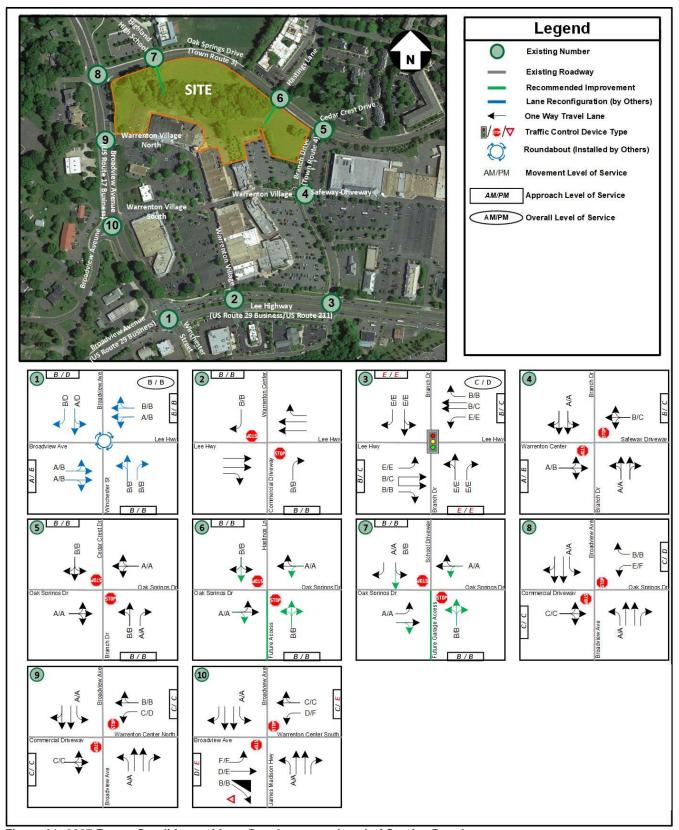


Figure 21: 2027 Future Conditions without Development – Level of Service Results

As mentioned previously, per the agreed upon scoping document, it would be considered desirable to achieve an approach LOS D or better for traffic operations using HCM methodology. Furthermore, if an overall intersection or approach was operating at an unacceptable LOS under future without development conditions, it was assumed acceptable to achieve non-degradation.

The planned roundabout is expected to operate at an overall LOS B with all approaches operating at LOS D or better during the AM and PM peak hours.

Based on the capacity analysis of 2027 Future Conditions without Development, the signalized study intersection is expected to continue to operate at overall levels of service of D or better during both the AM and PM peak hours.

Based on the capacity analysis of 2027 Future Conditions without Development, the approaches of all study intersections continue to operate at approach levels of service of D or better during both the AM and PM peak hours, except for the following study intersections that have at least one approach that would operate at level of service E of F (similar to 2027 Future Conditions without Development) during at least one peak hour:

- Study Intersection 3: Lee Highway (US 211/US 29 BUS) at Branch Drive
- Study Intersection 10: Broadview Avenue at Warrenton Village South

Based on the queuing analysis performed for 2027 Future Conditions without Development, all turning movements at the study intersections have maximum queue lengths that are accommodated within the available storage lengths of the turn bays.

Note that Study Intersection 10 (Broadview Avenue at Warrenton Village South) was previously identified by the Town for construction of a roundabout but was not selected for funding and therefore not included in the analysis. Therefore, no improvements are recommended for construction by the proposed Development.

In general, the signalized intersection would operate with longer vehicular delays for the side-streets and mainline left turning movements. These delays are a result of VDOT prioritization of through traffic on the mainline, as is typical along commuter corridors, to accommodate the largest possible volume of through traffic in the area along the mainlines and therefore have a better overall traffic operation than if all movements were prioritized equally.

No improvements are warranted or recommended as part of the proposed Development.

Preliminary Left and Right Turn Lane Warrant Assessments

Left and right turn lane warrants are based off VDOT's <u>Road Design Manual</u> (RDM), Appendix F. In order to determine the need for exclusive left and/or right turn lanes or tapers at the study intersections, the traffic data and anticipated development program provided in the 2027 Future Conditions with Development scenario section were utilized.

Warrants for right-turn storage lanes on two- and four-lane highways at intersections are based on Figure 3-26 and Figure 3-27 in Appendix F of VDOT's RDM. These figures provide a graphical representation for determining the necessity of a right turn lane by comparing the total volumes of a given approach with their respective right turn volumes.

Warrants for left-turn storage lanes on two-lane highways at unsignalized intersections are based on Figure 3-5 to Figure 3-21 in Appendix F of VDOT's RDM. The figures provide graphical representations for determining the necessity of a left turn lane by comparing the advancing volumes of a given approach and the respective opposing volumes with respect to the percentage of left turning vehicles of the advancing volumes and the design speed of a given roadway.

If the turn lanes and / or tapers are not provided or would not meet the minimum requirements per VDOT's RDM, turn lane waivers requests would need to be submitted as separate documentation and be approved by VDOT.

A summary of the turn lane warrant analysis is presented in **Table 8** through **Table 11**.

Table 8: Summary of Left Turn Lane Warrants at Site Entrances (2-Lane) - Build 2027

Study Scenario	Opposing Vol. (VPH)	Advancing Vol. (VPH)	Left Turn Vol. (VPH)	Left Turn %	Minimum Opposing Threshold (VPH)	VDOT RDM F Figure	Treatment
INT 6 - WBL AM - TF 2027	254	202	2	0.99%	1,208	Fig. 3-4	Not Warranted
INT 6 - WBL PM - TF 2027	217	246	6	2.44%	1,054	Fig. 3-4	Not Warranted
INT 7 - WBL AM - TF 2027	205	228	19	8.33%	841	Fig. 3-5	Not Warranted
INT 7 - WBL PM - TF 2027	194	281	62	22.06%	274	Fig. 3-8	Not Warranted

Table 9: Summary of Right Turn Lane Warrants at Site Entrances (2-Lane) - Build 2027

Study Scenario	Approach Volume	Right Turn Volume	Minimum Right Turn Taper Threshold	Minimum Right Turn Full Lane Threshold	Treatment
INT 4 - NBR - 2027 TF AM Peak	95	7	37	90	Not Warranted
INT 4 - NBR - 2027 TF PM Peak	149	12	36	90	Not Warranted
INT 4 - SBR - 2027 TF AM Peak	90	5	37	90	Not Warranted
INT 4 - SBR - 2027 TF PM Peak	119	32	36	90	Not Warranted

Table 10: Summary of Left Turn Lane Warrants at Brach Drive (Study Intersection 4) (4-Lane) - Existing 2023

Study Scenario	Opposing Vol. (VPH)	Advancing Vol. (VPH)	Left Turning Vol.	Left Turn %	Treatment
INT 4 - NBL - 2023 EX AM Peak	90	95	23	24.2%	Not Warranted
INT 4 - NBL - 2023 EX PM Peak	119	149	94	63.1%	Full-width Turn Lane and Taper Warranted (for Undivided and Divided)
INT 4 - SBL - 2023 EX AM Peak	95	90	18	20.0%	Not Warranted
INT 4 - SBL - 2023 EX PM Peak	149	119	48	40.3%	Full-width Turn Lane and Taper Warranted (for Undivided)

Table 11: Summary of Left Turn Lane Warrants at Brach Drive (Study Intersection 4) (4-Lane) - Build 2027

Study Scenario	Opposing Vol. (VPH)	Advancing Vol. (VPH)	Left Turning Vol.	Left Turn %	Treatment
INT 4 - NBL - 2027 TF AM Peak	145	115	24	20.9%	Not Warranted
INT 4 - NBL - 2027 TF PM Peak	155	210	97	46.2%	Full-width Turn Lane and Taper Warranted (for Undivided and Divided)
INT 4 - SBL - 2027 TF AM Peak	115	145	18	12.4%	Not Warranted
INT 4 - SBL - 2027 TF PM Peak	210	155	48	31.0%	Full-width Turn Lane and Taper Warranted (for Undivided)

No turn lanes are warranted at the site entrances. At the request of VDOT and the Town, turn lanes were evaluated at the Study Intersection 4 (Branch Drive at Warrenton Village Driveway / Safeway Driveway). The northbound left turn lane is warranted under Build 2027 conditions, but it is also warranted under existing conditions. Therefore, a northbound left turn

lane on Branch Drive is not recommended to be installed by the proposed Development. Graphics and information regarding the methodology used to determine the turn lane warrants are provided in Appendix J.

Preliminary Access Management Evaluation (Intersection Spacing)

The minimum spacing standards for the Commonwealth of Virginia are specified in VDOT's <u>Road Design Manual</u> (RDM). Appendix F of the RDM focuses primarily on access management practices. The minimum spacing standard are particularly specified in Table 2-2 through Table 2-4. Table 2-2 provides guidance on the minimum spacing standard for commercial entrances, intersections, and median crossovers, and are based on a roadway's speed limit and functional classification. Table 2-3 and 2-4 provide guidance for minimum spacing standards for the spacing between interchanges and intersections or commercial entrances.

As mentioned previously, Oak Springs Road is classified by VDOT as "Major Collector," with a posted speed limit of 25 mph. Based on the applicable intersection spacing requirements (centerline-to-centerline) per RDM Appendix F Table 2-2, **Table 12** lists the summary of the future intersections with corresponding roadway information and the appropriate distance requirements. **Figure 22** shows the approximate proposed distances between the study intersections and the corresponding required distances with the proposed intersections in place for the Site.

Table 12: Future Intersection Spacing

		Minimum Spacing (Distance) in Feet								
Functional Classification	Design Speed (See Note 2)	Type 1 (Signalized)	Type 2 (Unsignalized/ Full Crossover)	Type 3 (Full Access /Directional Crossover)	Type 4 (Partial Access)					
	≤ 30 mph	1,050	880	440	250					
Principal	35 to 45 mph	1,320	1,050	565	305					
Arterial	≥ 50 mph	2,640	1,320	750	495					
	≤ 30 mph	880	660	355	200					
Minor	35 to 45 mph	1,050	660	470	250					
Arterial	≥ 50 mph	1,320	1,050	555	425					
	≤ 30 mph	660	440	225	200					
Collector	35 to 45 mph	660	440	335	250					
	≥ 50 mph	1,050	660	445	360					
Local Street			See Note 1							

TABLE 2-2 MINIMUM SPACING STANDARDS FOR COMMERCIAL ACCESSES, INTERSECTIONS AND MEDIAN CROSSOVERS[†]

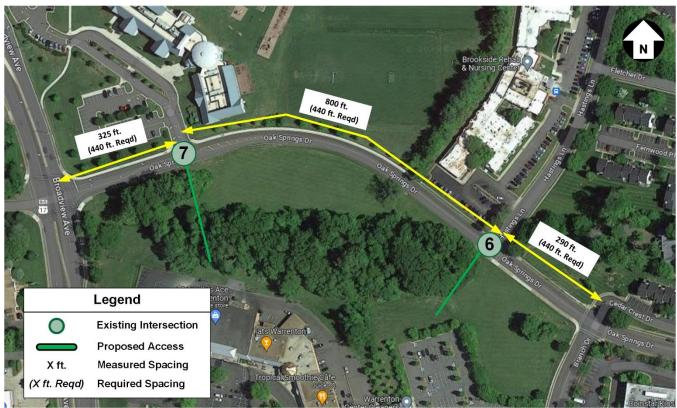


Figure 22: Future Intersection Spacing

As described in

Table 122 and depicted in **Figure 22**, the two proposed entrances do not meet the spacing requirements for unsignalized intersections on a 25 mph Major Collector. However, the entrances are proposed as the fourth leg to existing intersections instead of creating new entrances with offsets. However, Oak Springs Drive does not appear to be a VDOT maintained roadway, so an Access Management Exception (AM-E) request will not be submitted.

Preliminary Signal Warrant Analysis

Signal warrants are based on *Chapter 4C: Traffic Control Signal Needs Studies* of the Federal Highway Administration's (FHWA) <u>Manual on Uniform Traffic Control Devices</u> (MUTCD), 2009 Edition. Chapter 4C discusses nine (9) separate warrants, by which only one warrant needs to be satisfied to justify the installation of a traffic control signal. In order to provide an assessment for the possible signalization of Broadview Avenue at Oak Springs Road (Study Intersection 8) under the build 2027 traffic volumes, Warrant Two (Four-Hour Vehicular Volume) was analyzed, since the warrant usually is a significant factor signalization and is often the warrant that is most readily satisfied for typical conditions.

Portions of the MUTCD used in this analysis are provided in Appendix K.

Warrant Two: Four-Hour Vehicular Volume

Warrant Two is satisfied when the plotted points representing the vehicles per hour (vph) on the major street (total of both approaches and the corresponding vph on the high-volume minor-street approach (one direction only), for each of any four hours of an average day, all fall above either MUTCD Figure 4C-1 or Figure 4C-2 (depending on the applicability) for the future combination of approach lanes.

The traffic volumes utilized to evaluate Warrant Two, using Figure 4C-1 are shown in **Table 13** for the study intersection. It should be noted that the intersection was analyzed as being two lanes on the major approach and one lane on the minor approach. In addition, only two hourly volumes were utilized, the build 2027 AM and PM peak hour volumes, because it is not anticipated that the other hourly volumes would be any higher or more likely to satisfy the conditions than that of the two selected. Lastly, as the capacity analysis of future conditions indicated that 100% of right turners could perform right turn maneuvers on red from the side-street approaches and there are currently exclusive northbound and westbound right turn lanes, a 100% right turn on red (RTOR) reduction was applied to all approaches, as depicted below.

Table 13: Volume Projections - Broadview Avenue at Oak Springs Road (Intersection 8)

Time Period	Broadview Ave (NB/SB)	Oak Springs Dr (WBL)
7:30AM to 8:30 AM	872	80
4:00 PM to 5:00 PM	985	110

Note: 100% right turn reductions are applied on all approaches

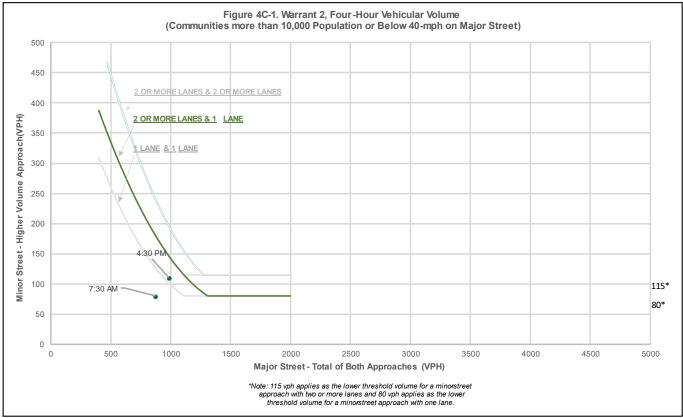


Figure 23: Four-Hour Warrant Analysis - Broadview Avenue at Oak Springs Road (Intersection 8)

As seen in the figure above, the build 2027 peak hour traffic volumes with a 100% RTOR reduction does not meet the threshold for two of the four hours required. As mentioned earlier, it is most likely that the next two hours with the highest traffic volume will generate even lower trips than the AM and PM peak hours. Therefore, based on traffic volumes, a signal would not be warranted at this intersection under this analysis.

The minor street volume is above the minimum threshold of 80 vehicles to warrant a signal; however, the major street volume is not high enough.

Additionally, the capacity analysis in the 2011 TIA shows that all reported movements at this unsignalized study intersection are anticipated to operate at LOS C or better during both AM and PM peak hours. This capacity analysis is acceptable and an indication that there is not an operational need for signalization.

Bicycle and Pedestrian Accommodations

The property currently contains a sidewalk with a buffer across the north side of the Oak Springs frontage. The existing sidewalk will be maintained with the proposed development, and sidewalk will be constructed along the south side of Oak Springs Road across the property frontage. There is at least one crosswalk at every study intersection, with the exception of Study Intersection 2 (Lee Highway at Warrenton Village / Chick-fil-a Driveway).

The school and mixed-use area create opportunities for the proposed Site to create paths and areas for multimodal connectivity. As shown on the concept plan, The Site is proposing a multitude of improvements that will increase pedestrian connectivity throughout the entire area. New sidewalks will be added along the entire perimeter of all residential blocks, including direct sidewalk connectivity to ground floor units. The extension of Hastings Lane and accompanying sidewalks will offer a new pedestrian access point from Oak Springs Drive. The proposed road that will connect the Hastings Lane extension through the existing commercial building and into the heart of the retail center via a new cut-through street that will allow maximum ease to walk from one side of the site to the other.

The unsignalized pedestrian crossings were reviewed as per TE-384.1 and will be submitted as a separate document.

Conclusions

This report presents the findings of a Traffic Impact Analysis (TIA) conducted for the proposed Warrenton Village Center (the Site / the Development / the Property) along the southern frontage of Oak Springs Drive (Town Route 3), east of Broadview Avenue (US Route 17 Business) and west of Branch Drive (Town Route 4) in the Town of Warrenton, Virginia

The development will be situated on a single parcel of vacant land (approximately 6.46 acres) and a portion of an adjacent developed parcel of land, which can be identified on Fauquier County Tax Maps with the following GPIN #s: 6985-20-7247-000, and 6984-29-6753-000, respectively. The property is currently zoned as C (Commercial District) with a Future Land Use of Mixed Use as part of the New Town Warrenton Character District (Lee Highway Urban Development Area [UDA]).

The Applicant is proposing to apply for a Special Use Permit (SUP) in order to construct approximately 386 multifamily residential dwelling units (320 multifamily apartments, 36 2-over-2 units, and 30 townhomes) and a parking deck. The site has an anticipated build-out date of 2027.

Access to the site will be provided via one full movement parking deck entry along Oak Springs Drive (Town Route 3) forming the fourth leg of the High School Driveway, one full movement driveway along Oak Springs Drive forming the fourth leg to the existing full-movement intersection of Hastings Lane, and via the existing shopping center accesses to the south.

Analysis Components

- 2023 existing volumes were derived via turning movement counts collected at intersections within the study area in February 2023.
- As determined based on review comments from VDOT and the Town, an inherent regional growth of 1.0% per year was
 applied to the Lee Highway mainline through movements at the intersection of Lee Highway at Broadview Avenue (US
 Route 17 Business). The growth volumes were balanced along the road network by increasing the mainline through
 movements at subsequent study intersections along the road network where applicable for the period between 2023 and
 2027 to account for 2027 conditions.
- The trip generation associated with the Site was based on the ITE <u>Trip Generation Manual</u>, 11th Edition publication. The Site in total is expected to generate approximately 154 new trips during the AM peak hour, 197 new trips during the PM peak hour, and 2,602 new daily trips on a typical weekday.
- Intersection capacity and queuing analyses were performed for all analysis scenarios at the study area intersections during
 the weekday morning (AM) and weekday afternoon (PM) peak hours. Synchro, version 11, was used to analyze the study
 intersections with results based on the Transportation Research Board's (TRB) Highway Capacity Manual (HCM)
 methodology and analysis guidelines provided in VDOT's Traffic Operations and Safety Analysis Manual (TOSAM) (version
 2). The analysis herein includes level of service (LOS), delay, and queue length comparisons for the turning movements
 analyzed.
- The analysis also considers an assessment of historical crash data at all existing study intersections.
- The analysis also includes preliminary access management assessment and turn lane warrant assessments for the Site
 access points along Oak Springs Drive.

Analysis Results

2023 Existing Conditions

• Based on the capacity analysis of Existing Conditions, the two signalized study intersections operate at an overall level of service D or better during both the AM and PM peak hours.

- Based on the capacity analysis of Existing Conditions, three study intersections have at least one approach that operates at levels of service (LOS E or F) for at least one peak hour. The remaining intersection approaches operate at acceptable levels of service during both peak hours.
- Based on the analysis of the Synchro 95th percentile queue lengths, all turning movements have queue lengths that can
 be accommodated within the available storage length of the turn bays, except the southbound left turn movement at Study
 Intersection 1 (Broadview Avenue / Lee Highway at Winchester Street).

2027 Future Conditions without Development

- Based on the capacity analysis of 2027 Future Conditions with Development, the signalized study intersection would
 operate at an overall level of service D or better during both the AM and PM peak hours.
- The planned roundabout is expected to operate at an overall LOS B or better with all approaches operating at LOS D or better during the AM and PM peak hours.
- Based on the capacity analysis of 2027 Future Conditions without Development, two study intersections have at least one
 approach that would operate at levels of service (LOS E or F) for at least one peak hour. The remaining intersection
 approaches would operate at acceptable levels of service during both peak hours.
- Based on the analysis of the Synchro 95th percentile queue lengths, all turning movements have queue lengths that could be accommodated within the available storage length of the turn bays.

2027 Future Conditions with Development

- The Site is expected to generate approximately 154 new total trips during the AM peak hour, 197 new trips during the PM peak hour and 2,602 new trips during a typical weekday.
- Based on the capacity analysis of 2027 Future Conditions with Development, the signalized study intersection would
 operate at an overall level of service D or better during both the AM and PM peak hours.
- The planned roundabout is expected to operate at an overall LOS B with all approaches operating at LOS D or better during the AM and PM peak hours.
- Based on the capacity analysis of the 2027 Future Conditions with Development, two study intersections have at least
 one approach that would operate at levels of service (LOS E or F) for at least one peak hour (similar to 2027 Future
 Conditions without Development) during the AM and PM peak hours. The remaining intersection approaches would
 operate at acceptable levels of service during both peak hours.
- Based on the queuing analysis performed for the 2027 Future Conditions with Development, all turning movements have queue lengths that could be accommodated within the available storage length of the turn bays.

Overall Conclusion

Based on the capacity and queueing analysis results, the proposed Development will not have a substantial impact to the surrounding transportation and roadway network, assuming that the site is constructed as depicted on the concept plan. No improvements are warranted or recommend to accommodate the proposed Development.

Transportation Technical Appendix

Warrenton Village Center

Town of Warrenton, Virginia



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- Appendix B Crash Data by Study Intersection
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- Appendix F 2023 Existing Conditions Capacity Analysis Worksheets
- Appendix G Background Development and Roadway Improvement Excepts
- Appendix H 2027 Future Conditions without Development Capacity Analysis Worksheets
- Appendix I 2027 Future Conditions with Development Capacity Analysis Worksheets
- Appendix J Turn Lane Warrant Tables and Charts
- Appendix K MUTCD 4-Hour Warrant

A. Signed Scoping Document

THIS IS NOT A CHAPTER 870 STUDY



PRE-SCOPE OF WORK MEETING FORM

Information on the Project Traffic Impact Analysis Base Assumptions

The applicant is responsible for entering the relevant information and submitting the form to VDOT and the locality no less than three (3) business days prior to the meeting. If a form is not received by this deadline, the scope of work meeting may be postponed.

Contact Information								
Consultant Name:	Kevin Sitzman, Gor	ove Slade Associa	ites, Inc.					
Tele: E-mail:	703.787.9595 kevin.sitzman@goroveslade.com							
Developer/Owner Name:	Jess Achenbach							
Tele:	Jess Achenbach							
E-mail:	jachenbach@castle	dp.com						
Project Information								
Project Name:	Warrenton Village Center	Locali	ty/County:	Town	of Warrenton			
Project Location: (Attach regional and site specific location map)	Springs Drive (Tow	The proposed development will be located primarily along the southern frontage of Oak Springs Drive (Town Route 3), east of Broadview Avenue (US Route 17 Business) and west of Branch Drive (Town Route 4) in the Town of Warrenton, Virginia. (See Figure 1).						
Submission Type	Comp Plan 🗌	REZ/SUP		Site Plan 🔲		Subd Plat 🗌		
Project Description: (Including details on the land use, acreage, phasing, access location, etc. Attach additional sheet if necessary)	The development will be situated on a single parcel of vacant land (approximately 6.46 acres) and a portion of an adjacent developed parcel of land, which can be identified on Fauquier County Tax Maps with the following GPIN #s: 6985-20-7247-000, and 6984-29-6753-000, respectively. The property is currently zoned as C (Commercial District) with a Future Land Use of Mixed Use as part of the New Town Warrenton Character District (Lee Highway Urban Development Area [UDA]). The Applicant is proposing to apply for a Special Use Permit (SUP) in order to construct approximately 376 multifamily residential dwelling units (320 multifamily apartments, 36 2-over-2 units, and 20 townhomes) and a parking deck. The site has an anticipated build-out date of 2027. Access to the site will be provided via one full movement parking deck entry along Oak Springs Drive (Town Route 3) forming the forth leg of the High School Driveway, one full movement driveway along Oak Springs Drive forming the fourth-leg to the existing full-movement							
	Residential 🛚	Commercial 🗌		Mixed Use 🗌		Other 🗌		
Proposed Use(s): (Check all that apply; attach additional pages as necessary)	Residential Uses (s ITE LU Code(s): 22 Number of Units: 3	0		Commercial U ITE LU Code(s) Square Ft or O):	riable:		

	ITE LU Code(s): Square Ft or Other Variable:							
Total Peak Hour Trip Projection:	Less	s than 100	100 -	499 🛛	500	- 999 🔲		1,000 or more
Traffic Impact Analys	is As	ssumptions	5					
Study Period	Existing Year: 2023 Build-out Year:				2027		Desig	n Year: N/A
Study Area Boundaries	Nor	th: Oak Sprin	gs Drive ('	Town Route 3)	Sout	h: US Route	211 /	29 Business
(Attach map)	Bus	st: Broadview iness)	US Route 17	East	: Branch Dri	ive (To	own Route 4)	
External Factors That Could Affect Project (Planned road improvements, other nearby developments)	Sing	art Scale Roun 1. Broadvie	nes along Idabouts	•	у			
Consistency With Comprehensive Plan (Land use, transportation plan)	Yes							
Available Traffic Data (Historical, forecasts)		2023 TMC's VDOT Historical AADT Data						
Trip Distribution (Please refer to attached		d Name: /from the Nor	th) - N/A		Road Name: (to/from the South) – N/A			
Figure 2 in Supplement)	Road Name: (to/from the West) - N/A				Road Name: (to/from the East) – N/A			
Annual Vehicle Trip Growth Rate:		%/yr.	Peak Period for Study (check all that apply)		⊠ AM ⊠ PM □ SAT			SAT
(See Note 2.)	(2023 to 2027)		(to be used	• • • • • • • • • • • • • • • • • • • •	AM: 150 / PM: 192 / Dai			aily: 2,534
	1.		at Broad	S Route 17) / view Avenue /	6.		_	re (Town Route 3) at Future Access
Study Intersections	2.	Lee Highway Warrenton V at Chick-fil-a	/illage Cer	nter Driveway	7.		School	re (Town Route 3) at Driveway / Future
and/or Road Segments (Attach additional sheets as necessary)	3.	Lee Highway Drive (Town		te 17) at Branch	8.	Broadview Avenue (US Route 17 Business) at Oak Springs Drive (Town Route 3)		
(Please refer to attached Figure 1.)	4.	Branch Drive Warrenton V Safeway Driv	/illage Dri	•	9.	Broadview Avenue (US Route 17 Business) at Warrenton Village Center South Driveway		
	5.	Oak Springs	Drive (To	wn Route 3) at Route 4) / Cedar	10.	Broadview	v Aven at Wa	ue (US Route 17 renton Village

	Internal allowance Reduction:	Pass-by allowance Reduction:					
Trip Adjustment Factors	☐ Yes ⊠ No	☐ Yes ⊠ No					
Software Methodology	⊠ Synchro ☐ HCS (v.2000/+) ⊠ SIDF	RA CORSIM Other					
Traffic Signal Proposed or Affected (Analysis software to be used, progression speed, cycle length)	Existing traffic signals that could be affected: 1. Broadview Avenue (US Route 17) / Lee Highway at Broadview Avenue / Winchester Street 2. Lee Highway (US Route 17) at Branch Drive (Town Route 4) Analysis Software: Synchro version 11 Results: HCM 6 Methodology (See Note 7) Queue Lengths to be Reported: 95th Percentile						
Improvement(s) Assumed or to be Considered	Smart Scale Roundabouts 1. Broadview/Winchester/Lee 2. Roebling/Broadview						
Background Traffic Studies Considered	Waterloo Junction Single Family homes along Patrick Ryan Way						
Plan Submission	☐ Master Development Plan (MDP) ☐ Gene ☐ Preliminary/Sketch Plan ☐ Othe	eralized Development Plan (GDP) er Plan type (Final Site, Subd. Plan)					
Additional Issues to be Addressed	□ Queuing analysis □ Actuation/Coording □ Merge analysis □ Bike/Ped Accommod □ TDM Measures □ Other (ation					

NOTES on ASSUMPTIONS:

- 1. The scenarios to be included in the study are Existing Conditions (2023), Future without Development (2027) and Future with Development (2027). The study will analyze AM and PM peak hours.
- 2. Existing traffic volumes will be based on 2023 traffic count data. In order to project 2027 future conditions, a regional growth of 1.0% per annum will be applied to all turning movements at all study intersections.
- 3. Existing peak hour factors will be based on the traffic counts and utilized on a by-intersection basis. Peak hours factors by intersection in the range of 0.85 to 1.00 will be used for existing scenario. Peak hour factors of 0.92 will be used for all future scenarios if the existing peak hour factor by intersection is less than 0.92.
- 4. Heavy vehicle percentages (HV%) will be based on existing counts per movement. For any new leg or intersection, the HV% will be based on a default *Synchro* value of 2.0% per movement.
- 5. For any approach, a level of service (LOS) D or better would be considered as acceptable/desirable traffic operation condition. For all approaches, the projected future conditions without development LOS and delay will be maintained in the future with development condition. Will show intersection, approach, and movement LOS.
- 6. 95th percentile queues will be provided from *Synchro*.
- 7. HCM 6 methodology will be utilized where applicable; HCM 2000 methodology will be utilized if HCM 6 methodology is not applicable.
- 8. Preliminary access management and turn lane warrant assessments will be conducted for the site entrances.
- 9. Crash Data obtained from VDOT's Crash Analysis Tool will be analyzed at existing intersections.

SIGNED:	Applicant or Consultant	DATE: 6/30/2023
PRINT NAME	: <u>Kevin Sitzman</u> Applicant or Consultant	
SIGNED:	VDOT Representative	DATE:
PRINT NAME	: VDOT Representative	
SIGNED:	Local Government Representative	DATE:
PRINT NAME	: Local Government Representative	_
	Local Government Representative	

Table 1: Historic Growth (Based on VDOT Traffic Data)

				Published VDOT AADT				Growth Rate				
Road Segment:	From:	То:	2015	2016	2017	2018	2019	2015 - 2019	2016 - 2019	2017 - 2019	2018 - 2019	
Broadview Avenue	Bus US 29 Lee Hwy	NCL Warrenton	10,000	10,000	10,000	10,000	11,000	2%	3%	5%	10%	
Oak Springs Drive	Broadview Ave	Branch Dr	3,200	3,200	3,200	3,200	3,100	-1%	-1%	-2%	-3%	
Branch Drive	Lee Highway	Oak Springs Drive	3,800	4,200	4,200	4,300	4,300	3%	1%	1%	0%	



Figure 1: Site Location and Study Intersections

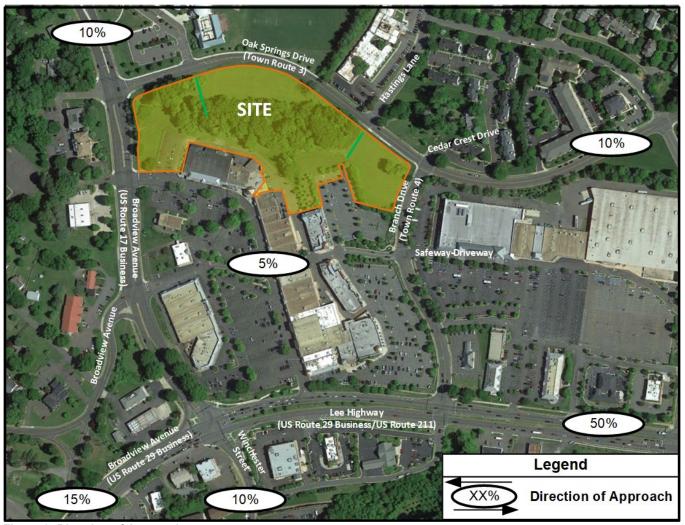


Figure 2: Direction of Approach

Table 2: Trip Generation – Peak Hour of the Adjacent Street (ITE 11th Edition) – To Be Used in Study

					W	eekd	ay		
Land Use	ITE Code	Size		AM Peak Hour		PM Peak Hour			Daily
			In	Out	Total	ln	Out	Total	Total
Multifamily Housing	220	376 DU	36	114	150	121	71	192	2,534

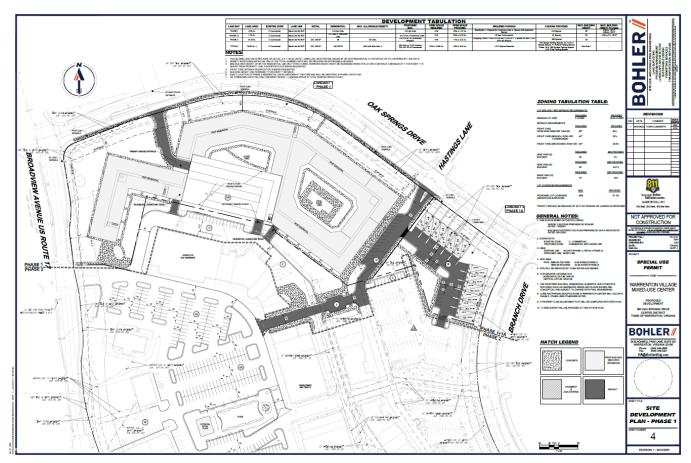


Figure 3: Illustrative Site Plan (Provided by Bohler)

Note: For conceptual purposes only.

B. Crash Data by Study Intersection

ntersection Crash Analysis	Crash Data for the Intersection of Lee Highway (US 211/US 29 BUS) and Broadview Avenue (US 17 BUS) (May 20 - April 2023)										
more section of a sin Panalyone	2018	2019	2020	2021	2022	2023	Total	Relative Frequency			
Crash Severity											
fatal Collision (Type K)								0.00%			
njury Collision (Type A, B, and C) Type A	2	6	1	1	2		12 1	30.00%			
Type B	,	2			2		4				
Type C	1	4	1	1	2		7				
			3	8	6		28	70.00%			
Property Damage Only (Type PDO) OTAL*	3 5	8 14	4	9	6 8		40	100.00%			
<u> </u>	<u> </u>	14	4	9	•		40	100.00%			
Crash Type						<u> </u>		1 0000/			
ixed Object/ Single-Vehicle Crash lead-On								0.00%			
ideswipe / Same Direction		1			2		3	7.50%			
ideswipe / Opposite Direction								0.00%			
ear-End Collision	3	8	4	5	4		24	60.00%			
ngle Collision	1	5		4	1		11	27.50%			
acked Into								0.00%			
edestrian Collision								0.00%			
eer/Animal								0.00%			
other	1				1		2	5.00%			
OTAL*	5	14	4	9	8		40	100.00%			
ther Factors											
istracted Driver								0.00%			
cohol**	1					Ĭ	1	2.50%			
ork-Zone								0.00%			
clement Weather (Non-Dry)		1			2	Ī	3	7.50%			
peeding	2						2	5.00%			
edestrian Injury***								N/A			
me of Day											
AM Peak Period (6 - 10 AM)	1	5		2			8	20.00%			
Off Peak - Daytime (10 AM - 3 PM)	1	5	3	4	4		17	42.50%			
PM Peak Period (3 - 7 PM)	2	3	1	3	2		11	27.50%			
Off Peak - Nighttime (7 PM - 6 AM)	1	1			2		4	10.00%			
CALCULATED CRASH RATE****							0.75	Crashes per MEV			

^{*}It should be noted that an intersection radius of 300 feet was used in this analysis. Crashes also thought to be caused by the intersection may have been added based on the description of the crash and engineering judgement.

^{**} Instances where the event was classified as "Unknown", "Not Known Whether Impaired", "Ability Not Impaired" were classified as alcohol related to provide a more conservative analysis.

^{***} Pedestrian injuries are based on the number of pedestrians injured and may not be directly be related to the number of crash incidences (i.e., if one crash occurred injuring two pedestrians, the table would show a "2" instead of a "1").

Crash Data for the Intersection of Lee Highway (US 211/US 29 BUS) and Broadview Avenue (US 17 BUS) (May 2018 - April 2023)

2010 - April 2023)												
Document Number	Date	Crash Severity	Collsion Type	Pedestrain Injury	Persons Injured	Fatalities	Work Zone Related	Adverse Weather Conditions	Distracted Driver			
182555077	9/11/2018	A. Severe Injury	16. Other	0	1	0		no	no			
181915232	7/5/2018	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			
181845228	6/28/2018	PDO. Property Damage Only	2. Angle	0	0	0		no	no			
182415104	8/20/2018	C. Nonvisible Injury	1. Rear End	0	1	0		no	no			
182885118	10/13/2018	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			
192075126	7/20/2019	B. Visible Injury	2. Angle	0	1	0		no	no			
193445038	8/21/2019	PDO. Property Damage Only	2. Angle	0	0	0		no	no			
191415326	5/15/2019	PDO. Property Damage Only PDO. Property	2. Angle	0	0	0		no	no			
191685219	5/22/2019	Damage Only	2. Angle	0	0	0		no	no			
190705057	3/5/2019	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			
190935057	4/2/2019	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			
192325410	8/20/2019	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			
191895108	7/5/2019	C. Nonvisible Injury	1. Rear End	0	5	0		no	no			
193445107	10/30/2019	C. Nonvisible Injury	1. Rear End	0	1	0		no	no			
193445122	11/14/2019	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			
193445083	10/13/2019	C. Nonvisible Injury	1. Rear End	0	1	0		no	no			
193445100	10/22/2019	C. Nonvisible Injury	1. Rear End	0	3	0		yes	no			
193445071	9/30/2019	PDO. Property Damage Only	Sideswipe - Same Direction	0	0	0		no	no			
191295165	5/8/2019	B. Visible Injury	2. Angle	0	1	0		no	no			
203495122	12/11/2020	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			
202175264	7/29/2020	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			
203175313	11/2/2020	C. Nonvisible Injury	1. Rear End	0	1	0		no	no			
201635154	6/2/2020	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			
212215197	7/25/2021	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			
212285259	8/6/2021	PDO. Property Damage Only	2. Angle	0	0	0		no	no			
211945123	7/6/2021	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			
211535051	5/26/2021	PDO. Property Damage Only	1. Rear End	0	0	0		no	no			

Crash Data for the Intersection of Lee Highway (US 211/US 29 BUS) and Broadview Avenue (US 17 BUS) (May 2018 - April 2023)

= / () =											
Document Number	Date	Crash Severity	Collsion Type	Pedestrain Injury	Persons Injured	Fatalities	Work Zone Related	Adverse Weather Conditions	Distracted Driver		
212725106	9/20/2021	C. Nonvisible Injury	1. Rear End	0	1	0		no	no		
213275307	11/17/2021	PDO. Property Damage Only	2. Angle	0	0	0		no	no		
211805101	6/21/2021	PDO. Property Damage Only	1. Rear End	0	0	0		no	no		
213145192	11/6/2021	PDO. Property Damage Only	2. Angle	0	0	0		no	no		
210905134	3/20/2021	PDO. Property Damage Only	2. Angle	0	0	0		no	no		
220205117	1/12/2022	PDO. Property Damage Only	1. Rear End	0	0	0		no	no		
222345164	8/21/2022	PDO. Property Damage Only	1. Rear End	0	0	0		no	no		
220975211	3/18/2022	PDO. Property Damage Only	1. Rear End	0	0	0		no	no		
222795285	10/6/2022	B. Visible Injury	8. Non-Collision	0	1	0		no	no		
222015106	7/14/2022	PDO. Property Damage Only	1. Rear End	0	0	0		no	no		
221295161	5/7/2022	B. Visible Injury	4. Sideswipe - Same Direction	0	1	0		yes	no		
220135226	1/6/2022	PDO. Property Damage Only	2. Angle	0	0	0		no	no		
222165194	7/8/2022	PDO. Property Damage Only	Sideswipe -Same Direction	0	0	0		yes	no		

Intersection Crash Analysis	Crash Data for the Intersection of Lee Highway (US 211/US 29 BUS) and Warrenton Village / Chick-fil-a Drivewa (May 2018 - April 2023)										
,	2018	2019	2020	2021	2022	2023	Total	Relative Frequency			
Crash Severity											
atal Collision (Type K)								0.00%			
njury Collision (Type A, B, and C)		1			1		2	40.00%			
Type A		1			1		2				
Туре В											
Type C											
roperty Damage Only (Type PDO)			1		2		3	60.00%			
OTAL*		1	1		3		5	100.00%			
rash Type											
ixed Object/ Single-Vehicle Crash			1		1		2	40.00%			
lead-On								0.00%			
ideswipe / Same Direction								0.00%			
ideswipe / Opposite Direction								0.00%			
lear-End Collision					1		1	20.00%			
ngle Collision		1			1		2	40.00%			
acked Into		-			-		_	0.00%			
edestrian Collision								0.00%			
leer/Animal								0.00%			
Other								0.00%			
OTAL*		1	1		3		5	100.00%			
ther Factors											
istracted Driver								0.00%			
cohol**					1		1	20.00%			
/ork-Zone								0.00%			
clement Weather (Non-Dry)			1				1	20.00%			
peeding					1		1	20.00%			
edestrian Injury***								N/A			
me of Day								0.000/			
AM Peak Period (6 - 10 AM)								0.00%			
Off Peak - Daytime (10 AM - 3 PM)					1		1	20.00%			
PM Peak Period (3 - 7 PM)		1	1		1 1		2 2	40.00% 40.00%			
Off Peak - Nighttime (7 PM - 6 AM) CALCULATED CRASH RATE****			7		7		0.13	40.00% Crashes per MEV			

^{*}It should be noted that an intersection radius of 300 feet was used in this analysis. Crashes also thought to be caused by the intersection may have been added based on the description of the crash and engineering judgement.

^{**} Instances where the event was classified as "Unknown", "Not Known Whether Impaired", "Ability Not Impaired" were classified as alcohol related to provide a more conservative analysis.

^{***} Pedestrian injuries are based on the number of pedestrians injured and may not be directly be related to the number of crash incidences (i.e., if one crash occurred injuring two pedestrians, the table would show a "2" instead of a "1").

Crash Data for the Intersection of Lee Highway (US 211/US 29 BUS) and Warrenton Village / Chickfil-a Driveway (May 2018 - April 2023)

						•			
Document Number	Date	Crash Severity	Collsion Type	Pedestrain Injury	Persons Injured	Fatalities	Work Zone Related	Adverse Weather Conditions	Distracted Driver
193445020	7/26/2019	A. Severe Injury	2. Angle	0	1	0		no	no
203025223	10/25/2020	PDO. Property Damage Only	9. Fixed Object -	0	0	0		yes	no
222785213	9/17/2022	A. Severe Injury	9. Fixed Object - Off Road	0	1	0		no	no
222135133	7/28/2022	PDO. Property Damage Only	1. Rear End	0	0	0		no	no
223325320	11/1/2022	PDO. Property Damage Only	2. Angle	0	0	0		no	no

ntersection Crash Analysis	Crash Da	ata for the In	tersection o	of Lee Highw	ay (US 211/	US 29 BUS) a	nd Branch Driv	e (May 2018 - April 2023
intersection orașii Analysis	2018	2019	2020	2021	2022	2023	Total	Relative Frequency
Crash Severity								
fatal Collision (Type K)								0.00%
njury Collision (Type A, B, and C) Type A	1		2	1	1		5	26.32%
Type B								
Type C	1		2	1	1		5	
roperty Damage Only (Type PDO)	2	1		3	8		14	73.68%
OTAL*	3	1	2	4	9	<u>=</u> _	19	100.00%
Crash Type								
ixed Object/ Single-Vehicle Crash				1			1	5.26%
ead-On								0.00%
ideswipe / Same Direction	1						1	5.26%
deswipe / Opposite Direction				1			1	5.26%
ear-End Collision	2			1	3		6	31.58%
ngle Collision			2	1	5		8	42.11%
acked Into		1					1	5.26%
edestrian Collision						ĺ		0.00%
eer/Animal								0.00%
ther					1		1	5.26%
OTAL*	3	1	2	4	9		19	100.00%
ther Factors						-		<u> </u>
stracted Driver								0.00%
cohol**								0.00%
ork-Zone								0.00%
clement Weather (Non-Dry)			4	2	11		3	15.79%
peeding edestrian Injury***			1		1		2	10.53% N/A
me of Day								IV/A
AM Peak Period (6 - 10 AM)	1			1	1		3	15.79%
Off Peak - Daytime (10 AM - 3 PM)	,		2	2	2		6	31.58%
PM Peak Period (3 - 7 PM)	2	1	-	1	6		10	52.63%
Off Peak - Nighttime (7 PM - 6 AM)	-	,		•	·		. •	0.00%
ALCULATED CRASH RATE****							0.45	Crashes per MEV

^{*}It should be noted that an intersection radius of 300 feet was used in this analysis. Crashes also thought to be caused by the intersection may have been added based on the description of the crash and engineering judgement.

^{**} Instances where the event was classified as "Unknown", "Not Known Whether Impaired", "Ability Not Impaired" were classified as alcohol related to provide a more conservative analysis.

^{***} Pedestrian injuries are based on the number of pedestrians injured and may not be directly be related to the number of crash incidences (i.e., if one crash occurred injuring two pedestrians, the table would show a "2" instead of a "1").

Crash Data for the Intersection of Lee Highway (US 211/US 29 BUS) and Branch Drive (May 2018 - April 2023)

Document Number	Date	Crash Severity	Collsion Type	Pedestrain Injury	Persons Injured	Fatalities	Work Zone Related	Adverse Weather Conditions	Distracted Driver
190035248	12/24/2018	PDO. Property Damage Only	4. Sideswipe -	0	0	0		no	no
182955427	10/20/2018	C. Nonvisible Injury	1. Rear End	0	2	0		no	no
183655065	12/17/2018	PDO. Property Damage Only	1. Rear End	0	0	0		no	no
193445084	10/13/2019	PDO. Property Damage Only	15. Backed Into	0	0	0		no	no
201995197	7/12/2020	C. Nonvisible Injury	2. Angle	0	1	0		no	no
201275157	4/1/2020	C. Nonvisible Injury	2. Angle	0	1	0		no	no
211335075	5/10/2021	PDO. Property Damage Only	2. Angle	0	0	0		no	no
212925308	10/10/2021	PDO. Property Damage Only PDO. Property	Fixed Object - Off Road	0	0	0		yes	no
212705186	9/20/2021	PDO. Property Damage Only	1. Rear End	0	0	0		no	no
211935132	6/22/2021	C. Nonvisible Injury	5. Sideswipe - Opposite Direction	0	2	0		yes	no
222805102	10/6/2022	PDO. Property Damage Only	2. Angle	0	0	0		no	no
220825133	3/21/2022	PDO. Property Damage Only	2. Angle	0	0	0		no	no
221965176	7/9/2022	PDO. Property Damage Only	2. Angle	0	0	0		yes	no
221965175	6/29/2022	PDO. Property Damage Only	2. Angle	0	0	0		no	no
221735151	6/2/2022	PDO. Property Damage Only	1. Rear End	0	0	0		no	no
222205137	8/6/2022	PDO. Property Damage Only	2. Angle	0	0	0		no	no
222695228	9/24/2022	C. Nonvisible Injury	1. Rear End	0	1	0		no	no
220385210	2/6/2022	PDO. Property Damage Only	1. Rear End	0	0	0		no	no
222975113	10/23/2022	PDO. Property Damage Only	16. Other	0	0	0		no	no

ntersection Crash Analysis								
	2018	2019	2020	2021	2022	2023	Total	Relative Frequency
Crash Severity								
atal Collision (Type K)								0.00%
njury Collision (Type A, B, and C) <i>Typ</i> e <i>A</i>					1		1	50.00%
Туре В								
Туре С					1		1	
roperty Damage Only (Type PDO)				1			1	50.00%
OTAL*				1	1		2	100.00%
rash Type								
ixed Object/ Single-Vehicle Crash								0.00%
ead-On								0.00%
ideswipe / Same Direction								0.00%
deswipe / Opposite Direction								0.00%
ear-End Collision								0.00%
ngle Collision				1	1		2	100.00%
acked Into					-		_	0.00%
edestrian Collision								0.00%
eer/Animal							***************************************	0.00%
ither								0.00%
OTAL*				1	1	-	2	100.00%
ther Factors								
stracted Driver								0.00%
cohol**				1			1	50.00%
ork-Zone						Ĭ		0.00%
clement Weather (Non-Dry)					1		1	50.00%
peeding						Ī		0.00%
edestrian Injury***								N/A
me of Day								
AM Peak Period (6 - 10 AM)					1		1	50.00%
Off Peak - Daytime (10 AM - 3 PM)								0.00%
PM Peak Period (3 - 7 PM)				1			1	50.00%
Off Peak - Nighttime (7 PM - 6 AM)								0.00%

^{*}It should be noted that an intersection radius of 300 feet was used in this analysis. Crashes also thought to be caused by the intersection may have been added based on the description of the crash and engineering judgement.

^{**} Instances where the event was classified as "Unknown", "Not Known Whether Impaired", "Ability Not Impaired" were classified as alcohol related to provide a more conservative analysis.

^{***} Pedestrian injuries are based on the number of pedestrians injured and may not be directly be related to the number of crash incidences (i.e., if one crash occurred injuring two pedestrians, the table would show a "2" instead of a "1").

Crash Data for the Intersection of Branch Drive and Warrenton Village / Safeway (May 2018 - April 2023)

Document Number	Date	Crash Severity	Collsion Type	Pedestrain Injury	Persons Injured	Fatalities	Work Zone Related	Adverse Weather Conditions	Distracted Driver
213055189	10/15/2021	Damage Only	2. Angle	0	0	0		no	no
223255325	11/11/2022	C. Nonvisible Injury	2. Angle	0	1	0		ves	no

ntersection Crash Analysis	Crash Data for the Intersection of Branch Drive and Oak Springs Drive (May 2018 - April 2023)									
	2018	2019	2020	2021	2022	2023	Total	Relative Frequency		
Crash Severity										
atal Collision (Type K)								0.00%		
njury Collision (Type A, B, and C) <i>Type A</i>								0.00%		
Туре В										
Type C										
roperty Damage Only (Type PDO)			1		1		2	100.00%		
OTAL*			1		1		2	100.00%		
rash Type										
ixed Object/ Single-Vehicle Crash								0.00%		
ead-On								0.00%		
ideswipe / Same Direction								0.00%		
ideswipe / Opposite Direction								0.00%		
ear-End Collision								0.00%		
ngle Collision			1		1		2	100.00%		
acked Into								0.00%		
edestrian Collision								0.00%		
eer/Animal								0.00%		
ther								0.00%		
OTAL*			1		1		2	100.00%		
ther Factors										
stracted Driver								0.00%		
cohol**								0.00%		
ork-Zone								0.00%		
clement Weather (Non-Dry)								0.00%		
peeding								0.00%		
edestrian Injury***								N/A		
me of Day										
AM Peak Period (6 - 10 AM)								0.00%		
Off Peak - Daytime (10 AM - 3 PM)					1		1	50.00%		
PM Peak Period (3 - 7 PM)			1				1	50.00%		
Off Peak - Nighttime (7 PM - 6 AM) CALCULATED CRASH RATE****							0.27	0.00% Crashes per MEV		

^{*}It should be noted that an intersection radius of 300 feet was used in this analysis. Crashes also thought to be caused by the intersection may have been added based on the description of the crash and engineering judgement.

^{**} Instances where the event was classified as "Unknown", "Not Known Whether Impaired", "Ability Not Impaired" were classified as alcohol related to provide a more conservative analysis.

^{***} Pedestrian injuries are based on the number of pedestrians injured and may not be directly be related to the number of crash incidences (i.e., if one crash occurred injuring two pedestrians, the table would show a "2" instead of a "1").

Crash Data for the Intersection of Branch Drive and Oak Springs Drive (May 2018 - April 2023)

Document Number	Date	Crash Severity	Collsion Type	Pedestrain Injury	Persons Injured	Fatalities	Work Zone Related	Adverse Weather Conditions	Distracted Driver
202745301	9/18/2020	Damage Only PDU. Property	2. Angle	0	0	0		no	no
220335106	1/31/2022	PDO. Property Damage Only	2. Angle	0	0	0		no	no

ntersection Crash Analysis	Cras	sh Data for t	he Intersect	ion of Broad	dview Avenu	e and Oak S	prings Drive (N	lay 2018 - April 2023)
mersection orașii Analysis	2018	2019	2020	2021	2022	2023	Total	Relative Frequency
Crash Severity								
atal Collision (Type K)								0.00%
njury Collision (Type A, B, and C)	1						1	33.33%
Type A	1						1	
Туре В								
Type C								
roperty Damage Only (Type PDO)			2				2	66.67%
OTAL*	1		2			<u>-</u>	3	100.00%
rash Type								
xed Object/ Single-Vehicle Crash								0.00%
ead-On								0.00%
ideswipe / Same Direction								0.00%
deswipe / Opposite Direction								0.00%
ear-End Collision								0.00%
ngle Collision	1		2				3	100.00%
acked Into	1		2				3	0.00%
edestrian Collision								0.00%
eer/Animal								0.00%
ther								0.00%
OTAL*	1		2			■	3	100.00%
ther Factors								
istracted Driver								0.00%
cohol**								0.00%
ork-Zone								0.00%
clement Weather (Non-Dry)								0.00%
peeding								0.00%
edestrian Injury***								N/A
me of Day								
AM Peak Period (6 - 10 AM)								0.00%
Off Peak - Daytime (10 AM - 3 PM)			1				1	33.33%
PM Peak Period (3 - 7 PM)	1		1				2	66.67%
Off Peak - Nighttime (7 PM - 6 AM)								0.00%
CALCULATED CRASH RATE****							0.14	Crashes per MEV

^{*}It should be noted that an intersection radius of 300 feet was used in this analysis. Crashes also thought to be caused by the intersection may have been added based on the description of the crash and engineering judgement.

^{**} Instances where the event was classified as "Unknown", "Not Known Whether Impaired", "Ability Not Impaired" were classified as alcohol related to provide a more conservative analysis.

^{***} Pedestrian injuries are based on the number of pedestrians injured and may not be directly be related to the number of crash incidences (i.e., if one crash occurred injuring two pedestrians, the table would show a "2" instead of a "1").

Crash Data for the Intersection of Broadview Avenue and Oak Springs Drive (May 2018 - April 2023)

Document Number	Date	Crash Severity	Collsion Type	Pedestrain Injury	Persons Injured	Fatalities	Work Zone Related	Adverse Weather Conditions	Distracted Driver
182435282	8/23/2018	A. Severe Injury	2. Angle	0	1	0		no	no
202585163	2/22/2020	PDO. Property	2. Angle	0	0	0		no	no
202115210	7/15/2020	PDO. Property	2. Angle	0	0	0		no	no

ntersection Crash Analysis	Crash I	Data for the	Intersection	of Broadvie	ew Avenue a	and Warrentoi	n Village North	(May 2018 - April 2023)
mersection orașii Analysis	2018	2019	2020	2021	2022	2023	Total	Relative Frequency
Crash Severity								
atal Collision (Type K)								0.00%
jury Collision (Type A, B, and C) Type A			1		1		2	50.00%
Type B			1				1	
Type C					1		1	
roperty Damage Only (Type PDO)		1		1			2	50.00%
OTAL*		1	1	1	1	•	4	100.00%
rash Type								
xed Object/ Single-Vehicle Crash								0.00%
ead-On								0.00%
deswipe / Same Direction								0.00%
deswipe / Opposite Direction								0.00%
ear-End Collision								0.00%
ngle Collision			1	1	1		3	75.00%
acked Into								0.00%
edestrian Collision								0.00%
eer/Animal		1					1	25.00%
ther								0.00%
OTAL*		1	1	1	1		4	100.00%
ther Factors								
stracted Driver								0.00%
cohol**					1		1	25.00%
ork-Zone								0.00%
clement Weather (Non-Dry)					1		1	25.00%
peeding						<u></u>		0.00%
edestrian Injury***								N/A
me of Day AM Peak Period (6 - 10 AM)		1					1	25.00%
Off Peak - Daytime (10 AM - 3 PM)		1					,	25.00%
PM Peak Period (3 - 7 PM)			1	1	1		3	75.00%
Off Peak - Nighttime (7 PM - 6 AM)			,	,	,		3	0.00%
CALCULATED CRASH RATE****							0.21	Crashes per MEV

^{*}It should be noted that an intersection radius of 300 feet was used in this analysis. Crashes also thought to be caused by the intersection may have been added based on the description of the crash and engineering judgement.

^{**} Instances where the event was classified as "Unknown", "Not Known Whether Impaired", "Ability Not Impaired" were classified as alcohol related to provide a more conservative analysis.

^{***} Pedestrian injuries are based on the number of pedestrians injured and may not be directly be related to the number of crash incidences (i.e., if one crash occurred injuring two pedestrians, the table would show a "2" instead of a "1").

Crash Data for the Intersection of Broadview Avenue and Warrenton Village North (May 2018 - April 2023)

Document Number	Date	Crash Severity	Collsion Type	Pedestrain Injury	Persons Injured	Fatalities	Work Zone Related	Adverse Weather Conditions	Distracted Driver
192545226	9/11/2019	PDO. Property Damage Only	10. Deer	0	0	0		no	no
202765309	9/20/2020	B. Visible Injury	2. Angle	0	1	0		no	no
211665121	5/27/2021	PDO. Property Damage Only	2. Angle	0	0	0		no	no
223465170	12/6/2022	C. Nonvisible Injury	2. Angle	0	1	0		yes	no

ntersection Crash Analysis								
	2018	2019	2020	2021	2022	2023	Total	Relative Frequency
Crash Severity								
atal Collision (Type K)								0.00%
njury Collision (Type A, B, and C) Type A	2			2	3		7	53.85%
Type B								
Type C	2			2	3		7	
roperty Damage Only (Type PDO)	1		2	2	1		6	46.15%
OTAL*	3		2	4	4		13	100.00%
rash Type								
xed Object/ Single-Vehicle Crash								0.00%
ead-On	1				2		3	23.08%
deswipe / Same Direction				1			1	7.69%
deswipe / Opposite Direction								0.00%
ear-End Collision			1				1	7.69%
ngle Collision	1		1	3	2		7	53.85%
acked Into								0.00%
edestrian Collision								0.00%
eer/Animal						ĺ		0.00%
ther	1						1	7.69%
OTAL*	3		2	4	4		13	100.00%
ther Factors								
stracted Driver						<u>.</u>		0.00%
cohol**	1						1	7.69%
ork-Zone								0.00%
clement Weather (Non-Dry)						<u> </u>		0.00%
peeding			1				1	7.69%
edestrian Injury***								N/A
me of Day								
AM Peak Period (6 - 10 AM)					1		1	7.69%
Off Peak - Daytime (10 AM - 3 PM)	1		2	2	2		7	53.85%
PM Peak Period (3 - 7 PM)	1			2	1		4	30.77%
Off Peak - Nighttime (7 PM - 6 AM)	1						1	7.69%

^{*}It should be noted that an intersection radius of 300 feet was used in this analysis. Crashes also thought to be caused by the intersection may have been added based on the description of the crash and engineering judgement.

^{**} Instances where the event was classified as "Unknown", "Not Known Whether Impaired", "Ability Not Impaired" were classified as alcohol related to provide a more conservative analysis.

^{***} Pedestrian injuries are based on the number of pedestrians injured and may not be directly be related to the number of crash incidences (i.e., if one crash occurred injuring two pedestrians, the table would show a "2" instead of a "1").

Crash Data for the Intersection of Broadview Avenue and Warrenton Village South (May 2018 - April 2023)

Document Number	Date	Crash Severity		Pedestrain Injury	Persons Injured	Fatalities	Work Zone Related	Adverse Weather Conditions	Distracted Driver
182505243	9/5/2018	C. Nonvisible Injury	6. Fixed Object in Road	0	1	0		no	no
182835057	10/4/2018	C. Nonvisible Injury	2. Angle	0	1	0		no	no
182135102	7/31/2018	PDO. Property Damage Only	3. Head On	0	0	0		no	no
201265208	2/25/2020	PDO. Property Damage Only	1. Rear End	0	0	0		no	no
201265233	3/12/2020	PDO. Property Damage Only	2. Angle	0	0	0		no	no
213625118	12/15/2021	C. Nonvisible Injury	2. Angle	0	2	0		no	no
213145191	11/3/2021	PDO. Property Damage Only	2. Angle	0	0	0		no	no
210135154	1/6/2021	C. Nonvisible Injury	2. Angle	0	1	0		no	no
212425152	8/23/2021	PDO. Property Damage Only	4. Sideswipe -	0	0	0		no	no
221235227	4/29/2022	C. Nonvisible Injury	3. Head On	0	1	0		no	no
221045273	3/28/2022	PDO. Property Damage Only	3. Head On	0	0	0		no	no
220945207	3/29/2022	C. Nonvisible Injury	2. Angle	0	1	0		no	no
223325319	11/23/2022	C. Nonvisible Injury	2. Angle	0	1	0		no	no

C. Turning Movement Counts Data

Location: US 17/Winchester St & US 17/US 211/Broadview Ave City: Warrenton Control: Signalized

Project ID: 23-260020-001 Date: 2/9/2023

Control:	Signalized													Date: 2	1/9/2023		
_								Data -	Total								
NS/EW Streets:		US 17/Wind	chester St			US 17/Wind	chester St		US 1	7/US 211/E	Broadview A	ive	US 1	7/US 211/B	roadview A	ve	
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTE	OUND		
AM	1 NL	1 NT	1 NR	0 NU	1.5 SL	0.5 ST	1 SR	0 SU	2 EL	1.5 ET	0.5 ER	0 EU	1 WL	2 WT	1 WR	0 WU	тот
6:00 AM	5	5	2	0	28	3	15	0	18	155	2	1	2	48	21	1	306
6:15 AM	7	Ō	6	ō	15	2	19	Ō	21	167	1	1	0	78	32	1	350
6:30 AM	7	9	8	ō	18	1	31	Ō	18	179	2	0	Ō	90	27	0	390
6:45 AM	12	11	8	ō	27	5	45	Ō	23	163	0	3	6	122	32	ō	45
7:00 AM	13	13	10	0	27	3	97	0	46	171	1	1	7	134	41	0	56
7:15 AM	20	8	11	0	31	8	89	0	58	208	5	2	6	119	31	1	59
7:30 AM	15	25	14	0	28	9	34	0	83	220	13	1	6	154	49	0	65
7:45 AM	27	42	32	ō	34	40	61	ō	73	169	5	2	5	162	64	1	71
8:00 AM	14	19	12	0	22	26	61	0	57	204	7	2	9	140	29	1	603
8:15 AM	17	17	12	0	26	18	59	0	44	165	6	0	11	159	29	1	564
8:30 AM	24	11	21	0	29	13	61	Ó	52	159	13	2	11	125	28	3	552
8:45 AM	16	17	8	0	45	26	54	0	53	170	16	4	4	141	24	3	58
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT
TOTAL VOLUMES:	177	177	144	0	330	154	626	0	546	2130	71	19	67	1472	407	12	633
APPROACH %'s:	35.54%	35.54%	28.92%	0.00%	29.73%	13.87%	56.40%	0.00%	19.74%	77.01%	2.57%	0.69%	3.42%	75.18%	20.79%	0.61%	
PEAK HR :		07:15 AM -															TOT
PEAK HR VOL:	76	94	69	0	115	83	245	0	271	801	30	7	26	575	173	3	256
PEAK HR FACTOR:	0.704	0.560	0.539	0.000	0.846	0.519	0.688	0.000	0.816	0.910	0.577	0.875	0.722	0.887	0.676	0.750	0.89
		0.59	92			0.8	20			0.87	/5			0.83	5/		
		NORTH	BOLIND			SOUTH	BOLIND			EASTB	OLIND			WESTE	OLIND		
PM	1	1	1	0	1.5	0.5	1	0	2	1.5	0.5	0	1	2	1	0	
FIVI	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER.	EU	WL	WT	WR	WU	тот
4:00 PM	29	18	21	0	72	18	94	1	51	194	14	0	7	309	23	1	857
4:15 PM	32	27	15	Ö	46	23	86	ī	69	167	9	1	19	240	40	1	770
4:30 PM	24	28	16	ŏ	50	23	103	ō	71	223	9	ī	17	261	24	4	85
4:45 PM	29	22	15	ō	44	19	94	Ō	67	210	8	0	13	264	19	4	80
5:00 PM	12	35	13	0	47	14	63	0	68	170	13	2	14	265	23	4	74
5:15 PM	18	34	18	ō	46	18	75	ō	60	180	11	1	13	284	28	1	78
5:30 PM	22	29	15	0	28	19	69	0	44	183	7	4	12	218	40	1	69
5:45 PM	16	27	16	0	37	23	74	0	47	176	8	1	8	252	25	6	71
6:00 PM	32	23	15	0	42	14	44	0	54	135	12	1	19	222	23	3	639
6:15 PM	14	12	17	0	42	19	45	0	47	144	6	1	17	236	34	4	638
6:30 PM	19	16	20	0	26	13	42	0	49	137	8	0	16	185	22	4	55
6:45 PM	14	17	20	0	25	10	35	0	43	107	9	1	13	194	24	4	516
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT
TOTAL VOLUMES :	261	288	201	0	505	213	824	2	670	2026	114	13	168	2930	325	37	857
APPROACH %'s:	34.80%	38.40%	26.80%	0.00%	32.71%	13.80%	53.37%	0.13%	23.73%	71.77%	4.04%	0.46%	4.86%	84.68%	9.39%	1.07%	-
PEAK HR:		04:00 PM -		•	242	00	277	,	250	704	40	2	F.C	1074	100	10	TOT
PEAK HR VOL :	114	95	67	0	212	83	377	2	258	794	40	2	56	1074	106	10	329
PEAK HR FACTOR:	0.891	0.848	0.798	0.000	0.736	0.902	0.915	0.500	0.908	0.890	0.714	0.500	0.737	0.869	0.663	0.625	0.96
		0.9	2/			0.9	11			().90	JU			0.91	D		

Location: US 17/Winchester St & US 17/US 211/Broadview Ave

PEAK HR VOL

PEAK HR FACTOR

94 0.870

0.798

City: Warrenton Control: Signalized **Project ID:** 23-260020-001 **Date:** 2/9/2023 Data - Cars US 17/US 211/Broadview Ave US 17/Winchester St US 17/Winchester St US 17/US 211/Broadview Ave NS/EW Streets: NORTHBOUND SOUTHBOUND EASTBOUND WESTBOUND AM TOTAL 296 338 372 439 536 563 624 692 579 517 509 548 27 15 17 27 26 28 25 33 22 24 27 43 6:00 AN 6:15 AN 149 163 171 160 165 196 213 159 199 157 155 166 14 19 16 18 15 22 39 55 81 70 54 39 51 52 48 74 87 112 127 112 7 7 12 19 14 25 12 16 23 14 31 6:30 AM 6:45 AM 7:00 AM 7:15 AM 9 11 13 7 25 42 18 16 9 17 29 43 92 83 30 61 61 57 49 50 27 31 40 30 48 63 27 11 7:30 AM 7:45 AM 8:00 AM 146 155 131 40 25 17 13 26 136 108 125 6 12 16 26 25 22 8:15 AM 8:30 AM 21 7 11 3 8:45 AM WU 12 0.66 TOTAL VOLUMES APPROACH %'s PEAK HR 0.009 314 29.79% 588 55.79% 68 2.56% 65 3.55% 391 21.389 140 512 19.31% 19 0.72 6013 TOTAL 168 77 0.667 0.827 108 0.818 82 0.513 767 0.900 0 0.000 235 0 0.000 260 0.802 29 0.558 544 0.877 2458 0.548 0 0.584 0.540 0.708 0.875 0.722 0.750 PEAK HR FACTOR 0.700 0.888 EASTBOUND 1.5 0.5 ET ER NORTHBOLIND SOUTHBOUND PM 1.5 SL 72 45 49 44 47 46 28 37 42 42 26 25 1.5 ET 190 164 220 205 168 177 WT 303 235 251 260 261 278 214 250 220 235 758 835 791 733 775 682 704 632 631 549 508 NL 29 32 24 29 12 18 22 16 31 14 19 14 50 67 69 64 67 59 44 45 53 46 48 42 4:00 PM 4:15 PM 4:30 PM 90 79 101 18 27 27 22 35 34 29 27 23 12 16 17 15 16 15 13 17 15 16 15 17 23 19 14 18 18 23 14 19 13 19 17 13 13 13 12 7 19 17 4:45 PM 5:00 PM 5:15 PM 91 74 67 72 44 44 42 35 11 28 40 24 23 5:30 PM 5:45 PM 6:00 PM 6:15 PM 181 172 132 141 0 0 0 0 33 22 23 6:30 PM 6:45 PM 137 104 179 191 16 13 WL 166 4.88% SL 503 33.16% EL 654 TOTAL VOLUMES 287 38.47% 212 13.97% 37 1.099 800 52.74% 1991 71.83% 114 4.11% 13 0.47 320 9.41% 8435

250 0.906

779 0.885

40 0.714

56 0.737

2 0.500

1049 0.866

104 0.650

10

0.625

210 0.729

0.000

361 0.894

0.500

0.902

TOTAL

3221

0.962

Location: US 17/Winchester St & US 17/US 211/Broadview Ave City: Warrenton

1 0 0.250 0.000 0.250

Location: City: Control:	Warrenton	hester St &	US 17/US :	211/Broadv	view Ave								Pro	oject ID: 2 Date: 2	23-260020- 2/9/2023	001	
								Data	- HT								
NS/EW Streets:		US 17/Wind	chester St			US 17/Wind	chester St		US 1	.7/US 211/E	Broadview A	ve	US 1	7/US 211/B	roadview A	ve	
		NORTH	IBOUND			SOUTH	BOUND			EASTB	OUND			WESTE	OUND		
AM	1	1	1	0	1.5	0.5	1	0	2	1.5	0.5	0	1	2	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
6:00 AM	0	0	0	0	1	0	1	0	2	6	0	0	0	0	0	0	10
6:15 AM	0	0	0	0	0	0	0	0	3	4 8	0	0	0	4	1	0	12
6:30 AM 6:45 AM	0	0	0	0	1 0	0	2	0	3	3	0	0	0 1	3 10	0 1	0	18 18
7:00 AM	1	0	0	0	1	0	5	0	7	5 6	0	0	0	7	1	0	28
7:15 AM	1	1	0	0	3	0	6	0	3	12	0	0	0	7	1	0	34
7:30 AM	i	Ô	1	o l	3	Ô	4	ñ	2	7	ñ	Ô	Ö	8	i	0	27
7:45 AM	2	Ö	1	0	1	Ö	0	0	3	10	Ö	Ö	Ö	7	1	Ö	25
8:00 AM	2	1	0	0	0	1	0	0	3	5	1	0	0	9	2	0	24
8:15 AM	1	1	1	Ō	2	1	2	Ō	5	8	Ō	ō	Ō	23	3	ō	47
8:30 AM	1	2	0	0	2	0	12	0	1	4	1	0	0	17	3	0	43
8:45 AM	2	0	1	0	2	0	4	0	1	4	0	0	1	16	2	0	33
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	11	5	4	0	16	2	38	0	34	77	3	0	2	111	16	0	319
APPROACH %'s:	55.00%	25.00%	20.00%	0.00%	28.57%	3.57%	67.86%	0.00%	29.82%	67.54%	2.63%	0.00%	1.55%	86.05%	12.40%	0.00%	
PEAK HR :		07:15 AM -	08:15 AM														TOTAL
PEAK HR VOL :	6	2	2	0	7	1	10	0	11	34	1	0	0	31	5	0	110
PEAK HR FACTOR :	0.750	0.500	0.500	0.000	0.583	0.250	0.417	0.000	0.917	0.708	0.250	0.000	0.000	0.861	0.625	0.000	0.809
		0.8	33			0.5	00			0.76	67			0.81	18		0.005
		NODTU	BOUND			SOUTH	DOLIND			EASTB	OLIND			WESTE	OLIND		
PM	1	1	1	0	1.5	0.5	1	0	2	1.5	0.5	0	1	2	1	0	
FIVI	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	4	0	1	4	0	0	0	6	0	0	15
4:15 PM	Ō	ō	ō	ō	1	Ō	7	ō	2	3	Ō	ō	Ō	5	Ō	ō	18
4:30 PM	0	1	0	0	1	Ó	2	0	2	3	0	0	0	10	0	0	19
4:45 PM	0	0	0	0	0	0	3	0	3	5	0	0	0	4	2	0	17
5:00 PM	0	0	0	0	0	0	2	0	1	2	0	0	1	4	0	0	10
5:15 PM	0	0	1	0	0	0	1	0	1	3	0	0	0	6	0	0	12
5:30 PM	0	0	0	0	0	1	2	0	0	2	0	0	0	4	0	0	9
5:45 PM 6:00 PM	0 1	0	0	0	0	0	0	0	2	3	0	0	0	2	0	0	12 7
6:15 PM	0	0	0	0	0	0	1	0	1	3	0	0	0	1	1	0	7
6:30 PM	0	0	1	0	0	0	0	0	1	0	0	0	0	6	0	0	8
6:45 PM	0	0	0	0	0	0	0	0	i	3	0	0	0	3	1	0	8
3.15111					_			_	_		-		-		_	_	_
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	1	1	2	0	2	1	24	0	16	35	0	0	2	53	5	0	142
APPROACH %'s:	25.00%	25.00% 04:00 PM -	50.00%	0.00%	7.41%	3.70%	88.89%	0.00%	31.37%	68.63%	0.00%	0.00%	3.33%	88.33%	8.33%	0.00%	TOTAL
PEAK HR : PEAK HR VOL :	0	04:00 PM - 1	05:00 PM 0	0	2	0	16	0	8	15	0	0	0	25	2	0	69
PEAK HR VOL :	0.000	0.250	0.000	0.000	0.500	0.000	0.571	0.000	0.667	0.750	0.000	0.000	0.000	0.625	0.250	0.000	
FEAR FIR FACIUR :	0.000	0.250		0.000	0.300	0.000		0.000	0.007	0.750		0.000	0.000	0.625		0.000	0.908

8 15 0 0 0.667 0.750 0.000 0.000 0.719

0 16 0.000 0.571 0.563

0 25 2 0.000 0.625 0.250 0.675

Location: US 17/Winchester St & US 17/US 211/Broadview Ave City: Warrenton Control: Signalized

Project ID: 23-260020-001 **Date:** 2/9/2023

								Data -	Bikes								
NS/EW Streets:		US 17/Wir	nchester St			US 17/Wir	nchester St		US	17/US 211/E	Broadview A	ve	US	17/US 211/	Broadview	Ave	
		NORTI	HBOUND			SOUTI	HBOUND			EASTE	OUND			WEST	BOUND		
AM	1	1	1	0	1.5	0.5	1	0	2	1.5	0.5	0	1	2	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR:		07:15 AM	- 08:15 AM														TOTAL
PEAK HR VOL : PEAK HR FACTOR :	0 0.000	0.000	0 0.000	0 0.000	0.000	0 0.000	0.000	0 0.000	0 0.000	0.000	0 0.000	0 0.000	0.000	0 0.000	0 0.000	0.000	0
		NORTI	HBOUND			COLITI	HBOUND			EASTE	OLIND			WECT	BOUND		
PM	1	1	1	0	1.5	0.5	1	0	2	1.5	0.5	0	1	2	1	0	
FIVI	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER.	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0				0
4:15 PM	Ö	Ö	Ŏ	Ŏ	0									0	0	0	
4:30 PM	Õ					0	0			0	0	0		0	0	0	
		0	0		0	0	0	0	0	0	0	0	0	0 0 0	0	0	0
4:45 PM	0	0	0	0				0	0				0	0	0	0	0
4:45 PM 5:00 PM	0		0 0 0		0	0	Ō	0	0	ŏ	Ō	0	0	0	0	0	0
		Ō	0	0	0	0	0	0 0 0	0 0 0	0	0	0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0
5:00 PM	0	0	0	0 0 0	0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0
5:00 PM 5:15 PM	0	0 0 0	0 0 0	0 0 0 0	0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0
5:00 PM 5:15 PM 5:30 PM	0 0 0	0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0 0
5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 1	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0
5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM	0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 1	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 1
5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 1	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0
5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 1 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 0 0 0
5:00 PM 5:15 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 1 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 0 0 0
5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:15 PM 6:45 PM TOTAL VOLUMES : APPROACH %'s :	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 0 0 0 0 0 0 TOTAL
5:00 PM 5:15 PM 5:30 PM 5:35 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR VOL:	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 0 0 0 0 0 0 0
5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:15 PM 6:45 PM TOTAL VOLUMES : APPROACH %'s :	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 To

National Data & Surveying Services Intersection Turning

Location: US 17/Winchester St & US 17/US 211/Broadview Ave Count Project ID: 23-260020-001 City: Warrenton Date: 2/9/2023

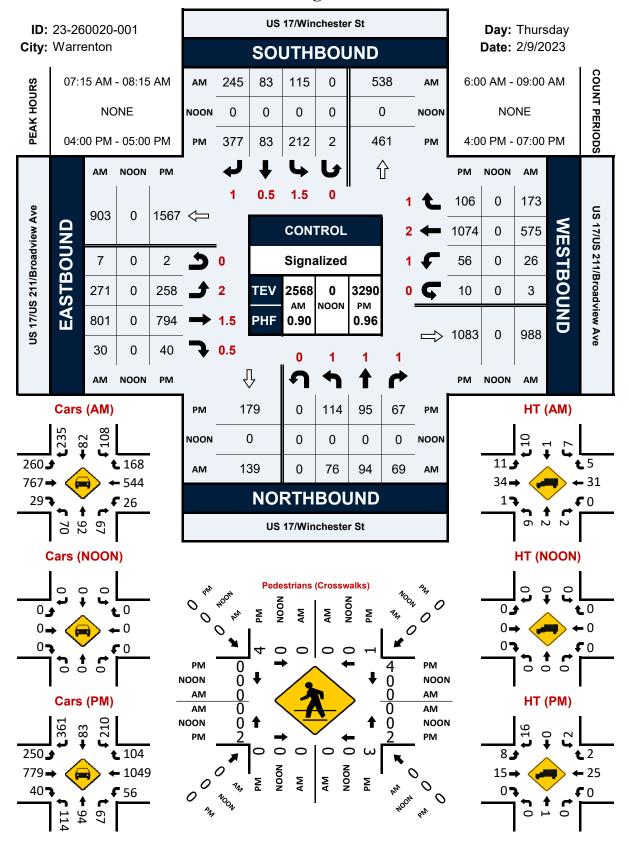
Data - Pedestrians (Crosswalks)

NS/EW Streets:	LIC 17/Min	chester St	LIC 17/Min	nchester St	US 17/US 21	1/Broadview	US 17/US 21	1/Broadview	
NS/EW Streets:	US 17/WII	ichester St	US 17/WII	ichester St		ve		ve	
AM		H LEG	SOUT	'H LEG	_	Γ LEG	_	Γ LEG	
Alvi	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0
6:15 AM		0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0
6:45 AM	0	0	0	0	0	0	0	0	0
7:00 AM	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	1	2	3
8:30 AM	1	0	0	0	0	0	0	0	1
8:45 AM	0	1	0	0	0	0	0	0	1
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	1	1	0	0	0	0	1	2	5
APPROACH %'s:	50.00%	50.00%					33.33%	66.67%	
PEAK HR:	07:15 AM	- 08:15 AM		·					TOTAL
PEAK HR VOL:	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR:									

PM	NORT	H LEG	SOUT	H LEG	EAST	LEG	WEST	LEG	
PIVI	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	0	1	1	2	0	0	4
4:15 PM	1	1	0	0	1	2	0	0	5
4:30 PM	1	0	0	0	0	0	0	0	1
4:45 PM	2	0	0	2	0	0	2	0	6
5:00 PM	0	0	0	0	0	4	0	0	4
5:15 PM	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	2	0	0	0	2
5:45 PM	0	0	0	0	0	0	0	0	0
6:00 PM	2	0	0	0	3	0	0	0	5
6:15 PM	1	0	0	0	0	0	0	0	1
6:30 PM	0	0	0	0	0	0	0	0	0
6:45 PM	0	0	1	1	0	0	0	0	2
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	7	1	1	4	7	8	2	0	30
APPROACH %'s:	87.50%	12.50%	20.00%	80.00%	46.67%	53.33%	100.00%	0.00%	
PEAK HR:	04:00 PM ·	- 05:00 PM							TOTAL
PEAK HR VOL :	4	1	0	3	2	4	2	0	16
PEAK HR FACTOR:	0.500	0.250		0.375	0.500	0.500	0.250		0.667
	0.6	525	0.3	375	0.5	500	0.2	50	0.667

US 17/Winchester St & US 17/US 211/Broadview Ave

Peak Hour Turning Movement Count



Location: Warrenton Village Center Dwy (Chipotle)/Walgreens Dwy & US 17/US 211/Broadview Ave

0.000

0.000

0.000

0.000

0 0.000

79 0.760

0.000

0.000

PEAK HR FACTOR

Project ID: 23-260020-002 **Date:** 2/9/2023 Warrenton Village Center Dwy Warrenton Village Center Dwy US 17/US 211/Broadview Ave US 17/US 211/Broadview Ave NS/EW Streets (Chipotle)/Walgreens Dwy NORTHBOUND (Chipotle)/Walgreens Dwy SOUTHBOUND EASTBOUND WESTBOUND AM TOTAL 252 307 318 356 402 414 477 487 413 416 383 428 WU 6:00 AM 6:15 AM 115 192 6:30 AM 6:45 AM 7:00 AM 7:15 AM 203 196 212 244 269 236 236 113 157 185 164 196 234 168 196 159 168 7:30 AM 7:45 AM 8:00 AM 207 8:15 AM 8:30 AM 7 10 23 208 230 8:45 AM SL 0 0.00% SU 0 0.009 NR 0 NU 0 EU TOTAL VOLUMES APPROACH %'s PEAK HR PEAK HR VOL 0 0.00% 39 100.00% 0.00% 1922 96.20% 0.009 4653 TOTAL 07:30 AM - 08:30 AN 794 0.848 0 0.849 948 U 0.881 0.000 0.881 0 0.000 0 0.000 0 0.000 0 0.000 31 0.861 0 0.000 1793 0.000 0.000 0.000 0.000 0.000 0.625 0.000 PEAK HR FACTOR 0.920 0.625 FASTROLIND NORTHBOLIND SOLITHBOLIND WESTROLIND PM TOTAL 653 555 616 605 586 597 499 574 507 527 4:00 PM 4:15 PM 4:30 PM 291 227 295 271 236 245 223 320 284 286 274 295 302 244 277 250 248 203 219 25 18 34 35 24 16 38 38 42 22 22 19 17 26 20 26 16 20 29 25 24 21 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 239 190 212 0 0 0 0 0 0 0 0 6:15 PM 6:30 PM 6:45 PM 185 158 434 420 0 0 0 0 0 0 NR 0 SL 0 0.00% NT 0 NU 0 TOTAL VOLUMES 260 100.00% 2772 100.00% 0.00% 0 0.00% 0 0.00% 3202 90.43% 339 9.57% 6573 APPROACH %'s PEAK HR PEAK HR VOL TOTAL

1084 0.919

0.000

0.000

0 0.000

1164 0.909

0.000

0.750 0.917 102

2429

0.930

0.000

Location: Warrenton Village Center Dwy (Chipotle)/Walgreens Dwy & US 17/US 211/Broadview Ave

Project ID: 23-260020-002 **Date:** 2/9/2023 Warrenton Village Center Dwy Warrenton Village Center Dwy US 17/US 211/Broadview Ave US 17/US 211/Broadview Ave NS/EW Streets (Chipotle)/Walgreens Dwy NORTHBOUND (Chipotle)/Walgreens Dwy SOUTHBOUND EASTBOUND WESTBOUND AM TOTAL 245 298 306 340 388 390 458 466 396 381 357 402 WU 6:00 AM 6:15 AM 176 188 110 6:30 AM 6:45 AM 7:00 AM 7:15 AM 194 193 205 229 258 224 231 110 144 178 156 188 225 156 172 137 7:30 AM 7:45 AM 8:00 AM 196 204 221 8:15 AM 8:30 AM 7 10 23 8:45 AM 151 SL 0 0.00% SU 0 0.009 NR 0 NU 0 EU TOTAL VOLUMES APPROACH %'s PEAK HR PEAK HR VOL 0 0 0.00% 38 100.00% 0.00% 0.009 4427 TOTAL 07:30 AM - 08:30 AN 31 3 0.861 0.825 909 U 0.881 0.000 0.881 0 0.000 0 0.000 0 0.000 0 0.000 1701 0.000 0.000 0.000 0.000 0.000 0.625 0.000 0.000 0.823 PEAK HR FACTOR 0.913 0.625 FASTROLIND NORTHBOLIND SOLITHBOLIND PM WT 314 277 278 268 291 296 241 273 248 246 197 215 TOTAL 642 544 604 594 579 587 493 566 502 522 427 413 4:00 PM 4:15 PM 4:30 PM 25 18 34 35 24 16 38 42 22 22 223 291 266 234 241 221 235 187 19 17 26 19 4:45 PM 5:00 PM 5:15 PM 26 15 20 29 25 24 21 5:30 PM 5:45 PM 6:00 PM 0 0 0 0 0 6:15 PM 209 0 0 0 6:30 PM 6:45 PM 184 155 0 0 0 0 0 0 NR 0 SL 0 0.00% NT 0 NU 0 TOTAL VOLUMES 258 100.00% 2732 100.00% 0 0.00% 0 0.00% 3144 90.27% 339 9.73% 6473 APPROACH %'s PEAK HR PEAK HR VOL 0.00% TOTAL 1066 0.916 0. 0.916 1137 0.000 0.000 0 0.000 79 0.760 102 2384 0.000 0.000 0.905 0.000 0.000 0.000 0.000 0.000 0.000 0.000 PEAK HR FACTOR 0.750

0.928

Location: Warrenton Village Center Dwy (Chipotle)/Walgreens Dwy & US 17/US 211/Broadview Ave

Project ID: 23-260020-002 **Date:** 2/9/2023 Warrenton Village Center Dwy Warrenton Village Center Dwy US 17/US 211/Broadview Ave US 17/US 211/Broadview Ave NS/EW Streets (Chipotle)/Walgreens Dwy SOUTHBOUND (Chipotle)/Walgreens Dwy NORTHBOUND EASTBOUND WESTBOUND AM TOTAL 6:00 AM 6:15 AM 6:30 AM 6:45 AM 7:00 AM 7:30 AM 7:35 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM 9 12 16 14 24 19 21 17 35 26 26 15 11 12 5 11 24 22 17 SU 0 0.00% SL 0 0.00% EL 0 0.00% ET 97 100.00% ER 0 0.00% EU 0 0.009 WL 0 0.00% NT 0 NR 0 NU 0 TOTAL VOLUMES : APPROACH %'s : PEAK HR : PEAK HR VOL : PEAK HR FACTOR : 0 0.00% 1 100.00% 128 100.00% 0 0.00% 226 TOTAL 53 U 0.552 0.000 0.552 39 0 0.813 0.000 0.813 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 92 0.000 0.000 0.000 0.000 0.657

4:10 PM			NORTH	HBOUND			SOUTH	BOUND			EASTB	OUND			WESTE	BOUND		
NL	PM	0	0	0	0	0	1	0	0	0	3	0	0		2	1	0	
## 4:30 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
## ## ## ## ## ## ## ## ## ## ## ## ##	4:00 PM	0	0	0	0	0	0	0	0	0	5	0	0	0	6	0	0	11
A:45 PM		0	0	0	0	0	0	0	0	0	4	0	0	0	7	0	0	
S:00 PM	4:30 PM	0	0	0	0	0	0	0	0	0	4	0	0	0	8	0	0	12
S:15 PM	4:45 PM	0	0	0	0	0	0	0	0	0	5	0	0	0	6	0	0	11
5:30 PM 0 0 0 0 0 0 0 1 0 0 2 0 0 0 3 0 0 6 8 5:45 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0	0	0	0	0	0	1	0	0	2	0	0	0	4	0	0	/
S:45 PM		0	0	0	0	0	0	0	0	0	4	0	0	0	6	0	0	10
6:00 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0	0	0	0	0	0	1	0	0	2	0	0	0	3	0	0	
6:15 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0	0	0		0	0	0	0	0	4	0	0	0	4	0	0	8
6:30 PM		0	0	0	0	0	0	0	0	0	3	0	0	0	2	0	0	5
6:45 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0	0	0	0	0	0	0	0	0	3	0	0	0	2	0	0	5
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU TOTAL VOLUMES: 0 0 0 0 0 0 0 0 2 0 0 40 0 0 0 0 58 0 0 100 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0	0	0		0	0	0		0	1	0	0	0	6	0	0	7
TOTAL VOLUMES: 0	6:45 PM	0	0	0	0	0	0	0	0	0	3	0	0	0	4	0	0	7
TOTAL VOLUMES: 0 0 0 0 0 0 2 0 0 40 0 0 0 58 0 0 100 APPROACH %'s: 04:00 PM - 05:00 PM PEAK HR VOL: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		NII	NT	ND	NILL	CI	CT	CD	CII			FD	TII.	14/1	\A/T	WD	14/11	TOTAL
APPROACH %'s: 0.00% 0.00% 100.00% 0.00% 100.00% 0.00%	TOTAL VOLUMES		INI			SL 0		3K		EL.		EK O		VVL				
PEAK HR VOL: 0 0 0 0 0 0 0 0 0 27 0 0 45 PEAK HR FACTOR: 0.000 0		U	U	U	U	0.00%		100.00%		0.00%		0.00%		0.00%				
PEAK HR FACTOR: 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	PEAK HR :		04:00 PM	- 05:00 PM														TOTAL
	PEAK HR VOL :	0	0	0		0	0	0	0	0	18	0	0	0	27	0	0	45
	PEAK HR FACTOR:	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000			0.000	0.000			0.000	0.020
0.900 0.844						•					0.9	00			0.8	44		0.938

Location: Warrenton Village Center Dwy (Chipotle)/Walgreens Dwy & US 17/US 211/Broadview Ave

City: Warrenton Control: 1-Way Stop(SB)

Project ID: 23-260020-002 **Date:** 2/9/2023 Warrenton Village Center Dwy Warrenton Village Center Dwy US 17/US 211/Broadview Ave US 17/US 211/Broadview Ave NS/EW Streets (Chipotle)/Walgreens Dwy SOUTHBOUND (Chipotle)/Walgreens Dwy NORTHBOUND EASTBOUND WESTBOUND AM TOTAL
0
0
0
0
0
0
0
0
0
0
0
0
0
0
0
0
0 6:00 AM 6:15 AM 6:30 AM 6:45 AM 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM SR 0 WU 0 NT 0 NR 0 NU 0 SL 0 ST 0 SU 0 ET 0 ER 0 EU 0 WL 0 WT 0 WR 0 TOTAL EL 0 TOTAL VOLUMES : APPROACH %'s : PEAK HR : PEAK HR VOL : PEAK HR FACTOR : 0 TOTAL 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0.000 0.000 0.000 0.000 0.000

		NORTI	HBOUND			SOUT	HBOUND			EASTE	BOUND			WEST	BOUND		
PM	0	0	0	0	0	1	0	0	0	3	0	0	0	2	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
6:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
APPROACH %'s:									0.00%	100.00%	0.00%	0.00%					
PEAK HR:		04:00 PM	- 05:00 PM														TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
					•		•	-			-					-	

National Data & Surveying Services Intersection Turning

Location: Warrenton Village Center Dwy (Chipotle)/Walgreens Dwy & US 1//L Project ID: 23-260020-002
City: Warrenton

Date: 2/9/2023

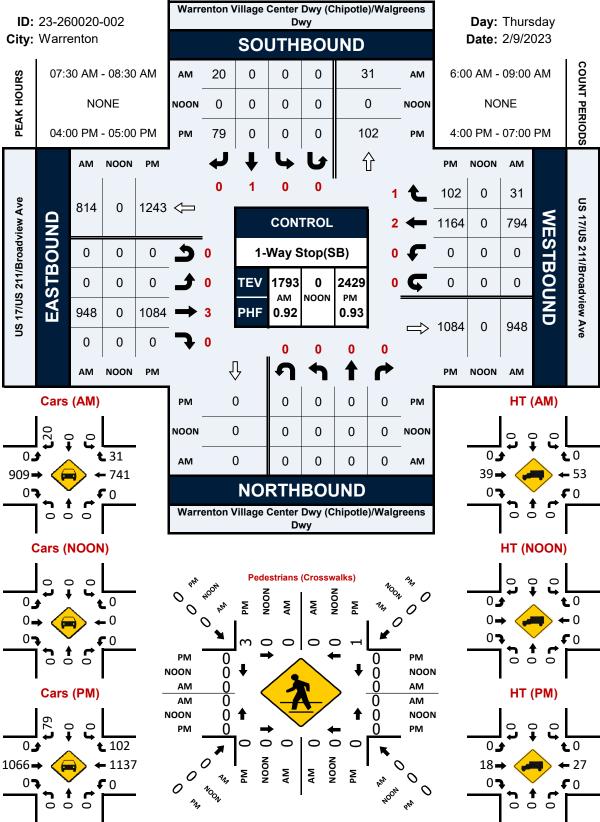
Data - Pedestrians (Crosswalks)

NC/EW Chrooter	Warrenton Vi	llage Center	Warrenton \	/illage Center	US 17/US 21	1/Broadview	US 17/US 21	1/Broadview	
NS/EW Streets:	Dwy (Chipotle	e)/Walgreens	Dwy (Chipot	le)/Walgreens	A	ve	A۱	/e	
ΛΝЛ	NORTH	1 LEG	SOUT	TH LEG	EAST	Γ LEG	WES	Γ LEG	
AM	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0
6:15 AM	0	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0
6:45 AM	0	0	0	0	0	0	0	0	0
7:00 AM	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0
8:30 AM	1	0	0	0	0	0	0	0	1
8:45 AM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	1	0	0	0	0	0	0	0	1
APPROACH %'s:	100.00%	0.00%							
PEAK HR:	07:30 AM -	08:30 AM							TOTAL
PEAK HR VOL:	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR:									

PM	NORT	H LEG	SOUT	'H LEG	EAST	LEG	WEST	Γ LEG	
PIVI	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0
4:15 PM	0	1	0	0	0	0	0	0	1
4:30 PM	1	0	0	0	0	0	0	0	1
4:45 PM	2	0	0	0	0	0	0	0	2
5:00 PM	0	2	0	0	0	0	0	0	2
5:15 PM	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0
6:00 PM	0	0	0	0	0	0	0	0	0
6:15 PM	1	0	0	0	0	0	0	0	1
6:30 PM	0	0	0	0	0	0	0	0	0
6:45 PM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	4	3	0	0	0	0	0	0	7
APPROACH %'s:	57.14%	42.86%							
PEAK HR :	04:00 PM	- 05:00 PM							TOTAL
PEAK HR VOL :	3	1	0	0	0	0	0	0	4
PEAK HR FACTOR :	0.375	0.250							0.500
	0.5	500							0.500

Warrenton Village Center Dwy (Chipotle)/Walgreens Dwy & US 17/US 211/Broadview Ave

Peak Hour Turning Movement Count Warrenton Village Center Dwy (Chipotle)/Walgreens



Location: Branch Dr & US 211/Lee Hwy/Broadview Ave City: Warrenton Control: Signalized

Data - Total

Project ID: 23-260020-003 Date: 2/9/2023

/Broadview Ave 30UND 1 0 WR WU 3 0 3 0 3 0 9 0 4 0 6 0 15 0 18 0 12 0	265 313 336 372 425 436
1 0 WR WU 3 0 3 0 9 0 4 0 6 0 15 0 18 0	265 313 336 372 425 436
WR WU 3 0 3 0 3 0 9 0 4 0 6 0 15 0 18 0	265 313 336 372 425 436
3 0 3 0 3 0 9 0 4 0 6 0 15 0 18 0	265 313 336 372 425 436
3 0 3 0 9 0 4 0 6 0 15 0 18 0	313 336 372 425 436
3 0 9 0 4 0 6 0 15 0 18 0	336 372 425 436
9 0 4 0 6 0 15 0 18 0	372 425 436
4 0 6 0 15 0 18 0	425 436
6 0 15 0 18 0	436
15 0 18 0	
18 0	
	505
12 0	526
	445
6 0	438
5 2	421
14 0	475
MD MIL	TOTAL
	4957
4./1% 0.10	TOTAL
E1 0	1914
	n .
	0.910
OUND	
WR WU	TOTAL
26 1	705
23 0	659
10 0	644
	685
	668
	623
	552
	636
	581
	547
	504
11 0	472
WR WU	TOTAL
221 11	
6.27% 0.31	
	TOTAL
84 1	2693
84 1 0.808 0.250 70	
	26 1 23 0

Location: Branch Dr & US 211/Lee Hwy/Broadview Ave

0.607

PEAK HR FACTOR

0.607

0.863

0.750

Project ID: 23-260020-003 **Date:** 2/9/2023 Data - Cars US 211/Lee Hwy/Broadview Ave Branch Dr US 211/Lee Hwy/Broadview Ave NS/EW Streets Branch Dr NORTHBOUND SOUTHBOUND EASTBOUND WESTBOUND AM TOTAL 259 303 325 353 411 412 487 505 428 402 392 447 6:00 AM 6:15 AM 174 176 183 173 206 210 235 208 211 69 102 6 11 6 11 10 10 11 11 6:15 AM 6:30 AM 6:45 AM 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 111 142 161 150 184 214 161 154 135 159 3 18 184 183 206 11 15 17 7 10 11 0 2 0 8:15 AM 8:30 AM 11 10 8 10 11 8:45 AM ER 4 0.16% SL 66 TOTAL VOLUMES APPROACH %'s PEAK HR PEAK HR VOL 0.009 0.009 122 6.21% 17 93 4724 50.82% TOTAL 51 3 0.708 0.830 41 57 0.569 0.683 33 0.750 43 0.977 0 0.000 29 0.806 0 0.000 1822 6 0.500 0.891 0.250 0.899 0.550 0.679 0.000 0.667 0.833 PEAK HR FACTOR 0.625 0.902 FASTROLIND NORTHBOUND SOUTHBOUND WESTROLIND PM 693 649 631 673 660 612 545 629 577 541 497 465 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 23 34 35 39 28 29 18 25 29 19 13 17 269 265 262 271 295 262 237 276 261 245 15 18 20 22 15 16 13 17 12 17 16 9 39 35 24 42 30 29 20 21 27 25 21 19 17 14 15 18 19 14 13 22 16 13 22 10 25 23 10 25 21 14 19 19 15 17 39 33 26 30 26 29 31 44 30 32 27 206 213 218 203 199 185 206 158 156 0 0 6:30 PM 6:45 PM 161 146 196 211 19 11 5 0 EL 309 11.69% TOTAL VOLUMES 46 387 49.94% 332 42.84% 2298 86.91% 33 1.25 193 5.56% 218 6.28% 11 0.329 7172 190 3050 87.85% APPROACH %'s PEAK HR PEAK HR VOL TOTAL 131 0.840 138 884 0.895 64 0.889 1067 0.984 75 0.852 0.000 140 0.833 0 0.000 2646 1 0.250

0.500

0.563

0.830

0.955

Location: Branch Dr & US 211/Lee Hwy/Broadview Ave
City: Warrenton

Location: E City: \ Control: S	Narrenton	& US 211/Le	ee Hwy/Broa	adview Ave	2			Data	. UT				Pro		23-260020- 2/9/2023	003	
NS/EW Streets:		Brand	h Dr			Brancl	h Dr	Data		1/Lee Hwy/	/Broadview	Ave	US 21	1/Lee Hwy,	/Broadview	Ave	
		NORTH	ROLIND			SOUTH	BOLIND			EASTB	OLIND			WESTE	OLIND		
AM	0.5 NL	0.5 NT	1 NR	0 NU	0.5 SL	0.5 ST	1 SR	0 SU	1 EL	2 ET	1 ER	0 EU	1 WL	2 WT	1 WR	0 WU	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0	6	0	0	0	0	0	0	6
6:15 AM	0	0	0	0	0	0	1	0	1	4	0	0	0	4	0	0	10
6:30 AM	0	0	0	0	0	0	0	0	1	7	0	0	0	3	0	0	11
6:45 AM	0	0	1	0	1	0	3	0	0	3	0	0	1	10	0	0	19
7:00 AM	0	0	0	0	0	0	1	0	0	7	0	0	0	6	0	0	14
7:15 AM	0	0	0	0	1	0	0	0	0	15	0	0	0	8	0	0	24
7:30 AM 7:45 AM	0	0	0	0	0	0	0	0	0	10 12	0	0	0	8 9	0	0	18 21
7:45 AM 8:00 AM	0	0	0	0	1	0	1	0	0	4	0	0	0	11	0	0	17
8:15 AM	0	0	0	0	0	0	8	0	0	11	0	1	1	15	0	0	36
8:30 AM	Ö	Ö	Ö	0	1	Ö	1	0	0	4	0	Ô	2	21	0	Ö	29
8:45 AM	Ö	1	Ö	Ö	1	Ö	î	Ö	Ö	8	Ŏ	Ö	Ō	17	Ö	Ö	28
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	1	1	0	5	0	16	0	2	91	0	1	4	112	0	0	233
APPROACH %'s : PEAK HR :	0.00%	50.00% 07:30 AM -	50.00%	0.00%	23.81%	0.00%	76.19%	0.00%	2.13%	96.81%	0.00%	1.06%	3.45%	96.55%	0.00%	0.00%	TOTAL
PEAK HR VOL :	0	07:30 AM - 0	08:30 AM	0	1	0	9	0	0	37	0	1	1	43	0	0	92
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.250	0.000	0.281	0.000	0.000	0.771	0.000	0.250	0.250	0.717	0.000	0.000	_
PLAKTIK PACTOR.	0.000	0.000	0.000	0.000	0.230	0.000		0.000	0.000	0.77		0.230	0.230	0.6		0.000	0.639
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTE	BOUND		
PM	0.5 NL	0.5 NT	1 NR	0 NU	0.5 SL	0.5 ST	1 SR	0 SU	1 EL	2 ET	1 ER	0 EU	1 WL	2 WT	1 WR	0 WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	5	0	0	0	6	1	0	12
4:15 PM	0	0	0	0	0	0	1	0	0	2	0	0	0	7	0	0	10
4:30 PM	0	0	0	0	1	0	0	0	0	5	0	0	0	7	0	0	13
4:45 PM	0	0	0	0	0	0	0	0	0	6	0	0	0	6	0	0	12
5:00 PM	0	0	1 0	0	0	0	1 2	0	0 0	2	0	0	0	3	1	0	8
5:15 PM 5:30 PM	0	0	0	0	1	0	0	0	0	4	0	0	0	4	0	0	11 7
5:45 PM	0	0	0	0	0	0	0	0	0	4	0	0	0	3	0	0	7
6:00 PM	0	0	0	0	0	0	1	0	0	2	0	0	0	1	0	0	4
6:15 PM	0	0	0	0	0	0	0	0	0	4	0	0	0	2	0	Ö	6
6:30 PM	Ŏ	Ö	Ö	ő	Ö	Ö	Ö	Ö	Ö	i	Ö	Ö	Ö	6	Ö	Ö	7
6:45 PM	Ö	Ö	Ŏ	Ö	ő	Ŏ	i	Ö	ő	3	Ŏ	Ö	Ö	3	Ŏ	Ö	7
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	0	1	0	2	0	6	0	0	40	0	0	0	52 94.55%	3	0	104
APPROACH %'s:	0.00%	0.00%	100.00%	0.00%	25.00%	0.00%	75.00%	0.00%	0.00%	100.00%	0.00%	0.00%	0.00%	94.55%	5.45%	0.00%	TOTAL
PEAK HR : PEAK HR VOL :	0	04:00 PM - 0	05:00 PM 0	0	1	0	1	0	0	18	0	0	0	26	1	0	TOTAL 47
PEAK HR VOL : PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.250	0.000	0.250	0.000	0.000	0.750 0.75	0.000	0.000	0.000	0.929	0.250	0.000	0.904

0 1 0.000 0.250 0.500

0 18 0 0.000 0.750 0.000 0.750

26 1 0.929 0.250 0.964

Location: Branch Dr & US 211/Lee Hwy/Broadview Ave **City:** Warrenton **Control:** Signalized

Project ID: 23-260020-003 **Date:** 2/9/2023

	signalized							Data -	Bikes						2/9/2023		
NS/EW Streets:		Bran	ch Dr			Bran	ch Dr		US 2	11/Lee Hwy	/Broadview	Ave	US 21	1/Lee Hwy	/Broadview	Ave	
		NORTI	HBOUND			SOUTI	HBOUND			EASTE	BOUND			WEST	BOUND		
AM	0.5 NL	0.5 NT	1 NR	0 NU	0.5 SL	0.5 ST	1 SR	0 SU	1 EL	2 ET	1 ER	0 EU	1 WL	2 WT	1 WR	0 WU	TOTA
6:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR:		07:30 AM	- 08:30 AM														TOT
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
		NORTH	HBOUND			SOUTI	HBOUND			FASTE	BOUND			WEST	BOUND		
PM	0.5	0.5	1	0	0.5	0.5	1	0	1	2	1	0	1	2	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
6:00 PM	0	0	0	0	0		0	0		0	0	0	0	0	0	0	0
6:15 PM 6:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 PM 6:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.43 PM	U	U	U	U	U	U	U	U	U	U	U	U	U	U	U	U	-
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT
TOTAL VOLUMES:	0	0	0	0	0	0	0	0	0	1	0	0	2	0	0	0	3
									0.00%	100.00%	0.00%	0.00%	100.00%	0.00%	0.00%	0.00%	
APPROACH %'s:																	TOT
PEAK HR:		04:00 PM															101
	0,000	0 0 0,000	- 05:00 PM 0 0.000	0	0	0 0.000	0	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	2 0.500	0 0.000	0 0.000	0 0.000	2

National Data & Surveying Services Intersection Turning

Location: Branch Dr & US 211/Lee Hwy/Broadview Ave
City: Warrenton

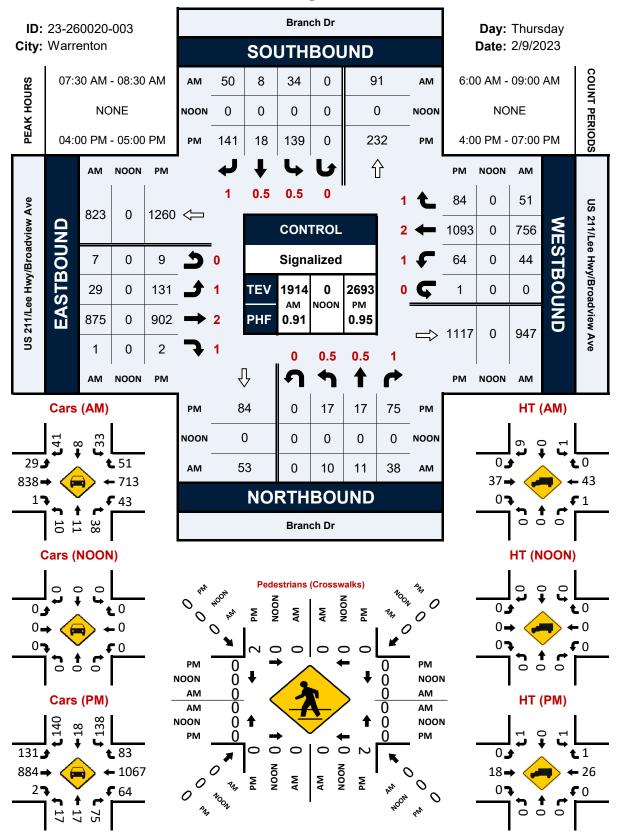
Data - Pedestrians (Crosswalks)

NS/EW Streets:	Branch Dr		Bron	nch Dr	US 21	.1/Lee	US 21	.1/Lee	
NS/EW Streets:	Diane	וט וו.	Didi	ICH DI	Hwy/Broa	dview Ave	Hwy/Broa	dview Ave	
AM	NORT	H LEG	SOUT	ΓH LEG	EAST	LEG	WES		
Alvi	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0
6:15 AM	2	0	0	0	0	0	0	0	2
6:30 AM	0	0	0	0	0	0	0	0	0
6:45 AM		0	0	0	0	0	0	0	0
7:00 AM	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0
7:45 AM		0	0	0	0	0	0	0	0
8:00 AM		0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0
8:30 AM	1	1	0	0	0	0	0	0	2
8:45 AM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	3	1	0	0	0	0	0	0	4
APPROACH %'s:	75.00%	25.00%							
PEAK HR:	07:30 AM -	08:30 AM							TOTAL
PEAK HR VOL:	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR:									

DNA	NORT	H LEG	SOUT	H LEG	EAS	T LEG	WEST	Γ LEG	
PM	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	1	0	0	0	0	0	0	0	1
4:15 PM	0	0	0	0	0	0	0	0	0
4:30 PM	1	0	0	0	0	0	0	0	1
4:45 PM	0	0	0	2	0	0	0	0	2
5:00 PM	0	2	0	0	0	0	0	0	2
5:15 PM	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	1	0	0	0	0	0	1
6:00 PM	0	0	0	0	0	0	0	0	0
6:15 PM	0	0	0	0	0	1	0	0	1
6:30 PM	0	0	0	0	0	0	0	0	0
6:45 PM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	2	2	1	2	0	1	0	0	8
APPROACH %'s:	50.00%	50.00%	33.33%	66.67%	0.00%	100.00%			
PEAK HR:	04:00 PM	- 05:00 PM							TOTAL
PEAK HR VOL:	2	0	0	2	0	0	0	0	4
PEAK HR FACTOR:	0.500			0.250					0.500
	0.5	500	0.2	250					0.500

Branch Dr & US 211/Lee Hwy/Broadview Ave

Peak Hour Turning Movement Count



Location: Branch Dr & Warrenton Village Center Dwy/Shopping Center Dwy City: Warrenton Control: 2-Way Stop(EB/WB)

Project ID: 23-260020-004 **Date:** 2/9/2023 Warrenton Village Center Dwy/Shopping Center Dwy

Control:	2-Way Stop	(EB/WB)												Date:	2/9/2023		
_								Data -									
NS/EW Streets:		Branc	h Dr			Branc	h Dr		Warrentor	n Village Ce		hopping	Warrentor	n Village Ce		hopping	
NO/EW Streets.						Center Dwy Center Dwy											
		NORTH			SOUTHBOUND			EASTBOUND			WESTBOUND						
AM	0	2	0	0	0	2	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT
6:00 AM	2	2	0	0	2	5	0	0	0	4	2	0	1	0	0	0	18
6:15 AM	0	1	1	0	1	2	0	0	0	1	0	0	4	2	0	0	12
6:30 AM	1	3	1	0	1	4	0	0	0	3	2	0	3	1	0	0	19
6:45 AM	7	2	0	0	3	8	0	0	0	1	0	0	2	2	0	0	25
7:00 AM	3	6	0	0	0	9	0	0	0	4	5	0	3	6	1	0	37
7:15 AM	3	6	1	0	5	8	2	0	1	5	5	0	3	3	5	0	47
7:30 AM	10	16	0	0	2	10	1	0	0	5	5	0	1	3	5	0	58
7:45 AM	5	26	3	0	5	21	1	0	4	3	9	0	3	2	3	0	85
8:00 AM	6	14	3	0	6	16	0	0	1	4	10	0	2	4	2	0	68
8:15 AM	2	9	1	0	5	20	3	0	1	3	14	0	8	2	4	0	72
8:30 AM	9	5	0	0	3	17	5	0	3	2	5	0	1	4	3	0	57
8:45 AM	8	9	1	0	2	14	4	0	1	6	7	0	3	2	0	0	57
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TO
TOTAL VOLUMES:	56	99	11	0	35	134	16	0	11	41	64	0	34	31	23	0	55
APPROACH %'s:	33.73%	59.64%	6.63%	0.00%	18.92%	72.43%	8.65%	0.00%	9.48%	35.34%	55.17%	0.00%	38.64%	35.23%	26.14%	0.00%	
PEAK HR :	(07:30 AM -	08:30 AM														TO
PEAK HR VOL:	23	65	7	0	18	67	5	0	6	15	38	0	14	11	14	0	28
PEAK HR FACTOR:	0.575	0.625	0.583	0.000	0.750	0.798	0.417	0.000	0.375	0.750	0.679	0.000	0.438	0.688	0.700	0.000	0.8
		0.6	99			0.8	04			0.8	19			0.6	96		0.0.
		NORTH	BOUND			SOUTH	BOUND		EASTBOUND				WESTBOUND				
PM	0	2	0	0	0	2	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TO
4:00 PM	32	10	0	0	11	13	8	0	3	22	29	0	14	12	6	0	16
4:15 PM	19	6	3	0	10	11	8	0	6	22	28	0	10	12	14	Ó	14
4:30 PM	15	16	5	ō	13	9	10	ō	2	20	33	0	7	10	12	ō	15
4:45 PM	28	11	4	0	14	6	6	0	6	13	26	0	14	16	9	0	15

		NORTH	BOUND			SOUTH	BOUND			EASTE	BOUND			WESTE	OUND		
PM	0 NL	2 NT	0 NR	0 NU	0 SL	2 ST	0 SR	0 SU	0 EL	1 ET	0 ER	0 EU	0 WL	1 WT	0 WR	0 WU	TOTAL
4:00 PM	32	10	0	0	11	13	8	0	3	22	29	0	14	12	6	0	160
4:15 PM	19	6	3	ō l	10	11	8	ñ	6	22	28	ñ	10	12	14	ō	149
4:30 PM	15	16	5	ō	13	9	10	ō	2	20	33	ō	7	10	12	ō	152
4:45 PM	28	11	4	0	14	6	6	Ō	6	13	26	Ō	14	16	9	ō	153
5:00 PM	28	9	1	0	12	13	10	0	3	12	35	0	7	12	12	0	154
5:15 PM	25	7	3	0	12	9	9	0	6	12	30	0	11	9	12	Ó	145
5:30 PM	27	15	4	0	6	0	10	0	11	26	32	0	6	14	10	0	161
5:45 PM	28	6	2	0	9	6	8	0	5	22	32	0	12	21	7	0	158
6:00 PM	29	9	1	0	5	6	9	0	8	22	48	0	10	17	13	0	177
6:15 PM	20	16	2	0	4	6	6	0	6	17	32	0	8	14	8	0	139
6:30 PM	18	8	2	0	3	9	4	0	4	10	25	0	10	17	4	0	114
6:45 PM	10	6	0	0	1	5	7	0	4	9	36	0	4	7	10	0	99
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	279	119	27	0	100	93	95	0	64	207	386	0	113	161	117	0	1761
APPROACH %'s:	65.65%	28.00%	6.35%	0.00%	34.72%	32.29%	32.99%	0.00%	9.74%	31.51%	58.75%	0.00%	28.90%	41.18%	29.92%	0.00%	
PEAK HR :	(05:15 PM -	06:15 PM														TOTAL
PEAK HR VOL:	109	37	10	0	32	21	36	0	30	82	142	0	39	61	42	0	641
PEAK HR FACTOR:	0.940	0.617	0.625	0.000	0.667	0.583	0.900	0.000	0.682	0.788	0.740	0.000	0.813	0.726	0.808	0.000	0.905
		0.84	48			0.7	42			0.8	14			0.88	38		0.905

Location: Branch Dr & Warrenton Village Center Dwy/Shopping Center Dwy

APPROACH %'s PEAK HR PEAK HR VOL

PEAK HR FACTOR

Project ID: 23-260020-004 **Date:** 2/9/2023 City: Warrenton Control: 2-Way Stop(EB/WB) Data - Cars Village Center Dwy/Shopping enton Village Center Dwy/Shopping Branch Dr Branch Dr NS/EW Streets NORTHBOUND SOUTHBOUND AM TOTAL
18
10
17
20
35
44
58
84
65
66
54
54 WU 6:00 AM 6:15 AM 6:30 AM 6:45 AM 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 10 5 6 14 16 13 8:15 AM 8:30 AM 8:45 AM SU 0 0.00% EU TOTAL VOLUMES APPROACH %'s PEAK HR PEAK HR VOL 98 60.12% **7:30 AM** 0.009 120 71.01% 15 8.88% 61 53.98% 0.009 30 37.50% 23 28.75% 10 6.139 11 9.73% 525 TOTAL 14 25 0.700 0.679 38 50 0.679 0.819 58 0.690 18 0 0.000 6 0.375 15 0.750 0 0.000 14 0.438 0 0.000 273 0.000 0.583 0.575 0.625 0.750 0.417 0.625 PEAK HR FACTOR 0.813 NORTHBOLIND FASTROLIND SOLITHBOLIND PM 0 NL 32 19 15 28 28 25 27 28 29 20 18 4:00 PM 4:15 PM 4:30 PM 13 10 9 14 10 7 11 10 13 14 12 12 22 20 13 12 12 26 22 27 17 10 9 29 27 32 26 35 30 32 32 48 32 25 36 145 150 153 152 143 161 157 176 139 8 10 11 10 16 11 9 14 20 17 14 16 7 4:45 PM 5:00 PM 5:15 PM 12 12 10 7 13 11 5:30 PM 5:45 PM 6:00 PM 6:15 PM 15 6 9 16 0 0 0 8 10 3 8 4 10 6:30 PM 6:45 PM 113 97 2 0 0 ET 207 31.60% WL 112 29.17% SL 100 35.46% ST 87 TOTAL VOLUMES 0.00% 95 33.69% 64 9.77% 115 29.95% 1745 118 27.83% 27 6.379

142 8 0.740 0.814

0.788

39 0.813

0 0.000

60 0.750

42 0.808

0 0.000

TOTAL

637

0.905

30.85%

0.643

36

0.900

0.000

0.682

0.000

0.667

0.617

0.625

Location: Branch Dr & Warrenton Village Center Dwy/Shopping Center Dwy City: Warrenton

TOTAL VOLUMES : APPROACH %'s : PEAK HR : PEAK HR VOL : PEAK HR FACTOR :

0 0.000

0.000

0.000

City:	Branch Dr 8 Warrenton 2-Way Stor	& Warrenton o(EB/WB)	Village Cer	iter Dwy/S	nopping Cei	nter Dwy							Pro		23-260020- 2/9/2023	004	
	,	, ,						Data	- HT								
NS/EW Streets:		Branch	n Dr			Branch	Dr		Warrenton Village Center Dwy/Shopping Center Dwy				Warrenton Village Center Dwy/Shopping Center Dwy				
		NORTH	BOUND		SOUTHBOUND			EASTBOUND			WESTBOUND						
AM	0	2	0	0	0	2	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT
6:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 AM	0	1	0	0	0	0	0	0	0	0	0	0	1	0	0	0	2
6:30 AM	0	0	1	0	0	0	0	0	0	0	1	0	0	0	0	0	2
6:45 AM	1	0	0	0	0	2	0	0	0	0	0	0	1	1	0	0	5
7:00 AM	0	0	0	0	0	1	0	0	0	0	0	0	0	1	0	0	2
7:15 AM	0	0	0	0	1	0	1	0	0	0	1	0	0	0	0	0	3
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
8:00 AM	0	0	0	0	0	3	0	0	0	0	0	0	0	0	0	0	3
8:15 AM	0	0	0	0	0	6 1	0	0	0	0	0	0	0	0 1	0	0	6
8:30 AM 8:45 AM	0	0	0	0	0	1	0	0	0	0	0	0	2	0	0	0	3
8:45 AM	U	U	U	U	U	1	U	U	U	U	U	U	2	U	U	U	3
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT
TOTAL VOLUMES :	1	1	1	0	1	14	1	0	0	0	3	0	4	4	0	0	30
APPROACH %'s:	33.33%	33.33% 07:30 AM -	33.33%	0.00%	6.25%	87.50%	6.25%	0.00%	0.00%	0.00%	100.00%	0.00%	50.00%	50.00%	0.00%	0.00%	TOT
PEAK HR :				0		•	0	0		0		•			0	0	
PEAK HR VOL :	0 0.000	0.000	0.000	0.000	0 0.000	9 0.375	0.000	0.000	0.000	0.000	0.000	0.000	0 0.000	1 0.250	0.000	0.000	10
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.373		0.000	0.000	0.000	0.000	0.000	0.000	0.230		0.000	0.4
		NORTH	OUIND			SOUTHE	OLIND			EACTE	BOUND			WECT	BOUND		
PM	0	2	0	0	0	2	0	0	0	1	0	0	0	1	0	0	
T IVI	NL	NT	NR	NU	SL	ST	SR	SU	EL	ĒΤ	ER	EU	WL	WT	WR	WU	тот
4:00 PM	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
4:15 PM	Ö	ō	Ö	ő	Ö	1	0	0	0	Ô	1	ő	Ö	1	1	Ö	4
4:30 PM	ŏ	ŏ	Ŏ	ŏ	ŏ	Ō	Ŏ	ŏ	ŏ	ŏ	î	ő	ŏ	ō	ī	ŏ	2
4:45 PM	Ō	Ō	Ō	0	Ō	Ō	Ō	0	Ō	Ō	Ō	0	Ō	Ō	Ō	Ō	0
5:00 PM	0	0	0	0	0	1	0	0	0	0	0	0	0	1	0	0	2
5:15 PM	Ó	0	0	0	Ö	2	0	0	0	0	0	0	0	0	Ö	0	2
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
6:00 PM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	1
6:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
6:45 PM	0	0	0	0	0	1	0	0	0	0	0	0	1	0	0	0	2
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT
TOTAL VOLUMES :	0	1	0	0	0	6	0	0	0	0	2	0	1	4	2	0	16
APPROACH %'s:	0.00%	100.00%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%	0.00%	0.00%	100.00%	0.00%	14.29%	57.14%	28.57%	0.00%	l

0 0.000

0 0.000

0 0.000

0 0.000

0 0.000

3 0 0.375 0.000 0.375

0 0.000 0.000

TOTAL 4

0.500

0 0.000

0 0.000

1 0 0.250 0.000 0.250

Location: Branch Dr & Warrenton Village Center Dwy/Shopping Center Dwy City: Warrenton Control: 2-Way Stop(EB/WB)

Project ID: 23-260020-004 Date: 2/9/2023

Control: 2																	
_								Data -	Bikes								_
NS/EW Streets:		Bran	ch Dr			Branc	h Dr		Warrentor	n Village Ce		hopping	Warrento	n Village Co		Shopping	
		NODTI	HBOUND			SOUTH	DOLIND		Center Dwy EASTBOUND				Center Dwy WESTBOUND				
AM	0	2	0	0	0	2	0	0	0	1 1	0000	0	0	1	0	0	
AIVI	NL	NT	NR	NU	SL	ST	SR	SU	EL	ĒŤ	ER	EU	WL	WT	WR	WU	TOTA
6:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	Ō	0
6:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	U	U	U	U	U	U	U	U	U	U	U	U	U	U	U	U	u
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TO
OTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	(
																	TO
PEAK HR :		07:30 AM	- 08:30 AM														
	0	07:30 AM	- 08:30 AM 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR:	0 0.000				0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	
PEAK HR : PEAK HR VOL :		0	0	0													
PEAK HR : PEAK HR VOL : EAK HR FACTOR :		0.000	0.000	0		0.000	0.000			0.000	0.000			0.000	0.000		
PEAK HR : PEAK HR VOL : EAK HR FACTOR :	0.000	0 0.000 NORTH	0	0 0.000	0.000	0.000 SOUTH	0.000	0.000	0.000		0.000 OUND		0.000	0.000 WEST		0.000	
PEAK HR : PEAK HR VOL :		0.000	0 0.000 HBOUND	0		0.000	0.000 BOUND			0.000 EASTB	0.000	0.000		0.000	0.000 BOUND		O
PEAK HR : PEAK HR VOL : EAK HR FACTOR : PM 4:00 PM	0.000	0 0.000 NORTH	0 0.000 HBOUND 0	0 0.000	0.000	0.000 SOUTH 2	0.000 BOUND 0	0.000	0.000	0.000 EASTB	0.000 OUND 0	0.000	0.000	0.000 WEST 1	0.000 BOUND 0	0.000	ТО
PEAK HR : PEAK HR VOL : EAK HR FACTOR : PIM 4:00 PM 4:15 PM	0.000 0 NL 0 0	0 0.000 NORTH 2 NT 0 0	0 0.000 HBOUND 0 NR 0 0	0 0.000	0.000 0 SL 0 0	0.000 SOUTH 2 ST 0 0	0.000 BOUND 0 SR 0 0	0.000 0 SU 0 0	0.000 0 EL 0 0	0.000 EASTE 1 ET 0 0	0.000 OUND 0 ER 0 0	0.000 0 EU 0 0	0.000 0 WL 0 0	0.000 WEST 1 WT 0	0.000 BOUND 0 WR 0	0.000 0 WU 0	TO
PEAK HR : PEAK HR VOL : EAK HR FACTOR : PIVI 4:00 PM 4:15 PM 4:30 PM	0.000 0 NL 0 0 0	0 0.000 NORTH 2 NT 0 0	0 0.000 HBOUND 0 NR 0 0	0 0.000	0.000 0 SL 0 0 0	0.000 SOUTH 2 ST 0 0 0	0.000 BOUND 0 SR 0 0 0	0.000 0 SU 0 0	0.000 0 EL 0 0	0.000 EASTE 1 ET 0 0 0	0.000 OUND 0 ER 0 0	0.000 0 EU 0 0	0.000 0 WL 0 0	0.000 WEST 1 WT 0 0 0	0.000 BOUND 0 WR 0 0 0	0.000 0 WU 0 0	TO
PEAK HR : PEAK HR VOL : EAK HR FACTOR : PM 4:00 PM 4:15 PM 4:30 PM 4:35 PM 4:45 PM	0.000 0 NL 0 0 0 0	0 0.000 NORTH 2 NT 0 0 0	0 0.000 HBOUND 0 NR 0 0 0	0 0.000	0.000 0 SL 0 0 0 0	0.000 SOUTH 2 ST 0 0 0	0.000 BOUND 0 SR 0 0 0	0.000 SU 0 0 0	0.000 0 EL 0 0 0	0.000 EASTE 1 ET 0 0 0	0.000 OUND 0 ER 0 0 0	0.000 0 EU 0 0 0	0.000 0 WL 0 0 0 0	0.000 WEST 1 WT 0 0 0 0	0.000 BOUND 0 WR 0 0 0	0.000 WU 0 0 0	TO
PEAK HR : PEAK HR VOL : EAK HR FACTOR : PIM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	0.000 0 NL 0 0 0 0	0 0.000 NORTH 2 NT 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0 0.000	0.000 SL 0 0 0 0	0.000 SOUTH 2 ST 0 0 0	0.000 BOUND 0 SR 0 0 0 0	0.000 0 SU 0 0 0 0	0.000 0 EL 0 0 0	0.000 EASTE 1 ET 0 0 0 0 0	0.000 OUND 0 ER 0 0 0	0.000 EU 0 0 0 0	0.000 WL 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0	0.000 WU 0 0 0 0	TO 0
PEAK HR : PEAK HR VOL : EAK HR FACTOR : PIVI 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	0.000 NL 0 0 0 0 0	0 0.000 NORTH 2 NT 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0 0.000	0.000 0 SL 0 0 0 0 0	0.000 SOUTH 2 ST 0 0 0 0	0.000 BOUND 0 SR 0 0 0 0 0	0.000 SU 0 0 0 0 0	0.000 0 EL 0 0 0 0	0.000 EASTE 1 ET 0 0 0 0 0 0	0.000 OUND 0 ER 0 0 0 0	0.000 EU 0 0 0 0 0	0.000 0 WL 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0	0.000 0 WU 0 0 0 0 0	TO () () () () () () () () () () () () ()
PEAK HR: PEAK HR VOL: EAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	0.000 NL 0 0 0 0 0 0	0 0.000 NORTH 2 NT 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0 0.000	0.000 0 SL 0 0 0 0 0	0.000 SOUTH 2 ST 0 0 0 0 0	0.000 BOUND 0 SR 0 0 0	0.000 SU 0 0 0 0 0	0.000 0 EL 0 0 0 0 0	0.000 EASTE 1 ET 0 0 0 0 0 0 0 0	0.000 OUND 0 ER 0 0 0 0 0	0.000 0 EU 0 0 0 0 0	0.000 WL 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0	TO 0
PEAK HR : PEAK HR VOL : EAK HR FACTOR : PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:34 PM	0.000 NL 0 0 0 0 0	0 0.000 NORTH 2 NT 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0 0.000	0.000 SL 0 0 0 0 0 0	0.000 SOUTH 2 ST 0 0 0 0 0 0	0.000 BOUND 0 SR 0 0 0 0 0 1	0.000 SU	0.000 0 EL 0 0 0 0 0 0	0.000 EASTE 1 ET 0 0 0 0 0 0	0.000 OUND 0 ER 0 0 0 0	0.000 EU 0 0 0 0 0 0	0.000 0 WL 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0	TO' 0
PEAK HR: PEAK HR VOL: EAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:30 PM	0.000 0 NL 0 0 0 0 0 0	0 0.000 NORTH 2 NT 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0 0.000	0.000 0 SL 0 0 0 0 0	0.000 SOUTH 2 ST 0 0 0 0 0	0.000 BOUND 0 SR 0 0 0 0 0	0.000 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 EL 0 0 0 0 0	0.000 EASTE 1 ET 0 0 0 0 0 0 0 0 0 0 0 0	0.000 OUND O ER O O O O O O O O O O O O O	0.000 0 EU 0 0 0 0 0	0.000 WL 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0	TO' 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR : PEAK HR VOL : EAK HR FACTOR : 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:15 PM 6:00 PM 6:15 PM 6:00 PM	0.000 NL 0 0 0 0 0 0 0	0 0.000 NORTH 2 NT 0 0 0 0 0 0	0 0.0000 HBOUND 0 NR 0 0 0 0 0	0 0.000	0.000 SL 0 0 0 0 0 0 0	0.000 SOUTH 2 ST 0 0 0 0 0 0 0	0.000 BOUND 0 SR 0 0 0 0 0 1 0	0.000 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 EL 0 0 0 0 0 0 1 0 0	0.000 EASTE 1 ET 0 0 0 0 0 0 0 0 0 0	0.000 OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 EU 0 0 0 0 0 0 0	0.000 WL 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0 0	TO 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR: PEAK HR VOL: EAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:30 PM	0.000 NL 0 0 0 0 0 0 0 0	0 0.000 NORTH 2 NT 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0 0	0 0.000	0.000 SL 0 0 0 0 0 0 0 0	0.000 SOUTH 2 ST 0 0 0 0 0 0 0	0.000 BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 EL 0 0 0 0 0 0 1	0.000 EASTE 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 OUND 0 ER 0 0 0 0 0 0 0 0 0 0	0.000 EU 0 0 0 0 0 0 0	0.000 WL 0 0 0 0 0 0 0	0.000 WEST 1 VT 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0	TO: 00 00 00 00 00 00 00 00 00 00 00 00 00
PEAK HR : PEAK HR VOL : EAK HR FACTOR : PIM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:10 PM 5:15 PM 5:45 PM 6:00 PM 6:15 PM 6:00 PM 6:15 PM 6:30 PM	0.000 NL 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.000	0 0.0000 HBOUND 0 NR 0 0 0 0 0 0 0 0	0 0.000	0.000 0 SL 0 0 0 0 0 0 0 0 0 0	SOUTH 2 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 SR 0 0 0 0 0 1 0 0 1 0 0	0.000 0	0.000 0 EL 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 EASTE 1 O 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 EU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WL 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WU 0 0 0 0 0 0 0 0 0	TOT 00 00 00 00 00 00 00 00 00 00 00 00 00
PEAK HR: PEAK HR VOL: EAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:30 PM 5:15 PM 6:00 PM 6:15 PM 6:30 PM 6:30 PM 6:45 PM	0.000 NL 0 0 0 0 0 0 0 0 0	0 0.000 NORTI 2 NT 0 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0 0	0 0.000	0.000 SL 0 0 0 0 0 0 0 0 0 0 0 0 0 SL	0.000 SOUTH 2 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 SR 0 0 0 0 1 0 1 0 SR	0.000 0	0.000 0 EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 EASTE 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 OUND O ER O O O O O O O O O O O O O O O O O O O	0.000 EU 0 0 0 0 0 0 0 0 0	0.000 WL 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 WR	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TO C C C C C C C C C C C C C C C C C C C
PEAK HR: PEAK HR VOL: EAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:30 PM 5:30 PM 6:15 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	0.000 NL 0 0 0 0 0 0 0 0 0 0 0 0 NL NL	0 0.0000 NORTH 2 NT 0 0 0 0 0 0 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.000	0.000 0 SL 0 0 0 0 0 0 0 0 0 0	0.000 SOUTH 2 ST 0 0 0 0 0 0 0 0 ST 0	0.000 BOUND 0 SR 0 0 0 0 0 0 1 0 SR 5 SR 2	0.000 O	0.000 0 EL 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 EASTE 1 0 0 0 0 0 0 0 0 ET 0	0.000 OUND OR ER OR OR OR OR OR OR OR OR	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 WT	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0	TO C C C C C C C C C C C C C C C C C C C
PEAK HR: PEAK HR VOL: EAK HR FACTOR: 4:00 PM 4:15 PM 4:15 PM 4:30 PM 5:15 PM 5:00 PM 5:15 PM 6:00 PM 6:30 PM 6:30 PM 6:35 PM 6:35 PM	0.000 0 NL 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.0000 NORTI 2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.000	0.000 SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SOUTH 2 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 SR 0 0 0 0 0 1 0 0 5 1 0 0 5 8 2 100.00%	0.000 SU	0.000 EL 0 0 0 0 0 0 0 0 0 0 1 1 0 0 0 1 1 100.00%	0.000 EASTE 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR: PEAK HR VOL: EAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:30 PM 6:30 PM 6:30 PM	0.000 NL 0 0 0 0 0 0 0 0 0 0 0 0 NL NL	0 0.0000 NORTH 2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.000	0.000 SL 0 0 0 0 0 0 0 0 0 0 SL 0 0 SL 0 0 0 0	0.000 SOUTH 2 ST 0 0 0 0 0 0 0 0 ST 0	0.000 BOUND 0 SR 0 0 0 0 0 0 1 0 SR 5 SR 2	0.000 O	0.000 0 EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 EASTE 1 0 0 0 0 0 0 0 0 ET 0	0.000 OUND OER O O O O O O O O O O O O O	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 WT	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 WR	0.000 0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0	

National Data & Surveying Services Intersection Turning

Location: Branch Dr & Warrenton Village Center Dwy/Shopping Center Dwy

Project ID: 23-260020-004

City: Warrenton

Date: 2/9/2023

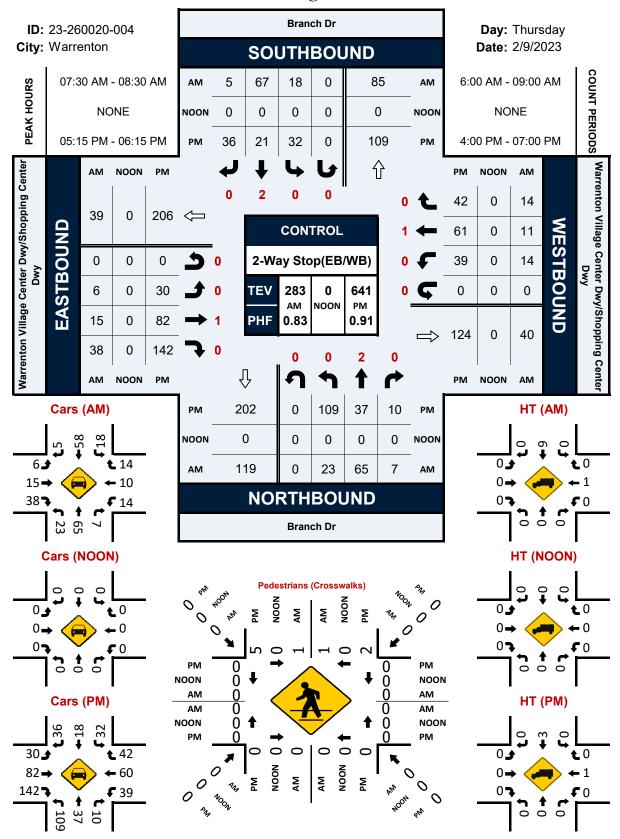
Data - Pedestrians (Crosswalks)

NC /EW/ Chrooker	Branch Dr		Pron	ich Dr	Warrenton V	'illage Center	Warrenton V	/illage Center	
NS/EW Streets:	Didil	CIT DI	Didi	ICH DI	Dwy/Shop	oing Center	Dwy/Shopp	ping Center	
AM	NORT	H LEG	SOUT	TH LEG	EAST	Γ LEG	WES		
Alvi	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
6:00 AM	0	2	0	0	0	0	0	0	2
6:15 AM	0	0	0	0	0	0	0	0	0
6:30 AM	1	0	0	0	0	0	0	0	1
6:45 AM	0	0	0	0	0	0	0	0	0
7:00 AM	0	0	0	0	0	0	0	0	0
7:15 AM	1	0	0	0	0	0	0	0	1
7:30 AM		0	0	0	0	0	0	0	0
7:45 AM		0	0	0	0	0	0	0	1
8:00 AM	0	0	0	0	0	0	0	0	0
8:15 AM		1	0	0	0	0	0	0	1
8:30 AM	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	3	3	0	0	0	0	0	0	6
APPROACH %'s:	50.00%	50.00%							
PEAK HR:	07:30 AM	- 08:30 AM							TOTAL
PEAK HR VOL:	1	1	0	0	0	0	0	0	2
PEAK HR FACTOR :	0.250	0.250							0.500
	0.5	500							0.500

DNA	NORT	NORTH LEG		'H LEG	EAST	LEG	WEST	Γ LEG	
PM	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	5	0	0	0	0	0	0	5
4:15 PM	1	2	0	0	1	0	0	0	4
4:30 PM	1	2	0	0	0	0	0	0	3
4:45 PM	3	0	0	0	0	1	0	0	4
5:00 PM	0	0	0	0	0	0	0	0	0
5:15 PM	2	1	0	0	0	0	0	0	3
5:30 PM	1	0	0	0	0	0	0	0	1
5:45 PM	0	0	0	0	0	0	0	0	0
6:00 PM	2	1	0	0	0	0	0	0	3
6:15 PM	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	0
6:45 PM	0	2	0	0	0	0	0	0	2
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	10	13	0	0	1	1	0	0	25
APPROACH %'s:	43.48%	56.52%			50.00%	50.00%			
PEAK HR:	05:15 PM ·	· 06:15 PM							TOTAL
PEAK HR VOL:	5	2	0	0	0	0	0	0	7
PEAK HR FACTOR:	0.625	0.500							0.583
	0.5	83							0.363

Branch Dr & Warrenton Village Center Dwy/Shopping Center Dwy

Peak Hour Turning Movement Count



Location: Branch Dr & Oak Springs Dr City: Warrenton Control: 2-Way Stop(NB/SB)

	Warrenton	& Oak Spring	ys Di					Data -	Total				Pr		23-260020- 2/9/2023	005	•
NS/EW Streets:		Brancl	h Dr			Branc	h Dr			Oak Spri	ngs Dr			Oak Spri	ings Dr		
0.04		NORTH		_		SOUTH		_		EASTB		_			BOUND	_	
AM	0 NL	2 NT	0 NR	0 NU	0 SL	1 ST	0 SR	0 SU	0 EL	1 ET	0 ER	0 EU	0 WL	1 WT	0 WR	0 WU	TOTA
6:00 AM	2	0	0	0	0	0	0	0	0	3	6	0	1	0	0	0	12
6:15 AM	0	0	1	0	0	0	0	0	0	2	3	0	0	4	0	0	10
6:30 AM	3	0	0	0	0	1	0	0	0	3	4	0	0	6	0	0	17
6:45 AM	2	0	0	0	0	0	0	0	1	3	9	0	2	6	1	0	24
7:00 AM	6	0	0	0	1	0	0	0	0	5	6	0	3	12	0	0	33
7:15 AM	12	0	1	0	0	2	0	0	0	15	9	0	4	10	0	0	53
7:30 AM	17	0	2	0	0	1	0	0	0	15	7	0	5	18	0	0	65
7:45 AM	31	0	4	0	0	0	0	0	0	20	23	0	4	49	0	0	132 75
8:00 AM 8:15 AM	14 11	0	3	0	0	0	0	0	0	14 27	21 24	0	1 4	22 17	0	0	75 86
8:30 AM	9	0	2	0	0	0	1	0	0	17	18	0	7	19	0	0	73
8:45 AM	7	0	3	0	0	2	1	0	1	26	15	0	3	19	0	0	77
								_									
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTA
TOTAL VOLUMES :	114	0	19	0	1	6	3	0	2	150	145	0	34	182	1	0	657
APPROACH %'s:	85.71%		14.29%	0.00%	10.00%	60.00%	30.00%	0.00%	0.67%	50.51%	48.82%	0.00%	15.67%	83.87%	0.46%	0.00%	TOTA
PEAK HR : PEAK HR VOL :	65	07:45 AM -	08:45 AM 12	0	0	0	2	0	0	78	86	0	16	107	0	0	366
PEAK HR VOL :	0.524	0.000	0.750	0.000	0.000	0.000	0.500	0.000	0.000	0.722	0.896	0.000	0.571	0.546	0.000	0.000	
PEAKTIK PACTOK.	0.521	0.55		0.000	0.000	0.50		0.000	0.000	0.8		0.000	0.571	0.5		0.000	0.693
		NORTH	DOLIND			SOUTH	DOLIND			EASTB	OLIND			WECT	BOUND		
PM	0	2	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
FIVI	NL	NT	NR	NU	SL	ST	SR	SU	ĔĹ	ĒŤ	ER	EU	WL	WT	WR	WU	TOTA
4:00 PM	15	0	4	0	1	1	0	0	1	34	21	0	9	25	1	0	112
4:15 PM	13	2	10	1	Ō	2	Ö	Ö	2	21	20	0	6	25	i	Ö	103
4:30 PM	19	Ō	11	Ō	ō	1	Ö	ō	Ō	30	26	Ö	5	33	ō	Ō	125
4:45 PM	14	0	12	0	0	1	0	0	0	20	19	0	8	29	0	0	103
5:00 PM	18	1	4	0	0	1	0	0	1	22	20	0	12	27	0	0	106
5:15 PM	19	1	6	0	0	3	0	0	1	12	21	0	6	29	0	0	98
5:30 PM	26	1	8	0	1	0	0	0	0	23	12	0	4	26	1	0	102
5:45 PM	12	1	6	0	0	0	0	0	0	20	15	0	8 8	20	2	0	84
6:00 PM	22 18	2 1	6 10	0	0	0	0	0	0	15 16	13	0	8 5	14	1	0	81
6:15 PM 6:30 PM	18 10	3	10 4	0	1	2	0 1	0	1	16 15	10 7	0	5 7	5 9	0	0	67 59
6:45 PM	13	0	6	0	0	0	0	0	0	12	5	0	8	3	1	0	48
35 111					-		-	_									
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTA
TOTAL VOLUMES : APPROACH %'s :	199 66,56%	12 4.01%	87 29.10%	1 0.33%	3 20.00%	11 73.33%	1 6.67%	0 0.00%	6 1.38%	240 55.17%	189 43.45%	0 0.00%	86 25.37%	245 72.27%	8 2.36%	0 0.00%	108
PEAK HR:	00.3070	04:00 PM -		0.3370	20.0070	7 3.33 70	0.0770	0.0070	1.30 70	33.1770	13.7370	0.0070	23.37 70	12.2170	2.3070	0.0070	TOTA
PEAK HR VOL :	61	2	37	1	1	5	0	0	3	105	86	0	28	112	2	0	443
PEAK HR FACTOR :	0.803	0.250	0.771	0.250	0.250	0.625	0.000	0.000	0.375	0.772	0.827	0.000	0.778	0.848	0.500	0.000	0.88

Location: Branch Dr & Oak Springs Dr City: Warrenton Control: 2-Way Stop(NB/SB)

Project ID: 23-260020-005 **Date:** 2/9/2023 Data - Cars Branch Dr Branch Dr Oak Springs Dr NS/EW Streets Oak Springs Dr NORTHBOUND SOUTHBOUND EASTBOUND WESTBOUND AM TOTAL 12 9 16 22 30 51 65 131 71 80 71 76 WU 6:00 AM 6:15 AM 0 3 2 6 12 17 31 14 11 9 7 6:15 AM 6:30 AM 6:45 AM 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 6 12 10 18 48 22 17 19 15 15 20 13 27 16 26 23 19 18 18 14 8:15 AM 8:30 AM 8:45 AM SU 0 0.00% WL 30 14.15% TOTAL VOLUMES APPROACH %'s PEAK HR PEAK HR VOL 114 0.00% 1 10.00% 6 60.00% 30.00% 145 51.79% 0.009 181 85.38% 634 TOTAL 0.500 0.500 106 U 0.552 0.000 0.577 76 78 0.704 0.848 0.856 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 14 0.583 0 0.000 353 0.524 0.000 0.750 0.000 PEAK HR FACTOR 0.674 FASTROLIND NORTHBOLIND SOLITHBOLIND WESTROLIND PM 0 NL 14 13 18 14 18 19 26 12 22 18 10 13 TOTAL 111 100 123 101 104 96 102 84 80 67 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 34 20 29 19 22 12 23 20 15 16 15 12 25 33 28 26 29 26 20 14 20 26 19 20 20 5:30 PM 5:45 PM 6:00 PM 6:15 PM 10 0 0 0 0 0 0 10 6:30 PM 6:45 PM 3 0 0 0 7 5 59 47 0 ō ET 237 54.99% WL 81 24.40% TOTAL VOLUMES 1 0.34% 0 243 73.19% 12 4.05% 86 11 73.33% 188 8 2.41% 1074 APPROACH %'s PEAK HR PEAK HR VOL TOTAL 27 0.750 36 0.750 86 0.827 0 0.000 435 2 0.250 1 0.250 PEAK HR FACTOR 0.250 0.625 0.000 0.000 0.375 0.750 0.841 0.500 0.000

0.884

${\tt National\ Data\ \&\ Surveying\ Services} \\ Intersection\ Turning\ Movement\ Count$

Location: Branch Dr & Oak Springs Dr City: Warrenton Control: 2-Way Stop(NB/SB)

Project ID: 23-260020-005 Date: 2/9/2023

Control:	2-way Stop	(NB/SB)												Date:	2/9/2023		
_								Data	- HT								_
NS/EW Streets:		Brand	th Dr			Bran	ch Dr			Oak Spri	ings Dr			Oak Spri	ngs Dr		1
		NORTH	IBOUND			SOUTI	HBOUND			EASTE	BOUND			WESTE	BOUND		
AM	0	2	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
7	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 AM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	1
6:30 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
6:45 AM	0	0	0	0	0	0	0	0	0	0	1	0	1	0	0	0	2
7:00 AM	0	0	0	0	0	0	0	0	0	2	1	0	0	0	0	0	3
7:15 AM	0	0	0	0	0	0	0	0	0	0	1	0	1	0	0	0	2
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
8:00 AM	0	0	0	0	0	0	0	0	0	1	2	0	1	0	0	0	4
8:15 AM	0	0	0	0	0	0	0	0	0	0	6	0	0	0	0	0	6
8:30 AM	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	2
8:45 AM	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	1
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	0	1	0	0	0	0	0	0	5	12	0	4	1	0	0	23
APPROACH %'s:	0.00%	0.00%		0.00%					0.00%	29.41%	70.59%	0.00%	80.00%	20.00%	0.00%	0.00%	
PEAK HR :		07:45 AM ·															TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	2	8	0	2	1	0	0	13
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.500	0.333	0.000	0.500	0.250	0.000	0.000	0.542
										0.4	17			0.7	50		0.512
DAA			IBOUND		_	SOUTI	HBOUND			EASTE	BOUND			WESTE			
PM	0	2	0	0	0	1	0	0	0	1	0	0	0	1	0	0	TOTAL
4.00.014	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
4:15 PM	0	Ú	1	0	0	0	0	0	0	1	Ü	Ü	1	Ü	0	0	3
4:30 PM	1	0	U	0	U	0	0	0	0	1	U	U	U	U	0	0	2
4:45 PM	0	0	0	0	0	0	0	0	0	<u>i</u>	0	0	0	<u></u>	0	0	2

		NONTH	DOUND			30011	IDOUIND			LASIL	JOUIND			WLJIL	JOUIND		
PM	0	2	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
4:15 PM	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	3
4:30 PM	1	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	2
4:45 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	0	2
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	1	1	0	0	2
5:15 PM	0	0	0	0	0	0	0	0	0	0	1	0	1	0	0	0	2
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1
6:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	2	0	1	0	0	0	0	0	0	3	1	0	5	2	0	0	14
APPROACH %'s:	66.67%	0.00%	33.33%	0.00%					0.00%	75.00%	25.00%	0.00%	71.43%	28.57%	0.00%	0.00%	
PEAK HR :	(04:00 PM -	05:00 PM														TOTAL
PEAK HR VOL:	2	0	1	0	0	0	0	0	0	3	0	0	1	1	0	0	8
PEAK HR FACTOR:	0.500	0.000	0.250	0.000	0.000	0.000	0.000	0.000	0.000	0.750	0.000	0.000	0.250	0.250	0.000	0.000	0.667
		0.7	50							0.7	50			0.5	00		0.007

Location: Branch Dr & Oak Springs Dr City: Warrenton Control: 2-Way Stop(NB/SB)

Data - Bikes

Project ID: 23-260020-005 Date: 2/9/2023

_								Data	Bikes								_
NS/EW Streets:		Branc	h Dr			Branc	h Dr			Oak Sp	rings Dr			Oak Sp	rings Dr		
		NORTH	BOUND			SOUTH	BOUND			EAST	BOUND			WEST	BOUND		
AM	0 NL	2 NT	0 NR	0 NU	0 SL	1 ST	0 SR	0 SU	0 EL	1 ET	0 ER	<mark>0</mark> EU	0 WL	1 WT	0 WR	0 WU	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM 8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0. 15 Al-1	٠	•	٠	·	·	•	٠	·	·	·	•	•	·	·	·	·	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR:		07:45 AM -	00:4E AM														TOTAL
PEAK HR VOL :	0	07.43 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0
· zak int i Aciok i	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
			IBOUND			SOUTH					BOUND				BOUND		
PM	0	2	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	2 NT	0 NR	NU	SL	1 ST	0 SR	SU	EL	1 ET	0 ER	EU	WL	1 WT	0 WR	WU	TOTAL
4:00 PM	NL 0	NT 0	0 NR 0	NU 0	SL 0	ST 0	O SR O	SU 0	EL 0	1 ET 0	0 ER 0	EU 0	WL 0	WT 0	0 WR 0	WU 0	0
4:00 PM 4:15 PM	NL 0 0	2 NT 0 0	0 NR 0 0	NU 0 0	SL 0 0	1 ST 0 0	0 SR 0 0	SU 0 0	0 0	1 ET 0 0	0 ER 0 0	0 0	0 0	1 WT 0 0	0 WR 0 0	0 0	0
4:00 PM 4:15 PM 4:30 PM	0 0 0	2 NT 0 0 0	0 NR 0 0	0 0 0	SL 0 0 0	1 ST 0 0 0	0 SR 0 0	SU 0 0 0	0 0 0	1 ET 0 0 0	0 ER 0 0	0 0 0	0 0 0	1 WT 0 0 0	0 WR 0 0	0 0 0	0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM	0 0 0 0	2 NT 0 0 0 0	0 NR 0 0 0	NU 0 0 0 0	SL 0 0 0 0	1 ST 0 0 0	0 SR 0 0 0	SU 0 0 0 0	EL 0 0 0 0	1 ET 0 0 0 0	0 ER 0 0 0	0 0 0 0	WL 0 0 0 0	1 WT 0 0 0 0	0 WR 0 0 0	0 0 0 0	0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	NL 0 0 0 0	2 NT 0 0 0 0	0 NR 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0	1 ST 0 0 0 0	0 SR 0 0	SU 0 0 0 0 0 0 0 0	EL 0 0 0 0 0	1 ET 0 0 0 0	0 ER 0 0 0 0	0 0 0	WL 0 0 0 0	1 WT 0 0 0	0 WR 0 0 0 0	0 0 0 0 0	0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 0 0 0 0 0	2 NT 0 0 0 0 0	0 NR 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0	1 ST 0 0 0	0 SR 0 0 0 0	SU 0 0 0 0 0	EL 0 0 0 0	1 ET 0 0 0 0	0 ER 0 0 0	0 0 0 0 0	WL 0 0 0 0	1 WT 0 0 0 0	0 WR 0 0 0	WU 0 0 0 0 0	0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	NL 0 0 0 0	2 NT 0 0 0 0	0 NR 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0	1 ST 0 0 0 0 0	0 SR 0 0 0 0 0	SU 0 0 0 0 0 0 0 0	EL 0 0 0 0 0	1 ET 0 0 0 0 0	0 ER 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0	1 WT 0 0 0 0 0	0 WR 0 0 0 0 0	0 0 0 0 0	0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 0 0 0 0 0 0	2 NT 0 0 0 0 0 0	0 NR 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0	1 ST 0 0 0 0 0 0	0 SR 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0	1 ET 0 0 0 0 0 0	0 ER 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0	0 WR 0 0 0 0 0	WU 0 0 0 0 0	0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0	0 SR 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM	NL 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 1	0 SR 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 2 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM	NL 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 2
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM	NL 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 2 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 2 0 0 1 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	NL 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 2 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 2 0 0 1 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 2 0 0 0 1 0 0 TOTAL
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 2 0 0 1 0 TOTAL 3
4:00 PM 4:15 PM 4:35 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:15 PM 6:30 PM 6:45 PM TOTAL VOLUMES : APPROACH %'s : PEAK MR :	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 1 1 0 0 0 1 1 0 0 ST 2 100.00%	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 2 0 0 1 0 TOTAL 3

National Data & Surveying Services Intersection Turning

Location: Branch Dr & Oak Springs Dr Project ID: 23-260020-005
City: Warrenton

Date: 2/9/2023

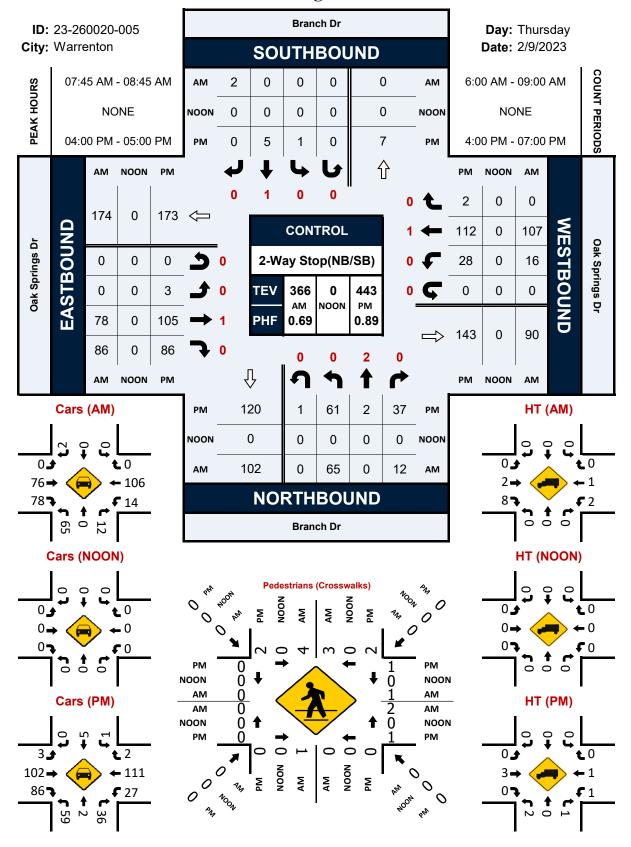
Data - Pedestrians (Crosswalks)

NS/EW Streets:	Bran	ch Dr	Branc	h Dr	Oak Spi	rings Dr	Oak Sp	orings Dr	
AM	NORT EB	H LEG WB	SOUTI EB	H LEG WB	EAST NB	LEG SB	WES NB	T LEG SB	TOTAL
6:00 AM 6:15 AM 6:30 AM 6:45 AM 7:00 AM 7:15 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM	0 1 0 0 0 1 0 0 1 1 2	0 0 0 1 0 0 1 0 1 0 2	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 1 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 1 0 0 0 0 0	0 1 0 3 0 1 1 1 0 2 4 5
TOTAL VOLUMES: APPROACH %'s: PEAK HR: PEAK HR VOL: PEAK HR FACTOR:	4 0.500	WB 5 45.45% - 08:45 AM 3 0.375 438	EB 1 100.00% 1 0.250	WB 0 0.00%	NB 3 75.00% 2 0.500 0.3	SB 1 25.00% 1 0.250	NB 0 0.00%	SB 1 100.00%	TOTAL 17 TOTAL 11 0.550

DNA	NORT	H LEG	SOUT	H LEG	EAST	LEG	WEST	Γ LEG	
PM	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	2	0	0	0	0	0	0	0	2
4:15 PM	0	0	0	0	1	0	0	0	1
4:30 PM	0	1	0	0	0	1	0	0	2
4:45 PM	0	1	0	0	0	0	0	0	1
5:00 PM	0	1	0	0	0	0	0	0	1
5:15 PM	0	1	0	0	1	0	0	0	2
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	1	0	1	0	0	2
6:00 PM	3	2	0	0	1	0	0	0	6
6:15 PM	1	0	0	0	0	1	0	0	2
6:30 PM	0	1	0	0	0	0	0	0	1
6:45 PM	0	0	1	0	0	1	0	0	2
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	6	7	1	1	3	4	0	0	22
APPROACH %'s:	46.15%	53.85%	50.00%	50.00%	42.86%	57.14%			
PEAK HR :	04:00 PM ·	- 05:00 PM							TOTAL
PEAK HR VOL :	2	2	0	0	1	1	0	0	6
PEAK HR FACTOR :	0.250	0.500			0.250	0.250			0.750
	0.5	500			0.5	500			0.750

Branch Dr & Oak Springs Dr

Peak Hour Turning Movement Count



Location: Hastings Ln & Oak Springs Dr City: Warrenton Control: 1-Way Stop(SB)

Project ID: 23-260020-006 **Date:** 2/9/2023

_								Data -	Total								
NS/EW Streets:		Hastin	ıgs Ln			Hasting	gs Ln			Oak Spri	ings Dr			Oak Spri	ngs Dr		Ī
		NORTH	IBOUND			SOUTH	BOUND			EASTE	OUND			WESTE	OUND		
AM	0	0	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
6:00 AM	0	0	0	0	4	0	0	0	1	5	0	0	0	1	1	0	12
6:15 AM	0	0	0	0	3	0	3	0	1	2	0	0	0	4	0	0	13
6:30 AM	0	0	0	0	2	0	5	0	3	5	0	0	0	6	3	0	24
6:45 AM	0	0	0	0	4	0	8	0	6	9	0	0	0	7	1	0	35
7:00 AM	0	0	0	0	5	0	5	0	7	7	0	0	0	14	4	0	42
7:15 AM	0	0	0	0	5	0	16	0	11	18	0	0	0	16	6	0	72
7:30 AM	0	0	0	0	2	0	13	0	17	20	0	0	0	24	10	0	86
7:45 AM	0	0	0	0	5	0	6	0	18	39	0	0	0	68	12	0	148
8:00 AM	0	0	0	0	14	0	20	0	24	20	0	0	0	27	10	0	115
8:15 AM	0	0	0	0	26	0	28	0	24	25	0	0	0	17	12	0	132
8:30 AM	0	0	0	0	16	0	20	0	8	19	0	0	0	21	7	0	91
8:45 AM	0	0	0	0	2	0	7	0	9	41	0	0	0	21	7	0	87
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	E)	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	0	0	0	88	0	131	0	129	210	0	0	0	226	73	0	857
APPROACH %'s:					40.18%	0.00%	59.82%	0.00%	38.05%	61.95%	0.00%	0.00%	0.00%	75.59%	24.41%	0.00%	
PEAK HR :		07:45 AM ·				_		_			_	_	_			_	TOTAL
PEAK HR VOL :	0	0	0	0	61	0	74	0	74	103	0	0	0	133	41	0	486
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.587	0.000	0.661 25	0.000	0.771	0.660	0.000 76	0.000	0.000	0.489	0.854 14	0.000	0.821

		NORT	HBOUND			SOUTH	BOUND			EASTE	BOUND			WESTE	OUND		
PM	0	0	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	24	0	12	0	7	32	0	0	0	39	1	0	115
4:15 PM	0	0	0	0	15	0	9	0	12	29	0	0	0	35	3	0	103
4:30 PM	0	0	0	0	21	0	14	0	12	36	0	0	0	46	6	0	135
4:45 PM	0	0	0	0	7	0	17	0	11	31	0	0	0	40	2	0	108
5:00 PM	0	0	0	0	13	0	2	0	16	30	0	0	0	43	3	0	107
5:15 PM	0	0	0	0	11	0	10	0	12	23	0	0	0	40	8	0	104
5:30 PM	0	0	0	0	2	0	11	0	14	32	0	0	0	43	8	0	110
5:45 PM	0	0	0	0	7	0	10	0	6	28	0	0	0	28	5	0	84
6:00 PM	0	0	0	0	15	0	6	0	8	14	0	0	0	31	5	0	79
6:15 PM	0	0	0	0	8	0	6	0	6	18	0	0	0	15	7	0	60
6:30 PM	0	0	0	0	5	0	4	0	4	18	0	0	0	16	5	0	52
6:45 PM	0	0	0	0	4	0	5	0	4	12	0	0	0	8	8	0	41
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	132 55.46%	0 0.00%	106 44.54%	0 0.00%	112 26.99%	303 73.01%	0 0.00%	0 0.00%	0 0.00%	384 86.29%	61 13.71%	0 0.00%	1098
PEAK HR:		04:00 PM	- 05:00 PM														TOTAL
PEAK HR VOL :	0	0	0	0	67	0	52	0	42	128	0	0	0	160	12	0	461
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.698	0.000	0.765 26	0.000	0.875	0.889	0.000 85	0.000	0.000	0.870	0.500 27	0.000	0.854

Location: Hastings Ln & Oak Springs Dr City: Warrenton Control: 1-Way Stop(SB)

City: \ Control: :	Warrenton 1-Way Sto							Data ·	· Cars				Pn		23-260020- 2/9/2023	006	
NS/EW Streets:		Hastir	ngs Ln			Hasting	ıs Ln		-	Oak Sprii	ngs Dr			Oak Spri	ings Dr		
		NORTI	HBOUND			SOUTH	OUND			EASTB	OUND			WESTE	BOUND		
AM	0 NL	0 NT	0 NR	0 NU	0 SL	1 ST	0 SR	0 SU	0 EL	1 ET	0 ER	0 EU	0 WL	1 WT	0 WR	0 WU	TOTA
6:00 AM	0	0	0	0	4	0	0	0	1	5	0	0	0	1	1	0	12
6:15 AM	0	0	0	0	3	0	3	0	1	2	0	0	0	4	0	0	13
6:30 AM	0	0	0	0	2	0	5	0	2	4	0	0	0	6	3	0	22
6:45 AM	0	0	0	0	3	0	8	0	5	9	0	0	0	7	1	0	33
7:00 AM	0	0	0	0	4	0	5	0	7	5	0	0	0	14	4	0	39
7:15 AM	0	0	0	0	5	0	16	0	11	17	0	0	0	16	6	0	71
7:30 AM	0	0	0	0	2 5	0	13 6	0	17 15	20 39	0	0	0	24 67	10 12	0	86 144
7:45 AM 8:00 AM	0	0	0	0	12	0	20	0	22	19	0	0	0	27	10	0	110
8:15 AM	0	0	0	0	20	0	28	0	24	25	0	0	0	17	12	0	126
8:30 AM	0	0	0	0	16	0	20	0	8	18	0	0	0	21	7	0	90
8:45 AM	0	ő	Ö	0	2	ő	7	Ö	9	40	ŏ	Ö	ő	21	7	Ö	86
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTA
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	78 37.32%	0 0.00%	131 62.68%	0 0.00%	122 37.54%	203 62.46%	0 0.00%	0 0.00%	0 0.00%	225 75.50%	73 24.50%	0 0.00%	832
PEAK HR :			- 08:45 AM														TOTA
PEAK HR VOL:	0	0	0	0	53	0	74	0	69	101	0	0	0	132	41	0	470
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.663	0.000	0.661 51	0.000	0.719	0.647	0.000 37	0.000	0.000	0.493 0.5	0.854 47	0.000	0.816
		NORTH	HBOUND			SOUTH	SOLIND			EASTB	OLIND			WEST	BOUND		
PM	0	0	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
1 171	NL	NT	NR	NU	SL	ST	SR	SU	ĔĹ	ĒŤ	ER	EU	WL	WT	WR	WU	TOTA
4:00 PM	0	0	0	0	24	0	12	0	7	32	0	0	0	38	1	0	114
4:15 PM	0	0	0	0	15	0	8	0	11	28	0	0	0	35	3	0	100
4:30 PM	0	0	0	0	21	0	14	0	12	35	0	0	0	45	6	0	133
4:45 PM	0	0	0	0	7	0	17	0	11	30	0	0	0	39	2	0	106
5:00 PM	0	0	0	0	12	0	2	0	15	30	0	0	0	42	3	0	104
5:15 PM	0	0	0	0	11	0	10	0	12	23	0	0	0	40	8	0	104
5:30 PM 5:45 PM	0	0	0	0	2 7	0	11	0	14 5	32 28	0	0	0	43 28	8 5	0	110 83
5:45 PM 6:00 PM	0	0	0	0	15	0	10 6	0	5 8	28 14	0	0	0	28 31	5 5	0	79
6:15 PM	0	0	0	0	8	0	6	0	6	18	0	0	0	15	7	0	60
	0	0	0	0	5	0	4	0	3	18	0	0	0	16	5	0	51
6:30 PM	ŏ	Ŏ	Ö	Ö	4	Ŏ	5	ŏ	4	12	Ŏ	ŏ	Ŏ	8	8	ŏ	41
6:30 PM 6:45 PM	U							SU	EL	ET	ER	EU	WL	WT	1116		TOTA
6:45 PM	NL	NT	NR	NU	SL	ST	SR								WR	WU	
	_	NT 0	NR 0	NU 0	SL 131 55.51%	ST 0 0.00%	SR 105 44.49%	0 0.00%	108 26.47%	300 73.53%	0	0 0.00%	0 0.00%	380 86.17%	61 13.83%	0 0.00%	108
6:45 PM	NL	0		0	131 55.51%	0.00%	105 44.49%	0 0.00%	108 26.47%	300 73.53%	0 0.00%	0.00%	0 0.00%	380 86.17%	61 13.83%	0 0.00%	108
6:45 PM TOTAL VOLUMES : APPROACH %'s :	NL	0	0		131	0	105	0	108	300	0	0	0	380	61	0	108 TOT/ 453

Location: Hastings Ln & Oak Springs Dr City: Warrenton Control: 1-Way Stop(SB)

Location: City: \ Control: :	Narrentor	n .	rings Dr					Data	- нт				Pr	oject ID: 1 Date: 1	23-260020- 2/9/2023	006	
NS/EW Streets:		Hastir	ngs Ln			Hasting	s Ln	Juli		Oak Sprir	ngs Dr			Oak Spri	ngs Dr		
		NORTI	HBOUND			SOUTHE	BOUND			EASTBO	OUND			WESTE	OUND		
AM	0 NL	0 NT	0 NR	0 NU	0 SL	1 ST	0 SR	0 SU	0 EL	1 ET	0 ER	0 EU	0 WL	1 WT	0 WR	0 WU	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	1	1	0	0	0	0	0	0	2
6:45 AM	0	0	0	0	1	0	0	0	1	0	0	0	0	0	0	0	2
7:00 AM	0	0	0	0	1	0	0	0	0	2	0	0	0	0	0	0	3
7:15 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0 2	0	0	0	3	0	0	0	0	1	0	0	4
8:00 AM 8:15 AM	0	0	0	0	6	0	0	0	0	0	0	0	0	0	0	0	5 6
8:30 AM	0	0	Ö	Ö	0	0	0	0	0	1	0	0	0	0	0	Ö	1
8:45 AM	Ö	ŏ	ő	0	ő	Ö	Ö	0	Ö	i	Ö	ő	ő	Ö	ŏ	Ö	1
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	10 100.00%	0 0.00%	0 0.00%	0 0.00%	7 50.00%	7 50.00%	0 0.00%	0 0.00%	0 0.00%	1 100.00%	0 0.00%	0 0.00%	25
PEAK HR :		07:45 AM	- 08:45 AM														TOTAL
PEAK HR VOL :	0	0	0	0	8	0	0	0	5	2	0	0	0	1	0	0	16
PEAK HR FACTOR:	0.000	0.000	0.000	0.000	0.333	0.000	0.000	0.000	0.417	0.500 0.58	0.000	0.000	0.000	0.250	0.000 50	0.000	0.667
		NORTH	HBOUND			SOUTHE	SOLIND			EASTBO	OLIND			WESTE	OLIND		
PM	0	0	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
FIVI	NL	NT	NR	NU	SL	ST	SR	SU	ĔĹ	ĒŤ	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
4:15 PM	0	0	0	0	0	0	1	0	1	1	0	0	0	0	0	0	3
4:30 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	0	2
4:45 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	0	2
5:00 PM	0	0	0	0	1	0	0	0	1	0	0	0	0	1	0	0	3
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM 5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0 1
5:45 PM 6:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	1
6:45 PM	Ö	ŏ	ő	Ö	ő	ŏ	ŏ	Ö	Ô	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	Ŏ	Ô
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	1 50.00%	0 0.00%	1 50.00%	0 0.00%	4 57.14%	3 42.86%	0 0.00%	0 0.00%	0 0.00%	4 100.00%	0 0.00%	0 0.00%	13
PEAK HR :		04:00 PM	- 05:00 PM														TOTAL
PEAK HR VOL :	0	0	0	0	0	0	1	0	1	3	0	0	0	3	0	0	8
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.250	0.000	0.250	0.750	0.000	0.000	0.000	0.750	0.000	0.000	0.667

Location: Hastings Ln & Oak Springs Dr City: Warrenton Control: 1-Way Stop(SB)

Data - Bikes

Project ID: 23-260020-006 Date: 2/9/2023

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NS/EW Streets:		Hastir	ngs Ln			Hastir	ngs Ln			Oak Sp	rings Dr			Oak Spi	rings Dr		
			HBOUND				HBOUND				BOUND				BOUND		
AM	0	0	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
6:00 AM	NL	NT	NR	NU	SL 0	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT.
6:00 AM 6:15 AM	0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	Ö	Ŏ	Ö	Ö	ő	Ö	ň	Ŏ	Ö	Ô	Ô	Ŏ	Ö	Ö	Ö	Ö	0
7:30 AM	ō	Ō	ō	Ō	0	ō	Ō	Ō	0	Ō	Ō	Ō	0	Ō	ō	Ō	0
7:45 AM	ō	Ö	ō	ō	Ō	ō	Ö	Ö	Ō	Ö	Ö	Ö	Ō	Ö	ō	ō	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
																	TOT
		07:45 AM	- 08:45 AM														
PEAK HR :	0	07:45 AM			0	0	0	0	0	0	0	0	0	0	0	0	0
	0 0.000	0.000	0 0.000	0.000	0 0.000	0 0.000 SOUTH	0 0.000 HBOUND	0 0.000	0 0.000	0 0.000	0 0.000 BOUND	0.000	0.000	0 0.000 WEST	0 0.000	0 0.000	0
PEAK HR : PEAK HR VOL :	0.000	0 0.000 NORTH 0	0 0.000 HBOUND 0	0 0.000	0.000	0.000 SOUTH	0.000 HBOUND 0	0.000	0.000	0.000 EAST 1	0.000 BOUND 0	0.000	0.000	0.000 WEST 1	0.000 BOUND 0	0.000	
PEAK HR: PEAK HR VOL: PEAK HR FACTOR:	0.000 0 NL	0 0.000 NORTH 0 NT	0 0.000 HBOUND 0 NR	0 0.000	0.000 0 SL	0.000 SOUTH 1 ST	0.000 HBOUND 0 SR	0.000 0 SU	0.000 0 EL	0.000 EAST 1 ET	0.000 BOUND 0 ER	0.000 0 EU	0.000 0 WL	0.000 WEST 1 WT	0.000 BOUND 0 WR	0.000 0 WU	тот
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM	0.000 0 NL 0	0 0.000 NORTH 0 NT 0	0 0.000 HBOUND 0 NR 0	0 0.000 0 NU 0	0.000 0 SL 0	0.000 SOUTH 1 ST 0	0.000 HBOUND O SR O	0.000 0 SU 0	0.000 0 EL 0	0.000 EAST 1 ET 0	0.000 BOUND 0 ER 0	0.000 0 EU 0	0.000 0 WL 0	0.000 WEST 1 WT	0.000 BOUND 0 WR	0.000 0 WU 0	тот
PEAK HR: PEAK HR VOL: PEAK HR FACTOR:	0.000 0 NL	0 0.000 NORTH 0 NT	0 0.000 HBOUND 0 NR	0 0.000	0.000 0 SL	0.000 SOUTH 1 ST	0.000 HBOUND 0 SR	0.000 0 SU	0.000 0 EL	0.000 EAST 1 ET	0.000 BOUND 0 ER	0.000 0 EU	0.000 0 WL	0.000 WEST 1 WT	0.000 BOUND 0 WR	0.000 0 WU	тот
PEAK HR : PEAK HR VOL : PEAK HR FACTOR : PM 4:00 PM 4:15 PM	0.000 0 NL 0 0	0 0.000 NORTH 0 NT 0 0	0 0.000 HBOUND 0 NR 0 0	0 0.000	0.000 0 SL 0 0	0.000 SOUTH 1 ST 0 0	0.000 HBOUND 0 SR 0 0	0.000 0 SU 0 0	0.000 0 EL 0	0.000 EAST 1 ET 0 0	0.000 BOUND 0 ER 0 0	0.000 0 EU 0 0	0.000 0 WL 0	0.000 WEST 1 WT 0 0	0.000 BOUND 0 WR 0 0	0.000 0 WU 0 0	TOT 0 0
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:35 PM 4:45 PM 5:00 PM	0.000 0 NL 0 0 0 0	0 0.000 NORTH 0 NT 0 0 0	0 0.000 HBOUND 0 NR 0 0 0	0 0.000	0.000 0 SL 0 0 0 0	0.000 SOUTH 1 ST 0 0 0 0	0.000 HBOUND 0 SR 0 0 0 0	0.000 0 SU 0 0 0 0	0.000 0 EL 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0	0.000 0 EU 0 0 0 0	0.000 WL 0 0 0 0	0.000 WEST 1 WT 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0	0.000 WU 0 0 0 0	TOT 0 0 0 0 0 0 0 0 0
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PIV 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	0.000 0 NL 0 0 0 0 0	0 0.000 NORTH 0 NT 0 0 0	0 0.000 HBOUND 0 NR 0 0 0	0 0.000	0.000 0 SL 0 0 0 0 0	0.000 SOUTH 1 ST 0 0 0 0 0	0.000 HBOUND 0 SR 0 0 0 0 0 0	0.000 0 SU 0 0 0 0 0	0.000 0 EL 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0	0.000 0 EU 0 0 0 0 0	0.000 0 WL 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0	0.000 0 WU 0 0 0 0 0	TOT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM	0.000 0 NL 0 0 0 0 0	0 0.000 NORTH 0 NT 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0 0.000	0.000 SL 0 0 0 0 0 0 0	0.000 SOUTH 1 ST 0 0 0 0 0 0 0	0.000 HBOUND O SR O O O O O O	0.000 SU 0 0 0 0 0 0	0.000 0 EL 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0	0.000 0 EU 0 0 0 0 0	0.000 WL 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0	0.000 WU 0 0 0 0 0	TOT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PIV 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:30 PM 5:30 PM 5:30 PM 5:34 PM 5:34 PM	0.000 NL 0 0 0 0 0 0	0 0.000 NORTH 0 NT 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0 0.000	0.000 SL 0 0 0 0 0	0.000 SOUTH 1 ST 0 0 0 0 0 0 0 0	0.000 HBOUND 0 SR 0 0 0 0 0 0 0	0.000 SU 0 0 0 0 0	0.000 EL 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0	0.000 EU 0 0 0 0 0 0	0.000 WL 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0	0.000 BOUND WR 0 0 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0	TOT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR : PEAK HR VOL : PEAK HR FACTOR : PM 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:30 PM 5:30 PM 5:30 PM 5:30 PM 5:30 PM	0.000 NL 0 0 0 0 0 0 0	0 0.000 NORTH 0 NT 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0 0	0 0.000	0.000 SL 0 0 0 0 0 0 0 0	0.000 SOUTH 1 ST 0 0 0 0 0 0 0 0 0 0	0.000 HBOUND 0 SR 0 0 0 0 0 0 0	0.000 SU 0 0 0 0 0 0 0 0	0.000 0 EL 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0	0.000 EU 0 0 0 0 0 0 0	0.000 WL 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0	TOT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:15 PM 5:30 PM 5:345 PM 6:00 PM 6:15 PM	0.000 0 NL 0 0 0 0 0 0 0 0	0 0.000 NORTH 0 NT 0 0 0 0 0 0	0 0.0000 HBOUND 0 NR 0 0 0 0 0	0 0.000	0.000 0 SL 0 0 0 0 0 0 0 0 0	0.000 SOUTH 1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 HBOUND O SR O O O O O O O O O O O O O	0.000 0 SU 0 0 0 0 0 0 0 0	0.000 0 EL 0 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0	0.000 0 EU 0 0 0 0 0 0 0 0	0.000 WL 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0	TO1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR : PEAK HR VOL : PEAK HR FACTOR : 4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 6:30 PM	0.000 NL 0 0 0 0 0 0 0 0 0	0 0.000 NORTH 0 NT 0 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0 0 0	0 0.000	0.000 SL 0 0 0 0 0 0 0 0 0	0.000 SOUTH 1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 HBOUND O SR O O O O O O O O O O O O O	0.000 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 EL 0 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 EU 0 0 0 0 0 0 0 0 0	0.000 WL 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TO 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:15 PM 5:30 PM 5:345 PM 6:00 PM 6:15 PM	0.000 0 NL 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.0000 NORTH 0 NT 0 0 0 0 0 0 0 0	0 0.0000 HBOUND 0 NR 0 0 0 0 0 0 0 0	0 0.000	0.000 0 SL 0 0 0 0 0 0 0 0 0	0.000 SOUTH 1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 1BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 SU 0 0 0 0 0 0 0 0 0 0	0.000 0 EL 0 0 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WL 0 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TO1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR : PEAK HR VOL : PEAK HR FACTOR : PM 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:30 PM 5:30 PM 5:30 PM 6:00 PM 6:44 PM 6:30 PM 6:45 PM	0.000 0 NL 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.0000 NORTH 0 NT 0 0 0 0 0 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0 0 0 0	0 0.000	0.000 O SL O O O O O O O O O O O O O O O O O O O	0.000 SOUTH 1 ST 0 0 0 0 0 0 0 0 0 0 The string of the st	0.000 HBOUND 0 SR 0 0 0 0 0 0 0 0 0 SR SR	0.000 0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 O EL O O O O O O O O O EL EL O O O O	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 ET ET	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 ER ER	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WEST 1 T 0 0 0 0 0 0 0 WT	0.000 (BOUND	0.000 0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0	TOT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:30 PM 5:30 PM 5:30 PM 6:15 PM 6:30 PM 6:30 PM 6:30 PM 6:30 PM 6:30 PM	0.000 0 NL 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.0000 NORTH 0 NT 0 0 0 0 0 0 0 0	0 0.0000 HBOUND 0 NR 0 0 0 0 0 0 0 0	0 0.000	0.000 0 SL 0 0 0 0 0 0 0 0 0	0.000 SOUTH 1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 1BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 SU 0 0 0 0 0 0 0 0 0 0	0.000 0 EL 0 0 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WL 0 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:30 PM 5:15 PM 5:30 PM 5:15 PM 6:00 PM 6:15 PM 6:30 PM 6:30 PM 6:30 PM 6:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR:	0.000 NL 0 0 0 0 0 0 0 0 0 0 0 0 0 NL 0 0 0 0	0 0.000 NORTH 0 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.0000 HBOUND 0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.000	0.000 SL 0 0 0 0 0 0 0 0 0 0 0 SL 0 0 0 0	0.000 SOUTH 1 ST 0 0 0 0 0 0 0 0 0 0 ST 0	0.000 HBOUND O SR O O O O O SR O O O SR O O O SR O O O O O O O O O O O O O	0.000 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0.000 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 ET 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 ER 0 0 0 0 0 0	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WL 0 0 0 0 0 0 0 0 0 0 WL 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 WT 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 WR 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTO 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR : PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:15 PM 5:30 PM 6:15 PM 6:15 PM 6:30 PM 6:35 PM 6:45 PM TOTAL VOLUMES: APPROACH %'s:	0.000 NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.0000 NORTH 0 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.000	0.000 O SL O O O O O O O O O O O O O O O O O O O	0.000 SOUTH 1 ST 0 0 0 0 0 0 0 0 0 0 The string of the st	0.000 HBOUND 0 SR 0 0 0 0 0 0 0 0 0 SR SR	0.000 0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 O EL O O O O O O O O O EL EL O O O O	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 ET ET	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 ER ER	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WEST 1 T 0 0 0 0 0 0 0 WT	0.000 (BOUND	0.000 0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0	TOT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

National Data & Surveying Services Intersection Turning

Location: Hastings Ln & Oak Springs Dr Vernento Count Project ID: 23-260020-006

Date: 2/9/2023

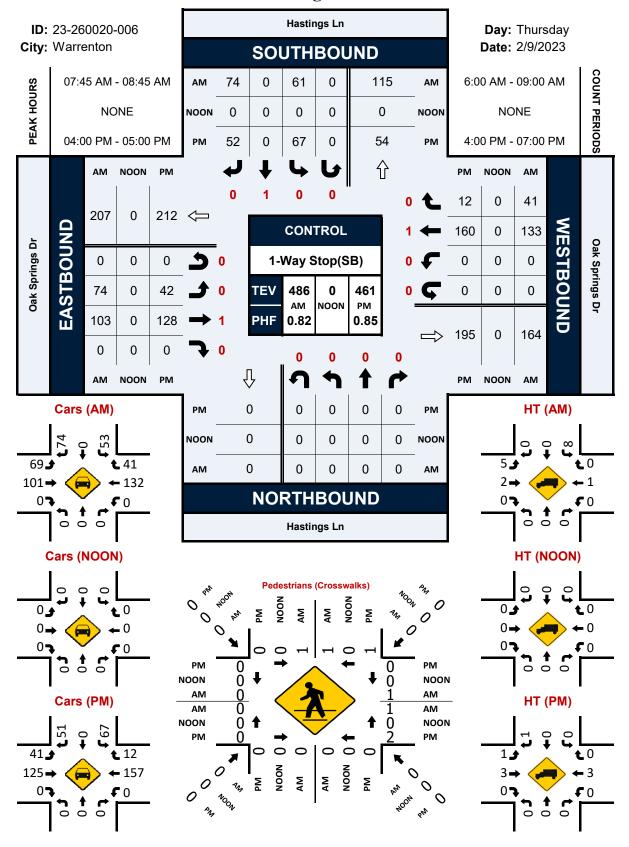
Data - Pedestrians (Crosswalks)

NS/EW Streets:	Hastir	ngs Ln	Hastir	ngs Ln	Oak Spi	rings Dr	Oak Spr	rings Dr	
AM	NORT	'H LEG	SOUT	'H LEG	EAST	LEG	WEST	LEG	
AIVI	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0
6:15 AM	0	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0
6:45 AM	1	0	0	0	0	0	0	0	1
7:00 AM	1	2	0	0	0	1	0	0	4
7:15 AM	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	1	0	0	1
8:15 AM	1	0	0	0	1	0	0	0	2
8:30 AM	0	1	0	0	0	0	0	0	1
8:45 AM	1	0	0	0	0	0	0	0	1
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	4	3	0	0	1	2	0	0	10
APPROACH %'s:	57.14%	42.86%	,		33.33%	66.67%	_		
PEAK HR:	07:45 AM	- 08:45 AM							TOTAL
PEAK HR VOL:	1	1	0	0	1	1	0	0	4
PEAK HR FACTOR:	0.250	0.250			0.250	0.250			0.500
	0.5	500			0.5	500			0.500

DNA	NORT	H LEG	SOUT	'H LEG	EAST	LEG	WEST	Γ LEG	
PM	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	0	0	2	0	0	0	2
4:15 PM	0	0	0	0	0	0	0	0	0
4:30 PM	0	1	0	0	0	0	0	0	1
4:45 PM	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0
5:15 PM	0	1	0	0	0	0	0	0	1
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0
6:00 PM	2	0	0	0	0	0	0	0	2
6:15 PM	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	0
6:45 PM	0	0	0	0	0	1	0	0	1
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	2	2	0	0	2	1	0	0	7
APPROACH %'s:	50.00%	50.00%			66.67%	33.33%			
PEAK HR :	04:00 PM	- 05:00 PM							TOTAL
PEAK HR VOL:	0	1	0	0	2	0	0	0	3
PEAK HR FACTOR :		0.250			0.250				0.275
	0.2	250			0.2	250			0.375

Hastings Ln & Oak Springs Dr

Peak Hour Turning Movement Count



Location: Highland School Dwy & Oak Springs Dr

0.000

0.438

0.382

0.000

0.375

PEAK HR FACTOR

City: Warrenton Control: 1-Way Stop(SB)

Project ID: 23-260020-007 **Date:** 2/9/2023 Data - Total Highland School Dwy Highland School Dwy Oak Springs Dr NS/EW Streets Oak Springs Dr NORTHBOUND SOUTHBOUND EASTBOUND WESTBOUND AM TOTAL WU 6:00 AM 6:15 AM 4 7 15 15 28 34 32 43 47 28 30 11 6:30 AM 6:45 AM 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 18 29 37 63 89 160 103 11 14 16 30 25 43 42 42 32 17 95 75 113 1 0 19 1 5 20 8:15 AM 8:30 AM 13 8:45 AM NT 0 NR 0 NU 0 EU SL 50 TOTAL VOLUMES APPROACH %'s PEAK HR PEAK HR VOL 0.00% 38 43.18% 0.009 0.00% 0.009 289 81.41% 800 TOTAL 07:30 AM - 08:30 AM 0 0 0.000 0.951 19 0 0.594 0.379 0 0.000 0 0.000 38 0.500 156 0.830 0 0.000 0 0.000 0 0.000 447 0.000 0.000 0.000 0.000 0.310 0.386 PEAK HR FACTOR 0.884 0.698 FASTROLIND NORTHBOLIND SOLITHBOLIND PM 91 93 126 102 91 85 102 72 60 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 35 39 44 44 59 57 44 49 54 37 38 21 41 46 34 47 33 22 23 22 16 45 43 29 0 0 0 0 0 6:30 PM 6:45 PM 0 0 0 20 13 ō NT 0 NR 0 NU 0 TOTAL VOLUMES 11 0 0.00% 30 73.17% 0.00% 0 0.00% 486 99.18% 4 0.82% 402 98.53% 939 APPROACH %'s PEAK HR PEAK HR VOL TOTAL 170 0.924 0.000 0.000 0 0.000 0.000 0 0.000 204 0.864 412 0.000

0.000

0.500

0.000

0.817

Location: Highland School Dwy & Oak Springs Dr City: Warrenton Control: 1-Way Stop(SB)

City: \ Control: :	Warrento 1-Way St							Data -	· Cars				Pro		23-260020- 2/9/2023	UU7	
NS/EW Streets:		Highland S	School Dwy			Highland Sc	thool Dwy	Data	Cars	Oak Sprii	ngs Dr			Oak Spri	ings Dr		1
		NORTI	HBOUND			SOUTH	ROLIND			EASTB	OLIND			WESTE	SOLIND		
AM	0 NL	0 NT	0 NR	0 NU	1 SL	0 ST	1 SR	0 SU	1 EL	1 ET	0 ER	0 EU	0 WL	1 WT	0 WR	0 WU	TOTA
6:00 AM	0	0	0	0	0	0	0	0	0	6	0	0	0	1	0	0	7
6:15 AM	0	0	0	0	0	0	0	0	0	4	0	0	0	7	0	0	11
6:30 AM	0	0	0	0	0	0	0	0	0	5	0	0	0	11	0	0	16
6:45 AM	0	0	0	0	0	0	0	0	0	14	0	0	0	14	0	0	28
7:00 AM	0	0	0	0	0	0	0	0	2	13	0	0	0	16	4	0	35
7:15 AM	0	0	0	0	0	0	2	0	1	27	0	0	0	30	2	0	62
7:30 AM 7:45 AM	0	0	0	0	3 25	0	4 8	0	13 19	34 29	0	0	0	25 42	10 33	0	89 156
7:45 AM 8:00 AM	0	0	0	0	25	0	6	0	5	40	0	0	0	42	5	0	100
8:15 AM	0	0	0	0	1	0	1	0	1	40 47	0	0	0	42	3	0	95
8:30 AM	Ö	Ö	ő	0	0	0	3	Ö	5	27	0	0	0	32	7	Ö	74
8:45 AM	Ö	Ö	Ö	Ö	19	Ö	14	Ö	20	29	Ö	Ö	Ö	17	13	Ŏ	112
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTA
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	50 56.82%	0 0.00%	38 43.18%	0 0.00%	66 19.35%	275 80.65%	0 0.00%	0 0.00%	0 0.00%	279 78.37%	77 21.63%	0 0.00%	785
PEAK HR :		07:30 AM	- 08:30 AM														TOTA
PEAK HR VOL:	0	0	0	0	31	0	19	0	38	150	0	0	0	151	51	0	440
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.310	0.000	0.594 79	0.000	0.500	0.798 0.97	0.000 79	0.000	0.000	0.899	0.386 73	0.000	0.70
		NORTI	HBOUND			SOUTH	ROLIND			EASTB	OLIND			WESTE	ROLIND		1
PM	0	0	0	0	1	0	1	0	1	1	0	0	0	1	0	0	
1 171	NL	NT	NR	NU	SL	ST	SR	SU	ĒĹ	ĒŤ	ER	EU	WL	WT	WR	WU	TOT
4:00 PM	0	0	0	0	2	0	1	0	2	35	0	0	0	49	1	0	90
4:15 PM	0	0	0	0	2	0	6	0	2	37	0	0	0	43	0	0	90
4:30 PM	0	0	0	0	4	0	17	0	1	43	0	0	0	58	1	0	124
4:45 PM	0	0	0	0	1	0	3	0	0	40	0	0	0	56	0	0	100
5:00 PM	0	0	0	0	0	0	0	0	0	45	0	0	0	43	1	0	89
5:15 PM	0	0	0	0	1	0	0	0	0	34	0	0	0	49	1	0	85
5:30 PM	0	0	0	0	0	0	0	0	1	47	0	0	0	54 37	0	0	102
5:45 PM 6:00 PM	0	0	0	0	0	0	0	0	0	32 22	0	0	0	37	0	0	71 60
6:00 PM	0	0	0	0	1	0	0	0	0	22	0	0	0	36 21	0	0	45
6:30 PM	0	0	0	0	0	0	1	0	0	21	0	0	0	20	0	0	42
6:45 PM	Ö	ő	ő	0	ő	ŏ	Ō	ŏ	Ŏ	16	ŏ	ŏ	Ŏ	13	ŏ	ŏ	29
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOT
TOTAL VOLUMES :	0	0	0	0	11 26.83%	0 0.00%	30 73.17%	0 0.00%	6 1.50%	395 98.50%	0 0.00%	0 0.00%	0 0.00%	481 99.18%	4 0.82%	0 0.00%	92
APPROACH %'s:																	TOT
PEAK HR :		04:15 PM	- 05:15 PM														101
	0	04:15 PM 0	- 05:15 PM 0	0	7 0.438	0 0.000	26 0.382	0	3	165	0	0	0	200	2 0.500	0	403

Project ID: 23-260020-007

Location: Highland School Dwy & Oak Springs Dr City: Warrenton

														Oak Springs Dr WESTBOUND 1 0 WT WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0	2/3/2023		
=								Data	- HT					WESTBOUND 1 0 WT WR 0			
NS/EW Streets:		Highland S	School Dwy			Highland S	School Dwy			Oak Sprii	ngs Dr			Oak Spri	ngs Dr		
		NORTI	HBOUND			SOUTI	HBOUND			EASTB	OUND			WESTE	BOUND		
AM	0	0	0	0	1	0	1	0	1	1	0	0	0			0	
6.00.111	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL			WU	TOT
6:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0			0	0
6:15 AM 6:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0			0	0
6:45 AM	0	0	0	0	0	0	0	0	0	1	0	0	0			0	1
7:00 AM	0	0	0	0	0	0	0	0	0	2	0	0	0			0	2
7:15 AM	0	Õ	Ö	Ö	0	Ô	0	Ö	0	1	0	0	Ö			Ö	1
7:30 AM	ō	Ō	ō	ō	0	ō	ō	ō	Ō	ō	Ō	Ō	ō		Ō	ō	0
7:45 AM	0	0	0	Ó	0	0	0	0	0	3	0	0	Ō	1	Ó	0	4
8:00 AM	0	0	0	0	0	0	0	0	0	3	0	0	0			0	3
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0			0	0
8:30 AM	0	0	0	0	0	0	0	0	0	1	0	0	0			0	1
8:45 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL			WU	TO
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0 0.00%	14 100.00%	0 0.00%	0 0.00%	0 0.00%	1 100.00%	0 0.00%	0 0.00%	1
PEAK HR:		07:30 AM	- 08:30 AM														TO
PEAK HR VOL:	0	0	0	0	0	0	0	0	0	6	0	0	0	1	0	0	7
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.500	0.000	0.000	0.000	0.250	0.000	0.000	0.4
										0.50	00			0.2	50		0.4.
		NORTI	HBOUND			SOUTI	HBOUND			EASTB	OUND			WESTE	BOUND		
PM	0	0	0	0	1	0	1	0	1	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TO
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
4:15 PM	0	0	0	0	0	0	0	0	0	2	0	0	0	1	0	0	3
4:30 PM 4:45 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	0	2
5:00 PM	0	0	0	0	0	0	0	0	0	-	0	0	0	1	0	0	2
5:15 PM	0	0	Ö	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	Ö	Ŏ	Ö	Ö	Ö	Ö	Ö	Ö	Ö	Ŏ	Ö	Ö	Ö	Ö	Ŏ	Ö	0
5:45 PM	ō	Ō	0	ō	0	ō	ō	ō	Ō	1	Ō	Ō	ō	Ö	Ō	ō	1
6:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
6:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TO
TOTAL VOLUMES :	0	0	0	0	0	0	0	0	0 0.00%	7 100.00%	0 0.00%	0 0.00%	0 0.00%	5 100.00%	0 0.00%	0 0.00%	1
APPROACH %'s:																	TO
PEAK HR :		04:15 PM	- 05:15 PM														101
	0,000	0 0 0.000	0 0 0.000	0.000	0	0	0	0 0.000	0 0.000	5 0.625	0 0.000	0 0.000	0 0.000	4 1.000	0 0.000	0 0.000	9

Location: Highland School Dwy & Oak Springs Dr City: Warrenton Control: 1-Way Stop(SB)

Project ID: 23-260020-007 Date: 2/9/2023

_									Bikes								
NS/EW Streets:		Highland S	School Dwy			Highland S	School Dwy			Oak Sp	rings Dr			Oak Sp	rings Dr		
		NORTI	HBOUND			SOUTI	HBOUND			EAST	BOUND			WEST	BOUND		
AM	0	0	0	0	1	0	1	0	1	1	0	0	0	1	0	0	
6:00 AM	NL 0	NT 0	NR 0	NU 0	SL 0	ST 0	SR 0	SU 0	EL 0	ET	ER 0	EU 0	WL 0	WT 0	WR 0	WU 0	TOTAL 0
6:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 AM	Ö	Ö	Ŏ	Ö	0	Ö	Ö	Ö	Ö	Ö	Ö	Ŏ	Ö	Ö	Ö	Ö	0
6:45 AM	ō	Ō	Ō	Ō	0	Ō	Ō	Ō	0	Ō	Ō	Ō	0	Ō	Ō	ō	0
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM 8:30 AM	0	0 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.13 AN	U	U	U	U	U	U	U	U		U	U	U	·	U	U	U	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
																	TOTAL
PEAK HR : I		07:30 AM	- 08:30 AM														
PEAK HR : PEAK HR VOL :	0	07:30 AM	- 08:30 AM 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	0 0.000			0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0
PEAK HR VOL :		0	0														0
PEAK HR VOL :		0 0.000	0 0.000			0.000	0.000			0.000	0.000			0.000	0.000		0
PEAK HR VOL : PEAK HR FACTOR :	0.000	0 0.000 NORTI	0 0.000 HBOUND	0.000	0.000	0.000 SOUTH	0.000 HBOUND	0.000	0.000	0.000 EAST	0.000 BOUND	0.000	0.000	0.000 WEST	0.000 BOUND	0.000	0
PEAK HR VOL :		0 0.000	0 0.000		0.000	0.000	0.000			0.000	0.000			0.000	0.000		TOTAL
PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM	0.000	0 0.000 NORTI	0 0.000 HBOUND 0	0.000	0.000	0.000 SOUTH 0	0.000 HBOUND	0.000	0.000	0.000 EAST 1	0.000 BOUND 0	0.000	0.000	0.000 WEST 1	0.000 BOUND 0	0.000	
PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM	0.000 0 NL 0 0	0 0.000 NORTI 0 NT 0	0 0.000 HBOUND 0 NR 0 0	0.000 0 NU 0 0	0.000 1 SL 0	0.000 SOUTH 0 ST 0	0.000 HBOUND 1 SR 0 0	0.000 0 SU 0 0	0.000 1 EL 0 0	0.000 EAST 1 ET 0 0	0.000 BOUND 0 ER 0	0.000 0 EU 0 0	0.000 0 WL 0	0.000 WEST 1 WT 0 0	0.000 BOUND 0 WR 0 0	0.000 0 WU 0	TOTAL 0 0
PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM	0.000 0 NL 0 0	0 0.000 NORTH 0 NT 0 0	0 0.000 HBOUND 0 NR 0 0	0.000 0 NU 0 0	0.000 1 SL 0 0 0	0.000 SOUTH 0 ST 0 0	0.000 HBOUND 1 SR 0 0 0	0.000 0 SU 0 0	0.000 1 EL 0 0	0.000 EAST 1 ET 0 0 0	0.000 BOUND 0 ER 0 0	0.000 0 EU 0 0	0.000 0 WL 0 0 0	0.000 WEST 1 WT 0 0 0	0.000 BOUND 0 WR 0 0	0.000 0 WU 0 0	TOTAL 0 0 0 0
PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:45 PM	0.000 0 NL 0 0 0 0	0 0.000 NORTI 0 NT 0 0 0	0 0.000 HBOUND 0 NR 0 0 0	0.000 0 NU 0 0 0 0	0.000 1 SL 0 0 0 0	0.000 SOUTH 0 ST 0 0 0	0.000 HBOUND SR 0 0 0 0	0.000 0 SU 0 0 0	0.000 1 EL 0 0 0 0	0.000 EAST 1 ET 0 0 0	0.000 BOUND 0 ER 0 0 0	0.000 0 EU 0 0 0 0	0.000 WL 0 0 0 0	0.000 WEST 1 WT 0 0 0 0	0.000 BOUND 0 WR 0 0 0	0.000 0 WU 0 0 0	TOTAL 0 0 0 0 0 0
PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:35 PM 4:45 PM 5:00 PM	0.000 0 NL 0 0 0 0	0 0.000 NORTI 0 NT 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0.000 0 NU 0 0 0 0 0	0.000 1 SL 0 0 0 0	0.000 SOUTH 0 ST 0 0 0 0	0.000 HBOUND 1 SR 0 0 0 0	0.000 0 SU 0 0 0	1 EL 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0	0.000 0 EU 0 0 0 0	0.000 WL 0 0 0 0	0.000 WEST 1 WT 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0	0.000 0 WU 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	0.000 0 NL 0 0 0 0 0	0 0.000 NORTI 0 NT 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0.000 0 NU 0 0 0 0 0	0.000 1 SL 0 0 0 0 0	0.000 SOUTH 0 ST 0 0 0 0	0.000 HBOUND 1 SR 0 0 0 0 0	0.000 0 SU 0 0 0 0	0.000 1 EL 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0	0.000 0 EU 0 0 0 0 0	0.000 WL 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0	0.000 0 WU 0 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:10 PM 5:30 PM	0.000 0 NL 0 0 0 0 0 0	0 0.000 NORTI 0 NT 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0.000 0 NU 0 0 0 0 0 0	0.000 1 SL 0 0 0 0 0 0	0.000 SOUTH 0 ST 0 0 0 0 0	0.000 HBOUND 1 SR 0 0 0 0 0 0	0.000 0 SU 0 0 0 0 0 0	0.000 1 EL 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0	0.000 EU 0 0 0 0 0 0	0.000 WL 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR VOL : PEAK HR FACTOR : PIM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	0.000 0 NL 0 0 0 0 0 0	0 0.000 NORTI 0 NT 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0.000 NU 0 0 0 0 0 0 0	0.000 1 SL 0 0 0 0 0 0	0.000 SOUTH 0 ST 0 0 0 0	0.000 HBOUND 1 SR 0 0 0 0 0	0.000 SU 0 0 0 0 0	0.000 1 EL 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0	0.000 0 EU 0 0 0 0 0	0.000 WL 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0	0.000 WU 0 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:10 PM 5:30 PM	0.000 0 NL 0 0 0 0 0 0	0 0.000 NORTI 0 NT 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0	0.000 0 NU 0 0 0 0 0 0	0.000 1 SL 0 0 0 0 0 0	0.000 SOUTH 0 ST 0 0 0 0 0 0 0	0.000 HBOUND 1 SR 0 0 0 0 0 0	0.000 0 SU 0 0 0 0 0 0	0.000 1 EL 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0	0.000 EU 0 0 0 0 0 0	0.000 WL 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0	0.000 BOUND WR 0 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM	0.000 0 NL 0 0 0 0 0 0 0	0 0.000 NORTI 0 NT 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0 0	0.000 NU 0 0 0 0 0 0 0 0	0.000 1 SL 0 0 0 0 0 0 0 0	0.000 SOUTH 0 ST 0 0 0 0 0 0 0 0 0	0.000 HBOUND 1 SR 0 0 0 0 0 0 0 0	0.000 0 SU 0 0 0 0 0 0 0	0.000 1 EL 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0	0.000 EU 0 0 0 0 0 0 0 0	0.000 WL 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0	0.000 WU 0 0 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR VOL : PEAK HR FACTOR : PIM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:30 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM	0.000 0 NL 0 0 0 0 0 0 0 0	0 0.000 NORTI 0 NT 0 0 0 0 0	0 0.000 HBOUND 0 NR 0 0 0 0 0 0	0.000 0 NU 0 0 0 0 0 0 0 0	0.000 1 SL 0 0 0 0 0 0 0 0 0	0.000 SOUTH 0 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 HBOUND 1 SR 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 SU 0 0 0 0 0 0 0	0.000 1 EL 0 0 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 EU 0 0 0 0 0 0 0 0	0.000 WL 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WU 0 0 0 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:10 PM 5:30 PM 6:30 PM 6:15 PM 6:30 PM 6:30 PM	0.000 0 NL 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.000	0 0.0000 HBOUND 0 NR 0 0 0 0 0 0 0 0	0.000 0 NU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 1 SL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 SOUTH 0 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 HBOUND 1 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 SU 0 0 0 0 0 0 0 0 0 0	1 EL 0 0 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WL 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR VOL : PEAK HR FACTOR : PIM 4:00 PM 4:10 PM 4:15 PM 4:30 PM 5:15 PM 5:00 PM 5:15 PM 6:30 PM 6:31 PM 6:30 PM 6:34 PM	0.000 0 NL 0 0 0 0 0 0 0 0 0	0 0.0000 NORTI 0 0 0 0 0 0 0 0 0 0 0	0 0.0000 HBOUND 0 NR 0 0 0 0 0 0 0 0	0.000 0 NU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 1 SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 SOUTH 0 0 ST 0 0 0 0 0 0 0 0 0 0 0 0 This is a second of the seco	0.000 HBOUND 1 SR 0 0 0 0 0 0 0 0 0 0 0 SR SR	0.000 0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 1 EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 ET ET	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 ER ER	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 EU	0.000 0 WL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 WT	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 WR	0.000 0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:10 PM 5:30 PM 6:30 PM 6:15 PM 6:30 PM 6:30 PM	0.000 ONL OO OO OO OO OO OO OO OO O	0 0.000	0 0.0000 HBOUND 0 NR 0 0 0 0 0 0 0 0	0.000 0 NU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 1 SL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 SOUTH 0 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 HBOUND 1 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 SU 0 0 0 0 0 0 0 0 0 0	1 EL 0 0 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WL 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR VOL: PEAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:15 PM 5:30 PM 6:15 PM 6:30 PM 6:35 PM 6:30 PM 6:45 PM	0.000 ONL OO OO OO OO OO OO OO OO O	0 0.000 NORTI 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.0000 HBOUND 0 NR 0 0 0 0 0 0 0 0	0.000 0 NU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 1 SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 SOUTH 0 0 ST 0 0 0 0 0 0 0 0 0 0 0 0 This is a second of the seco	0.000 HBOUND 1 SR 0 0 0 0 0 0 0 0 0 0 0 SR SR	0.000 0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 1 EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 ET ET	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 ER ER	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 EU	0.000 0 WL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 WT	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 WR	0.000 0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PEAK HR VOL: PEAK HR FACTOR: PIM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 6:30 PM 6:15 PM 6:30 PM 6:15 PM 6:30 PM 6:45 PM TOTAL VOLUMES: APPROACH %'s:	0.000 ONL OO OO OO OO OO OO OO OO O	0 0.000 NORTI 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0.0000 HBOUND 0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 NU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 1 SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 SOUTH 0 0 ST 0 0 0 0 0 0 0 0 0 0 0 0 This is a second of the seco	0.000 HBOUND 1 SR 0 0 0 0 0 0 0 0 0 0 0 SR SR	0.000 0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 1 EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 EAST 1 ET 0 0 0 0 0 0 0 0 0 0 ET ET	0.000 BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 ER ER	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 EU	0.000 0 WL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 WEST 1 WT 0 0 0 0 0 0 0 0 0 0 WT	0.000 BOUND 0 WR 0 0 0 0 0 0 0 0 0 0 WR 0 0 WR	0.000 0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

National Data & Surveying Services Intersection Turning

Location: Highland School Dwy & Oak Springs Dr Count Project ID: 23-260020-007 City: Warrenton Date: 2/9/2023

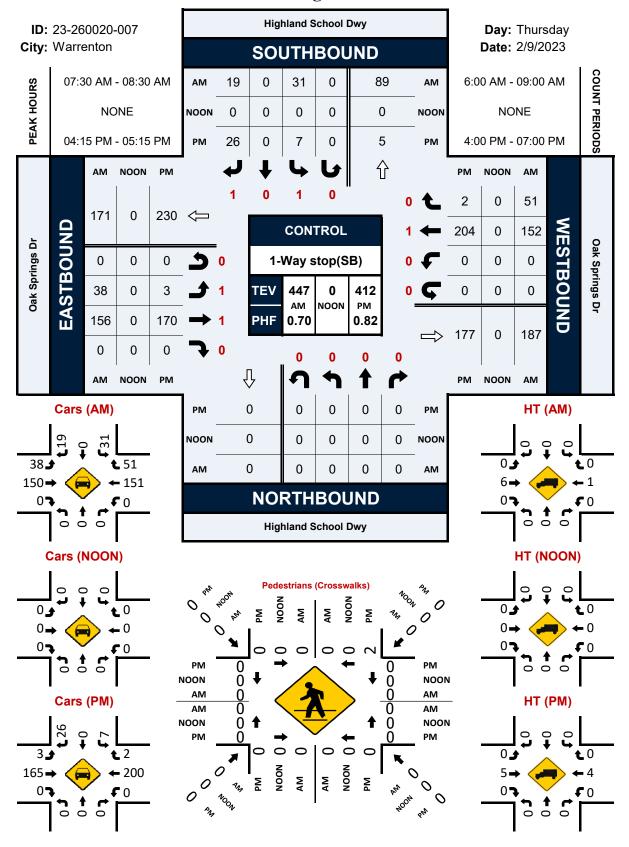
Data - Pedestrians (Crosswalks)

NS/EW Streets:	Highland S	chool Dwy	Highland :	School Dwy	Oak Sp	rings Dr	Oak Spi	rings Dr	
AM	NORT EB	H LEG WB	SOUT EB	TH LEG WB	EAST NB	Γ LEG SB	WEST NB	Γ LEG SB	TOTAL
6:00 AM 6:15 AM 6:30 AM 6:45 AM 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0
TOTAL VOLUMES : APPROACH %'s : PEAK HR : PEAK HR VOL : PEAK HR FACTOR :	EB 1 100.00%	WB 0 0.00% - 08:30 AM	EB 0	WB 0	NB 0	SB 0	NB 0	SB 0	TOTAL 1 TOTAL 0

DNA	NORT	TH LEG	SOUT	'H LEG	EAST	LEG	WEST	Γ LEG	
PM	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0
4:30 PM	0	1	0	0	0	0	0	0	1
4:45 PM	0	0	0	0	0	0	0	0	0
5:00 PM	0	1	0	0	0	0	0	0	1
5:15 PM	0	1	0	0	0	0	0	0	1
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0
6:00 PM	0	0	0	0	0	0	0	0	0
6:15 PM	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	0
6:45 PM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	0	3	0	0	0	0	0	0	3
APPROACH %'s:	0.00%	100.00%							
PEAK HR :	04:15 PM	- 05:15 PM							TOTAL
PEAK HR VOL :	0	2	0	0	0	0	0	0	2
PEAK HR FACTOR :		0.500							0.500
	0.	500							0.300

Highland School Dwy & Oak Springs Dr

Peak Hour Turning Movement Count



Location: US 17/US 211/Broadview Ave & Oak Springs Dr City: Warrenton Control: 2-Way Stop(EB/WB)

Project ID: 23-260020-008 **Date:** 2/9/2023

NS/EW Streets																		
AVI 1	NS/EW Streets:	US 1	17/US 211/E	Broadview A	ve	US 1	7/US 211/E	Broadview A	ve		Oak Spri	ngs Dr			Oak Spri	ngs Dr		
NIL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU			NORTH	BOUND			SOUTH	BOUND			EASTE	OUND			WESTE	OUND		
6:00 AM 0 38 1 0 5 29 0 0 0 0 0 0 0 0 0 0 1 0 0 1 0 0 6 6 0 6 6 0 6 6 0 6 6 0 6 0	AM																	
6:15 AM																		TOTAL
6:30 AM											-							74
6:45 AM											-	•						76
7:00 AM								•			•	•						106
7:15 AM																		135
7:30 AM											•	0						215
TOTAL VOLUMES NORTHBOUND SUST SR SU EL ET ER EU WL WT WR WU MT KR KATON CO.854 CO.85		-						-			•	1						220
S:00 AM 0																		276
8:15 AM 0 59 21 0 26 78 0 0 0 0 0 0 0 22 1 20 0 8:35 AM 8 0 60 18 0 19 74 1 0 0 0 0 0 0 0 0 22 1 20 0 0 0 8:45 AM 1 61 31 1 15 93 2 0 0 0 0 0 0 0 0 22 0 10 0 0 0 0 0 0 0																		364
8:30 AM											•	•						258
8:45 AM 1 61 31 1 15 93 2 0 0 0 0 0 0 22 0 10 0 0 0 0 0 0 0 0 0																		227
TOTAL VOLUMES: 3 835 186 1 160 100% 83.52% 0.48% 0.00% 0.00% 50.00% 50.00% 0.00% 48.43% 0.63% 50.94% 0.00% PEAK HR: 0: 0.29% 81.46% 18.15% 0.10% 16.00% 83.52% 0.48% 0.00% 0.00% 50.00% 50.00% 50.00% 0.00% 48.43% 0.63% 50.94% 0.00% PEAK HR: 0: 1 405 98 0 95 355 1 0 0 0 1 0 0 63 1 105 0 0 0.716 0.250 0.640 0.000 0.848 0.852 0.250 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.854 0.000 0.848 0.852 0.250 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.716 0.250 0.000 0.000 0.716 0.000 0.000 0.716 0.000 0.000 0.716 0.000 0.000 0.716 0.000 0.000 0.716 0.000 0.000 0.716 0.000 0.000 0.716 0.0000 0.000 0.716 0.0000 0.000 0.716 0.0000 0.000 0.716 0.0000 0.000 0.716 0.0000 0.000 0.716 0.0000 0.000 0.716 0.0000 0.000 0.716 0.0000 0.000 0.716 0.0000 0.000 0.716 0.0000 0.000 0.0000 0.716 0.0000 0.0000 0.0000 0.716 0.0000 0.0000 0.716 0.0000 0.0000 0.716 0.0000 0.0000 0.0000 0.716 0.0000 0.0000 0.716 0.0000 0.0000 0.716 0.0000 0.0000 0.0000 0.716 0.00000 0.0000 0.0000 0.716 0.0000 0.0000 0.0000 0.716 0.0000 0.0000											•							208
TOTAL VOLUMES: 0.29% 81.46% 181.5% 0.10% 16.00% 83.52% 0.48% 0.00% 0.00% 50.00% 50.00% 0.00% 0.00% 48.43% 0.63% 50.94% 0.00% 0.0	8:45 AM	1	61	31	1	15	93	2	U	U	U	U	U	22	0	10	U	236
TOTAL VOLUMES: 3 835 186 1 1 168 877 5 0 0 0 1 1 1 0 154 2 162 0 0.00% PEAK HR:		NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
PPROACH % s: 0.29% 81.46% 18.15% 0.10% 16.00% 83.52% 0.48% 0.00% 0.00% 50.00% 50.00% 0.00% 48.43% 0.63% 50.94% 0.00% 0.00%	TOTAL VOLUMES:	3	835	186	1	168	877			0		1	0	154	2	162	0	2395
PEAK HR VOL: 1 405 98 0 95 355 1 0 0 0 1 0 0 63 1 105 0 0.848 0.822 0.250 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.848 0.822 0.250 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.854 0.000 0.854 0.000 0.854 0.000 0.854 0.000 0.250 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.854 0.000 0.854 0.000 0.854 0.000 0.250 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.250 0.000 0.000 0.250 0.000 0.000 0.716 0.250 0.640 0.000 0.000 0.250 0.0000 0.00000 0.00000 0.00000 0.0000 0.00000 0.00000 0.00000 0.0000 0.00000 0.00000		0.29%						0.48%	0.00%	0.00%		50.00%	0.00%					
PM Northbound	PEAK HR :	-																TOTAL
PM	PEAK HR VOL:	1	405			95			0	0	1	0	0	63		105	0	1125
PM	PEAK HR FACTOR:	0.250			0.000	0.848			0.000	0.000	0.250	0.000	0.000	0.716			0.000	0.773
PN			0.70	04			0.85	54			0.2	50			0.79	97		0.773
PM 1																		
Hard																		
4:00 PM	PM																	
4:15 PM 0 95 24 0 16 142 0 0 1 0 0 0 13 0 34 0 4:30 PM 0 119 16 0 30 108 0 0 0 0 2 0 40 0 39 0 4:45 PM 1 75 18 0 21 119 2 0 0 1 1 0 24 0 34 0 5:00 PM 1 94 19 0 27 107 0 0 0 1 1 0 13 0 33 0 5:15 PM 0 85 14 0 19 116 0 0 0 0 1 0 13 0 33 0 5:30 PM 1 68 21 0 26 93 0 0 0 1 0 0 22 0 18 0 31 0 0 22 0 18 0 </th <th></th> <td></td> <td></td> <td>NR</td> <td>NU</td> <td>SL</td> <td>ST</td> <td>SR</td> <td></td> <td></td> <td>ET</td> <td>ER</td> <td>EU</td> <td></td> <td></td> <td></td> <td></td> <td></td>				NR	NU	SL	ST	SR			ET	ER	EU					
4:30 PM 0 119 16 0 30 108 0 0 0 2 0 40 0 39 0 4:45 PM 1 75 18 0 21 119 2 0 0 1 1 0 24 0 34 0 5:00 PM 1 94 19 0 27 107 0 0 0 1 1 0 13 0 33 0 5:15 PM 0 85 14 0 19 116 0 0 0 1 0 18 0 31 0 33 0 5:30 PM 1 68 21 0 26 93 0 0 0 0 0 25 0 28 0 5:45 PM 0 83 9 0 24 106 1 0 0 0 0 0 22 0 18 0 6:15 PM 0 66 11 0 10		1																TOTAL
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5:00 PM 1 94 19 0 27 107 0 0 0 1 1 1 0 13 0 33 0 35 0 5:15 PM 0 85 14 0 19 116 0 0 0 0 0 1 1 0 18 0 31 0 18 0 18 0 19 116 0 0 0 0 0 1 1 0 18 0 31 0 19 116 0 0 0 0 0 1 1 0 0 0 0 0 0 0 0 0 0 0			95	24	0	19 16	142	0	0	1 1	0	1	0	20 13	0	32 34	0	302 325
5:15 PM 0 85 14 0 19 116 0 0 0 0 1 0 18 0 31 0 0 5:30 PM 1 68 21 0 26 93 0 0 0 1 0 1 0 0 25 0 28 0 18 0 5:45 PM 0 83 9 0 24 106 1 0 0 0 0 0 0 0 22 0 18 0 6:00 PM 0 66 11 0 13 64 0 0 0 0 1 0 13 0 23 0 6:15 PM 0 66 11 0 10 87 0 0 0 0 0 0 1 0 13 0 23 0 6:15 PM 0 66 12 0 10 87 0 0 0 0 0 0 0 8 0 14 0 13 0 23 0 6:45 PM 0 56 12 0 10 54 0 0 1 0 1 0 1 0 1 0 9 0 13 0 6:45 PM 0 55 12 0 10 54 0 0 1 1 0 1 0 1 0 9 0 13 0 6:45 PM 0 55 2 8 0 8 53 0 0 0 0 0 0 0 0 0 3 1 1 8 0 0 14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4:30 PM		95 119	24 16	0 0	19 16 30	142 108	0 0 0	0 0 0	1 1 0	0	1	0 0 0	20 13 40	0 0 0	32 34 39	0 0 0	302 325 354
5:30 PM	4:30 PM 4:45 PM	0	95 119 75	24 16 18	0 0 0	19 16 30 21	142 108 119	0 0 0 2	0 0 0	1 1 0 0	0 0 0 1	1	0 0 0	20 13 40 24	0 0 0	32 34 39 34	0 0 0	302 325 354 296
5:45 PM 0 83 9 0 24 106 1 0 0 0 0 22 0 18 0 6:00 PM 0 66 11 0 13 64 0 0 0 0 13 0 23 0 6:15 PM 0 66 11 0 10 87 0 0 0 0 0 0 8 0 14 0 6:30 PM 0 56 12 0 10 54 0 0 1 0 9 0 13 0 6:45 PM 0 52 8 0 8 53 0 0 0 0 0 9 0 13 0 6:45 PM 0 52 8 0 8 53 0 0 0 0 0 3 1 8 0 TOTAL YOLUMES: <	4:30 PM 4:45 PM 5:00 PM	0 1 1	95 119 75 94	24 16 18 19	0 0 0	19 16 30 21 27	142 108 119 107	0 0 0 2	0 0 0 0	1 1 0 0	0 0 0 1	1	0 0 0 0	20 13 40 24 13	0 0 0 0	32 34 39 34 33	0 0 0 0	302 325 354 296 296
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6:15 PM 0 66 11 0 10 87 0 0 0 0 0 0 0 8 0 14 0 630 PM 0 56 12 0 10 54 0 0 1 1 0 1 0 9 0 13 0 6:45 PM 0 52 8 0 8 53 0 0 0 0 0 0 0 0 3 1 1 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	0 1 1 0 1	95 119 75 94 85 68	24 16 18 19 14 21	0 0 0 0 0	19 16 30 21 27 19 26	142 108 119 107 116 93	0 0 0 2 0 0	0 0 0 0 0	1 0 0 0	0 0 0 1 1 0 1	1 0 2 1 1 1 0	0 0 0 0 0	20 13 40 24 13 18 25	0 0 0 0 0	32 34 39 34 33 31 28	0 0 0 0 0	302 325 354 296 296 284 263
6:30 PM 6:45 PM 0 56 12 0 10 54 0 0 1 1 0 1 0 9 0 13 0 6:45 PM 0 52 8 0 8 53 0 0 0 0 0 0 0 0 0 3 1 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	0 1 1 0 1 0	95 119 75 94 85 68 83	24 16 18 19 14 21 9	0 0 0 0 0 0	19 16 30 21 27 19 26 24	142 108 119 107 116 93 106	0 0 0 2 0 0 0	0 0 0 0 0 0	1 0 0 0 0 0	0 0 0 1 1 0 1	1 0 2 1 1 1 0	0 0 0 0 0 0 0	20 13 40 24 13 18 25 22	0 0 0 0 0 0 0	32 34 39 34 33 31 28 18	0 0 0 0 0 0 0	302 325 354 296 296 284 263 263
6:45 PM 0 52 8 0 8 53 0 0 0 0 0 0 0 3 1 8 0 NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU TOTAL VOLUMES: 4 940 182 0 223 11.77 3 0 3 3 8 8 0 208 1 307 0 APPROACH %'s: 0.36% 83.48% 16.16% 0.00% 15.89% 83.89% 0.21% 0.00% 21.43% 21.43% 57.14% 0.00% 40.31% 0.19% 59.50% 0.00%	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM	0 1 1 0 1 0 0	95 119 75 94 85 68 83 66	24 16 18 19 14 21 9	0 0 0 0 0 0 0	19 16 30 21 27 19 26 24	142 108 119 107 116 93 106 64	0 0 0 2 0 0 0 0	0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0	0 0 0 1 1 0 1 0	1 0 2 1 1 1 0 0	0 0 0 0 0 0 0 0	20 13 40 24 13 18 25 22	0 0 0 0 0 0 0 0	32 34 39 34 33 31 28 18	0 0 0 0 0 0 0	302 325 354 296 296 284 263 263 191
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU TOTAL VOLUMES: 4 940 182 0 223 11.77 3 0 3 3 8 0 208 1 307 0 APPROACH %'s: 0.36% 83.48% 16.16% 0.00% 15.89% 83.89% 0.21% 0.00% 21.43% 21.43% 57.14% 0.00% 40.31% 0.19% 59.50% 0.00%	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM	0 1 1 0 1 0 0 0	95 119 75 94 85 68 83 66 66	24 16 18 19 14 21 9	0 0 0 0 0 0 0	19 16 30 21 27 19 26 24 13	142 108 119 107 116 93 106 64 87	0 0 0 2 0 0 0 0	0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0	0 0 0 1 1 0 1 0 0	1 0 2 1 1 1 0 0	0 0 0 0 0 0 0 0	20 13 40 24 13 18 25 22 13 8	0 0 0 0 0 0 0	32 34 39 34 33 31 28 18 23 14	0 0 0 0 0 0 0	302 325 354 296 296 284 263 263 191 196
TOTAL VOLUMES: 4 940 182 0 223 1177 3 0 3 3 8 0 208 1 307 0 APPROACH %'s: 0.36% 83.48% 16.16% 0.00% 15.89% 83.89% 0.21% 0.00% 21.43% 21.43% 57.14% 0.00% 40.31% 0.19% 59.50% 0.00%	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM	0 1 1 0 1 0 0 0 0	95 119 75 94 85 68 83 66 66 56	24 16 18 19 14 21 9 11 11 12	0 0 0 0 0 0 0 0	19 16 30 21 27 19 26 24 13 10	142 108 119 107 116 93 106 64 87 54	0 0 0 2 0 0 0 1 0 0	0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0	0 0 0 1 1 0 1 0 0 0	1 0 2 1 1 1 0 0 0 1	0 0 0 0 0 0 0 0	20 13 40 24 13 18 25 22 13 8 9	0 0 0 0 0 0 0 0	32 34 39 34 33 31 28 18 23 14	0 0 0 0 0 0 0 0	302 325 354 296 296 284 263 263 191 196 156
APPROACH %'s: 0.36% 83.48% 16.16% 0.00% 15.89% 83.89% 0.21% 0.00% 21.43% 21.43% 57.14% 0.00% 40.31% 0.19% 59.50% 0.00%	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM	0 1 1 0 1 0 0 0 0	95 119 75 94 85 68 83 66 66 56	24 16 18 19 14 21 9 11 11 11 12 8	0 0 0 0 0 0 0 0	19 16 30 21 27 19 26 24 13 10	142 108 119 107 116 93 106 64 87 54	0 0 0 2 0 0 0 1 0 0	0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0	0 0 0 1 1 0 1 0 0 0	1 0 2 1 1 1 1 0 0 0 1 0	0 0 0 0 0 0 0 0	20 13 40 24 13 18 25 22 13 8 9	0 0 0 0 0 0 0 0	32 34 39 34 33 31 28 18 23 14	0 0 0 0 0 0 0 0	302 325 354 296 296 284 263 263 191 196 156 133
	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	0 1 1 0 1 0 0 0 0 0	95 119 75 94 85 68 83 66 66 56 52	24 16 18 19 14 21 9 11 11 11 12 8	0 0 0 0 0 0 0 0 0	19 16 30 21 27 19 26 24 13 10 10 8	142 108 119 107 116 93 106 64 87 54 53	0 0 0 2 0 0 0 1 0 0 0	0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0	0 0 0 1 1 0 1 0 0 0 0 0	1 0 2 1 1 1 0 0 0 1 0 1 0	0 0 0 0 0 0 0 0 0	20 13 40 24 13 18 25 22 13 8 9 3	0 0 0 0 0 0 0 0 0 0 0	32 34 39 34 33 31 28 18 23 14 13 8	0 0 0 0 0 0 0 0 0	302 325 354 296 296 284 263 263 191 196 156 133
PEAK HD - 04:00 PM - 05:00 PM	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	0 1 1 0 1 0 0 0 0 0 0	95 119 75 94 85 68 83 66 66 56 52 NT 940	24 16 18 19 14 21 9 11 11 12 8 NR 182	0 0 0 0 0 0 0 0 0 0	19 16 30 21 27 19 26 24 13 10 8 SL 223	142 108 119 107 116 93 106 64 87 54 53 ST 1177	0 0 0 2 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 0 1 0 0 0 0 0	1 0 2 1 1 1 0 0 0 1 0 1 0	0 0 0 0 0 0 0 0 0 0	20 13 40 24 13 18 25 22 13 8 9 3 WL 208	0 0 0 0 0 0 0 0 0 0 0 0 0	32 34 39 34 33 31 28 18 23 14 13 8 WR 307	0 0 0 0 0 0 0 0 0	302 325 354 296 296 284 263 263 191 196 156 133
	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:35 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:30 PM 6:45 PM	0 1 1 0 1 0 0 0 0 0 0 0 0 NL 4 0.36%	95 119 75 94 85 68 83 66 66 56 52 NT 940 83.48%	24 16 18 19 14 21 9 11 11 12 8 NR 182 16.16%	0 0 0 0 0 0 0 0 0 0	19 16 30 21 27 19 26 24 13 10 8 SL 223	142 108 119 107 116 93 106 64 87 54 53 ST 1177	0 0 0 2 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 0 1 0 0 0 0 0	1 0 2 1 1 1 0 0 0 1 0 1 0	0 0 0 0 0 0 0 0 0 0	20 13 40 24 13 18 25 22 13 8 9 3 WL 208	0 0 0 0 0 0 0 0 0 0 0 0 0	32 34 39 34 33 31 28 18 23 14 13 8 WR 307	0 0 0 0 0 0 0 0 0	302 325 354 296 296 284 263 263 191 196 156 133 TOTAL 3059
	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:30 PM 6:45 PM	0 1 1 0 1 0 0 0 0 0 0 0 0 0 NL 4 0.36%	95 119 75 94 85 68 83 66 66 56 52 NT 940 83.48%	24 16 18 19 14 21 9 11 11 12 8 NR 182 16.16%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	19 16 30 21 27 19 26 24 13 10 10 8 SL 223 15.89%	142 108 119 107 116 93 106 64 87 54 53 ST 1177 83.89%	0 0 0 2 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0	0 0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 2 1 1 0 0 0 0	1 0 2 1 1 1 0 0 0 1 0 1 0 ER 8 57.14%	0 0 0 0 0 0 0 0 0 0 0 0	20 13 40 24 13 18 25 22 13 8 9 3 WL 208 40.31%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1	32 34 39 34 33 31 28 18 23 14 13 8 WR 307 59.50%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	302 325 354 296 296 284 263 191 196 156 133 TOTAL 3059
	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 6:30 PM 6:35 PM 6:30 PM 70 PM 6:45 PM	0 1 1 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	95 119 75 94 85 68 83 66 66 56 52 NT 940 83.48% 04:00 PM -	24 16 18 19 14 21 9 11 11 12 8 NR 182 16.16% 05:00 PM	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	19 16 30 21 27 19 26 24 13 10 10 8 SL 223 15.89%	142 108 119 107 116 93 106 64 87 54 53 ST 1177 83.89%	0 0 0 2 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 0 0 0 0 0 0 0	1 0 2 1 1 1 0 0 0 1 0 1 0 0 1 0 0 1 0 0 1 4 4 4 5 7 1 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0 0 0 0 0 0 0 0 0 0 0 0 0	20 13 40 24 13 18 25 22 13 8 9 3 WL 208 40.31%	0 0 0 0 0 0 0 0 0 0 0 0 0 1 1	32 34 39 34 33 31 28 18 23 14 13 8 WR 307 59,50%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	302 325 354 296 296 284 263 263 191 196 156 133 TOTAL 3059
0.831 0.926 0.875 0.747	4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 6:30 PM 6:35 PM 6:30 PM 70 PM 6:45 PM	0 1 1 0 1 0 0 0 0 0 0 0 0 0 NL 4 0.36%	95 119 75 94 85 68 83 66 66 65 52 NT 940 83.48% 04:00 PM - 370	24 16 18 19 14 21 9 11 11 12 8 NR 182 16.16% 05:00 PM 77 0.802	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	19 16 30 21 27 19 26 24 13 10 10 8 SL 223 15.89%	142 108 119 107 116 93 106 64 87 54 53 ST 1177 83.89%	0 0 0 2 0 0 0 0 1 1 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 0	1 0 2 1 1 1 0 0 0 1 0 1 0 0 1 0 0 ER 8 57.14%	0 0 0 0 0 0 0 0 0 0 0 0 0	20 13 40 24 13 18 25 22 13 8 9 3 WL 208 40.31%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	32 34 39 34 33 31 28 18 23 14 13 8 WR 307 59.50%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	302 325 354 296 296 284 263 191 196 156 133 TOTAL 3059

Location: US 17/US 211/Broadview Ave & Oak Springs Dr

City: Warrenton Control: 2-Way Stop(EB/WB)

Project ID: 23-260020-008 **Date:** 2/9/2023 Data - Cars US 17/US 211/Broadview Ave US 17/US 211/Broadview Ave Oak Springs Dr NS/EW Streets Oak Springs Dr NORTHBOUND SOUTHBOUND EASTBOUND WESTBOUND AM 70 73 100 128 197 208 264 353 248 214 188 227 WU 6:00 AM 6:15 AM 35 47 45 57 67 28 36 56 106 81 71 107 89 72 59 88 6:30 AM 6:45 AM 7:00 AM 7:15 AM 6 13 18 9 12 20 22 23 22 9 12 17 22 25 26 19 14 11 15 14 18 40 26 20 12 10 7:30 AM 7:45 AM 8:00 AM 117 146 67 52 56 58 21 17 31 8:15 AM 8:30 AM 8:45 AM SU 0 0.00% EL 0 0.00% EU TOTAL VOLUMES APPROACH %'s PEAK HR PEAK HR VOL 782 80.87% 7:30 AM 1 0.10% 821 83.43% 4 0.41% 1 50.00% 1 50.00% 0.009 2270 TOTAL 104 0 0.650 0.808 339 1 0.792 0.250 0.833 90 0.865 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 1 0.250 1079 0.654 (0.698 0.836 0.250 0.000 0.716 0.250 PEAK HR FACTOR 0.764 SOUTHBOUND NORTHBOUND FASTROLIND PM 2 ST 124 134 105 116 105 115 92 105 64 86 53 52 296 312 345 287 291 281 262 260 190 195 154 131 SL 19 16 30 20 27 19 26 24 13 10 10 8 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 80 93 115 19 22 15 18 18 14 21 8 11 20 12 40 24 13 18 25 22 13 71 93 83 68 82 65 66 56 51 31 28 18 23 5:30 PM 5:45 PM 6:00 PM 6:15 PM 14 13 8 11 0 0 0 6:30 PM 6:45 PM 11 8 0 0 1 0 WL 207 40.51% SL 222 16.13% TOTAL VOLUMES 923 83.68% 1151 83.65% 0 303 59.30% 3 21.43% 3004 APPROACH %'s PEAK HR PEAK HR VOL TOTAL 85 0.708 479 0.894 96 0.600 136 0.895 0.000 4 0.500 0 0.000 0 0.000 0 0.000 1240 2 0.500 0.780 0.841 0.250 0.000 0.500 0.250 PEAK HR FACTOR 0.899

Location: US 17/US 211/Broadview Ave & Oak Springs Dr City: Warrenton Control: 2-Way Stop(EB/WB)

Project ID: 23-260020-008

Control:	2-Way Stop	(EB/WB)						Data	u.					Date:	2/9/2023		
i								Data	- 111								1
NS/EW Streets:	US 1	17/US 211/E	Broadview A	ive	US 1	7/US 211/E	Broadview A	ive		Oak Sp	rings Dr			Oak Spr	ings Dr		
		NORTH	BOUND			SOUTH		'		EAST	BOUND				BOUND		
AM	1	2	1	0	1	2	0	0	0	1	0	0	1	0	1	0	TOTAL
6:00 AM	NL 0	NT 3	NR 0	NU 0	SL 0	ST	SR 0	SU	EL 0	ET	ER 0	EU 0	WL 0	WT 0	WR 0	WU 0	TOTAL 4
6:15 AM	0	3	0	0	0	1	0	0	0	Ü	0	0	0	0	0	0	3
6:30 AM	0	3	Ů.	0	U	2	0	0	0	Ü	U	0	0	0	0	0	
6:30 AM 6:45 AM	0	2	1	0	1	3	0	0	0	Ü	0	0	0	U	0	0	6 7
7:00 AM	0		2	0	0	3		0	0	<u>V</u>	0	0	0	0	0	0	18
	0	8	2		U	<u> </u>	1			Ü	0			U			
7:15 AM	0	4	U	0	1	/	0	0	0	Ü	•	0	0	U	0	0	12
7:30 AM	•	4	Ů.	0	0	8	0	0	0	0	0	0	0	0	0	0	12
7:45 AM	0	6	1	0	2	1	0	0	0	0	0	0	0	0	1	0	11
8:00 AM	0	6	0	0	3	1	0	0	0	0	0	0	0	0	0	0	10
8:15 AM	0	7	0	0	0	6	0	0	0	0	0	0	0	0	0	0	13
8:30 AM	0	4	1	0	0	15	0	0	0	0	0	0	0	0	0	0	20
8:45 AM	0	3	0	0	1	5	0	0	0	0	0	0	0	0	0	0	9
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	53	5	0	9	56	1	0	0	0	0	0	0	0	1	0	125
APPROACH %'s:	0.00%	91.38%	8.62%	0.00%	13.64%	84.85%	1.52%	0.00%					0.00%	0.00%	100.00%	0.00%	
PEAK HR:		07:30 AM -	08:30 AM														TOTAL
PEAK HR VOL :	0	23	1	0	5	16	0	0	0	0	0	0	0	0	1	0	46
PEAK HR FACTOR :	0.000	0.821	0.250	0.000	0.417	0.500	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.250	0.000	
· LAK IIK I AGI GK I	0.000	0.8		0.000	0.117	0.6		0.000	0.000	0.000	0.000	0.000	0.000	0.2		0.000	0.885
		NODTU	IBOUND			SOUTH	DOLIND			FACT	BOUND			MECT	BOUND		
PM			DOUND	0				0		EASI	0 O	0		0		0	
PIVI	1 NL	2 NT	NR	NU	1 SL	2 ST	0 SR	0 SU	0 EL	ET	ER.	0 EU	1 WL	WT	1 WR	WU	TOTAL
4:00 PM	0 0	1 1	0	0	0 0	4	0 0	0	0	0	0 0	0	O O	0	1 VVK	0	
4:00 PM 4:15 PM	0	1	U		0	8	-	0	0	U	0	0	U	U	1		6
4:15 PM 4:30 PM	0	4	2	0	0	8 3	0	0	0	Ü	0	0	0	U	U	0	13
	•	4	1	0	U	3	•			Ü	0			U	1		9
4:45 PM	0	4	0	0	1		0	0	0	0		0	0	0	<u>i</u>	0	9
5:00 PM	0	1	1	0	0	2	0	0	0	0	0	0	0	U	1	0	5
5:15 PM	0	2	0	0	0	1	0	0	0	0	0	0	0	U U	0	0	3

		NORTH	DOUIND			300111	DOUIND			LAST	DOUIND			WESTE	OUITE		
PM	1	2	1	0	1	2	0	0	0	1	0	0	1	0	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	1	0	0	0	4	0	0	0	0	0	0	0	0	1	0	6
4:15 PM	0	2	2	0	0	8	0	0	0	0	0	0	1	0	0	0	13
4:30 PM	0	4	1	0	0	3	0	0	0	0	0	0	0	0	1	0	9
4:45 PM	0	4	0	0	1	3	0	0	0	0	0	0	0	0	1	0	9
5:00 PM	0	1	1	0	0	2	0	0	0	0	0	0	0	0	1	0	5
5:15 PM	0	2	0	0	0	1	0	0	0	0	0	0	0	0	0	0	3
5:30 PM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	1
5:45 PM	0	1	1	0	0	1	0	0	0	0	0	0	0	0	0	0	3
6:00 PM	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
6:15 PM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	1
6:30 PM	0	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	2
6:45 PM	0	1	0	0	0	1	0	0	0	0	0	0	0	0	0	0	2
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	17	6	0	1	26	0	0	0	0	0	0	1	0	4	0	55
APPROACH %'s:	0.00%	73.91%	26.09%	0.00%	3.70%	96.30%	0.00%	0.00%					20.00%	0.00%	80.00%	0.00%	
PEAK HR :	(04:00 PM -	05:00 PM														TOTAL
PEAK HR VOL :	0	11	3	0	1	18	0	0	0	0	0	0	1	0	3	0	37
PEAK HR FACTOR:	0.000	0.688	0.375	0.000	0.250	0.563	0.000	0.000	0.000	0.000	0.000	0.000	0.250	0.000	0.750	0.000	0.712
		0.70	00			0.5	94							1.0	00		0.712

Location: US 17/US 211/Broadview Ave & Oak Springs Dr City: Warrenton Control: 2-Way Stop(EB/WB)

Project ID: 23-260020-008 Date: 2/9/2023

-								Data -	Bikes								
NS/EW Streets:	US	5 17/US 211,	Broadview	Ave	US	17/US 211/	Broadview	Ave		Oak Sp	rings Dr			Oak Sp	rings Dr		
		NORTI	HBOUND			SOUTH	IBOUND			EAST	BOUND			WEST	BOUND		
AM	1	2	1	0	1	2	0	0	0	1	0	0	1	0	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
APPROACH %'s:																	
PEAK HR :		07:30 AM	- 08:30 AM					·		·	<u> </u>	·		·	·	·	TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR:	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
									-								

		NORT	HBOUND			SOUT	HBOUND			EAST	BOUND			WEST	BOUND		
PM	1	2	1	0	1	2	0	0	0	1	0	0	1	0	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR :		04:00 PM	- 05:00 PM					·			·			·		·	TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	

National Data & Surveying Services Intersection Turning

Location: US 17/US 211/Broadview Ave & Oak Springs Dr Project ID: 23-260020-008 City: Warrenton Date: 2/9/2023

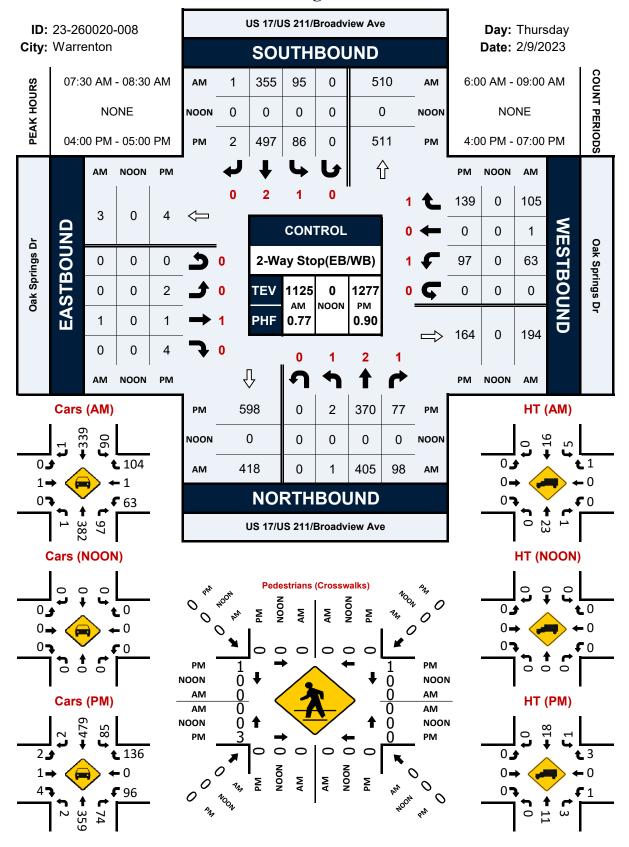
Data - Pedestrians (Crosswalks)

NS/EW Streets:	•	.1/Broadview ve	•	11/Broadview ve	Oak Spi		Oak Spi	rings Dr	
AM	_	'H LEG		TH LEG		LEG		Γ LEG	TOTAL
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
6:00 AM	_	0	0	0	0	0	0	0	0
6:15 AM	_	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0
6:45 AM	0	0	0	0	0	0	1	0	1
7:00 AM	0	0	0	0	0	0	0	1	1
7:15 AM	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	1	0	0	0	1
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	0	0	0	0	1	0	1	1	3
APPROACH %'s:					100.00%	0.00%	50.00%	50.00%	
PEAK HR:	07:30 AM	- 08:30 AM							TOTAL
PEAK HR VOL : PEAK HR FACTOR :	0	0	0	0	0	0	0	0	0

PM	NORT	TH LEG	SOUT	'H LEG	EAS ⁻	Γ LEG	WES	Γ LEG	
PIVI	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	1	1	2
4:30 PM	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	1	2	0	3
5:00 PM	0	1	0	0	0	0	0	1	2
5:15 PM	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	1	0	1
5:45 PM	0	0	0	0	0	0	1	0	1
6:00 PM	0	0	0	0	3	0	0	0	3
6:15 PM	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	0
6:45 PM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	0	1	0	0	3	1	5	2	12
APPROACH %'s:	0.00%	100.00%			75.00%	25.00%	71.43%	28.57%	
PEAK HR :	04:00 PM	- 05:00 PM		·					TOTAL
PEAK HR VOL :	0	0	0	0	0	1	3	1	5
PEAK HR FACTOR :						0.250	0.375	0.250	0.417
					0	250	0.5	500	0.417

US 17/US 211/Broadview Ave & Oak Springs Dr

Peak Hour Turning Movement Count



Location: US 17/US 211/Broadview Ave & Warrenton Village North Dwy City: Warrenton
Control: 1-Way stop(WB)

Data - Total

Project ID: 23-260020-009 Date: 2/9/2023

_																	
NS/EW Streets:	US 1	7/US 211/B	roadview A	ve	US 1	7/US 211/B	roadview A	ve	Warı	enton Villa	ge North Dv	vy	Warr	enton Villag	ge North D	wy	
		NORTHE	BOLIND			SOUTHE	ROLIND			EASTB	OLIND			WESTB	OLIND		
AM	1	2	1	0	1	2	0	0	0	1	0	0	1	0.5	0.5	0	
AIVI .	NL	NT	NR	NU	SL	ST	SR	SU	ĔĹ	ĒŤ	ER	EU	WL	WT	WR	WU	TOTAL
6:00 AM	0	38	1	0	0	28	1	0	0	0	1	0	1	0	0	0	70
6:15 AM	Ô	41	ō	ő	ő	31	Ō	Ö	ő	0	ō	0	ō	0	Ö	Ö	72
6:30 AM	Ö	51	Ö	ő	1	43	Ö	ő	Ö	0	Ô	0	Ö	Ö	0	Ö	95
6:45 AM	Ô	52	0	ő	î	64	0	ő	ő	0	Ô	0	Ö	0	ĭ	Ö	118
7:00 AM	6	78	0	0	2	123	0	0	0	0	1 i	0	2	0	2	0	214
7:15 AM	1	84	ĭ	ő	0	107	0	ő	ő	ň	ī	0	ō	0	ī	ő	195
7:30 AM	2	153	i	0	3	82	Ō	Ō	ō	Ō	ō	0	Ö	1	Ō	0	242
7:45 AM	7	169	2	ŏ	4	118	ĭ	ŏ	ŏ	ŏ	ŏ	ŏ	ĭ	ō	8	ŏ	310
8:00 AM	3	89	5	0	4	106	1	0	0	0	0	0	3	0	5	0	216
8:15 AM	1	77	2	ō	4	95	1	Ō	ō	Ō	3	0	i	Ō	5	0	189
8:30 AM	4	75	4	ō	3	92	ī	ō	ō	Ō	2	ō	2	ō	5	ō	188
8:45 AM	8	83	1	ō	ī	116	0	0	2	Ō	4	0	4	Ō	5	Ō	224
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	32	990	17	0	23	1005	5	0	2	0	12	0	14	1	32	0	2133
	3.08%	95.28%	1.64%	0.00%	2.23%	97.29%	0.48%	0.00%	14.29%	0.00%	85.71%	0.00%	29.79%	2.13%	68.09%	0.00%	
APPROACH % S :1																	TOTAL
APPROACH %'s : PEAK HR :		07:15 AM - (
		17:15 AM - 0	9	0	11	413	2	0	0	0	1	0	4	1	14	0	963
PEAK HR :	(0 0.000	11 0.688	413 0.875	2 0.500	0.000	0 0.000	0 0.000	1 0.250	0.000	4 0.333	1 0.250	14 0.438	0 0.000	
PEAK HR : PEAK HR VOL :	13	495	9 0.450				0.500				0.250				0.438		963 0.777
PEAK HR : PEAK HR VOL :	13	495 0.732 0.72	9 0.450 26			0.875 0.86	0.500 6			0.000	0.250 60			0.250 0.52	0.438 !8		
PEAK HR : PEAK HR VOL : PEAK HR FACTOR :	13 0.464	495 0.732 0.72 NORTHE	9 0.450 26	0.000	0.688	0.875 0.86	0.500 6 BOUND	0.000	0.000	0.000	0.250 60 OUND	0.000	0.333	0.250 0.52 WESTB	0.438 !8	0.000	
PEAK HR : PEAK HR VOL :	13 0.464	495 0.732 0.72 NORTHE	9 0.450 26 BOUND 1	0.000	0.688	0.875 0.86 SOUTHE 2	0.500 66 BOUND 0	0.000	0.000	0.000 0.25 EASTB	0.250 60 OUND 0	0.000	0.333	0.250 0.52 WESTB 0.5	0.438 88 OUND 0.5	0.000	0.777
PEAK HR: PEAK HR VOL: PEAK HR FACTOR:	13 0.464 1 NL	495 0.732 0.72 NORTHE 2 NT	9 0.450 26 BOUND 1 NR	0.000 0 NU	0.688 1 SL	0.875 0.86 SOUTHE 2 ST	0.500 66 BOUND 0 SR	0.000 O SU	0.000 0 EL	0.000 0.25 EASTB 1 ET	0.250 50 OUND 0 ER	0.000 0 EU	0.333 1 WL	0.250 0.52 WESTB 0.5 WT	0.438 28 OUND 0.5 WR	0.000 0 WU	0.777 TOTAL
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM	13 0.464 1 NL 3	495 0.732 0.72 NORTHE 2 NT 87	9 0.450 26 BOUND 1	0.000	0.688 1 SL 17	0.875 0.86 SOUTHE 2 ST 131	0.500 66 BOUND 0 SR 2	0.000 0 SU 0	0.000 0 EL 2	0.000 0.25 EASTB	0.250 50 OUND 0 ER 4	0.000 0 EU 0	0.333 1 WL 11	0.250 0.52 WESTB 0.5 WT	0.438 28 OUND 0.5 WR 11	0.000 WU 0	0.777 TOTAL 275
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM	13 0.464 1 NL 3 5	495 0.732 0.72 NORTHE 2 NT 87 104	9 0.450 26 BOUND 1 NR 6 1	0.000 0 NU 0 1	0.688 1 SL 17 8	0.875 0.86 SOUTHE 2 ST 131 146	0.500 66 BOUND 0 SR 2	0.000 0 SU 0 0	0.000 0 EL 2 2	0.000 0.25 EASTB 1 ET	0.250 00 OUND 0 ER 4 3	0.000 0 EU 0 0	0.333 1 WL 11 3	0.250 0.52 WESTB 0.5 WT 1 0	0.438 28 OUND 0.5 WR 11 13	0.000 0 WU 0 0	0.777 TOTAL 275 287
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PIV 4:00 PM 4:15 PM 4:30 PM 4:30 PM	13 0.464 1 NL 3 5 2	495 0.732 0.72 NORTHE 2 NT 87 104 124	9 0.450 26 BOUND 1 NR 6 1 8	0.000 0 NU 0 1	0.688 1 SL 17 8 8	0.875 0.86 SOUTHE 2 ST 131 146 140	0.500 66 BOUND 0 SR 2 1	0.000 0 SU 0 0	0.000 0 EL 2 2 4	0.000 0.25 EASTB 1 ET 0 0	0.250 50 OUND 0 ER 4 3 5	0.000 0 EU 0 0	0.333 1 WL 11 3 10	0.250 0.52 WESTB 0.5 WT 1 0	0.438 28 OUND 0.5 WR 11 13 8	0.000 0 WU 0 0	0.777 TOTAL 275 287 312
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PIM 4:00 PM 4:15 PM 4:30 PM 4:45 PM	13 0.464 1 NL 3 5 2 3	495 0.732 0.722 NORTHE 2 NT 87 104 124 85	9 0.450 26 BOUND 1 NR 6 1 8	0.000 0 NU 0 1 1 0	0.688 1 SL 17 8 8 7	0.875 0.86 SOUTHE 2 ST 131 146 140 135	0.500 66 BOUND 0 SR 2 1 1	0.000 0 SU 0 0 0 0 1	0.000 0 EL 2 2 4 2	0.000 0.25 EASTB 1 ET 0	0.250 00 00 00 ER 4 3 5 5	0.000 0 EU 0 0 0 0	0.333 1 WL 11 3 10 9	0.250 0.52 WESTB 0.5 WT 1 0 0	0.438 88 OUND 0.5 WR 11 13 8 5	0.000 WU 0 0 0	0.777 TOTAL 275 287 312 254
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	13 0.464 1 NL 3 5 2 3	495 0.732 0.722 NORTHE 2 NT 87 104 124 85 102	9 0.450 26 BOUND 1 NR 6 1 8 0	0.000 0 NU 0 1 1 0 0	0.688 1 SL 17 8 8 7 9	0.875 0.86 SOUTHE 2 ST 131 146 140 135	0.500 66 BOUND 0 SR 2 1 1 2	0.000 0 SU 0 0 0 1	0.000 0 EL 2 2 4 2 3	0.000 0.25 EASTB 1 ET 0 0	0.250 00 00 00 ER 4 3 5 5 6	0.000 0 EU 0 0 0 0	0.333 1 WL 11 3 10 9 6	0.250 0.52 WESTB 0.5 WT 1 0 0	0.438 88 OUND 0.5 WR 11 13 8 5	0.000 WU 0 0 0 0	0.777 TOTAL 275 287 312 254 255
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PIM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	13 0.464 1 NL 3 5 2 3 5 8	495 0.732 0.722 NORTHE 2 NT 87 104 124 85 102 91	9 0.450 26 BOUND 1 NR 6 1 8 0	0.000 NU 0 1 1 0 0 0 0	0.688 1 SL 17 8 8 7 9 12	0.875 0.86 SOUTHE 2 ST 131 146 140 135 108 121	0.500 6 BOUND 0 SR 2 1 1 2 4 1	0.000 0 SU 0 0 0 1 0 0	0.000 EL 2 2 4 2 3 1	0.000 0.25 EASTB 1 ET 0 0	0.250 00 00 00 ER 4 3 5 5 6 6	0.000 EU 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9	0.250 0.52 WESTB 0.5 WT 1 0 0 0	0.438 28 OUND 0.5 WR 11 13 8 5 9 7	0.000 WU 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:34 PM 5:00 PM 5:15 PM 5:30 PM	13 0.464 1 NL 3 5 2 3 5 8 5	495 0.732 0.722 NORTHE 2 NT 87 104 124 85 102 91 83	9 0.450 26 BOUND 1 NR 6 1 8 0 2 1 3	0.000 0 NU 0 1 1 0 0 0 0	0.688 1 SL 17 8 8 7 9 12 5	0.875 0.865 SOUTHE 2 ST 131 146 140 135 108 121 114	0.500 66 BOUND 0 SR 2 1 1 2 4 1 0	0.000 0 SU 0 0 0 1 0 0 0	0.000 EL 2 2 4 2 3 1 0	0.000 0.25 EASTB 1 ET 0 0 1 0 1 1	0.250 00 00 00 ER 4 3 5 5 6	0.000 0 EU 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9 8	0.250 0.52 WESTB 0.5 WT 1 0 0 0 0	0.438 88 OUND 0.5 WR 11 13 8 5 9 7 8	0.000 WU 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PIVI 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:30 PM 5:30 PM 5:30 PM 5:34 FM	13 0.464 1 NL 3 5 2 3 5 8 8 5	495 0.732 0.722 NORTHE 2 NT 87 104 124 85 102 91 83 81	9 0.450 26 BOUND 1 NR 6 1 8 0 2 1 3 3	0.000 NU 0 1 1 0 0 0 0	0.688 1 SL 17 8 8 7 9 12 5 13	0.875 0.86 SOUTHE 2 ST 131 146 140 135 108 121 114 113	0.500 66 BOUND 0 SR 2 1 1 2 4 1 0 1	0.000 SU 0 0 0 0 1 0 0 0	0.000 0 EL 2 4 2 3 1 0	0.000 0.25 EASTB 1 ET 0 0	0.250 00 00 00 ER 4 3 5 5 6 6 6 3 1	0.000 EU 0 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9 8 2	0.250 0.52 WESTB 0.5 WT 1 0 0 0 0	0.438 28 OUND 0.5 WR 11 13 8 5 9 7 8	0.000 WU 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230 226
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 6:00 PM	13 0.464 1 NL 3 5 2 3 5 8 5 2 2 5	NORTHE 2 NT 104 124 85 102 91 83 81 70	9 0.450 26 BOUND 1 NR 6 1 8 0 2 1 1 3 3 3	0.000 NU 0 1 1 0 0 0 0 0	0.688 1 SL 17 8 8 7 9 12 5 13 10	0.875 0.86 SOUTHE 2 ST 131 146 140 135 108 121 114 113 68	0.500 6 BOUND 0 SR 2 1 1 2 4 1 0 1 1	0.000 0 0 0 0 0 0 0 0	0.000 EL 2 2 4 2 3 1 0 0 2	0.000 0.29 EASTB 1 ET 0 0 1 0 1 1 0	0.250 00UND 0 ER 4 3 5 6 6 6 3 1 5	0.000 EU 0 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9 8 2 2	0.250 0.52 WESTB 0.5 WT 1 0 0 0 0 0	0.438 .8 OUND 0.5 WR 11 13 8 5 9 7 8 10 5	0.000 WU 0 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230 226 172
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:15 PM 6:00 PM 6:15 PM	13 0.464 1 NL 3 5 2 3 5 8 5 2 2 3	495 0.732 0.722 NORTHE 2 NT 87 104 124 85 102 91 83 81 70 62	9 0.450 266 BOUND 1 NR 6 1 8 0 2 1 3 3 3	0.000 NU 0 1 1 0 0 0 0 0 0 0 0	0.688 1 SL 17 8 8 7 9 12 5 13 10 7	0.875 0.86 SOUTHE 2 ST 131 146 140 135 108 121 114 113 68 88	0.500 6 BOUND 0 SR 2 1 1 2 4 1 0 0 1	0.000 0 0 0 0 0 0 0 0	0.000 0 EL 2 4 2 3 1 0 0 0	0.000 0.25 EASTB 1 ET 0 0 1 0 1 1 1 0 1	0.250 00 00 ER 4 3 5 5 6 6 3 1 5	0.000 EU 0 0 0 0 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9 8 2 2 9	0.250 0.52 WESTB 0.5 WT 1 0 0 0 0 0 0 0 0	0.438 .88 OUND 0.5 WR 11 13 8 5 9 7 8 10 5 15	0.000 WU 0 0 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230 226 172 184
PEAK HR : PEAK HR VOL: PEAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM	13 0.464 1 NL 3 5 2 3 5 8 5 2 5	495 0.732 0.722 NORTHE 2 NT 87 104 124 85 102 91 83 83 81 70 62 60	9 0.450 266 BOUND 1 NR 6 1 8 0 2 1 3 3 3 0 3	0.000 NU 0 1 1 0 0 0 0 0 0 0	0.688 1 SL 17 8 8 7 9 12 5 13 10 7 4	0.875 0.86 SOUTHE 2 ST 131 146 140 135 108 121 114 113 68 88 89 59	0.500 6 30UND 0 SR 2 1 1 2 4 1 0 1 1	0.000 0 0 0 0 0 0 0 0	0.000 0 EL 2 2 4 2 3 1 0 0 2 0	0.000 0.25 1 ET 0 0 1 0 1 1 1 1 0 0	0.250 10 DUND 0 ER 4 3 5 5 6 6 6 3 1 5 2 2	0.000 EU 0 0 0 0 0 0 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9 8 2 2 9 9	0.250 0.52 WESTB 0.5 WT 1 0 0 0 0 0 0 0 0	0.438 .8 OUND 0.5 WR 11 13 8 5 9 7 8 10 5 15 7	0.000 WU 0 0 0 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230 226 172 184 146
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:15 PM 6:00 PM 6:15 PM	13 0.464 1 NL 3 5 2 3 5 8 5 2 2 3	495 0.732 0.722 NORTHE 2 NT 87 104 124 85 102 91 83 81 70 62	9 0.450 266 BOUND 1 NR 6 1 8 0 2 1 3 3 3	0.000 NU 0 1 1 0 0 0 0 0 0 0 0	0.688 1 SL 17 8 8 7 9 12 5 13 10 7	0.875 0.86 SOUTHE 2 ST 131 146 140 135 108 121 114 113 68 88	0.500 6 BOUND 0 SR 2 1 1 2 4 1 0 0 1	0.000 0 0 0 0 0 0 0 0	0.000 0 EL 2 4 2 3 1 0 0 0	0.000 0.25 EASTB 1 ET 0 0 1 0 1 1 1 0 1	0.250 00 00 ER 4 3 5 5 6 6 3 1 5	0.000 EU 0 0 0 0 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9 8 2 2 9	0.250 0.52 WESTB 0.5 WT 1 0 0 0 0 0 0 0 0	0.438 .88 OUND 0.5 WR 11 13 8 5 9 7 8 10 5 15	0.000 WU 0 0 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230 226 172 184
PEAK HR : PEAK HR VOL: PEAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM	13 0.464 1 NL 3 5 2 2 3 5 8 8 5 2 2 5	495 0.732 0.722 0.722 NORTHE 2 NT 87 104 124 85 102 91 83 81 70 62 60 59	9 0.450 266 BOUND 1 NR 6 1 8 0 2 1 1 3 3 3 0 3 1	0.000 NU 0 1 1 0 0 0 0 0 0 0 0	1 SL 17 8 8 7 9 12 5 13 10 7 7 4 8 8	0.875 0.866 SOUTHE 2 ST 131 146 140 135 108 121 114 113 68 88 88 59 48	0.500 6 SOUND 0 SR 2 1 1 1 2 4 1 1 0 1 1 0	0.000 O	0.000 0 EL 2 2 4 4 2 3 1 0 0 2 0 1	0.000 0.25 1 1 ET 0 0 0 1 1 0 1 1 0 0 0 0 0 0	0.250 00 DUND 0 ER 4 3 5 5 6 6 6 3 1 5 2 2 2	0.000 0 EU 0 0 0 0 0 0 0 0 0 0	0.333 1 WL 111 3 100 9 6 6 9 8 2 2 9 9 3	0.250 0.52 0.52 WESTB 0.5 WT 1 0 0 0 0 0 0 0 0 0 0 0	0.438 .8 OUND 0.5 WR 11 13 8 5 7 8 10 5 15 7	0.000 WU 0 0 0 0 0 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230 226 172 184 146 129
PEAK HR : PEAK HR VOL: PEAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:30 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 6:35 PM 6:30 PM 6:45 PM	13 0.464 1 NL 3 5 2 3 5 8 5 2 5 1 0 3	495 0.732 0.722 0.722 NORTHE 2 NT 87 104 124 85 102 91 83 81 70 62 60 59	9 0.450 26 BOUND 1 NR 6 1 8 0 0 2 1 1 3 3 3 0 3 1	0.000 0 NU 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0	1 SL 17 8 8 7 9 12 5 13 10 7 4 8 8	0.875 0.866 SOUTHE 2 ST 131 140 135 108 121 114 113 68 88 88 99 48	0.500 66 SOUND 0 SR 2 1 1 2 4 1 0 1 1 0 1 0 SR	0.000 0 0 0 0 0 0 0 0	0.000 0 EL 2 2 4 2 3 1 0 0 2 0 1 0 0	0.000 0.25 EASTB 1 ET 0 0 1 1 1 1 0 0 1 1 0 0 1 1 0 0 1 1 0 0 1 1 0 0 0 1 0	0.250 0.00 DUND 0 ER 4 3 5 5 6 6 6 6 3 1 5 2 2 2 5	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9 8 2 2 9 9 3 WL	0.250 0.52 WESTB 0.5 WT 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0.438 8.8 OUND 0.5 WR 11 13 8 5 9 7 8 10 5 15 7 1	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230 226 172 184 146 129 TOTAL
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:15 PM 6:00 PM 6:15 PM 6:30 PM 6:35 PM 6:30 PM 6:45 PM C:45 PM	13 0.464	495 0.732 0.722 NORTHE 2 NT 87 104 124 85 102 91 83 81 70 62 60 59 NT	9 9 0.450 26 30UND 1 NR 6 1 8 0 2 1 3 3 3 0 3 1 1 NR 311	0.000 0 NU 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0.688 1 SL 17 8 8 7 9 12 5 13 10 7 4 8 8	0.875 0.866 SOUTHE 2 ST 131 146 140 135 108 121 114 113 68 88 88 59 48 ST 1271	0.500 6 80UND 0 SR 2 1 1 2 4 1 0 1 1 0 5 8 8 8 8 9 1 1 0 0 1 0 0 1 0 0 1 0 1 0 0 1 0 0 1 0 0 1 0	0.000 0 0 0 0 0 0 0 0	0.000 O EL 2 2 4 4 2 2 3 1 0 0 0 2 0 0 1 0 0 EL EL 17	0.000 0.25 EASTB 1 ET 0 0 1 1 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.250 000 DUND 0 ER 4 3 5 5 6 6 3 1 5 2 2 5 5 6 6 4 7 8 8 8 8 8 8 8 8 8 8 8 8 8	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WL 11 3 100 9 8 8 2 2 2 9 9 9 3 3 WL 81	0.250 0.52 0.52 0.52 WT 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.438 .88 OUND 0.5 WR 11 13 8 5 9 7 8 10 5 15 7 1	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230 226 172 184 146 129
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:15 PM 6:00 PM 6:35 PM 6:35 PM 6:45 PM	13 0.464 1 NL 3 5 2 3 5 8 5 2 2 3 5 1 0 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	495 0.732 0.722 NORTHE 2 NT 104 124 85 102 91 83 81 70 62 60 59 NT 1008 93.07%	9 0.450 26 30UND 1 NR 6 1 8 0 2 1 3 3 3 3 0 0 3 1 1 NR 31 2.86%	0.000 0 NU 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0	1 SL 17 8 8 7 9 12 5 13 10 7 4 8 8	0.875 0.866 SOUTHE 2 ST 131 140 135 108 121 114 113 68 88 88 99 48	0.500 66 SOUND 0 SR 2 1 1 2 4 1 0 1 1 0 1 0 SR	0.000 0 0 0 0 0 0 0 0	0.000 0 EL 2 2 4 2 3 1 0 0 2 0 1 0 0	0.000 0.25 EASTB 1 ET 0 0 1 1 1 1 0 0 1 1 0 0 1 1 0 0 1 1 0 0 1 1 0 0 0 1 0	0.250 0.00 DUND 0 ER 4 3 5 5 6 6 6 6 3 1 5 2 2 2 5	0.000 0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9 8 2 2 9 9 3 WL	0.250 0.52 WESTB 0.5 WT 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0.438 8.8 OUND 0.5 WR 11 13 8 5 9 7 8 10 5 15 7 1	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230 226 172 184 146 129 TOTAL 2728
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:30 PM 5:30 PM 6:30 PM 6:30 PM 6:30 PM 6:45 PM 7 PM 6:45 PM 6:45 PM 7 PM 6:45 PM	13 0.464 1 NL 3 5 2 3 5 8 5 5 2 2 3 3 5 1 0 0 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	495 0.732 0.722 NORTHE 2 NT 104 124 85 102 91 83 81 102 91 91 83 81 70 62 60 60 59 NT 100 87	9 9 0.450 26 30UND 1 NR 6 1 8 0 0 2 1 1 3 3 3 0 3 1 1 NR 31 1 2.86% 05:00 PM	0.000 0 NU 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0.688 1 SL 17 8 8 7 9 12 5 13 10 7 4 8 SL 108 7,75%	0.875 0.865 SOUTHE 2 ST 131 146 140 135 108 121 114 113 68 88 88 59 48 ST 1271 91.18%	0.500 6 80UND 0 SR 2 1 1 2 4 1 1 0 1 1 0 1 1 0 SR 1 1 1 0 0 1 1 0 0 1 0 1 0 1 0 0 1 0 0 1 0	0.000 0 0 0 0 0 0 0 0	0 EL 2 2 4 4 2 3 1 0 0 0 2 0 1 0 1 0	0.000 0.25 EASTB 1 ET 0 0 1 1 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0	0.250 00000000000000000000000000000000000	0.000 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9 8 2 2 2 9 9 9 3 WL 81 44.51%	0.250 0.520 0.52 WESTB 0.5 WT 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.438 .88 OUND 0.5 WR 11 13 8 5 9 7 8 10 5 15 17 1	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230 226 172 184 146 129 TOTAL 2728
PEAK HR : PEAK HR VOL : PEAK HR FACTOR : 4:00 PM 4:05 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 6:15 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM TOTAL VOLUMES : APPROACH %'s : PEAK HR : PEAK HR VOL :	13 0.464 1 NL 3 5 2 3 5 8 5 2 2 3 7 1 0 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	495 0.732 0.722 NORTHE 2 NT 104 124 85 102 91 83 81 70 62 60 59 NT 1008 93.07% 34:00 PM -1	9 9 0.450 26 6 1 1 8 8 0 2 1 3 3 3 0 0 3 1 1 2.86% 05:00 PM 15	0 NU 0 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.688 1 SL 17 8 8 8 7 9 12 5 13 110 7 4 4 8 8 SL SL 108 7.75%	0.875 0.866 SOUTHE 2 ST 131 146 140 135 108 121 114 113 68 88 88 59 48 ST 1271 91.18%	0.500 6 SOUND 0 SR 2 1 1 2 4 1 0 1 1 0 SR 1 4 1 0 SR 1 1 0 SR 4 1 1 0 SR 4 1 1 0 6 6 6 6 7 8 8 8 8 8 8 8 8 8 8 8 8 8	0.000 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 EL 2 2 4 2 3 1 0 0 2 0 1 0 EL 17 24.64%	0.000 0.25 EASTB ET 0 0 1 1 1 0 1 1 0 0 0 ET 5 7.25%	0.250 60 00UND 0 ER 4 3 5 5 6 6 6 6 3 1 5 2 2 2 5 5 8 1	0.000 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9 8 8 2 2 9 9 3 3 WL 81 44.51%	0.250 0.52 0.52 WESTB 0.5 WT 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0.438 28 OUND 0.5 WR 11 13 8 5 9 7 8 10 5 15 7 1 WR 99 54.40%	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.777 TOTAL 275 287 312 254 255 258 230 226 172 184 146 129 TOTAL 2728 TOTAL 1128
PEAK HR: PEAK HR VOL: PEAK HR FACTOR: 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:30 PM 5:30 PM 6:30 PM 6:30 PM 6:30 PM 6:45 PM 7 PM 6:45 PM 6:45 PM 7 PM 6:45 PM	13 0.464 1 NL 3 5 2 3 5 8 5 5 2 2 3 3 5 1 0 0 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	495 0.732 0.722 NORTHE 2 NT 104 124 85 102 91 83 81 102 91 91 83 81 70 62 60 60 59 NT 100 87	9 9 0.450 26 0.450 21 1 NR 6 1 1 8 0 2 1 1 3 3 3 1 1 NR 31 1 2.86% 05:00 PM 15 0.469	0.000 0 NU 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0.688 1 SL 17 8 8 7 9 12 5 13 10 7 4 8 SL 108 7,75%	0.875 0.865 SOUTHE 2 ST 131 146 140 135 108 121 114 113 68 88 88 59 48 ST 1271 91.18%	0.500 6 30UND 0 SR 2 1 1 2 4 1 1 0 1 1 0 SR 1 1 0 1 1 0 1 1 0 0 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0 0 0 0 0 0 0 0	0 EL 2 2 4 4 2 3 1 0 0 0 2 0 1 0 1 0	0.000 0.25 EASTB 1 ET 0 0 1 1 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0	0.250 0.000 0.250 0.	0.000 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.333 1 WL 11 3 10 9 6 9 8 2 2 2 9 9 9 3 WL 81 44.51%	0.250 0.520 0.52 WESTB 0.5 WT 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.438 (28) OUND 0.5 (WR) 11 13 8 5 9 7 7 8 8 10 5 15 7 1 WR 99 54.40%	0.000 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.7777 TOTAL 275 287 3112 254 255 258 230 226 172 184 146 129 TOTAL 2728

Location: US 17/US 211/Broadview Ave & Warrenton Village North Dwy City: Warrenton
Control: 1-Way stop(WB)

Data - Cars

Project ID: 23-260020-009 **Date:** 2/9/2023

								Data	Cais								
NS/EW Streets:	US 1	7/US 211/E	Broadview A	ive	US 1	7/US 211/E	Broadview A	ive	War	renton Villa	ge North D	wy	Wan	renton Villa	ge North D	wy	
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTE	OUND		
AM	1	2	1	0	1	2	0	0	0	1	0	0	1	0.5	0.5	0	
Auvi	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
6:00 AM	0	35	1	0	0	28	0	0	0	0	0	0	1	0	0	0	65
6:15 AM	0	38	0	0	0	31	0	0	0	0	0	0	0	0	0	0	69
6:30 AM	0	48	0	0	1	41	0	0	0	0	0	0	0	0	0	0	90
6:45 AM	0	50	0	0	0	62	0	0	0	0	0	0	0	0	0	0	112
7:00 AM	6	68	0	0	2	117	0	0	0	0	0	0	2	0	2	0	197
7:15 AM	1	80	1	0	0	99	0	0	0	0	1	0	0	0	1	0	183
7:30 AM	2	149	1	0	3	74	0	0	0	0	0	0	0	1	0	0	230
7:45 AM	7	163	2	0	4	117	1	0	0	0	0	0	1	0	7	0	302
8:00 AM	3	83	5	0	4	105	1	0	0	0	0	0	3	0	5	0	209
8:15 AM	1	70	2	0	4	89	1	0	0	0	3	0	1	0	5	0	176
8:30 AM	4	71	2	0	3	77	1	0	0	0	2	0	2	0	4	0	166
8:45 AM	8	81	1	0	1	111	0	0	2	0	4	0	4	0	4	0	216
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	32	936	15	0	22	951	4	0	2	0	10	0	14	1	28	0	2015
APPROACH %'s:	3.26%	95.22%	1.53%	0.00%	2.25%	97.34%	0.41%	0.00%	16.67%	0.00%	83.33%	0.00%	32.56%	2.33%	65.12%	0.00%	
PEAK HR :)7:15 AM -															TOTAL
PEAK HR VOL:	13	475	9	0	11	395	2	0	0	0	1	0	4	1	13	0	924
PEAK HR FACTOR:	0.464	0.729	0.450	0.000	0.688	0.844	0.500	0.000	0.000	0.000	0.250	0.000	0.333	0.250	0.464	0.000	0.765
		0.7	22			0.8	36			0.25	50			0.56	53		0.703
		NORTH	BOUND			SOUTH				EASTB				WESTE			
PM	1	2	1	0	1	2	0	0	0	1	0	0	1	0.5	0.5	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	3	86	6 6	0	17	127	2	0	2	0	4	0	11	1	11	0	270
4:15 PM	3 5	86 102	6 1	0 1	17 8	127 137	2	0	2	0	4 3	0	11 3	1 0	11 11	0	270 274
4:15 PM 4:30 PM	3 5 2	86 102 119	6 1 8	0 1 1	17 8 8	127 137 137	2 1 1	0 0 0	2 2 4	0 0 1	4 3 5	0 0 0	11 3 10	1 0 0	11 11 8	0 0 0	270 274 304
4:15 PM 4:30 PM 4:45 PM	3 5 2 3	86 102 119 81	6 1 8 0	0 1 1 0	17 8 8 7	127 137 137 132	2 1 1 2	0 0 0 1	2 2 4 2	0 0 1 0	4 3 5 5	0 0 0 0	11 3 10 9	1 0 0 0	11 11 8 5	0 0 0 0	270 274 304 247
4:15 PM 4:30 PM 4:45 PM 5:00 PM	3 5 2 3	86 102 119 81 101	6 1 8	0 1 1 0	17 8 8 7	127 137 137 132 106	2 1 1	0 0 0 1	2 2 4 2	0 0 1	4 3 5 5	0 0 0 0	11 3 10 9	1 0 0	11 11 8 5	0 0 0 0	270 274 304 247 251
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	3 5 2 3	86 102 119 81 101 89	6 1 8 0 2 1	0 1 1 0 0	17 8 8 7 9	127 137 137 132 106 120	2 1 1 2 4 1	0 0 0 1 0	2 2 4 2 3 1	0 0 1 0	4 3 5 5 6 6	0 0 0 0 0	11 3 10 9 6 9	1 0 0 0 0	11 11 8 5 8 7	0 0 0 0 0	270 274 304 247 251 255
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	3 5 2 3 5 8 4	86 102 119 81 101 89 83	6 1 8 0 2 1 3	0 1 1 0 0 0 0	17 8 8 7 9 12 5	127 137 137 132 106 120 113	2 1 1 2	0 0 0 1 0 0 0	2 2 4 2 3 1	0 0 1 0	4 3 5 5	0 0 0 0 0	11 3 10 9 6 9	1 0 0 0 0	11 11 8 5 8 7 8	0 0 0 0 0	270 274 304 247 251 255 227
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM	3 5 2 3	86 102 119 81 101 89 83 80	6 1 8 0 2 1 3 3	0 1 1 0 0 0 0 0	17 8 8 7 9 12 5	127 137 137 132 106 120 113 112	2 1 1 2 4 1	0 0 0 1 0 0 0	2 2 4 2 3 1 0	0 0 1 0	4 3 5 5 6 6 2 1	0 0 0 0 0 0	11 3 10 9 6 9 8	1 0 0 0 0 0 0	11 11 8 5 8 7 8 7	0 0 0 0 0 0	270 274 304 247 251 255 227 223
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM	3 5 2 3 5 8 4	86 102 119 81 101 89 83 80 69	6 1 8 0 2 1 3 3	0 1 1 0 0 0 0 0	17 8 8 7 9 12 5 13	127 137 137 132 106 120 113 112 68	2 1 1 2 4 1 0 1	0 0 0 1 0 0 0 0	2 2 4 2 3 1 0 0	0 0 1 0 1 1 1 1 0	4 3 5 5 6 6 2 1	0 0 0 0 0 0 0	11 3 10 9 6 9 8 2	1 0 0 0 0 0 0 0 0	11 11 8 5 8 7 8 9	0 0 0 0 0 0 0	270 274 304 247 251 255 227 223 170
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM	3 5 2 3 5 8 4 2 4	86 102 119 81 101 89 83 80 69 62	6 1 8 0 2 1 3 3 3	0 1 1 0 0 0 0 0 0	17 8 8 7 9 12 5 13 10 7	127 137 137 132 106 120 113 112 68 87	2 1 1 2 4 1 0 1 1	0 0 0 1 0 0 0 0	2 2 4 2 3 1 0 0 2	0 0 1 0 1 1 1 1 0	4 3 5 5 6 6 2 1 5	0 0 0 0 0 0 0 0	11 3 10 9 6 9 8 2 2	1 0 0 0 0 0 0 0 0	11 11 8 5 8 7 8 9 5	0 0 0 0 0 0 0 0	270 274 304 247 251 255 227 223 170 183
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM	3 5 2 3 5 8 4 2 4 1	86 102 119 81 101 89 83 80 69 62 60	6 1 8 0 2 1 3 3 3 0 3	0 1 1 0 0 0 0 0 0 0	17 8 8 7 9 12 5 13 10 7	127 137 137 132 106 120 113 112 68 87 59	2 1 1 2 4 1 0 1 1 1 0	0 0 0 1 0 0 0 0 0	2 2 4 2 3 1 0 0 2 0	0 0 1 0 1 1 1 1 0 0	4 3 5 5 6 6 2 1 5 2 2	0 0 0 0 0 0 0 0	11 3 10 9 6 9 8 2 2 9	1 0 0 0 0 0 0 0 0	11 11 8 5 8 7 8 9 5 15 6	0 0 0 0 0 0 0 0 0	270 274 304 247 251 255 227 223 170 183 144
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM	3 5 2 3 5 8 4 2 4	86 102 119 81 101 89 83 80 69 62	6 1 8 0 2 1 3 3 3	0 1 1 0 0 0 0 0 0	17 8 8 7 9 12 5 13 10 7	127 137 137 132 106 120 113 112 68 87	2 1 1 2 4 1 0 1 1	0 0 0 1 0 0 0 0	2 2 4 2 3 1 0 0 2	0 0 1 0 1 1 1 1 0	4 3 5 5 6 6 2 1 5	0 0 0 0 0 0 0 0	11 3 10 9 6 9 8 2 2	1 0 0 0 0 0 0 0 0	11 11 8 5 8 7 8 9 5	0 0 0 0 0 0 0 0	270 274 304 247 251 255 227 223 170 183
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM	3 5 2 3 5 8 4 2 4 1	86 102 119 81 101 89 83 80 69 62 60	6 1 8 0 2 1 3 3 3 0 3	0 1 1 0 0 0 0 0 0 0	17 8 8 7 9 12 5 13 10 7 3 8	127 137 137 132 106 120 113 112 68 87 59	2 1 1 2 4 1 0 1 1 1 0	0 0 0 1 0 0 0 0 0	2 2 4 2 3 1 0 0 2 0	0 0 1 0 1 1 1 1 0 0	4 3 5 5 6 6 2 1 5 2 2	0 0 0 0 0 0 0 0	11 3 10 9 6 9 8 2 2 9	1 0 0 0 0 0 0 0 0	11 11 8 5 8 7 8 9 5 15 6	0 0 0 0 0 0 0 0 0	270 274 304 247 251 255 227 223 170 183 144
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM	3 5 2 3 5 8 4 2 4 1 0 3	86 102 119 81 101 89 83 80 69 62 60 58	6 1 8 0 2 1 3 3 3 0 3 1	0 1 1 0 0 0 0 0 0 0 0	17 8 8 7 9 12 5 13 10 7	127 137 137 132 106 120 113 112 68 87 59 47	2 1 1 2 4 1 0 1 1 0 1	0 0 0 1 0 0 0 0 0	2 2 4 2 3 1 0 0 0 2 0	0 0 1 0 1 1 1 1 0 1 0 0	4 3 5 6 2 1 5 2 2 5	0 0 0 0 0 0 0 0	11 3 10 9 6 9 8 2 2 9 9	1 0 0 0 0 0 0 0 0 0 0	11 11 8 5 8 7 8 9 5 15 6	0 0 0 0 0 0 0 0 0	270 274 304 247 251 255 227 223 170 183 144 127
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	3 5 2 3 5 8 4 2 4 1 0 3	86 102 119 81 101 89 83 80 69 62 60 58	6 1 8 0 2 1 3 3 3 0 3 1	0 1 1 0 0 0 0 0 0 0 0 0	17 8 8 7 9 12 5 13 10 7 3 8	127 137 137 132 106 120 113 112 68 87 59 47	2 1 1 2 4 1 0 1 1 0 1 0 1 0 SR	0 0 0 1 0 0 0 0 0 0	2 2 4 2 3 1 0 0 2 0 1 0	0 0 1 0 1 1 1 0 1 0 0 0	4 3 5 5 6 6 2 1 5 2 2 5	0 0 0 0 0 0 0 0 0	11 3 10 9 6 9 8 2 2 9 9	1 0 0 0 0 0 0 0 0 0 0 0	11 11 8 5 8 7 8 9 5 15 6 1	0 0 0 0 0 0 0 0 0 0	270 274 304 247 251 255 227 223 170 183 144 127
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:30 PM 6:30 PM 6:45 PM	3 5 2 3 5 8 4 2 4 1 0 3 NL 40 3.76%	86 102 119 81 101 89 83 80 69 62 60 58 NT 990 93.13%	6 1 8 0 2 1 3 3 3 0 3 1	0 1 1 0 0 0 0 0 0 0 0 0 0	17 8 8 7 9 12 5 13 10 7 3 8 SL	127 137 137 132 106 120 113 112 68 87 59 47 ST 1245	2 1 1 2 4 1 0 1 0 1 0 1 0 SR	0 0 0 1 0 0 0 0 0 0 0 0 0	2 2 4 2 3 1 0 0 0 2 0 1 0	0 0 1 0 1 1 1 1 0 0 0 0	4 3 5 6 6 2 1 5 2 2 5	0 0 0 0 0 0 0 0 0	11 3 10 9 6 9 8 2 2 9 3	1 0 0 0 0 0 0 0 0 0 0 0 0	11 11 8 5 8 7 8 9 5 15 6 1	0 0 0 0 0 0 0 0 0	270 274 304 247 251 255 227 223 170 183 144 127
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	3 5 2 3 5 8 4 2 4 1 0 3 NL 40 3.76%	86 102 119 81 101 89 83 80 69 62 60 58 NT 990 93.13%	6 1 8 0 2 1 3 3 3 0 3 1 NR 31 2.92%	0 1 1 0 0 0 0 0 0 0 0 0 0	17 8 8 7 9 12 5 13 10 7 3 8 SL	127 137 137 132 106 120 113 112 68 87 59 47 ST 1245	2 1 1 2 4 1 0 1 0 1 0 1 0 SR	0 0 0 1 0 0 0 0 0 0 0 0 0	2 2 4 2 3 1 0 0 0 2 0 1 0	0 0 1 0 1 1 1 1 0 0 0 0	4 3 5 6 6 2 1 5 2 2 5	0 0 0 0 0 0 0 0 0	11 3 10 9 6 9 8 2 2 9 3	1 0 0 0 0 0 0 0 0 0 0 0 0	11 11 8 5 8 7 8 9 5 15 6 1	0 0 0 0 0 0 0 0 0	270 274 304 247 251 255 227 223 170 183 144 127 TOTAL 2675
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:15 PM 6:15 PM 6:30 PM 6:45 PM TOTAL VOLUMES : APPROACH %'s:	3 5 2 3 5 8 4 4 2 4 1 0 0 3 NL 40 3.76%	86 102 119 81 101 89 83 80 69 62 60 58 NT 990 93.13%	6 1 8 0 2 1 3 3 3 3 0 3 1 NR 31 2.92%	0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	17 8 8 7 9 12 5 13 10 7 3 8 SL 107 7.83%	127 137 137 132 106 120 113 112 68 87 59 47 ST 1245 91.08%	2 1 1 2 4 1 0 0 1 1 1 0 SR 14 1.02%	0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 2 4 2 3 1 0 0 2 0 1 0 1 0 EL 17 25.00%	0 0 1 0 1 1 1 0 1 0 0 0 0 ET 5 7.35%	4 3 5 5 6 6 6 2 1 5 2 2 2 5 5 5 ER 46 67.65%	0 0 0 0 0 0 0 0 0 0 0 0	11 3 10 9 6 9 8 2 2 2 9 9 3 WL 81 45.76%	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	11 11 8 5 8 7 8 9 5 15 6 1 WR 94 53.11%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	270 274 304 247 251 255 227 170 183 144 127 TOTAL 2675

Location: US 17/US 211/Broadview Ave & Warrenton Village North Dwy

6:30 PM 6:45 PM

0.000

18

0.600

0.000

TOTAL VOLUMES

APPROACH %'s PEAK HR PEAK HR VOL

PEAK HR FACTOR

City: Warrenton Control: 1-Way stop(WB) **Project ID:** 23-260020-009 **Date:** 2/9/2023 Data - HT US 17/US 211/Broadview Ave US 17/US 211/Broadview Ave Warrenton Village North Dwy NS/EW Streets Warrenton Village North Dwy NORTHBOUND SOUTHBOUND EASTBOUND WESTBOUND AM TOTAL 6:00 AM 6:15 AM 3 5 6:30 AM 6:45 AM 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 6 17 12 12 8 7 13 22 8:15 AM 8:30 AM 6 15 5 8:45 AM ST 54 96.43% SU 0 0.00% EL 0 0.00% ER 2 100.00% EU TOTAL VOLUMES APPROACH %'s PEAK HR PEAK HR VOL 0.00% 0.00% 0 0.00% 0.00% 0 0.00% 4 100.00% 118 TOTAL 18 0.563 0 0.000 0.250 20 0.833 0.833 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 39 0.000 0.563 0.000 0.000 0.000 0.000 0.000 PEAK HR FACTOR 0.250 0.813 NORTHBOUND SOLITHBOLIND FASTROLIND PM TOTAL 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 13 8 0 0 0

0

0.00%

0.000

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0.000

0.528

0.00%

0.000

0

0.000

0

EL 0 0.00%

0 0.000

0

0.00%

0 0.000

1 100.00%

0.000

0

0.00%

0.000

0 0.00%

0.000

0

0.000

ō

5 100.00%

0.250

0 0.00%

0 0.000

2

53

TOTAL

33

0.635

Location: US 17/US 211/Broadview Ave & Warrenton Village North Dwy City: Warrenton
Control: 1-Way stop(WB)

Data - Bikes

Project ID: 23-260020-009 Date: 2/9/2023

NS/EW Streets:	US	17/US 211/	Broadview	Ave	US	17/US 211/	/Broadview	Ave	Wa	rrenton Vill	age North [Owy	Wa	rrenton Vill	age North D	Dwy	
		NORTH	HBOUND			SOUTH	HBOUND			EAST	BOUND			WEST	BOUND		
AM	1	2	1	0	1	2	0	0	0	1	0	0	1	0.5	0.5	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:00 AM 7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM 7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	Ô	0	Ö	Ö	Ö	Ö	Ö	Ö	0	Ö	Ô	ñ	0	0	n	Ö	0
8:30 AM	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	Ö	ŏ	ŏ	ŏ	Ö	ŏ	ŏ	ŏ	Ö
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
APPROACH %'s:																	
PEAK HR:			- 08:15 AM		_		•		_			•	_		•	•	TOTAL
PEAK HR VOL :	0	0 0.000	0 0.000	0.000	0.000	0 0.000	0.000	0.000	0.000	0.000	0.000	0 0.000	0.000	0.000	0 0.000	0 0.000	0
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
		NORTH	HBOUND			SOUTH	HBOUND			EAST	BOUND			WEST	BOUND		
PM	1	NORTH 2	HBOUND 1	0	1	2	0	0	0	EAST 1	BOUND 0	0	1	0.5	BOUND 0.5	0	
PM	NL	2 NT	1 NR	NU	SL	2 ST	0 SR	SU	EL	1 ET	0 ER	EU	WL	0.5 WT	0.5 WR	WU	TOTAL
4:00 PM	NL 0	NT 0	1 NR 0	NU 0	SL 0	ST 0	O SR O	SU 0	EL 0	1 ET 0	0 ER 0	EU 0	WL 0	0.5 WT 0	0.5 WR 0	WU 0	0
4:00 PM 4:15 PM	NL 0 0	2 NT 0 0	1 NR 0 0	NU 0 0	SL 0 0	2 ST 0 0	0 SR 0 0	SU 0 0	0 0	1 ET 0 0	0 ER 0 0	0 0	0 0	0.5 WT 0 0	0.5 WR 0 0	0 0	0
4:00 PM 4:15 PM 4:30 PM	0 0 0	2 NT 0 0 0	1 NR 0 0 0	0 0 0	SL 0 0 0	2 ST 0 0 0	0 SR 0 0	0 0 0	EL 0 0 0	1 ET 0 0 0	0 ER 0 0	0 0 0	0 0 0	0.5 WT 0 0 0	0.5 WR 0 0 0	0 0 0	0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM	NL 0 0 0 0	2 NT 0 0 0	1 NR 0 0 0 0	NU 0 0 0 0	SL 0 0 0 0	2 ST 0 0 0	0 SR 0 0 0	0 0 0 0	EL 0 0 0 0	1 ET 0 0 0 0	0 ER 0 0 0	0 0 0 0 0	WL 0 0 0 0	0.5 WT 0 0 0	0.5 WR 0 0 0	0 0 0 0	0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	NL 0 0 0 0	2 NT 0 0 0 0	1 NR 0 0 0 0	NU 0 0 0 0 0 0 0	SL 0 0 0 0 0	2 ST 0 0 0 0	0 SR 0 0 0 0	SU 0 0 0 0	0 0 0 0 0	1 ET 0 0 0 0	0 ER 0 0 0 0	EU 0 0 0 0	WL 0 0 0 0	0.5 WT 0 0 0 0	0.5 WR 0 0 0 0	WU 0 0 0 0	0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 0 0 0 0 0	2 NT 0 0 0 0 0	1 NR 0 0 0 0 0	NU 0 0 0 0 0	SL 0 0 0 0 0	2 ST 0 0 0 0 0	0 SR 0 0 0 0	SU 0 0 0 0 0	EL 0 0 0 0 0	1 ET 0 0 0 0 0	0 ER 0 0 0 0 0	0 0 0 0 0 0	WL 0 0 0 0 0	0.5 WT 0 0 0 0 0	0.5 WR 0 0 0 0 0	WU 0 0 0 0 0	0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 0 0 0 0	2 NT 0 0 0 0	1 NR 0 0 0 0 0 0	NU 0 0 0 0 0 0	SL 0 0 0 0 0 0	2 ST 0 0 0 0	0 SR 0 0 0 0 0	SU 0 0 0 0 0 0	EL 0 0 0 0 0 0	1 ET 0 0 0 0	0 ER 0 0 0 0	EU 0 0 0 0	WL 0 0 0 0	0.5 WT 0 0 0 0	0.5 WR 0 0 0 0	WU 0 0 0 0 0 0	0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 0 0 0 0 0 0	2 NT 0 0 0 0 0 0	1 NR 0 0 0 0 0	NU 0 0 0 0 0	SL 0 0 0 0 0	2 ST 0 0 0 0 0 0	0 SR 0 0 0 0	SU 0 0 0 0 0	EL 0 0 0 0 0	1 ET 0 0 0 0 0 0	0 ER 0 0 0 0 0	0 0 0 0 0 0 0	WL 0 0 0 0 0 0	0.5 WT 0 0 0 0 0	0.5 WR 0 0 0 0 0	WU 0 0 0 0 0	0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0	1 NR 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0	2 ST 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0	SU 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0	0 ER 0 0 0 0 0 0	0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0	0.5 WT 0 0 0 0 0 0	0.5 WR 0 0 0 0 0 0	WU 0 0 0 0 0 0	0 0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM	NL 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0	1 NR 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 ST 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WT 0 0 0 0 0 0 0 0	0.5 WR 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM	NL 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0	1 NR 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 ST 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WT 0 0 0 0 0 0 0 0 0	0.5 WR 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM	NL 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WT 0 0 0 0 0 0 0 0 0 0	0.5 WR 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:30 PM 5:30 PM 6:00 PM 6:30 PM 6:30 PM 6:45 PM	NL 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WT 0 0 0 0 0 0 0 0 0 0	0.5 WR 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:15 PM 6:15 PM 6:30 PM 6:45 PM TOTAL VOLUMES: APPROACH %s:	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:00 PM 5:30 PM 5:30 PM 6:00 PM 6:15 PM 6:00 PM 6:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR' 21	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:15 PM 6:15 PM 6:30 PM 6:45 PM TOTAL VOLUMES: APPROACH %s:	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.5 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

National Data & Surveying Services Intersection Turning

Location: US 17/US 211/Broadview Ave & Warrenton Village North Dwy
City: Warrenton

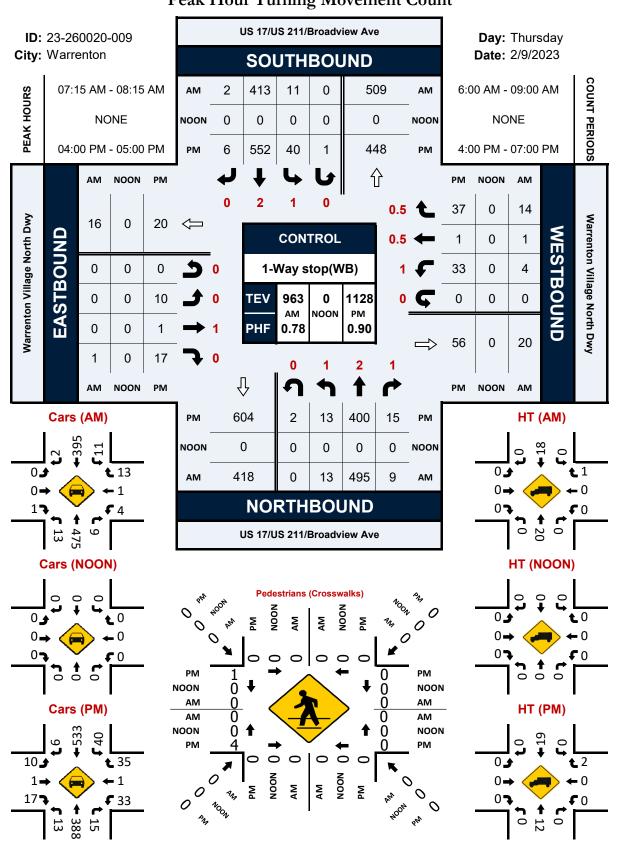
Novement Count
Project ID: 23-260020-009
Date: 2/9/2023

Data - Pedestrians (Crosswalks)

NS/EW Streets:	US 17/US 21	1/Broadview	US 17/US 2:	11/Broadview	Warrenton \	Village North	Warrenton \	/illage North	
NS/EW Streets:	A۱	<i>r</i> e	Α	ve	Di	wy	Dv	vy	
AM	NORT	H LEG	SOUT	TH LEG	EAST	Γ LEG	WES	Γ LEG	
Alvi	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
6:00 AM	0	0	0	0	0	0	0	0	0
6:15 AM	0	0	0	0	0	0	0	0	0
6:30 AM	0	0	0	0	0	0	0	0	0
6:45 AM	0	0	0	0	0	0	1	0	1
7:00 AM	0	0	0	0	0	0	0	1	1
7:15 AM	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0
8:45 AM	1	0	0	0	0	0	0	0	1
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	1	0	0	0	0	0	1	1	3
APPROACH %'s:	100.00%	0.00%					50.00%	50.00%	
PEAK HR:	07:15 AM -	08:15 AM							TOTAL
PEAK HR VOL:	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR:									

PM	NORT	ΓH LEG	SOUTH	1 LEG	EAST	LEG	WES	Γ LEG	
FIVI	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	1	1	2
4:30 PM	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	3	0	3
5:00 PM	0	0	2	0	0	0	0	1	3
5:15 PM	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0
6:00 PM	0	0	0	0	2	0	0	0	2
6:15 PM	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	0
6:45 PM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	0	0	2	0	2	0	4	2	10
APPROACH %'s:			100.00%	0.00%	100.00%	0.00%	66.67%	33.33%	
PEAK HR :	04:00 PM	- 05:00 PM							TOTAL
PEAK HR VOL :	0	0	0	0	0	0	4	1	5
PEAK HR FACTOR:							0.333	0.250	0.417
							0.4	117	0.417

US 17/US 211/Broadview Ave & Warrenton Village North Dwy Peak Hour Turning Movement Count



Location: US 17/US 211/Broadview Ave/Winchester St & Warrenton Village South Dwy/Broadview Ave
City: Warrenton
Control: 2-Way Stop(EB/WB)

Project ID: 23-260020-010 Date: 2/9/2023

									Total								
NS/EW Streets:	US 17/US	211/Broadv	riew Ave/Wi	nchester	US 17/US	211/Broadv	iew Ave/Wi	nchester	Warrentor	n Village So	uth Dwy/Bro	oadview	Warrenton	Village So	uth Dwy/Br	oadview	
NS/EW Streets:		St				St				Ave				Av			
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTE	BOUND		
AM	1	2	1	0	1	2	1	0	1	1	1	0	1	0.5	0.5	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
6:00 AM	25	17	2	0	0	20	8	0	22	4	24	0	0	1	0	0	123
6:15 AM	29	21	2	0	0	26	7	0	20	1	13	0	0	2	0	0	121
6:30 AM	27	26	1	1	0	35	8	0	26	2	12	0	0	3	0	0	141
6:45 AM	32	31	3	0	0	57	7	0	20	2	21	0	0	2	0	0	175
7:00 AM	32	58	7	1	1	117	7	0	24	5	16	0	3	1	2	0	274
7:15 AM	26	66	6	0	0	98	11	0	26	8	19	0	1	0	0	0	261
7:30 AM	30	120	8	0	4	59	19	0	30	5	13	0	0	3	3	0	294
7:45 AM	34	136	7	0	1	106	11	0	39	4	25	0	1	0	0	0	364
8:00 AM	20	78	9	0	1	98	11	0	22	4	20	0	0	0	0	0	263
8:15 AM	26	55	7	1	1	89	7	0	23	4	13	0	1	0	0	0	227
8:30 AM	20	65	7	0	0	91	7	0	17	1	16	0	0	5	0	0	229
8:45 AM	14	71	9	0	0	108	15	0	20	8	19	0	0	1	2	0	267
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	315	744	68	3	8	904	118	0	289	48	211	0	6	18	7	0	2739
APPROACH %'s :	27.88%	65.84%	6.02%	0.27%	0.78%	87.77%	11.46%	0.00%	52.74%	8.76%	38.50%	0.00%	19.35%	58.06%	22.58%	0.00%	2/33
PEAK HR :		07:00 AM -		0.27 70	017 0 70	0717770	1111070	0.0070	5217 170	017 0 70	50.5070	010070	13.5570	5010070	ELISO 70	0.0070	TOTAL
PEAK HR VOL :	122	380	28	1	6	380	48	0	119	22	73	0	5	4	5	0	1193
PEAK HR FACTOR :	0.897	0.699	0.875	0.250	0.375	0.812	0.632	0.000	0.763	0.688	0.730	0.000	0.417	0.333	0.417	0.000	
· LARTIR FACTOR	0.037	0.75		0.250	0.575	0.86		0.000	0.705	0.78		0.000	0.117	0.58		0.000	0.819
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTE	BOUND		
PM	1	2	1	0	1	2	1	0	1	1	1	0	1	0.5	0.5	0	
							SR				ER	EU					
	NL	NT	NR	NU	SL	ST		SU	EL	ET			WL	WT	WR	WU	TOTAL
4:00 PM	15	66	12	0	3	124	21	0	21	10	46	0	14	7	9	0	348
4:15 PM	15 28	66 93	12 18	0	3 2	124 124	21 27	0	21 20	10 12	46 39	0	14 6	7 3	9	0	348 374
4:15 PM 4:30 PM	15 28 14	66 93 87	12 18 20	0 0 0	3 2 0	124 124 121	21 27 33	0 0 0	21 20 34	10 12 27	46 39 44	0 0 0	14 6 9	7 3 7	9 2 10	0 0 0	348 374 406
4:15 PM 4:30 PM 4:45 PM	15 28 14 19	66 93 87 64	12 18 20 27	0 0 0	3 2 0 2	124 124 121 124	21 27 33 25	0 0 0	21 20 34 21	10 12 27 12	46 39 44 35	0 0 0	14 6 9 14	7 3 7 10	9 2 10 4	0 0 0	348 374 406 357
4:15 PM 4:30 PM 4:45 PM 5:00 PM	15 28 14 19	66 93 87 64 86	12 18 20 27 18	0 0 0 0	3 2 0 2	124 124 121 124 88	21 27 33 25 26	0 0 0 0	21 20 34 21 18	10 12 27 12	46 39 44 35 23	0 0 0 0	14 6 9 14	7 3 7 10 15	9 2 10 4	0 0 0 0	348 374 406 357 321
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	15 28 14 19 17 17	66 93 87 64 86 77	12 18 20 27 18 32	0 0 0 0 0	3 2 0 2 6 4	124 124 121 124 88 100	21 27 33 25 26 31	0 0 0 0 0	21 20 34 21 18 13	10 12 27 12 11 10	46 39 44 35 23 30	0 0 0 0 0	14 6 9 14 9 13	7 3 7 10 15 10	9 2 10 4 4 10	0 0 0 0 0	348 374 406 357 321 348
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	15 28 14 19 17 17 34	66 93 87 64 86 77 54	12 18 20 27 18 32 23	0 0 0 0 0	3 2 0 2 6 4 2	124 124 121 124 88 100 96	21 27 33 25 26 31 28	0 0 0 0 0	21 20 34 21 18 13 32	10 12 27 12 11 10 16	46 39 44 35 23 30 16	0 0 0 0 0	14 6 9 14 9 13 10	7 3 7 10 15 10 11	9 2 10 4 4 10 6	0 0 0 0 0	348 374 406 357 321 348 328
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	15 28 14 19 17 17 17 34 16	66 93 87 64 86 77 54 64	12 18 20 27 18 32 23 21	0 0 0 0 0 1	3 2 0 2 6 4 2 5	124 124 121 124 88 100 96 97	21 27 33 25 26 31 28 14	0 0 0 0 0 0 0	21 20 34 21 18 13 32	10 12 27 12 11 10 16 9	46 39 44 35 23 30 16 27	0 0 0 0 0 0 0	14 6 9 14 9 13 10 7	7 3 7 10 15 10 11 9	9 2 10 4 4 10 6	0 0 0 0 0 0 0	348 374 406 357 321 348 328 291
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4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM	15 28 14 19 17 17 34 16 14 20	66 93 87 64 86 77 54 64 57 49	12 18 20 27 18 32 23 21 27 25	0 0 0 0 0 1 0 0 0	3 2 0 2 6 4 2 5 1 7	124 124 121 124 88 100 96 97 60 72	21 27 33 25 26 31 28 14 13 21	0 0 0 0 0 0 0	21 20 34 21 18 13 32 10	10 12 27 12 11 10 16 9 14	46 39 44 35 23 30 16 27 35 22	0 0 0 0 0 0 0 0	14 6 9 14 9 13 10 7 10 8	7 3 7 10 15 10 11 9 14 7	9 2 10 4 4 10 6 12 7 5	0 0 0 0 0 0 0	348 374 406 357 321 348 328 291 267 261
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM	15 28 14 19 17 17 17 34 16 14 20	66 93 87 64 86 77 54 64 57 49	12 18 20 27 18 32 23 21 27 25 22	0 0 0 0 0 1 0 0 0	3 2 0 2 6 4 2 5 1 7	124 124 121 124 88 100 96 97 60 72 55	21 27 33 25 26 31 28 14 13 21	0 0 0 0 0 0 0 0	21 20 34 21 18 13 32 10 15 8	10 12 27 12 11 10 16 9 14 16 11	46 39 44 35 23 30 16 27 35 22 16	0 0 0 0 0 0 0 0 0	14 6 9 14 9 13 10 7 10 8 8	7 3 7 10 15 10 11 9 14 7	9 2 10 4 4 10 6 12 7 5	0 0 0 0 0 0 0 0	348 374 406 357 321 348 328 291 267 261 218
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4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM	15 28 14 19 17 17 17 34 16 14 20	66 93 87 64 86 77 54 64 57 49	12 18 20 27 18 32 23 21 27 25 22	0 0 0 0 0 1 0 0 0	3 2 0 2 6 4 2 5 1 7	124 124 121 124 88 100 96 97 60 72 55	21 27 33 25 26 31 28 14 13 21	0 0 0 0 0 0 0 0	21 20 34 21 18 13 32 10 15 8	10 12 27 12 11 10 16 9 14 16 11	46 39 44 35 23 30 16 27 35 22 16	0 0 0 0 0 0 0 0 0	14 6 9 14 9 13 10 7 10 8 8	7 3 7 10 15 10 11 9 14 7	9 2 10 4 4 10 6 12 7 5	0 0 0 0 0 0 0 0	348 374 406 357 321 348 328 291 267 261 218
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4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:33 PM 5:33 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	15 28 14 19 17 17 17 34 16 14 20 15 21 NL 230 17.87%	666 93 87 64 86 77 54 64 57 49 46 37 NT 780 60.61% 04:00 PM -	12 18 20 27 18 32 21 27 25 22 27 NR 272 21.13% 05:00 PM	0 0 0 0 0 1 0 0 0 1 3 0 0 NU 5 0.39%	3 2 0 2 6 4 2 5 1 7 2 2 SL 36 2.57%	124 124 121 121 124 88 100 96 97 60 72 55 48 ST 1109 79,04%	21 27 33 25 26 31 28 14 13 21 13 6	0 0 0 0 0 0 0 0 0 0 0	21 20 34 21 18 13 32 10 15 8 9 17	10 12 27 12 11 10 16 9 14 16 11 11 11	46 39 44 43 35 23 30 16 27 35 22 16 10 ER 343 47.64%	0 0 0 0 0 0 0 0 0 0	14 6 9 14 9 13 10 7 10 8 8 14 WL 122	7 3 7 10 15 10 11 9 14 7 11 4 WT 108 34.29%	9 2 10 4 4 4 10 6 12 7 5 7 9 WR 85 26.98%	0 0 0 0 0 0 0 0 0 0	348 374 406 357 321 348 328 291 267 261 218 206 TOTAL 3725
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM TOTAL VOLUMES: APPROACH %'s:	15 28 14 19 17 17 17 34 16 14 20 15 21 NL 230 17.87%	66 93 87 64 86 77 54 64 57 49 46 37 NT 780 60.61%	12 18 20 27 18 32 23 21 27 25 22 27 NR 272 21.13% 05:00 PM	0 0 0 0 0 1 0 0 0 1 3 0 0 NU 5 0.39%	3 2 0 2 6 4 2 5 1 7 2 2 2 SL 36 2.57%	124 124 121 121 124 88 100 96 97 60 72 55 48 ST 1109 79.04%	21 27 33 25 26 31 28 14 13 21 13 6 SR 258 18.39%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	21 20 34 21 18 13 32 10 15 8 9 17 EL 218 30.28%	10 12 27 12 11 10 16 9 14 16 11 11 ET 159 22.08%	46 39 44 35 23 30 16 27 35 22 16 10 ER 343 47.64%	0 0 0 0 0 0 0 0 0 0 0 0	14 6 9 14 9 13 10 7 10 8 8 14 WL 122 38.73%	7 3 7 10 15 10 11 9 14 7 11 4 WT 108 34.29%	9 2 10 4 4 10 6 12 7 7 5 7 9 WR 85 26.98%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	348 374 406 357 321 348 328 291 267 261 218 206 TOTAL 3725

Location: US 17/US 211/Broadview Ave/Winchester St & Warrenton Village South Dwy/Broadview Ave City: Warrenton
Control: 2-Way Stop(EB/WB)

	Warrenton 2-Way Stop		W AVE/WIII	uriester St	& warrentor	n Village Sou	utn Dwy/Br						Pro		23-260020- 2/9/2023	010	
_								Data ·									
NS/EW Streets:	US 17/US	211/Broadv		nchester	US 17/US 2	211/Broadvi	ew Ave/Wi	nchester	Warrenton		uth Dwy/Bro	oadview	Warrenton		uth Dwy/Br	oadview	
no, zu sereces.		St				St				Ave				Av			
ARA		NORTH		_		SOUTHE				EASTB				WESTE			
AM	1 NL	2 NT	1 NR	0 NU	1 SL	2 ST	1 SR	0 SU	1 EL	1 ET	1 ER	0 EU	1 WL	0.5 WT	0.5 WR	0 WU	TOTAL
6:00 AM	25	15	2	0	0 0	19	8 8	0	21	4	23	0	0 0	1	0	0	118
6:15 AM	29	18	1	0	0	26	7	0	20	1	13	0	0	2	0	0	117
6:30 AM	27	23	i	1	Ö	33	8	0	26	2	11	0	0	3	Ô	0	135
6:45 AM	32	29	3	ō	ő	55	7	ő	20	2	21	0	Ö	2	Ô	Ö	171
7:00 AM	32	50	7	1	1	111	6	0	23	5	15	0	3	1	1	0	256
7:15 AM	25	62	6	0	0	91	10	0	26	8	19	0	0	0	0	0	247
7:30 AM	30	117	8	0	4	53	17	0	30	5	12	0	0	3	2	0	281
7:45 AM	34	132	7	0	1	106	10	0	37	4	24	0	1	0	0	0	356
8:00 AM	20	72	9	0	1	97	11	0	22	4	20	0	0	0	0	0	256
8:15 AM	25	48 59	7	1	1 0	84	6	0	23 17	4	13 15	0	1 0	0 5	0	0	213
8:30 AM 8:45 AM	19 13	59 69	9	0	0	77 104	6 14	0	20	1 8	15 18	0	0	1	0 2	0	206 258
6:45 AM	13	09	9	U	U	104	14	U	20	•	10	U	U	1	2	U	256
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	311	694	67	3	8	856	110	0	285	48	204	0	5	18	5	0	2614
APPROACH %'s:	28.93%	64.56%	6.23%	0.28%	0.82%	87.89%	11.29%	0.00%	53.07%	8.94%	37.99%	0.00%	17.86%	64.29%	17.86%	0.00%	
PEAK HR :		07:00 AM -															TOTAL
PEAK HR VOL :	121	361	28	1	6	361	43	0	116	22	70	0	4	4	3	0	1140
PEAK HR FACTOR :	0.890	0.684	0.875	0.250	0.375	0.813	0.632	0.000	0.784	0.688	0.729	0.000	0.333	0.333	0.375	0.000	0.801
		0.73	88			0.86	19			0.80)()			0.5	50		
ſ																	
		NORTH	BOUND			SOUTHE	BOUND			FASTB	OUND			WESTE	BOUND		
PM	1	NORTHI 2	BOUND 1	0	1	SOUTHE 2	BOUND 1	0	1	EASTB 1	OUND 1	0	1	WESTE 0.5	BOUND 0.5	0	
PM	1 NL			0 NU	1 SL	SOUTHE 2 ST		0 SU	1 EL			0 EU	1 WL			0 WU	TOTAL
4:00 PM	NL 15	2 NT 65	1 NR 12	NU 0	SL 3	2 ST 120	1 SR 21	SU 0	EL 21	1 ET 10	1 ER 46	EU 0	WL 14	0.5 WT 7	0.5 WR 9	WU 0	343
4:00 PM 4:15 PM	NL 15 28	2 NT 65 91	1 NR 12 18	NU 0 0	SL 3 2	2 ST 120 116	1 SR 21 26	SU 0 0	EL 21 20	1 ET 10 12	1 ER 46 39	0 0	WL 14 6	0.5 WT 7 3	0.5 WR 9 2	0 0	343 363
4:00 PM 4:15 PM 4:30 PM	NL 15 28 14	2 NT 65 91 84	1 NR 12 18 20	0 0 0	SL 3 2 0	2 ST 120 116 118	1 SR 21 26 33	0 0 0	EL 21 20 32	1 ET 10 12 27	1 ER 46 39 43	0 0 0	WL 14 6 9	0.5 WT 7 3 7	0.5 WR 9 2 10	0 0 0	343 363 397
4:00 PM 4:15 PM 4:30 PM 4:45 PM	NL 15 28 14 18	2 NT 65 91 84 60	1 NR 12 18 20 27	NU 0 0 0 0	SL 3 2 0 2	2 ST 120 116 118 121	1 SR 21 26 33 25	SU 0 0 0 0	EL 21 20 32 21	1 ET 10 12 27 12	1 ER 46 39 43 35	EU 0 0 0 0	WL 14 6 9 14	0.5 WT 7 3 7 10	0.5 WR 9 2 10 4	WU 0 0 0 0	343 363 397 349
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	NL 15 28 14 18	2 NT 65 91 84 60 85	1 NR 12 18 20 27 18	0 0 0	SL 3 2 0 2	2 ST 120 116 118 121 86	1 SR 21 26 33 25 26	SU 0 0 0 0 0	EL 21 20 32 21 18	1 ET 10 12 27 12	1 ER 46 39 43 35 23	EU 0 0 0 0 0	WL 14 6 9 14	0.5 WT 7 3 7 10	0.5 WR 9 2 10 4	WU 0 0 0 0 0	343 363 397 349 317
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 15 28 14 18 17 17	2 NT 65 91 84 60 85 76	1 NR 12 18 20 27 18 32	NU 0 0 0 0 0 0	SL 3 2 0 2 6 4	2 ST 120 116 118 121 86 99	1 SR 21 26 33 25 26 31	SU 0 0 0 0	EL 21 20 32 21 18 13	1 ET 10 12 27 12 11 10	1 ER 46 39 43 35 23 30	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 14 6 9 14 9	0.5 WT 7 3 7 10 14 10	0.5 WR 9 2 10 4	WU 0 0 0 0 0	343 363 397 349 317 345
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 15 28 14 18 17 17 17	2 NT 65 91 84 60 85 76 54	1 NR 12 18 20 27 18 32 23	NU 0 0 0 0	SL 3 2 0 2	2 ST 120 116 118 121 86 99 94	1 SR 21 26 33 25 26 31 28	SU 0 0 0 0 0	EL 21 20 32 21 18 13 31	1 ET 10 12 27 12 11 10 16	1 ER 46 39 43 35 23 30 16	EU 0 0 0 0 0 0	WL 14 6 9 14	0.5 WT 7 3 7 10 14 10 11	0.5 WR 9 2 10 4 4 9 6	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	343 363 397 349 317 345 324
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 15 28 14 18 17 17	2 NT 65 91 84 60 85 76	1 NR 12 18 20 27 18 32	NU 0 0 0 0 0 0 0 1 0 0	SL 3 2 0 2 6 4 2 5	2 ST 120 116 118 121 86 99	1 SR 21 26 33 25 26 31	SU 0 0 0 0 0 0	EL 21 20 32 21 18 13	1 ET 10 12 27 12 11 10	1 ER 46 39 43 35 23 30	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 14 6 9 14 9 13 9	0.5 WT 7 3 7 10 14 10	0.5 WR 9 2 10 4	WU 0 0 0 0 0	343 363 397 349 317 345
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 15 28 14 18 17 17 17 34 16	2 NT 65 91 84 60 85 76 54 62	1 NR 12 18 20 27 18 32 23 20	NU 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0	SL 3 2 0 2 6 4 2 5 1 7	2 ST 120 116 118 121 86 99 94 96	1 SR 21 26 33 25 26 31 28 14	SU 0 0 0 0 0 0 0	EL 21 20 32 21 18 13 31 10	1 ET 10 12 27 12 11 10 16 9	1 ER 46 39 43 35 23 30 16 27	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 14 6 9 14 9 13 9 7	0.5 WT 7 3 7 10 14 10 11 9	0.5 WR 9 2 10 4 4 9 6 12	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	343 363 397 349 317 345 324 287
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM	NL 15 28 14 18 17 17 34 16 14 19 15	2 NT 65 91 84 60 85 76 54 62 56 49 46	1 NR 12 18 20 27 18 32 23 20 27 24 21	NU 0 0 0 0 0 1 0 0 0 1 3	SL 3 2 0 2 6 4 2 5 1 7 2	2 ST 120 116 118 121 86 99 94 96 60 71 55	1 SR 21 26 33 25 26 31 28 14 13 21 13	SU 0 0 0 0 0 0 0 0 0	EL 21 20 32 21 18 13 31 10 15 8 9	1 ET 10 12 27 12 11 10 16 9 14 16 11	1 ER 46 39 43 35 23 30 16 27 35 22 16	EU 0 0 0 0 0 0 0 0 0	WL 14 6 9 14 9 13 9 7 10 8 8	0.5 WT 7 3 7 10 14 10 11 9 14 7	0.5 WR 9 2 10 4 4 9 6 12 7 5	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	343 363 397 349 317 345 324 287 266 258 217
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM	NL 15 28 14 18 17 17 34 16 14	2 NT 65 91 84 60 85 76 54 62 56 49	1 NR 12 18 20 27 18 32 23 20 27 24	NU 0 0 0 0 0 1 0 0 0 0 1 1 0 0 1 1	SL 3 2 0 2 6 4 2 5 1 7	2 ST 120 116 118 121 86 99 94 96 60 71	1 SR 21 26 33 25 26 31 28 14 13 21	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 21 20 32 21 18 13 31 10 15 8	1 ET 10 12 27 12 11 10 16 9 14 16	1 ER 46 39 43 35 23 30 16 27 35 22	EU 0 0 0 0 0 0 0 0 0	WL 14 6 9 14 9 13 9 7 10 8	0.5 WT 7 3 7 10 14 10 11 9 14 7	0.5 WR 9 2 10 4 4 9 6 12 7 5	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	343 363 397 349 317 345 324 287 266 258
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM	NL 15 28 14 18 17 17 17 34 16 14 19 15 21	2 NT 65 91 84 60 85 76 54 62 56 49 46 36	1 NR 12 18 20 27 18 32 23 20 27 24 21 26	NU 0 0 0 0 0 1 0 0 0 0 1 3 0	SL 3 2 0 2 6 4 2 5 1 7 2 2	2 ST 120 116 118 121 86 99 94 96 60 71 55 47	1 SR 21 26 33 25 26 31 25 28 14 13 21 13 6	SU 0 0 0 0 0 0 0 0 0	EL 21 20 32 21 18 13 31 10 15 8 9 17	1 ET 10 12 27 12 11 10 16 9 14 16 11	1 ER 46 39 43 35 23 30 16 27 35 22 16 10	EU 0 0 0 0 0 0 0 0 0	WL 14 6 9 14 9 13 9 7 10 8 8 14	0.5 WT 7 3 7 10 14 10 11 9 14 7 11 4	0.5 WR 9 2 10 4 4 9 6 12 7 5 7	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	343 363 397 349 317 345 324 287 266 258 217 203
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	NL 15 28 14 18 17 17 17 34 16 14 19 15 21	2 NT 65 91 84 60 85 76 54 62 56 49 46 36	1 NR 12 18 20 27 18 32 23 20 27 24 21 26	NU 0 0 0 0 0 1 0 0 0 1 3 0 0 NU	SL 3 2 0 2 6 4 2 5 1 7 2	2 ST 120 116 118 121 86 99 94 96 60 71 55 47	1 SR 21 26 33 25 26 31 28 14 13 21 13 6	SU 0 0 0 0 0 0 0 0 0	EL 21 20 32 21 18 13 31 10 15 8 9 17	1 ET 10 12 27 12 11 10 16 9 14 16 11 11	1 ER 46 39 43 35 23 30 16 27 35 22 16 10	EU 0 0 0 0 0 0 0 0 0	WL 14 6 9 14 9 13 9 7 10 8 8 14	0.5 WT 7 3 7 10 14 10 11 9 14 7 11 4	0.5 WR 9 2 10 4 9 6 12 7 5 7 9	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	343 363 397 349 317 345 324 287 266 258 217 203
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM 6:00 PM 6:15 PM 6:30 PM	NL 15 28 14 18 17 17 17 34 16 14 19 15 21	2 NT 65 91 84 60 85 76 54 62 56 49 46 36	1 NR 12 18 20 27 18 32 23 20 27 24 21 26	NU 0 0 0 0 0 1 0 0 0 0 1 3 0	SL 3 2 0 2 6 4 2 5 1 7 2 2 2 SL	2 ST 120 116 118 121 86 99 94 96 60 71 55 47	1 SR 21 26 33 25 26 31 25 28 14 13 21 13 6	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 21 20 32 21 18 13 31 10 15 8 9 17	1 ET 10 12 27 12 11 10 16 9 14 16 11	1 ER 46 39 43 35 23 30 16 27 35 22 16 10	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 14 6 9 14 9 13 9 7 10 8 8 14	0.5 WT 7 3 7 10 14 10 11 9 14 7 11 4	0.5 WR 9 2 10 4 4 9 6 12 7 5 7	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	343 363 397 349 317 345 324 287 266 258 217 203
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 6:30 PM	NL 15 28 14 18 17 17 34 16 14 19 15 21 NL 228 18.02%	2 NT 65 91 84 60 85 76 54 62 56 49 46 36 NT 764	1 NR 12 18 18 20 27 18 32 23 20 27 24 21 26 NR 268 21.19%	NU 0 0 0 0 0 0 1 0 0 0 1 3 0 0 NU 5	SL 3 2 0 2 6 4 2 5 1 7 2 2 SL 36	2 ST 120 116 118 121 86 99 94 96 60 71 55 47 ST 1083	1 SR 21 26 33 25 26 31 28 14 13 6 SR 257	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 21 20 32 21 18 13 31 10 15 8 9 17	1 ET 10 12 27 12 11 10 16 9 14 16 11 11 11	1 ER 46 39 43 35 23 30 16 27 35 22 16 10 ER 342	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 14 6 9 14 9 13 9 7 10 8 8 14 WL 121	0.5 WT 7 3 7 10 14 10 11 9 14 7 11 4	0.5 WR 9 2 10 4 4 9 6 12 7 5 7 9	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	343 363 397 349 317 345 324 287 266 258 217 203
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 6:45 PM	NL 15 28 14 18 17 17 17 34 16 14 19 15 21 NL 228 18.02%	2 NT 655 91 84 60 85 76 54 62 55 49 46 36 NT 764 60.40% 04:00 PM -	1 NR 12 18 20 27 18 32 23 20 27 24 21 26 NR 268 21.19% 05:00 PM 77	NU 0 0 0 0 0 0 1 1 0 0 0 1 1 3 0 0 NU 5 0.40%	SL 3 2 0 2 0 2 6 4 4 2 5 5 1 7 7 2 2 2 SL 36 2.62%	2 ST 120 116 118 121 86 99 94 96 60 71 55 47 ST 1083 78.71%	1 SR 21 26 33 25 26 31 28 14 13 21 13 6 SR 257 18.68%	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 21 20 32 21 18 13 31 10 15 8 9 17 EL 215 30.03%	1 ET 10 12 27 12 11 10 16 9 14 16 11 11 11 ET 159 22.21%	1 ER 46 39 43 35 23 30 16 27 35 22 16 10 ER 342 47.77%	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 14 6 9 14 9 13 9 7 10 8 8 14 WL 121 38.78%	0.5 WT 7 3 7 10 14 10 11 9 14 7 11 4 WT 107 34.29%	0.5 WR 9 2 10 4 4 9 6 6 11 7 7 5 7 9 9 WR 84 26.92%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	343 363 397 349 317 345 324 287 266 258 217 203 TOTAL 3669
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:30 PM 6:15 PM 6:30 PM 6:45 PM TOTAL VOLUMES : APPROACH %'s :	NL 15 28 14 18 17 17 17 34 16 14 19 15 21 NL 228 18.02%	2 NT 65 91 84 60 85 76 62 54 62 56 49 46 36 NT 764 60.40%	1 NR 12 18 20 27 18 32 23 23 20 27 24 21 26 NR 268 21.19% 05:00 PM 77 0.713	NU 0 0 0 0 0 0 1 1 0 0 0 0 1 3 0 0 NU 5 0.40%	SL 3 2 0 2 6 4 2 5 1 7 2 2 SL 36 2.62%	2 ST 120 116 118 121 86 99 94 96 60 71 71 55 47 ST 1083 78.71%	1 SR 211 226 33 25 225 226 31 14 13 21 13 6 SR 257 18.68% 105 0.795	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 21 20 32 21 18 13 31 10 15 8 9 17 EL 215 30.03%	1 ET 10 10 12 27 11 10 16 9 14 16 11 11 ET 159 22.21%	1 ER 46 39 43 35 23 30 16 27 35 22 16 10 ER 342 47.77%	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 14 6 9 14 9 13 9 7 10 8 8 14 WL 121 38.78%	0.5 WT 7 3 7 10 14 10 11 9 14 7 11 4 WT 107 34.29%	0.5 WR 9 2 110 4 4 9 6 112 7 7 9 WR 84 26.92%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	343 363 397 349 317 345 324 287 266 258 217 203 TOTAL 3669

Location: US 17/US 211/Broadview Ave/Winchester St & Warrenton Village South Dwy/Broadview Ave City: Warrenton Control & Warrenton Control & Warrenton Village South Dwy/Broadview Ave

Project ID: 23-260020-010

Control: 2	2-Way Stop	(EB/WB)												Date:	2/9/2023		
		,						Data	- HT								
NS/EW Streets:	US 17/US	211/Broadv		nchester	US 17/US		iew Ave/Wi	nchester	Warrentor		uth Dwy/Br	oadview	Warrentor	n Village So		oadview	
NS/ LW Streets.		St				St				Av				Av			
A B A		NORTH				SOUTH			_	EASTE				WESTE			
AM	1	2 NT	1 NR	0 NU	1 SL	2 ST	1 SR	0	1 EL	1	1	0 EU	1	0.5	0.5	0 WU	TOTAL
6:00 AM	NL 0	N1	NR	0	0 0	1	SR	SU	EL 1	ET	ER	EU	WL 0	WT	WR 0	0	5
6:15 AM	0	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4
6:30 AM	Õ	3	Ō	Ô	Ö	2	Ô	Ô	Ö	Ô	1	Ô	Ö	Ö	Õ	Ö	6
6:45 AM	Ō	2	Ō	Ō	0	2	Ō	ō	0	Ō	Ō	ō	Ō	ō	Ō	Ō	4
7:00 AM	0	8	0	0	0	6	1	0	1	0	1	0	0	0	1	0	18
7:15 AM	1	4	0	0	0	7	1	0	0	0	0	0	1	0	0	0	14
7:30 AM	0	3	0	0	0	6	2	0	0	0	1	0	0	0	1	0	13
7:45 AM	0	4	0	0	0	0	1	0	2	0	1	0	0	0	0	0	8
8:00 AM	0	6 7	0	0	0	1 5	0	0	0	0	0	0	0	0	0	0	7
8:15 AM 8:30 AM	1	6	0	0	0	5 14	1	0	0	0	1	0	0	0	0	0	14 23
8:45 AM	1	2	0	0	0	4	1	0	0	0	1	0	0	0	0	0	9
0. 15 Al-1	-	-	•	•	•			٠		•	•	٠	·	·	•	·	,
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	4	50	1	0	0	48	8	0	4	0	7	0	1	0	2	0	125
APPROACH %'s:	7.27%	90.91%	1.82%	0.00%	0.00%	85.71%	14.29%	0.00%	36.36%	0.00%	63.64%	0.00%	33.33%	0.00%	66.67%	0.00%	
PEAK HR :		07:00 AM -					_		_								TOTAL
PEAK HR VOL :	1 0.250	19 0.594	0.000	0.000	0.000	19 0.679	5 0.625	0 0.000	3 0.375	0.000	3 0.750	0.000	1 0.250	0 0.000	2 0.500	0.000	53
PEAK HR FACTOR :	0.250	0.594		0.000	0.000	0.679		0.000	0.3/5	0.000		0.000	0.250	0.000		0.000	0.736
		0.0				017	30			0.5	-			0.,	30		
		NORTH	BOUND			SOUTH	BOUND			EASTE	OUND			WESTE	BOUND		
PM	1	2	1	0	1	2	1	0	1	1	1	0	1	0.5	0.5	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	1 2	0	0	0	4	0	0	0	0	0	0	0	0	0	0	5
4:15 PM 4:30 PM	0	3	0	0	0	8	0	0	2	0	1	0	0	0	0	0	11 9
4:45 PM	1	4	0	0	0	3	0	0	o o	0	0	0	0	0	0	0	8
5:00 PM	0	1	0	0	0	2	0	0	0	0	0	0	0	1	0	0	4
5:15 PM	ō	1	Ö	ō	0	1	Ō	ō	Ō	Ö	ō	ō	Ō	Ō	i	Ō	3
5:30 PM	0	0	0	0	0	2	0	0	1	0	0	0	1	0	0	0	4
5:45 PM	0	2	1	0	0	1	0	0	0	0	0	0	0	0	0	0	4
6:00 PM	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
6:15 PM	1	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	3
6:30 PM 6:45 PM	0	0 1	1	0	0	0 1	0	0	0	0	0	0	0	0	0	0	1
0.45 FM	U	1	-	U	J	1	U	U	U	U	v	U	J	U	U	v	3
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	2	16	4	0	0	26	1	0	3	0	1	0	1	1	1	0	56
APPROACH %'s:	9.09%	72.73%	18.18%	0.00%	0.00%	96.30%	3.70%	0.00%	75.00%	0.00%	25.00%	0.00%	33.33%	33.33%	33.33%	0.00%	
PEAK HR :		04:00 PM -								_			_				TOTAL
PEAK HR VOL :	1	10	0	0	0	18	1	0	2	0	1	0	0	0	0	0	33
PEAK HR FACTOR :	0.250			0.000	0.000			0.000	0.250			0.000	0.000	0.000	0.000	0.000	0.750
PEAK HR FACTOR :	0.250	0.625 0.5	0.000 50	0.000	0.000	0.563 0.53	0.250 28	0.000	0.250	0.000	0.250 50	0.000	0.000	0.000	0.000	0.000	0.7

Location: US 17/US 211/Broadview Ave/Winchester St & Warrenton Village South Dwy/Broadview Ave

6:30 PM 6:45 PM

0.000

TOTAL VOLUMES

APPROACH %'s
PEAK HR
PEAK HR VOL

PEAK HR FACTOR

0

NT 0

0.000

0

NR 0

0.000

NU 0

0.000

Project ID: 23-260020-010 **Date:** 2/9/2023 City: Warrenton Control: 2-Way Stop(EB/WB) Data - Bikes US 17/US 211/Broadview Ave/Winchester US 17/US 211/Broadview Ave/Winchester Warrenton Village South Dwy/Broadview Warrenton Village South Dwy/Broadview NS/EW Streets St NORTHBOUND St SOUTHBOUND Ave EASTBOUND Ave WESTBOUND AM 0.5 WR TOTAL WU 6:00 AM 6:15 AM 0 0 0 0 0 0 0 6:15 AM 6:30 AM 6:45 AM 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 0 0 0 8:45 AM WU 0 NT 0 NR 0 NU 0 ST 0 SR 0 SU 0 ET 0 ER 0 EU 0 WL 0 WT 0 WR 0 TOTAL SL 0 EL 0 TOTAL VOLUMES APPROACH %'s PEAK HR PEAK HR VOL TOTAL 07:00 AM - 08:00 AN 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0.000 0.000 0 0.000 0.000 0.000 0.000 0.000 PEAK HR FACTOR SOLITHBOLIND NORTHBOLIND FASTROLIND WESTBOUND PM TOTAL 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 6:00 PM 6:15 PM 6:30 PM 0 0 0 0 0 0 0 0

0

ST 0

0.000

0

SR 0

0 0.000

SU 0

0.000

0

EL 0

0 0.000

0

ET 0

0 0.000

0

ER 0

0.000

EU 0

0 0.000

0

WL 0

0.000

WT 0

0 0.000

0

WR 0

0.000

WU 0

0.000

TOTAL

0

TOTAL

0

SL 0

0.000

National Data & Surveying Services Intersection Turning

Location: US 17/US 211/Broadview Ave/Winchester St & Warrenton Village Sc Project ID: 23-260020-010
City: Warrenton

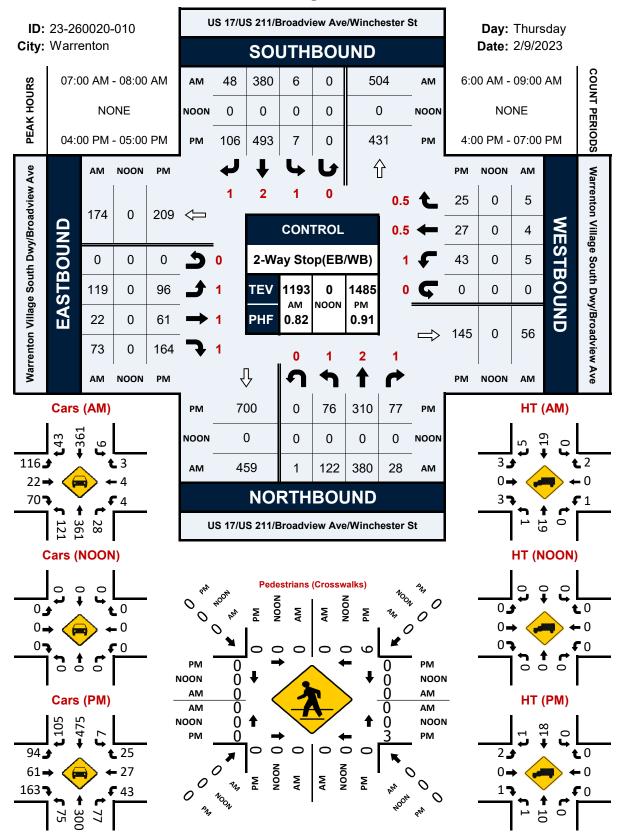
Date: 2/9/2023

Data - Pedestrians (Crosswalks)

NS/EW Streets:	US 17/US 2	11/Broadview	US 17/US 2	11/Broadview	Warrenton '	Village South	Warrenton V	/illage South	
NS/EW Streets:	Ave/Win	chester St	Ave/Win	chester St	Dwy/Broa	adview Ave	Dwy/Broa	dview Ave	
AM	NORT	TH LEG	SOUT	TH LEG	EAS	T LEG	WEST	Γ LEG	
Alvi	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
6:00 AM	0	0	0	0	0	2	0	0	2
6:15 AM	0	0	0	0	0	0	0	0	0
6:30 AM	0	1	0	0	0	0	0	0	1
6:45 AM	0	0	0	0	0	0	0	0	0
7:00 AM	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0
7:45 AM		0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	0	1	0	0	0	2	0	0	3
APPROACH %'s:	0.00%	100.00%			0.00%	100.00%			
PEAK HR:	07:00 AM	- 08:00 AM							TOTAL
PEAK HR VOL:	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR:									

PM	NORT	'H LEG	SOUT	'H LEG	EAST	LEG	WEST	Γ LEG	
PIVI	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	1	0	0	0	0	0	0	1
4:15 PM	0	4	0	0	3	0	0	0	7
4:30 PM	0	1	0	0	0	0	0	0	1
4:45 PM	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0
6:00 PM	0	0	0	0	0	0	0	0	0
6:15 PM	0	0	0	0	0	0	0	0	0
6:30 PM	0	0	0	0	0	0	0	0	0
6:45 PM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	0	6	0	0	3	0	0	0	9
APPROACH %'s:	0.00%	100.00%			100.00%	0.00%			
PEAK HR :	04:00 PM	- 05:00 PM							TOTAL
PEAK HR VOL :	0	6	0	0	3	0	0	0	9
PEAK HR FACTOR :		0.375			0.250				0.321
	0.3	375			0.2	.50			0.321

Peak Hour Turning Movement Count



D. HCM Level of Service Definitions



TECHNICAL MEMORANDUM

Subject: Level of Service Definitions

Introduction

The purpose of this memorandum is to define the level of service (LOS) metric that commonly used as a measure of effectiveness (MOE) for traffic operations.

All capacity analyses are based on the procedures specified by the Transportation Research Board's (TRB) <u>Highway Capacity Manual</u> (HCM), which is currently on its sixth edition. Level of service ranges from A to F. A brief description of each level of service for signalized and unsignalized intersections is provided below.

Signalized Intersections

Level of service is based upon the traffic volume present in each lane on the roadway, the capacity of each lane at the intersection and the delay associated with each directional movement. The levels of service for signalized intersections are defined below:

- <u>Level of Service A</u> describes operations with very low average delay per vehicle, i.e., less than 10.0 seconds. This occurs when progression is extremely favorable, and most vehicles arrive during the green phase. Most vehicles do not stop. Short signal cycle lengths may also contribute to low delay.
- <u>Level of Service B</u> describes operations with average delay in the range of 10.1 to 20.0 seconds per vehicle. This generally occurs with good progression and/or short cycle lengths. More vehicles stop than for LOS A, causing higher levels of average delay.
- Level of Service C describes operations with delay in the range of 20.1 to 35.0 seconds per vehicle. These higher delays may result from fair progression and/or longer cycle lengths. Individual cycle failures may begin to appear at this level. The number of vehicles stopping is significant at this level although many still pass through the intersection without stopping. This is generally considered the lower end of the range of the acceptable level of service in rural areas.
- Level of Service D describes operations with delay in the range of 35.1 to 55.0 seconds per vehicle. At LOS D, the influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, and/or high traffic volumes as compared to the roadway capacity. Many vehicles are required to stop and the number of vehicles that do not have to stop declines. Individual signal cycle failures, where all waiting vehicles do not clear the intersection during a single green time, are noticeable. This is generally considered the lower end of the range of the acceptable level of service in urban areas.
- Level of Service E describes operations with delay in the range of 55.1 to 80.0 seconds per vehicle. These higher delay values generally indicate poor progression, long cycle lengths, and high traffic volumes. Individual cycle failures are frequent occurrences. LOS E has been set as the limit of acceptable conditions.
- Level of Service F describes operations with average delay in excess of 80.0 seconds per vehicle. This is considered to be unacceptable to most drivers. This condition often occurs with over-saturation, i.e., when traffic arrives at a flow rate that exceeds the capacity of the intersection. It may also occur at high volumes with many individual cycle failures. Poor progression and long cycle lengths may also contribute to such delays.

Level of Service Definitions Page 2

Unsignalized Intersections

At an unsignalized intersection, the major street through traffic and right-turns are assumed to operate unimpeded and therefore receive no level of service rating. The level of service for the minor street and the major street left-turn traffic is dependent on the volume and capacity of the available lanes, and, the number and frequency of acceptable gaps in the major street traffic to make a conflicting turn. The level of service grade is provided for each conflicting movement at an unsignalized intersection and is based on the total average delay experienced by each vehicle. The delay includes the time it takes a vehicle to move from the back of a queue through the intersection.

The unsignalized intersection level of service analysis does not account for variations in driver behavior or the effects of nearby traffic signals. Therefore, the results from this analysis usually indicate worse levels of service than may be experienced in the field. The unsignalized intersection level of service descriptions are provided below:

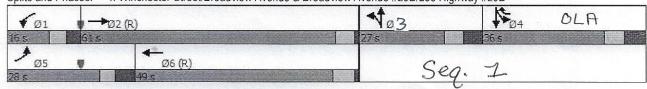
- <u>Level of Service A</u> describes operations where there is very little to no conflicting traffic for a minor side street movement, i.e., an average total delay of less than 10.0 seconds per vehicle.
- Level of Service B describes operations with average total delay in the range of 10.1 to 15.0 seconds per vehicle.
- Level of Service C describes operations with average total delay in the range of 15.1 to 25.0 second per vehicle.
- Level of Service D describes operations with average total delay in the range of 25.1 to 35.0 seconds per vehicle.
- <u>Level of Service E</u> describes operations with average total delay in the range of 35.1 to 50.0 seconds per vehicle.
- Level of Service F describes operations with average total delay of 50 seconds per vehicle. LOS F exists when there are insufficient gaps of suitable size to allow a side street demand to cross safely through or enter a major street traffic stream. This level of service is generally evident from extremely long total delays experienced by side street traffic and by queuing on the minor approaches. It is important to note that LOS F may not always result in long queues but may result in adjustments to normal driver behavior.

E. VDOT Signal Timings

4: Winchester Street/Broadview Avenue & Broadview Avenue #29B/Lee Highway #29B 01/02/2020

	1	\rightarrow	1	*	4	*
Phase Number	1	2	4	5	6	3
Movement	WBL	EBT	SBTL	EBL	WBT	NBTL
Lead/Lag	Lead	Lag		Lead	Lag	
Lead-Lag Optimize						
Recall Mode	None	C-Min	None	None	C-Min	None
Maximum Split (s)	16	61	36	28	49	27
Maximum Split (%)	11.4%	43.6%	25.7%	20.0%	35.0%	19.3%
Minimum Split (s)	12.9	27.2	15.4	13.8	32.8	14.2
Yellow Time (s)	3.8	4.2	4.5	3.4	4.8	4.1
All-Red Time (s)	3.1	1	4.9	4.4	1	4.2
Minimum Initial (s)	6	15	6	6	15	6
Vehicle Extension (s)	3	3	3	3	3	3
Minimum Gap (s)	3	3	3	3	3	3
Time Before Reduce (s)	0	0	0	0	0	0
Time To Reduce (s)	0	0	0	0	0	0
Walk Time (s)		7	7		7	7
Flash Dont Walk (s)		15	24		20	29
Dual Entry	No	Yes	No	No	Yes	No
Inhibit Max	Yes	yes	yes	yes	Yes	yes
Start Time (s)	112	128	76	112	0	49
End Time (s)	128	49	112	0	49	76
Yield/Force Off (s)	121.1	43.8	102.6	132.2	43.2	67.7
Yield/Force Off 170(s)	121.1	28.8	78.6	132.2	23.2	39.7
Local Start Time (s)	124	0	88	124	12	61
Local Yield (s)	133.1	55.8	114.6	4.2	55.2	79.7
Local Yield 170(s)	133.1	40.8	90.6	4.2	35.2 46	51.7
MAX 1	40	40	25	25	48	25
Intersection Summary			440			
Cycle Length			140			
Control Type	Actua	ated-Coor				
Natural Cycle	1	0 EDT	80	r 0: .		
Offset: 128 (91%), Reference	ced to phase	e Z:EBT a	ing p:WB	i, Start o	r ist Gree	en

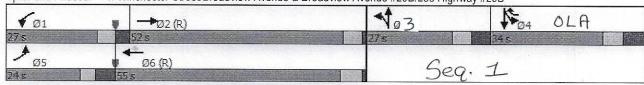
Splits and Phases: 4: Winchester Street/Broadview Avenue & Broadview Avenue #29B/Lee Highway #29B



4: Winchester Street/Broadview Avenue & Broadview Avenue #29B/Lee Highway #29B 01/02/2020

	•	-	*	*	4	*
Phase Number	1	2	4	5	6	3
Movement	WBL	EBT	SBTL	EBL	WBT	NBTL
Lead/Lag	Lead	Lag		Lead	Lag	
Lead-Lag Optimize					3	
Recall Mode	None	C-Min	None	None	C-Min	None
Maximum Split (s)	27	52	34	24	55	27
Maximum Split (%)	19.3%	37.1%	24.3%	17.1%	39.3%	19.3%
Minimum Split (s)	12.9	27.2	15.4	13.8	32.8	14.3
Yellow Time (s)	3.8	4.2	4.5	3.4	4.8	4.1
All-Red Time (s)	3.1	1	4.9	4.4	1	4.2
Minimum Initial (s)	6	15	6	6	15	6
Vehicle Extension (s)	3	3	3	3	3	3
Minimum Gap (s)	3	3	3	3	3	3
Time Before Reduce (s)	0	0	0	0	0	0
Time To Reduce (s)	0	0	0	0	0	0
Walk Time (s)		7	7		7	7
Flash Dont Walk (s)		15	24		20	29
Dual Entry	No	Yes	No	No	Yes	No
Inhibit Max	Yes	Yes	Yes	Yes	Yes	Yes
Start Time (s)	121	8	87	121	5	60
End Time (s)	8	60	121	5	60	87
Yield/Force Off (s)	1.1	54.8	111.6	137.2	54.2	78.7
Yield/Force Off 170(s)	1.1	39.8	87.6	137.2	34.2	50.7
Local Start Time (s)	116	3	82	116	0	55
Local Yield (s)	136.1	49.8	106.6	132.2	49.2	73.7
Local Yield 170(s)	136.1	34.8	82.6 25	132 <u>.2</u>	29.2 46	45.7 25
MAX 1. Intersection Summary	40	40	25	25	40	25
			140			
Cycle Length	A -1	-1-10	140			
Control Type	ACIU	ated-Coo				
Natural Cycle	1 1 0	EDT '	80			
Offset: 5 (4%), Referenced	to phase 2:	FRI and	p:WBI, S	start of 1s	t Green	

Splits and Phases: 4: Winchester Street/Broadview Avenue & Broadview Avenue #29B/Lee Highway #29B

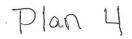


4: Winchester Street/Broadview Avenue & Broadview Avenue #29B/Lee Highway #29B01/03/2020

	1	-	100	۶	4	1
Phase Number	1	2	4	5	6	3
Movement	WBL	EBT	SBTL	EBL	WBT	NBTL
Lead/Lag	Lead	Lag		Lead	Lag	150
Lead-Lag Optimize		J			3	
Recall Mode	None	C-Min	None	None	C-Min	None
Maximum Split (s)	25	65	33	26	64	27
Maximum Split (%)	16.7%	43.3%	22.0%	17.3%	42.7%	18.0%
Minimum Split (s)	14.9	27.2	15.4	13.8	32.8	14.3
Yellow Time (s)	3.8	4.2	4.5	3.4	4.8	4.1
All-Red Time (s)	3.1	1	4.9	4.4	1	4.2
Minimum Initial (s)	6	15	6	6	15	6
Vehicle Extension (s)	3	3	3	3	3	3
Minimum Gap (s)	3	3	3	3	3	3
Time Before Reduce (s)	0	0	0	0	0	0
Time To Reduce (s)	0	0	0	0	0	0
Walk Time (s)		7	7		7	7
Flash Dont Walk (s)		15	24		20	29
Dual Entry	No	Yes	No	No	Yes	No
Inhibit Max	yes	Yes	yes	yes	yes	yes
Start Time (s)	31	56	121	31	57	4
End Time (s)	56	121	4	57	121	31
Yield/Force Off (s)	49.1	115.8	144.6	49.2	115.2	22.7
Yield/Force Off 170(s)	49.1	100.8	120.6	49.2	95.2	144.7
Local Start Time (s)	125	0	65	125	1	98
Local Yield (s)	143.1	59.8	88.6	143.2	59.2	116.7
Local Yield 170(s)	143.1	44.8	64.6	143.2	39.2	88.7
MAX 1	40	46	25	25	40	25
Intersection Summary						
Cycle Length			150			
Control Type	Actua	ted-Coor				
Natural Cycle			90 d 6:WBT,			

Splits and Phases: 4: Winchester Street/Broadview Avenue & Broadview Avenue #29B/Lee Highway #29B

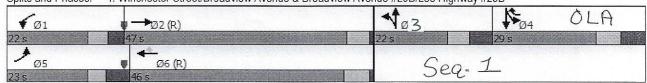
ÿ1	₽ → Ø2 (R)	№ ø4	OLA	₹ø3
25s	65 s	33.5		27 s
Ø5 26.5	Ø6 (R)	4	Seq. 3	



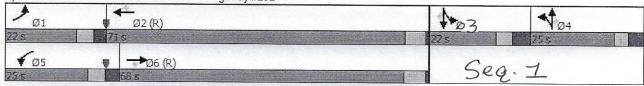
4: Winchester Street/Broadview Avenue & Broadview Avenue #29B/Lee Highway #29B 01/03/2020

	1	-	1/2	*	4-	**
Phase Number	1	2	4	5	6	3
Movement	WBL	EBT	SBTL	EBL	WBT	NBTL
Lead/Lag	Lead	Lag		Lead	Lag	
Lead-Lag Optimize		3			3	
Recall Mode	None	C-Min	None	None	C-Min	None
Maximum Split (s)	22	47	29	23	46	22
Maximum Split (%)	18.3%	39.2%	24.2%	19.2%	38.3%	18.3%
Minimum Split (s)	12.9	27.2	15.4	13.8	32.8	14.3
Yellow Time (s)	3.8	4.2	4.5	3.4	4.8	4.1
All-Red Time (s)	3.1	1	4.9	4.4	1	4.2
Minimum Initial (s)	6	15	6	6	15	6
Vehicle Extension (s)	3	3	3	3	3	3
Minimum Gap (s)	3	3	3	3	3	3
Time Before Reduce (s)	0	0	0	0	0	0
Time To Reduce (s)	0	0	0	0	0	0
Walk Time (s)		7	7		7	7
Flash Dont Walk (s)		15	24		20	29
Dual Entry	No	Yes	No	No	Yes	No
Inhibit Max	yes	yes	yes	Yes	Yes	yes
Start Time (s)	115	17	86	115	18	64
End Time (s)	17	64	115	18	64	86
Yield/Force Off (s)	10.1	58.8	105.6	10.2	58.2	77.7
Yield/Force Off 170(s)	10.1	43.8	81.6	10.2	38.2	49.7
Local Start Time (s)	98	0	69	98	1	47
Local Yield (s)	113.1	41.8	88.6	113.2	41.2	60.7
Local Yield 170(s)	1,13.1	26.8	64.6	113.2	21.2 40	32.7 25
MAX 1_ Intersection Summary	40	40	25	25	40	25
			120			
Cycle Length	Antu	ated-Coor				
Control Type	Actua	aleu-Coor	umateu 80			
Natural Cycle	nd to phone	2.EDT		Ctart of	1st Cross	2
Offset: 17 (14%), Reference	eu to phase	z.Ebi ar	iu o:wBT	, Start of	ist Gree	I

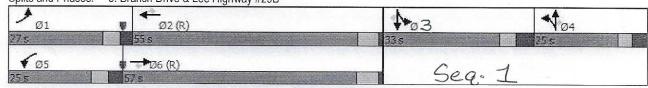
Splits and Phases: 4: Winchester Street/Broadview Avenue & Broadview Avenue #29B/Lee Highway #29B



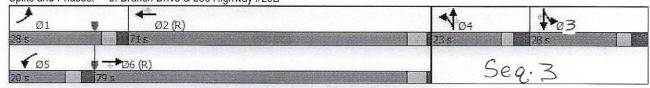
	*	4*	*	•	-	*
Phase Number	1	2	4	5	6	3
Movement	EBL	WBT	NBTL	WBL	EBT	SBTL
Lead/Lag	Lead	Lag		Lead	Lag	
Lead-Lag Optimize						
Recall Mode	None	C-Min	None	None	C-Min	None
Maximum Split (s)	22	71	25	25	68	22
Maximum Split (%)	15.7%	50.7%	17.9%	17.9%	48.6%	15.7%
Minimum Split (s)	12.4	27.6	12.6	12.8	27.7	13.5
Yellow Time (s)	3.7	4.6	3	3.7	4.7	3.5
All-Red Time (s)	2.7	1	3	3.1	1	4
Minimum Initial (s)	6	15	6	6	15	6
Vehicle Extension (s)	3	3	3	3	3	3
Minimum Gap (s)	3	3	3	3	3	3
Time Before Reduce (s)	0	0	0	0	0	0
Time To Reduce (s)	0	0	0	0	0	0
Walk Time (s)		7	7		7	
Flash Dont Walk (s)		17	27		12	
Dual Entry	No	Yes	No	No	Yes	No
Inhibit Max	yes	yes	yes	yes	yes	Yes 72
Start Time (s)	119	1	94	119	4	72
End Time (s)	1-	72	119	4	72	94
Yield/Force Off (s)	134.6	66.4	112.4	137.2	66.3	86.5
Yield/Force Off 170(s)	134.6	51.4	84.4	137.2	51.3	86.5
Local Start Time (s)	118	0	93	118	3	71
Local Yield (s)	133.6	65.4	111.4	136.2	65.3	85.5
Local Yield 170(s)	133.6	50.4 4.5	83.4	136.2	50.3	85.5
MAX I	18	45	35	18	45	35
Intersection Summary			440	Same		
Cycle Length	Λ - 1	4 10	140			
Control Type	Actua	ted-Coord	000000000000000000000000000000000000000			
Natural Cycle	to phe - 01	MDT I	70	1 14	0	
Offset: 1 (1%), Referenced	to phase 2:V	ARI and	b:EBI, SI	tart of 1st	Green	



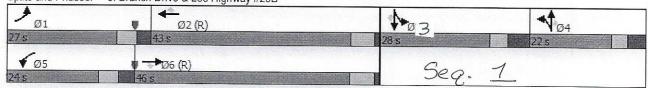
	*	4*	*	1		1
Phase Number	1	2	4	5	6	3
Movement	EBL	WBT	NBTL	WBL	EBT	SBTL
Lead/Lag	Lead	Lag		Lead	Lag	
Lead-Lag Optimize					3	
Recall Mode	None	C-Min	None	None	C-Min	None
Maximum Split (s)	27	55	25	25	57	33
Maximum Split (%)	19.3%	39.3%	17.9%	17.9%	40.7%	23.6%
Minimum Split (s)	12.4	27.6	12.6	12.8	27.7	13.5
Yellow Time (s)	3.7	4.6	3	3.7	4.7	3.5
All-Red Time (s)	2.7	1	3.6	3.1	1	4
Minimum Initial (s)	6	15	6	6	15	6
Vehicle Extension (s)	3	3	3	3	3	3
Minimum Gap (s)	3	3	3	3	3	3
Time Before Reduce (s)	0	0	0	0	0	0
Time To Reduce (s)	0	0	0	0	0	0
Walk Time (s)		7	7		7	
Flash Dont Walk (s)		17	27		12	
Dual Entry	No	Yes	No	No	Yes	No
Inhibit Max	Yes	Yes	Yes	Yes	Yes	Yes
Start Time (s)	125	12	100	125	10	67
End Time (s)	12	67	125	10	67	100
Yield/Force Off (s)	5.6	61.4	118.4	3.2	61.3	92.5
Yield/Force Off 170(s)	5.6	46.4	90.4	3.2	46.3	92.5
Local Start Time (s)	115	2	90	115	0	57
Local Yield (s)	135.6	51.4	108.4	133.2	51.3	82.5
Local Yield 170(s)	135.6	36.4 45	80.4	133.2	36.3	82. <u>5</u> 35
THAXI	18	45	35	18	45	35
Intersection Summary						
Cycle Length			140			
Control Type	Actu	ated-Coor				
Natural Cycle			80			
Offset: 10 (7%), Referenced	d to phase 2	2:WBT and	d 6:EBT,	Start of 1	st Green	·



	*	*	*	1		1
Phase Number	1	2	4	5	6	3
Movement	EBL	WBT	NBTL	WBL	EBT	SBTL
Lead/Lag	Lead	Lag		Lead	Lag	
Lead-Lag Optimize						
Recall Mode	None	C-Min	None	None	C-Min	None
Maximum Split (s)	28	71	23	20	79	28
Maximum Split (%)	18.7%	47.3%	15.3%	13.3%	52.7%	18.7%
Minimum Split (s)	12.4	27.6	12.6	12.8	27.7	13.5
Yellow Time (s)	3.7	4.6	3	3.7	4.7	3.5
All-Red Time (s)	2.7	1	3.6	3.1	1	4
Minimum Initial (s)	6	15	6	6	15	6
Vehicle Extension (s)	3	3	3	3	3	3
Minimum Gap (s)	3	3	3	3	3	3
Time Before Reduce (s)	0	0	0	0	0	0
Time To Reduce (s)	0	0	0	0	0	0
Walk Time (s)		7	7		7	
Flash Dont Walk (s)		17	a7	199-19-1	12	90.00 PM
Dual Entry	No	Yes	No	No	Yes	No
Inhibit Max	Yes	Yes	Yes	Yes	Yes	Yes
Start Time (s)	26	54	125	26	46	Y€S 148
End Time (s)	54	125	148	46	125	26
Yield/Force Off (s)	47.6	119.4	141.4	39.2	119.3	18.5
Yield/Force Off 170(s)	47.6	104.4	113.4	39.2	104.3	18.5
Local Start Time (s)	130	8	79	130	0	102
Local Yield (s)	1.6	73.4	95.4	143.2	73.3	122.5
Local Yield 170(s)	1.6	58.4	67.4 35	143.2	58. <u>3</u>	122.5
MAX I Intersection Summary	18	45	35	18	45	35
			450			
Cycle Length	A - 1	-41 C-	150			
Control Type	Actua	ated-Coor				
Natural Cycle			80			
Offset: 46 (31%), Referenc	ed to phase	2:WBT a	nd 6:EBT,	Start of 1	st Green	



	*	4*	*	1		1
Phase Number	1	2	4	5	6	3
Movement	EBL	WBT	NBTL	WBL	EBT	SBTL
Lead/Lag	Lead	Lag		Lead	Lag	
Lead-Lag Optimize		5			- 3	
Recall Mode	None	C-Min	None	None	C-Min	None
Maximum Split (s)	27	43	22	24	46	28
Maximum Split (%)	22.5%	35.8%	18.3%	20.0%	38.3%	23.3%
Minimum Split (s)	12.4	27.6	12.6	12.8	27.7	13.5
Yellow Time (s)	3.7	4.6	3	3.7	4.7	3.5
All-Red Time (s)	2.7	1	3.6	3.1	1	4
Minimum Initial (s)	6	15	6	6	15	6
Vehicle Extension (s)	3	3	3	3	3	3
Minimum Gap (s)	3	3	3	3	3	3
Time Before Reduce (s)	0	0	0	0	0	0
Time To Reduce (s)	0	0	0 -	0	0	0
Walk Time (s)		7	7		7	
Flash Dont Walk (s)		17	27		12	
Dual Entry	No	Yes	No	No	Yes	No
Inhibit Max	yes	yes	yes	Yes	yes	yes
Start Time (s)	100	7	78	100	4	50
End Time (s)	7	50	100	4	50	78
Yield/Force Off (s)	0.6	44.4	93.4	117.2	44.3	70.5
Yield/Force Off 170(s)	0.6	29.4	65.4	117.2	29.3	70.5
Local Start Time (s)	96	3	74	96	0	46
Local Yield (s)	116.6	40.4	89.4	113.2	40.3	66.5
Local Yield 170(s)	116.6	25.4	61.4	113.2	25.3_	66.5
Interspetion Summers	18	45	35	18	45	35
Intersection Summary			400			
Cycle Length			120			
Control Type	Actua	ted-Coord				
Natural Cycle	. 1 01	NDT .	75		_	
Offset: 4 (3%), Referenced	to phase 2:V	VB1 and	6:EBT, St	art of 1st	Green	



F. 2023 Existing Conditions – Capacity Analysis Worksheets

Queues

1: WINCHESTER ST & JAMES MADISON HWY & LEE HWY

	۶	→	•	←	•	•	†	/	\	ļ	4	
Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Group Flow (vph)	298	896	38	699	194	83	117	80	117	122	244	
v/c Ratio	0.72	0.51	0.37	0.48	0.21	0.49	0.62	0.21	0.59	0.58	0.41	
Control Delay	69.1	26.2	96.7	21.6	3.5	68.2	73.8	1.2	69.4	67.7	11.1	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	69.1	26.2	96.7	21.6	3.5	68.2	73.8	1.2	69.4	67.7	11.1	
Queue Length 50th (ft)	141	287	38	249	32	76	108	0	112	116	41	
Queue Length 95th (ft)	186	428	78	143	46	126	166	0	167	171	95	
Internal Link Dist (ft)		1315		334			509			538		
Turn Bay Length (ft)	250		130		200	250		125	215			
Base Capacity (vph)	481	1758	118	1450	1006	224	249	447	313	335	621	
Starvation Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.62	0.51	0.32	0.48	0.19	0.37	0.47	0.18	0.37	0.36	0.39	
Intersection Summary												

Synchro 11 Report Page 1

		۶	→	\rightarrow	F	•	←	•	•	†	<i>></i>	>
Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBL	NBT	NBR	SBL
Lane Configurations		ሽኘ	∱ }			ă	^	7	ሻ	1	7	ሻ
Traffic Volume (vph)	5	257	758	31	3	31	615	171	73	103	70	117
Future Volume (vph)	5	257	758	31	3	31	615	171	73	103	70	117
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Grade (%)			0%				-1%			2%		
Total Lost time (s)		7.8	5.2			6.9	5.8	9.4	8.3	8.3	6.9	9.4
Lane Util. Factor		0.97	0.95			1.00	0.95	1.00	1.00	1.00	1.00	0.95
Frpb, ped/bikes		1.00	1.00			1.00	1.00	1.00	1.00	1.00	1.00	1.00
Flpb, ped/bikes		1.00	1.00			1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		1.00	0.99			1.00	1.00	0.85	1.00	1.00	0.85	1.00
Flt Protected		0.95	1.00			0.95	1.00	1.00	0.95	1.00	1.00	0.95
Satd. Flow (prot)		3338	3452			1814	3359	1561	1655	1844	1537	1649
Flt Permitted		0.95	1.00			0.95	1.00	1.00	0.95	1.00	1.00	0.95
Satd. Flow (perm)		3338	3452			1814	3359	1561	1655	1844	1537	1649
Peak-hour factor, PHF	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Adj. Flow (vph)	6	292	861	35	3	35	699	194	83	117	80	133
RTOR Reduction (vph)	0	0	1	0	0	0	0	87	0	0	67	0
Lane Group Flow (vph)	0	298	895	0	0	38	699	107	83	117	13	117
Confl. Peds. (#/hr)					•							
Heavy Vehicles (%)	0%	5%	4%	3%	0%	0%	8%	4%	8%	2%	4%	5%
Turn Type	Prot	Prot	NA		Prot	Prot	NA	pm+ov	Split	NA	custom	Split
Protected Phases	5	5	2		1	1	6	4	3	3	COCCOTT	4
Permitted Phases		•	_		•	•		6			13	
Actuated Green, G (s)		17.4	71.0			8.1	60.2	77.0	14.3	14.3	22.4	16.8
Effective Green, g (s)		17.4	71.0			8.1	60.2	77.0	14.3	14.3	22.4	16.8
Actuated g/C Ratio		0.12	0.51			0.06	0.43	0.55	0.10	0.10	0.16	0.12
Clearance Time (s)		7.8	5.2			6.9	5.8	9.4	8.3	8.3	0.10	9.4
Vehicle Extension (s)		3.0	3.0			3.0	3.0	3.0	3.0	3.0		3.0
Lane Grp Cap (vph)		414	1750			104	1444	858	169	188	245	197
v/s Ratio Prot		c0.09	c0.26			0.02	0.21	0.01	0.05	c0.06	240	c0.07
v/s Ratio Perm		60.03	60.20			0.02	0.21	0.05	0.00	60.00	0.01	60.07
v/c Ratio		0.72	0.51			0.37	0.48	0.03	0.49	0.62	0.05	0.59
Uniform Delay, d1		59.0	23.0			63.5	28.7	15.2	59.4	60.3	49.8	58.4
Progression Factor		1.00	1.00			1.38	0.65	2.21	1.00	1.00	1.00	1.00
Incremental Delay, d2		5.9	1.00			2.1	1.1	0.1	2.2	6.3	0.1	4.7
Delay (s)		64.9	24.0			89.7	19.8	33.6	61.7	66.5	49.9	63.1
Level of Service		04.3 E	24.0 C			69.7 F	19.0 B	33.0 C	01.7 E	00.5 E	49.9 D	03.1 E
Approach Delay (s)		<u> </u>	34.2				25.5	U	<u> </u>	60.3	U	<u> </u>
Approach LOS			34.2 C				23.3 C			00.3 E		
<u> </u>			C				U					
Intersection Summary												
HCM 2000 Control Delay			36.4	Н	CM 2000	Level of	Service		D			
HCM 2000 Volume to Capacit	y ratio		0.59									
Actuated Cycle Length (s)			140.0		um of lost				31.3			
Intersection Capacity Utilization	n		70.8%	IC	CU Level o	of Service			С			
Analysis Period (min)			15									
c Critical Lane Group												

Movement SBT SBR Lane Configurations Image: Configuration of the processing of the		↓	4
Lane Configurations ↑ Traffic Volume (vph) 93 215 Future Volume (vph) 93 215 Ideal Flow (vphpl) 1900 1900 Grade (%) -2% -2% Total Lost time (s) 9.4 9.4 Lane Util. Factor 0.95 1.00 Frpb, ped/bikes 1.00 0.98 Flpb, ped/bikes 1.00 1.00 Frt 1.00 0.85 Flt Protected 0.99 1.00 Satd. Flow (prot) 1769 1558 Flt Permitted 0.99 1.00 Satd. Flow (perm) 1769 1558 Flt Permitted 0.99 1.00 Satd. Flow (perm) 1769 1558 Flt Permitted 0.99 1.00 Satd. Flow (perm) 1769 1558 Flt Permitted 0.99 1.00 Satd. Flow (perm) 1769 1558 Peak-hour factor, PHF 0.88 0.88 Adj. Flow (vph) <t< td=""><td>Movement</td><td>SBT</td><td>SBR</td></t<>	Movement	SBT	SBR
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Level of Service E D Approach Delay (s) 49.2 Approach LOS D			
Approach LOS 49.2 Approach LOS D			
Approach LOS D			U
Intersection Summary		U	
	Intersection Summary		

HCM 6th Edition methodology expects strict NEMA phasing.

Intersection												
Int Delay, s/veh	0.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		^	7		^	7			7			7
Traffic Vol, veh/h	0	885	63	0	800	31	0	0	29	0	0	20
Future Vol, veh/h	0	885	63	0	800	31	0	0	29	0	0	20
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	110	-	-	300	-	-	0	-	-	0
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	1	-	-	3	-	-	3	-	-	-11	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	4	3	0	7	0	0	0	3	0	0	0
Mvmt Flow	0	962	68	0	870	34	0	0	32	0	0	22
Major/Minor M	lajor1			laior?		N.	/linor1		A	/linor2		
		^		//ajor2								125
Conflicting Flow All	-	0	0	-	-	0	-	-	481	-	-	435
Stage 1	-	-	-	-	-	-	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-	-	-	7.26	-	-	5.8
Critical Hdwy	-	-	-	-	-	-	-	-	1.20	-	-	5.0
Critical Hdwy Stg 1		-	-	-	-	-	-	-	_	-	-	-
Critical Hdwy Stg 2 Follow-up Hdwy	-	-	-	-			-	-	3.33	- -	-	3.3
Pot Cap-1 Maneuver	0	-	-	0	-	-	0	0	508	0	0	5.5 656
Stage 1	0	_	-	0	_	-	0	0	500	0	0	000
Stage 2	0	-	-	0	-	-	0	0	-	0	0	<u>-</u>
Platoon blocked, %	U	-	_	U	_	_	U	U	_	U	U	-
Mov Cap-1 Maneuver	_	-	-	_	-	-	_	_	508		_	656
Mov Cap-1 Maneuver	-	_	_	<u>-</u>	_	_	<u>-</u>	_	500	-	_	000
Stage 1	_	-	_	_			-		_	_		<u>-</u> -
Stage 2	_	_	_	_	_	_	_	_	_	_	_	_
Olaye Z	_	<u>-</u>	_	_	_	-	_	_	_	_	<u>-</u>	<u>-</u>
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			0			12.6			10.7		
HCM LOS							В			В		
Minor Lane/Major Mvmt	N	NBLn1	EBT	EBR	WBT	WBR S	BLn1					
Capacity (veh/h)		508	-	-	-	-	656					
HCM Lane V/C Ratio		0.062	-	-	_	-	0.033					
HCM Control Delay (s)		12.6	_	-	-	-	10.7					
HCM Lane LOS		В	-	-	-	-	В					
HCM 95th %tile Q(veh)		0.2	-	-	-	-	0.1					

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBT	NBR	SBT	SBR	
Lane Group Flow (vph)	40	964	1	48	840	56	23	42	46	55	
v/c Ratio	0.36	0.41	0.00	0.41	0.37	0.05	0.15	0.16	0.40	0.28	
Control Delay	84.6	7.2	0.0	72.4	16.2	0.1	56.4	1.4	71.9	3.4	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	84.6	7.2	0.0	72.4	16.2	0.1	56.4	1.4	71.9	3.4	
Queue Length 50th (ft)	40	127	0	44	188	0	21	0	43	0	
Queue Length 95th (ft)	m80	133	m0	88	394	0	43	0	86	0	
Internal Link Dist (ft)		457			1504		131		565		
Turn Bay Length (ft)	240		330	150		150		60			
Base Capacity (vph)	199	2364	1143	227	2284	1125	286	358	185	248	
Starvation Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.20	0.41	0.00	0.21	0.37	0.05	0.08	0.12	0.25	0.22	
Intersection Summary											

m Volume for 95th percentile queue is metered by upstream signal.

		۶	→	*	•	←	4	1	†	~	/	+
Movement	EBU	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT
Lane Configurations		ă	^	7	ሻ	^↑	7		4	7		ર્ન
Traffic Volume (vph)	7	29	877	1	44	764	51	10	11	38	34	8
Future Volume (vph)	7	29	877	1	44	764	51	10	11	38	34	8
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Grade (%)			-4%			2%			0%			-1%
Total Lost time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.0	6.0		7.5
Lane Util. Factor		1.00	0.95	1.00	1.00	0.95	1.00		1.00	1.00		1.00
Frt		1.00	1.00	0.85	1.00	1.00	0.85		1.00	0.85		1.00
Flt Protected		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (prot)		1791	3541	1647	1752	3372	1599		1856	1615		1792
Flt Permitted		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (perm)		1791	3541	1647	1752	3372	1599		1856	1615		1792
Peak-hour factor, PHF	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91
Adj. Flow (vph)	8	32	964	1	48	840	56	11	12	42	37	9
RTOR Reduction (vph)	0	0	0	0	0	0	21	0	0	39	0	0
Lane Group Flow (vph)	0	40	964	1	48	840	35	0	23	3	0	46
Heavy Vehicles (%)	14%	0%	4%	0%	2%	6%	0%	0%	0%	0%	3%	0%
Turn Type	Prot	Prot	NA	Perm	Prot	NA	Perm	Split	NA	Perm	Split	NA
Protected Phases	1	1	6	0	5	2	0	4	4		3	3
Permitted Phases		7.5	07.0	6	0.4	00.4	2		40.7	4		7.0
Actuated Green, G (s)		7.5	87.3	87.3	8.1	88.4	88.4		10.7	10.7		7.9
Effective Green, g (s)		7.5	87.3	87.3	8.1	88.4	88.4		10.7	10.7		7.9
Actuated g/C Ratio		0.05	0.62	0.62	0.06	0.63	0.63		0.08	0.08		0.06
Clearance Time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.0	6.0		7.5
Vehicle Extension (s)		3.0	3.0	3.0	3.0	3.0	3.0		3.0	3.0		3.0
Lane Grp Cap (vph)		95	2208	1027	101	2129	1009		141	123		101
v/s Ratio Prot		0.02	c0.27	0.00	c0.03	0.25	0.02		c0.01	0.00		c0.03
v/s Ratio Perm v/c Ratio		0.42	0.44	0.00	0.48	0.39	0.02		0.16	0.00		0.46
Uniform Delay, d1		64.1	13.6	0.00 9.9	63.9	12.7	9.7		60.5	59.8		0.46 64.0
Progression Factor		1.23	0.40	1.00	1.00	1.00	1.00		1.00	1.00		1.00
Incremental Delay, d2		2.7	0.40	0.0	3.5	0.5	0.1		0.5	0.1		3.2
Delay (s)		81.5	6.0	9.9	67.4	13.2	9.8		61.0	59.9		67.2
Level of Service		F	Α	3.5 A	67. 4	В	3.0 A		E	55.5 E		67.Z
Approach Delay (s)			9.0	А	_	15.8	А		60.3	_		64.7
Approach LOS			3.0 A			В			E			E
Intersection Summary			,,						_			_
HCM 2000 Control Delay			16.2	Н	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capaci	ty ratio		0.41		CIVI ZUUU	Level OI	Del VICE		Б			
Actuated Cycle Length (s)	ty ratio		140.0	9	um of lost	time (s)			26.0			
Intersection Capacity Utilization	on		57.4%		CU Level		<u> </u>		20.0 B			
Analysis Period (min)	U11		15	ıc	O LGVEI (JI OOI VICE			U			
Critical Lang Group			10									

c Critical Lane Group



	_
Movement	SBR
Lane Configurations	7
Traffic Volume (vph)	50
Future Volume (vph)	50
Ideal Flow (vphpl)	1900
Grade (%)	
Total Lost time (s)	7.5
Lane Util. Factor	1.00
Frt	0.85
Flt Protected	1.00
Satd. Flow (prot)	1375
Flt Permitted	1.00
Satd. Flow (perm)	1375
Peak-hour factor, PHF	0.91
Adj. Flow (vph)	55
RTOR Reduction (vph)	52
Lane Group Flow (vph)	3
Heavy Vehicles (%)	18%
Turn Type	Perm
Protected Phases	1 61111
Permitted Phases	3
Actuated Green, G (s)	7.9
Effective Green, g (s)	7.9
Actuated g/C Ratio	0.06
Clearance Time (s)	7.5
Vehicle Extension (s)	3.0
	77
Lane Grp Cap (vph)	- 11
v/s Ratio Prot	0.00
v/s Ratio Perm	0.00
v/c Ratio	0.04
Uniform Delay, d1	62.5
Progression Factor	1.00
Incremental Delay, d2	0.2
Delay (s)	62.7
Level of Service	Е
Approach Delay (s)	
Approach LOS	
Intersection Summary	

HCM 6th Edition methodology expects strict NEMA phasing.

Intersection												
Int Delay, s/veh	4.4											
	EDI	EDT	EDD	WDI	WDT	WDD	NDI	NDT	NDD	CDI	CDT	CDD
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	^	4	00	4.4	4	4.4	00	€ ÎÞ	-	40	414	_
Traffic Vol, veh/h	6	15	38	14	11	14	23	65	7	18	67	5
Future Vol, veh/h	6	15	38	14	11	14	23	65	7	18	67	5
Conflicting Peds, #/hr	0	0	2	2	0	0	_ 0	_ 0	0	_ 0	_ 0	_ 0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	-8	-	-	-2	-	-	1	-	-	-1	-
Peak Hour Factor	85	85	85	85	85	85	85	85	85	85	85	85
Heavy Vehicles, %	0	0	0	0	9	0	0	0	0	0	13	0
Mvmt Flow	7	18	45	16	13	16	27	76	8	21	79	6
Major/Minor N	linor2			Minor1			Major1		N	Major2		
Conflicting Flow All	223	262	45	227	261	42	85	0	0	84	0	0
Stage 1	124	124	-	134	134	-	-	-	-	-	-	-
Stage 2	99	138	_	93	127	<u>-</u>	_	_	_	_	_	_
Critical Hdwy	5.9	4.9	6.1	7.1	6.28	6.7	4.1			4.1		
Critical Hdwy Stg 1	4.9	3.9	-	6.1	5.28	0.1	7.1	_		-T. I	_	_
Critical Hdwy Stg 2	4.9	3.9	_	6.1	5.28	_						
Follow-up Hdwy	3.5	3.9	3.3	3.5	4.09	3.3	2.2	_	_	2.2	_	_
Pot Cap-1 Maneuver	794	726	1032	733	645	1028	1524	_	<u>-</u>	1526	-	<u>-</u>
Stage 1	922	842	1032	874	780	1020	1324	-	-	1320	_	_
Stage 1	943	836	-	919	785	-	-	-	-	-	-	-
Platoon blocked, %	343	030	-	313	100	-	-	-	-	-	-	-
Mov Cap-1 Maneuver	750	702	1030	669	624	1028	1524	_	-	1526	_	-
•	750	702		669	624	1020	1524	_	=	1520	-	-
Mov Cap-2 Maneuver		830	-		765	-	-	-	-	-	-	-
Stage 1	904	820	-	857 847	765	-	-	-	-	-	-	-
Stage 2	895	020	-	047	114	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	9.4			10.1			1.8			1.5		
HCM LOS	Α			В								
Minor Lane/Major Mvmt		NBL	NBT	NRR	EBLn1V	WRI n1	SBL	SBT	SBR			
Capacity (veh/h)		1524	HDT		890	748	1526	ופט	ODIX			
· · · · · · · · · · · · · · · · · · ·			-	-				-	-			
HCM Central Delay (a)		0.018	-	-	0.078	0.061	0.014	-	-			
HCM Long LOS		7.4	0	-	9.4	10.1	7.4	0	-			
HCM Of the O(vola)		Α	Α	-	A	В	A	Α	-			
HCM 95th %tile Q(veh)		0.1	-	-	0.3	0.2	0	-	-			

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Intersection												
Int Delay, s/veh	3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4		1,02	4	1,51		4	7	UDL	4	OBIN
Traffic Vol, veh/h	1	76	75	14	106	1	73	1	12	1	1	1
Future Vol, veh/h	1	76	75	14	106	1	73	1	12	1	1	1
Conflicting Peds, #/hr	4	0	1	1	0	4	0	0	2	2	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	_	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	0	-	-	-
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	1	-	-	2	-	-	-5	-
Peak Hour Factor	85	85	85	85	85	85	85	85	85	85	85	85
Heavy Vehicles, %	0	1	11	7	1	0	0	0	0	0	0	0
Mvmt Flow	1	89	88	16	125	1	86	1	14	1	1	1
Major/Minor M	1ajor1			Major2		1	Minor1		N	Minor2		
Conflicting Flow All	130	0	0	178	0	0	295	298	136	307	342	130
Stage 1	-	-	-	-	-	-	136	136	-	162	162	-
Stage 2	-	-	-	-	-	-	159	162	-	145	180	-
Critical Hdwy	4.1	-	-	4.17	-	-	7.5	6.9	6.4	6.1	5.5	5.7
Critical Hdwy Stg 1	-	-	-	-	-	-	6.5	5.9	-	5.1	4.5	-
Critical Hdwy Stg 2	-	-	-	-	_	-	6.5	5.9	-	5.1	4.5	-
Follow-up Hdwy	2.2	-	-	2.263	-	-	3.5	4	3.3	3.5	4	3.3
Pot Cap-1 Maneuver	1468	-	-	1368	-	-	640	597	911	707	642	942
Stage 1	-	-	-	-	-	-	859	776	-	884	803	-
Stage 2	-	-	-	-	-	-	833	754	-	898	793	-
Platoon blocked, %		-	-		-	-						
Mov Cap-1 Maneuver	1463	-	-	1367	-	-	631	586	909	684	630	939
Mov Cap-2 Maneuver	-	-	-	-	-	-	631	586	-	684	630	-
Stage 1	-	-	-	-	-	-	857	774	-	880	790	-
Stage 2	-	-	-	-	-	-	820	742	-	880	791	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			0.9			11.2			10		
HCM LOS							В			В		
Minor Lane/Major Mvmt		NBLn11	NBLn2	EBL	EBT	EBR	WBL	WBT	WBR S	SBLn1		
Capacity (veh/h)		630	909				1367	-	-			
HCM Lane V/C Ratio			0.016		_		0.012	_		0.005		
HCM Control Delay (s)		11.6	9	7.5	0	_	7.7	0	-	10		
HCM Lane LOS		В	A	A	A	-	A	A	_	В		
HCM 95th %tile Q(veh)		0.5	0	0	-	_	0	-	-	0		

Intersection						
Int Delay, s/veh	4.1					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations			₽		, A	
Traffic Vol, veh/h	83	104	136	44	47	67
Future Vol, veh/h	83	104	136	44	47	67
Conflicting Peds, #/hr	1	0	0	1	0	2
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage	,# -	0	0	-	0	-
Grade, %	<u>-</u>	-3	1	-	-5	-
Peak Hour Factor	85	85	85	85	85	85
Heavy Vehicles, %	6	1	1	0	17	0
Mvmt Flow	98	122	160	52	55	79
	Major1		Major2		Minor2	
Conflicting Flow All	213	0	-	0	505	189
Stage 1	-	-	-	-	187	-
Stage 2	-	-	-	-	318	-
Critical Hdwy	4.16	-	-	-	5.57	5.7
Critical Hdwy Stg 1	-	-	-	-	4.57	-
Critical Hdwy Stg 2	-	-	-	-	4.57	-
	2.254	-	-	-	3.653	3.3
Pot Cap-1 Maneuver	1334	-	-	-	577	881
Stage 1	_	_	_	_	853	-
Stage 2	-	_	-	_	770	_
Platoon blocked, %		<u>-</u>	_	_		
Mov Cap-1 Maneuver	1333	_	_	_	530	879
Mov Cap-2 Maneuver	-	_	_	_	530	-
Stage 1	_	_			785	_
Stage 2	_	_	_	_	769	_
Staye 2		-			703	_
Approach	EB		WB		SB	
HCM Control Delay, s	3.5		0		11.5	
HCM LOS					В	
Min and an a/Mainn M		EDI	EDT	MOT	W/DD (2DL 4
Minor Lane/Major Mvm	l	EBL	EBT	WBT	WBR S	
Capacity (veh/h)		1333	-	-	-	691
HCM Lane V/C Ratio		0.073	-	-		0.194
HCM Control Delay (s)		7.9	-	-	-	11.5
HCM Lane LOS		Α	-	-	-	В
HCM 95th %tile Q(veh)		0.2				0.7

laters estimate							
Intersection	4.0						
Int Delay, s/veh	1.9						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	ķ	†	†		ķ	7	
Traffic Vol, veh/h	38	156	152	51	31	19	
Future Vol, veh/h	38	156	152	51	31	19	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	75	-	-	-	0	50	
Veh in Median Storage	e,# -	0	0	-	0	-	
Grade, %	-	-5	3	-	0	-	
Peak Hour Factor	85	85	85	85	85	85	
Heavy Vehicles, %	0	4	1	0	0	0	
Mvmt Flow	45	184	179	60	36	22	
Major/Minor I	Major1	N	Major2	N	Minor2		
Conflicting Flow All	239	0	- viajuiz	0	483	209	
Stage 1	239	-	-	-	209	209	
Stage 2	_	_		_	274	_	
Critical Hdwy	4.1	_	_	_	6.4	6.2	
Critical Hdwy Stg 1	7.1	_	_	_	5.4	- 0.2	
Critical Hdwy Stg 2	_		_	_	5.4	_	
Follow-up Hdwy	2.2	_	_	_	3.5	3.3	
Pot Cap-1 Maneuver	1340		_	_	546	836	
Stage 1	-	_	_	_	831	-	
Stage 2	_	_	_	_	777	_	
Platoon blocked, %		<u>-</u>	_	<u>-</u>	111		
Mov Cap-1 Maneuver	1340	_	_	_	527	836	
Mov Cap-1 Maneuver	-	_	_	<u> </u>	527	-	
Stage 1	_	_	_	_	803	_	
Stage 2	<u>-</u>	<u>-</u>	_	_	777	_	
Olugo Z					,,,,		
Approach	EB		WB		SB		
HCM Control Delay, s	1.5		0		11.2		
HCM LOS					В		
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR	SBLn1	SBLn2
Capacity (veh/h)		1340			-	527	836
HCM Lane V/C Ratio		0.033	<u>-</u>	<u>-</u>		0.069	
HCM Control Delay (s)		7.8	_	_	_	12.3	9.4
HCM Lane LOS		Α.	_	-	_	12.0 B	Α.
HCM 95th %tile Q(veh)	0.1	_	_	_	0.2	0.1
HOW JOHN JOHN Q (VEH)	1	0.1	_			0.2	0.1

Intersection												
Int Delay, s/veh	4.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4	7	ች	^	1		^	
Traffic Vol, veh/h	1	1	1	64	1	106	1	407	98	95	355	1
Future Vol, veh/h	1	1	1	64	1	106	1	407	98	95	355	1
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	100	-	0	90	-	130	225	-	-
Veh in Median Storage,	, # -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	-2	-	-	4	-	-	2	-	-	3	-
Peak Hour Factor	85	85	85	85	85	85	85	85	85	85	85	85
Heavy Vehicles, %	0	0	0	0	0	1	0	6	1	5	5	0
Mvmt Flow	1	1	1	75	1	125	1	479	115	112	418	1
Major/Minor N	/linor2		<u> </u>	Minor1			Major1		<u> </u>	Major2		
Conflicting Flow All	885	1239	210	915	1124	240	419	0	0	594	0	0
Stage 1	643	643	-	481	481	-	-	-	-	-	-	-
Stage 2	242	596	-	434	643	-	-	-	-	-	-	-
Critical Hdwy	7.1	6.1	6.7	8.3	7.3	7.32	4.1	-	-	4.2	-	-
Critical Hdwy Stg 1	6.1	5.1	-	7.3	6.3	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.1	5.1	-	7.3	6.3	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4	3.3	3.5	4	3.31	2.2	-	-	2.25	-	-
Pot Cap-1 Maneuver	268	203	811	188	161	744	1151	-	-	958	-	-
Stage 1	465	506	-	486	501	-	-	-	-	-	-	-
Stage 2	766	529	-	523	409	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	202	179	811	170	142	744	1151	-	-	958	-	-
Mov Cap-2 Maneuver	202	179	-	170	142	-	-	-	-	-	-	-
Stage 1	465	447	-	486	500	-	-	-	-	-	-	-
Stage 2	636	528	-	460	361	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	19.3			23			0			1.9		
HCM LOS	С			С								
Minor Lane/Major Mvm	t	NBL	NBT	NBR	EBLn1\	VBLn1V	VBLn2	SBL	SBT	SBR		
Capacity (veh/h)		1151	-	-	255	169	744	958		_		
HCM Lane V/C Ratio		0.001	_	_		0.452			_	_		
HCM Control Delay (s)		8.1	-	_	19.3	42.8	10.8	9.3	_	-		
HCM Lane LOS		A	_	-	C	E	В	A	_	_		
HCM 95th %tile Q(veh)		0	-	-	0	2.1	0.6	0.4	-	-		
2011)							- 0.5					

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Intersection												
Int Delay, s/veh	0.7											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4		ሻ	f)		ች	^	7	ሻ	^	
Traffic Vol, veh/h	1	1	3	5	1	18	13	488	10	15	401	3
Future Vol, veh/h	1	1	3	5	1	18	13	488	10	15	401	3
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	0	-	-	150	-	135	110	-	-
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	5	-	-	3	-	-	4	-	-	-2	-
Peak Hour Factor	85	85	85	85	85	85	85	85	85	85	85	85
Heavy Vehicles, %	0	0	0	0	0	6	0	5	0	0	4	0
Mvmt Flow	1	1	4	6	1	21	15	574	12	18	472	4
Major/Minor M	1inor2		N	Minor1			Major1		N	/lajor2		
Conflicting Flow All	828	1126	238	877	1116	287	476	0	0	586	0	0
Stage 1	510	510	-	604	604	-	-	-	-	-	-	-
Stage 2	318	616	_	273	512	-	_	_	_	_	-	-
Critical Hdwy	8.5	7.5	7.4	8.1	7.1	7.32	4.1	_	-	4.1	_	_
Critical Hdwy Stg 1	7.5	6.5	-	7.1	6.1	-	-	-	-	-	-	-
Critical Hdwy Stg 2	7.5	6.5	-	7.1	6.1	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4	3.3	3.5	4	3.36	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	212	151	744	212	174	681	1097	-	-	999	-	-
Stage 1	451	469	-	413	444	-	-	-	-	-	-	-
Stage 2	616	409	-	684	496	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	199	146	744	205	168	681	1097	-	-	999	-	-
Mov Cap-2 Maneuver	199	146	-	205	168	-	-	-	-	-	-	-
Stage 1	445	461	-	407	438	-	-	-	-	-	-	-
Stage 2	587	403	-	667	487	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	16.7			13.8			0.2			0.3		
HCM LOS	С			В								
Minor Lane/Major Mvmt		NBL	NBT	NBR I	EBLn1V	VBLn1V	VBLn2	SBL	SBT	SBR		
Capacity (veh/h)		1097	-	-	314	205	587	999	-	-		
HCM Lane V/C Ratio		0.014	_	_		0.029			-	-		
HCM Control Delay (s)		8.3	-	_	16.7	23.1	11.4	8.7	-	-		
HCM Lane LOS		A	-	-	С	С	В	A	-	-		
HCM 95th %tile Q(veh)		0	-	-	0.1	0.1	0.1	0.1	-	-		
4(1011)		-										

Intersection												
Int Delay, s/veh	8											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ች		1	ሻ	ĵ.		ች	^	7	ሻ	^	7
Traffic Vol. veh/h	119	17	71	2	3	3	111	389	31	7	352	50
Future Vol, veh/h	119	17	71	2	3	3	111	389	31	7	352	50
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	Yield	-	-	None	-	-	None	-	-	None
Storage Length	100	_	230	0	_	-	160	_	175	160	_	125
Veh in Median Storage		0	-	-	0	_	-	0	-	-	0	-
Grade, %	,	0	_	_	0	_	_	3	_	_	-3	_
Peak Hour Factor	85	85	85	85	85	85	85	85	85	85	85	85
Heavy Vehicles, %	2	0	3	0	0	33	1	5	0	0	3	8
Mymt Flow	140	20	84	2	4	4	131	458	36	8	414	59
	170	20	0-7		7	T	101	,00	- 00		- 11-1	- 00
NA - ' /NA'	4' 0			P 4			1.1.4			\4.:C		
	/linor2	44		Minor1	1000		Major1			Major2		
Conflicting Flow All	923	1186	207	953	1209	229	473	0	0	494	0	0
Stage 1	430	430	-	720	720	-	-	-	-	-	-	-
Stage 2	493	756	-	233	489	-	-	-	-	-	-	-
Critical Hdwy	7.54	6.5	6.96	7.5	6.5	7.56	4.12	-	-	4.1	-	-
Critical Hdwy Stg 1	6.54	5.5	-	6.5	5.5	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.5	-	6.5	5.5	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4	3.33	3.5	4	3.63	2.21	-	-	2.2	-	-
Pot Cap-1 Maneuver	225	190	796	217	184	687	1092	-	-	1080	-	-
Stage 1	574	587	-	390	435	-	-	-	-	-	-	-
Stage 2	526	419	-	755	553	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	199	166	796	159	161	687	1092	-	-	1080	-	-
Mov Cap-2 Maneuver	199	166	-	159	161	-	-	-	-	-	-	-
Stage 1	505	583	-	343	383	-	-	-	-	-	-	-
Stage 2	456	369	-	648	549	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	38.8			21.4			1.8			0.1		
HCM LOS	Е			С								
Minor Lane/Major Mvm	t	NBL	NBT	NBR I	EBLn1 I	EBLn2 l	EBLn3V	VBLn1V	VBLn2	SBL	SBT	SBR
Capacity (veh/h)		1092	-	-	199	166	796	159	261	1080	-	-
HCM Lane V/C Ratio		0.12	-	_	0.704			0.015			-	-
HCM Control Delay (s)		8.7	-	-	57.3	29.6	10.1	28	19.2	8.4	_	-
HCM Lane LOS		A	-	-	F	D	В	D	С	A	-	-
HCM 95th %tile Q(veh)		0.4	_	-	4.4	0.4	0.3	0	0.1	0	-	-

Queues

1: WINCHESTER ST & JAMES MADISON HWY & LEE HWY

	ᄼ	→	1	•	•	4	†	-	-	↓	4	
Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Group Flow (vph)	275	869	68	1119	110	119	99	70	161	166	402	
v/c Ratio	0.74	0.54	0.51	0.77	0.12	0.67	0.54	0.19	0.55	0.55	0.70	
Control Delay	76.6	31.9	101.5	23.6	3.3	83.1	74.3	3.8	64.7	64.4	40.0	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	76.6	31.9	101.5	23.6	3.3	83.1	74.3	3.8	64.7	64.4	40.0	
Queue Length 50th (ft)	140	356	58	582	38	119	97	0	152	156	257	
Queue Length 95th (ft)	193	428	m119	192	m15	188	160	17	251	257	417	
Internal Link Dist (ft)		1315		334			509			538		
Turn Bay Length (ft)	250		130		200	250		125	215			
Base Capacity (vph)	412	1607	218	1486	922	222	232	465	301	311	581	
Starvation Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.67	0.54	0.31	0.75	0.12	0.54	0.43	0.15	0.53	0.53	0.69	
Intersection Summary												

m Volume for 95th percentile queue is metered by upstream signal.

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Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBL	NBT	NBR	SBL
Lane Configurations		ሽኘ	ħβ			ă	^	7	ሻ		7	ች
Traffic Volume (vph)	2	262	794	40	10	56	1074	106	114	95	67	231
Future Volume (vph)	2	262	794	40	10	56	1074	106	114	95	67	231
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Grade (%)			0%				-1%			2%		
Total Lost time (s)		7.8	5.2			6.9	5.8	9.4	8.3	8.3	6.9	9.4
Lane Util. Factor		0.97	0.95			1.00	0.95	1.00	1.00	1.00	1.00	0.95
Frpb, ped/bikes		1.00	1.00			1.00	1.00	0.99	1.00	1.00	0.98	1.00
Flpb, ped/bikes		1.00	1.00			1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		1.00	0.99			1.00	1.00	0.85	1.00	1.00	0.85	1.00
Flt Protected		0.95	1.00			0.95	1.00	1.00	0.95	1.00	1.00	0.95
Satd. Flow (prot)		3400	3512			1814	3557	1570	1787	1862	1563	1715
Flt Permitted		0.95	1.00			0.95	1.00	1.00	0.95	1.00	1.00	0.95
Satd. Flow (perm)		3400	3512			1814	3557	1570	1787	1862	1563	1715
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	2	273	827	42	10	58	1119	110	119	99	70	241
RTOR Reduction (vph)	0	0	2	0	0	0	0	37	0	0	58	0
Lane Group Flow (vph)	0	275	867	0	0	68	1119	73	119	99	12	161
Confl. Peds. (#/hr)				3	•			5	2		6	6
Heavy Vehicles (%)	0%	3%	2%	0%	0%	0%	2%	2%	0%	1%	0%	1%
Turn Type	Prot	Prot	NA		Prot	Prot	NA	pm+ov	Split	NA	custom	Split
Protected Phases	5	5	2		1	1	6	4	3	3	Cactom	4
Permitted Phases		· ·	=		•	•		6	Ū		13	•
Actuated Green, G (s)		16.5	68.6			11.1	61.7	87.3	14.9	14.9	26.0	25.6
Effective Green, g (s)		16.5	68.6			11.1	61.7	87.3	14.9	14.9	26.0	25.6
Actuated g/C Ratio		0.11	0.46			0.07	0.41	0.58	0.10	0.10	0.17	0.17
Clearance Time (s)		7.8	5.2			6.9	5.8	9.4	8.3	8.3	0.11	9.4
Vehicle Extension (s)		3.0	3.0			3.0	3.0	3.0	3.0	3.0		3.0
Lane Grp Cap (vph)		374	1606			134	1463	913	177	184	270	292
v/s Ratio Prot		0.08	c0.25			0.04	c0.31	0.01	c0.07	0.05	210	0.09
v/s Ratio Perm		0.00	00.20			0.04	60.01	0.03	00.07	0.00	0.01	0.03
v/c Ratio		0.74	0.54			0.51	0.76	0.08	0.67	0.54	0.04	0.55
Uniform Delay, d1		64.6	29.3			66.8	37.9	13.7	65.2	64.3	51.7	56.9
Progression Factor		1.00	1.00			1.36	0.51	1.22	1.00	1.00	1.00	1.00
Incremental Delay, d2		7.3	1.3			2.6	3.3	0.0	9.6	3.0	0.1	2.2
Delay (s)		72.0	30.6			93.8	22.7	16.8	74.8	67.3	51.7	59.2
Level of Service		72.0 E	C			55.0 F	C	В	74.0 E	67.5	D	55.Z E
Approach Delay (s)		<u>L</u>	40.6			1	25.9	D	<u>L</u>	66.6	U	
Approach LOS			70.0 D				23.3 C			E		
Intersection Summary												
HCM 2000 Control Delay			39.4	Н	CM 2000	Level of	Service		D			
HCM 2000 Volume to Capacity	/ ratio		0.77									
Actuated Cycle Length (s)			150.0	S	um of lost	time (s)			31.3			
Intersection Capacity Utilization	n		98.1%		CU Level o)		F			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	SBT	SBR
Lane Configurations	<u>ુટ</u> ા	7
Traffic Volume (vph)	83	386
Future Volume (vph)	83	386
Ideal Flow (vphpl)	1900	1900
Grade (%)	-2%	,,,,,
Total Lost time (s)	9.4	9.4
Lane Util. Factor	0.95	1.00
Frpb, ped/bikes	1.00	0.99
Flpb, ped/bikes	1.00	1.00
Frt	1.00	0.85
Flt Protected	0.98	1.00
Satd. Flow (prot)	1772	1545
Flt Permitted	0.98	1.00
Satd. Flow (perm)	1772	1545
Peak-hour factor, PHF	0.96	0.96
Adj. Flow (vph)	86	402
RTOR Reduction (vph)	0	60
Lane Group Flow (vph)	166	342
Confl. Peds. (#/hr)	100	2
Heavy Vehicles (%)	0%	4%
Turn Type		custom
Protected Phases	4	odotom
Permitted Phases		4 5
Actuated Green, G (s)	25.6	51.5
Effective Green, g (s)	25.6	51.5
Actuated g/C Ratio	0.17	0.34
Clearance Time (s)	9.4	J.0-7
Vehicle Extension (s)	3.0	
Lane Grp Cap (vph)	302	530
v/s Ratio Prot	0.09	550
v/s Ratio Perm	0.03	c0.22
v/c Ratio	0.55	0.64
Uniform Delay, d1	56.9	41.5
Progression Factor	1.00	1.00
Incremental Delay, d2	2.0	2.7
Delay (s)	59.0	44.2
Level of Service	59.0 E	44.2 D
Approach Delay (s)	50.9	U
Approach LOS	50.9 D	
Intersection Summary		

HCM 6th Edition methodology expects strict NEMA phasing.

Intersection												
Int Delay, s/veh	0.6											
	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Movement	EDL			WDL			INDL	INDI		ODL	ODI	
Lane Configurations	^	^	7	^	^	100	^	^	7	^	0	70
Traffic Vol, veh/h	0	1019	83	0	1167	102	0	0	25	0	0	79
Future Vol, veh/h	0	1019	83	0	1167	102	0	0	25	0	0	79
Conflicting Peds, #/hr	_ 0	0	0	0	0	4	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	110	-	-	300	-	-	0	-	-	0
Veh in Median Storage,		0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	1	-	-	3	-	-	3	-	-	-11	-
Peak Hour Factor	93	93	93	93	93	93	93	93	93	93	93	93
Heavy Vehicles, %	0	2	0	0	2	0	0	0	4	0	0	0
Mvmt Flow	0	1096	89	0	1255	110	0	0	27	0	0	85
Major/Minor M	lajor1		N	/lajor2		N	/linor1		N	/linor2		
Conflicting Flow All	-	0	0	-	-	0	-	-	548	-	-	632
Stage 1	-	_	-	_	_	-	-	-		-	-	
Stage 2	_	_	_	_	_	_	_	_	_	_	_	_
Critical Hdwy	_	-	-	_	-	_	-	-	7.28	_	-	5.8
Critical Hdwy Stg 1	_	_	_	_	_	_	_	_	-	_	_	-
Critical Hdwy Stg 2	_	-	-	_	-	_	_	-	-	_	-	_
Follow-up Hdwy	_	_	_	_	_	_	_	_	3.34	_	_	3.3
Pot Cap-1 Maneuver	0	-	-	0	_	_	0	0	454	0	0	519
Stage 1	0	_	_	0	_	_	0	0	-	0	0	-
Stage 2	0	_	_	0	_	_	0	0	_	0	0	_
Platoon blocked, %	_	_	_		_	_						
Mov Cap-1 Maneuver	_	-	-	_	-	_	-	-	454	_	-	517
Mov Cap-2 Maneuver	_	_	_	_	_	_	_	_	-	_	_	-
Stage 1	_	_	_	_	_	_	_	_	_	_	_	_
Stage 2	_	_	_	_	_	_	_	_	_	_	_	_
Clayo L												
A				14/0			ND			0.0		
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			0			13.4			13.3		
HCM LOS							В			В		
Minor Lane/Major Mvmt		NBLn1	EBT	EBR	WBT	WBR S	SBLn1					
Capacity (veh/h)		454	-	-	_	-	517					
HCM Lane V/C Ratio		0.059	_	_	_	_	0.164					
HCM Control Delay (s)		13.4	-	_	_	_	13.3					
HCM Lane LOS		В	_	_	_	_	В					
HCM 95th %tile Q(veh)		0.2	-	_	-	_	0.6					
		J.L					3.0					

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBT	NBR	SBT	SBR	
Lane Group Flow (vph)	147	949	2	68	1160	88	36	79	165	148	
v/c Ratio	0.72	0.44	0.00	0.54	0.63	0.10	0.31	0.30	0.76	0.44	
Control Delay	87.4	12.5	0.0	82.0	28.6	0.2	72.2	3.0	85.8	10.0	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	87.4	12.5	0.0	82.0	28.6	0.2	72.2	3.0	85.8	10.0	
Queue Length 50th (ft)	157	212	0	68	427	0	36	0	164	0	
Queue Length 95th (ft)	225	226	m0	123	610	0	73	0	249	53	
Internal Link Dist (ft)		457			1504		131		565		
Turn Bay Length (ft)	240		330	150		150		60			
Base Capacity (vph)	260	2159	993	157	1853	907	202	327	250	363	
Starvation Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.57	0.44	0.00	0.43	0.63	0.10	0.18	0.24	0.66	0.41	
Intersection Summary											

m Volume for 95th percentile queue is metered by upstream signal.

	•	۶	→	•	•	•	•	•	†	/	>	
Movement	EBU	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT
Lane Configurations		ă	^	7	ሻ	^	7		4	7		4
Traffic Volume (vph)	9	131	902	2	65	1102	84	17	17	75	139	18
Future Volume (vph)	9	131	902	2	65	1102	84	17	17	75	139	18
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Grade (%)			-4%			2%			0%			-1%
Total Lost time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.6	6.6		7.5
Lane Util. Factor		1.00	0.95	1.00	1.00	0.95	1.00		1.00	1.00		1.00
Frpb, ped/bikes		1.00	1.00	0.97	1.00	1.00	0.98		1.00	1.00		1.00
Flpb, ped/bikes		1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00
Frt		1.00	1.00	0.85	1.00	1.00	0.85		1.00	0.85		1.00
Flt Protected		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (prot)		1807	3682	1602	1787	3504	1558		1854	1615		1813
Flt Permitted		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (perm)		1807	3682	1602	1787	3504	1558		1854	1615		1813
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	9	138	949	2	68	1160	88	18	18	79	146	19
RTOR Reduction (vph)	0	0	0	1	0	0	41	0	0	74	0	0
Lane Group Flow (vph)	0	147	949	1	68	1160	47	0	36	5	0	165
Confl. Peds. (#/hr)				2			2					
Heavy Vehicles (%)	0%	2%	0%	0%	0%	2%	1%	0%	0%	0%	1%	0%
Turn Type	Prot	Prot	NA	Perm	Prot	NA	Perm	Split	NA	Perm	Split	NA
Protected Phases	1	1	6	. 0	5	2	. 0	4	4	. 0	3	3
Permitted Phases	•	•	•	6	•	=	2	•	•	4		J
Actuated Green, G (s)		17.1	86.7	86.7	9.3	79.4	79.4		9.5	9.5		17.9
Effective Green, g (s)		17.1	86.7	86.7	9.3	79.4	79.4		9.5	9.5		17.9
Actuated g/C Ratio		0.11	0.58	0.58	0.06	0.53	0.53		0.06	0.06		0.12
Clearance Time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.6	6.6		7.5
Vehicle Extension (s)		3.0	3.0	3.0	3.0	3.0	3.0		3.0	3.0		3.0
Lane Grp Cap (vph)		205	2128	925	110	1854	824		117	102		216
v/s Ratio Prot		c0.08	0.26	320	0.04	c0.33	UZT		c0.02	102		c0.09
v/s Ratio Perm		60.00	0.20	0.00	0.04	00.00	0.03		00.02	0.00		00.03
v/c Ratio		0.72	0.45	0.00	0.62	0.63	0.06		0.31	0.05		0.76
Uniform Delay, d1		64.1	18.0	13.4	68.6	24.8	17.1		67.1	66.0		64.0
Progression Factor		1.10	0.61	1.00	1.00	1.00	1.00		1.00	1.00		1.00
Incremental Delay, d2		10.2	0.6	0.0	9.9	1.6	0.1		1.5	0.2		14.8
Delay (s)		80.8	11.6	13.4	78.5	26.4	17.3		68.6	66.2		78.8
Level of Service		F	В	13. 4 B	70.5 E	C	17.3 B		E	60.2 E		70.0 E
Approach Delay (s)		ı	20.9	U	<u> </u>	28.5	U		67.0	<u> </u>		69.4
Approach LOS			20.9 C			20.5 C			67.0 E			03.4 E
<u> </u>												
Intersection Summary												
HCM 2000 Control Delay			31.6	H	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capacity	/ ratio		0.64									
Actuated Cycle Length (s)			150.0		um of los				26.6			
Intersection Capacity Utilization	n		73.7%	IC	U Level	of Service			D			
Analysis Period (min)			15									
c Critical Lane Group												



Movement	SBR
Lane Configurations	SDR 7
Traffic Volume (vph)	141
Future Volume (vph)	141
Ideal Flow (vphpl)	1900
Grade (%)	1900
Total Lost time (s)	7.5
Lane Util. Factor	1.00
Frpb, ped/bikes	1.00
Flpb, ped/bikes	1.00
Fipo, pea/bikes Frt	0.85
Fit Protected	1.00
	1607
Satd. Flow (prot) Flt Permitted	1.00
Satd. Flow (perm)	1607
Peak-hour factor, PHF	0.95
Adj. Flow (vph)	148
RTOR Reduction (vph)	130
Lane Group Flow (vph)	18
Confl. Peds. (#/hr)	
Heavy Vehicles (%)	1%
Turn Type	Perm
Protected Phases	
Permitted Phases	3
Actuated Green, G (s)	17.9
Effective Green, g (s)	17.9
Actuated g/C Ratio	0.12
Clearance Time (s)	7.5
Vehicle Extension (s)	3.0
Lane Grp Cap (vph)	191
v/s Ratio Prot	
v/s Ratio Perm	0.01
v/c Ratio	0.09
Uniform Delay, d1	58.8
Progression Factor	1.00
Incremental Delay, d2	0.2
Delay (s)	59.0
Level of Service	E
Approach Delay (s)	
Approach LOS	
Intersection Summary	

HCM 6th Edition methodology expects strict NEMA phasing.

Movement EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR SBL SBT SBL SBT SBR SBL SBT	Intersection												
Lane Configurations		8.9											
Traffic Vol, veh/h Traffi	Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Traffic Vol, veh/h Traffi	Lane Configurations		4			43-			4Tb			4Tb	
Conflicting Peds, #/hr		17		116	45		41	94		12	48		32
Conflicting Peds, #/hr	Future Vol., veh/h	17	77	116	45	50	41	94	43	12	48	39	32
Sign Control Stop	<u> </u>	0	0	14	14	0	0	0	0	0	0	0	0
RT Channelized	•	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
Storage Length													None
Veh in Median Storage, # 0 - - 0 - - 0 - 0 - 0 - 0 - 0 - 0 - 0 0 - 0 0 - - 0 96	Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Peak Hour Factor		# -	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	Grade, %	-	-8	-	-	-2	-	-	1	-	-	-1	-
Mynt Flow 18 80 121 47 52 43 98 45 13 50 41 33 Major/Minor Minor2 Minor1 Major1 Major2 Conflicting Flow All 403 412 51 423 422 29 74 0 0 58 0 0 Stage 1 158 158 - 248 248 -	Peak Hour Factor	96	96	96	96	96	96	96	96	96	96	96	96
Mymt Flow 18 80 121 47 52 43 98 45 13 50 41 33 Major/Minor Minor1 Major1 Major2 Conflicting Flow All 403 412 51 423 422 29 74 0 0 58 0 0 Stage 1 158 158 - 248 248 -	Heavy Vehicles, %	0	0	2	0	2	5	0	2	0	0	3	0
Conflicting Flow All	Mvmt Flow	18	80	121	47	52	43	98	45	13	50	41	33
Conflicting Flow All													
Stage 1 158 158 - 248 248 -	Major/Minor N	/linor2		N	Minor1			Major1		<u> </u>	Major2		
Stage 1 158 158 - 248 248 -	Conflicting Flow All	403	412	51	423	422	29	74	0	0	58	0	0
Stage 2		158	158	-	248	248	-	-	-	-	-	-	-
Critical Hdwy 5.9 4.9 6.14 7.1 6.14 6.8 4.1 - - 4.1 -		245	254	-	175	174	-	-	-	-	-	-	-
Critical Hdwy Stg 1 4.9 3.9 - 6.1 5.14 - - - - - - - - - - - - - - - - - <		5.9	4.9	6.14	7.1	6.14	6.8	4.1	-	-	4.1	-	-
Follow-up Hdwy 3.5 4 3.32 3.5 4.02 3.35 2.2 - 2.2 2.2 Pot Cap-1 Maneuver 642 640 1018 545 547 1031 1538 - 1559 Stage 1 895 827 - 760 720		4.9	3.9	-	6.1	5.14	-	-	-	-	-	-	-
Follow-up Hdwy 3.5 4 3.32 3.5 4.02 3.35 2.2 - 2.2 2.2 Pot Cap-1 Maneuver 642 640 1018 545 547 1031 1538 - 1559 Stage 1 895 827 - 760 720	, ,			-	6.1		-	-	-	-	-	-	-
Pot Cap-1 Maneuver		3.5	4	3.32	3.5	4.02	3.35	2.2	-	-	2.2	-	-
Stage 1 895 827 - 760 720 -			640			547		1538	-	-		-	-
Stage 2 828 784 - 832 769 -	•		827			720	-	-	-	-	-	-	-
Platoon blocked, %		828	784	-	832	769	-	-	-	-	-	-	-
Mov Cap-2 Maneuver 524 577 - 392 493 - </td <td>Platoon blocked, %</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td>-</td> <td></td> <td>-</td> <td>-</td>	Platoon blocked, %								-	-		-	-
Stage 1 836 799 - 710 672 -	Mov Cap-1 Maneuver	524	577	1006	392	493	1031	1538	-	-	1559	-	-
Stage 2 684 732 - 629 743 -	Mov Cap-2 Maneuver	524	577	-	392	493	-	-	-	-	-	-	-
Approach EB WB NB SB HCM Control Delay, s 11.8 14.2 4.7 3 HCM LOS B B Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR Capacity (veh/h) 1538 - - 747 531 1559 - - HCM Lane V/C Ratio 0.064 - - 0.293 0.267 0.032 - - HCM Control Delay (s) 7.5 0 - 11.8 14.2 7.4 0 - HCM Lane LOS A A - B B A A -	Stage 1	836	799	-	710	672	-	-	-	-	-	-	-
HCM Control Delay, s 11.8	Stage 2	684	732	-	629	743	-	-	-	-	-	-	-
HCM Control Delay, s 11.8													
Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR Capacity (veh/h) 1538 - - 747 531 1559 - - HCM Lane V/C Ratio 0.064 - - 0.293 0.267 0.032 - - HCM Control Delay (s) 7.5 0 - 11.8 14.2 7.4 0 - HCM Lane LOS A A - B B A A -	Approach	EB											
Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR Capacity (veh/h) 1538 - - 747 531 1559 - - HCM Lane V/C Ratio 0.064 - - 0.293 0.267 0.032 - - HCM Control Delay (s) 7.5 0 - 11.8 14.2 7.4 0 - HCM Lane LOS A A - B B A A	•	11.8			14.2			4.7			3		
Capacity (veh/h) 1538 - - 747 531 1559 - - HCM Lane V/C Ratio 0.064 - - 0.293 0.267 0.032 - - HCM Control Delay (s) 7.5 0 - 11.8 14.2 7.4 0 - HCM Lane LOS A A - B B A A	HCM LOS	В			В								
Capacity (veh/h) 1538 - - 747 531 1559 - - HCM Lane V/C Ratio 0.064 - - 0.293 0.267 0.032 - - HCM Control Delay (s) 7.5 0 - 11.8 14.2 7.4 0 - HCM Lane LOS A A - B B A A -													
HCM Lane V/C Ratio 0.064 - - 0.293 0.267 0.032 - - HCM Control Delay (s) 7.5 0 - 11.8 14.2 7.4 0 - HCM Lane LOS A A - B B A A -		t		NBT	NBR I				SBT	SBR			
HCM Control Delay (s) 7.5 0 - 11.8 14.2 7.4 0 - HCM Lane LOS A A - B B A A -				-	-				-	-			
HCM Lane LOS A A - B B A A -					-					-			
	• • • • • • • • • • • • • • • • • • • •				-					-			
HCM 95th %tile Q(veh) 0.2 1.2 1.1 0.1				Α	-				Α	-			
	HCM 95th %tile Q(veh)		0.2	-	-	1.2	1.1	0.1	-	-			

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Intersection												
Int Delay, s/veh	3.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			र्स	7		4	
Traffic Vol, veh/h	3		86	28	112	2	62	2	37	1	5	1
Future Vol, veh/h	3	106	86	28	112	2	62	2	37	1	5	1
Conflicting Peds, #/hr	4	0	0	0	0	4	0	0	2	2	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	_	None	-	-	None	-	-	None	-	-	None
Storage Length	-	_	-	-	-	-	-	-	0	-	-	-
Veh in Median Storage.	.# -	0	-	_	0	-	-	0	_	-	0	_
Grade, %	-	0	-	-	1	_	-	2	_	-	-5	-
Peak Hour Factor	89	89	89	89	89	89	89	89	89	89	89	89
Heavy Vehicles, %	0	3	0	4	1	0	3	0	3	0	0	0
Mvmt Flow	3	119	97	31	126	2	70	2	42	1	6	1
Major/Minor N	/lajor1			Major2		ı	Minor1		N	/linor2		
Conflicting Flow All	132	0	0	216	0	0	367	368	170	391	415	131
Stage 1	-	-	_		-	-	174	174	-	193	193	-
Stage 2	_	_	_	_	_	-	193	194	_	198	222	_
Critical Hdwy	4.1	-	-	4.14	_	_	7.53	6.9	6.43	6.1	5.5	5.7
Critical Hdwy Stg 1	-	_	_	-	_	-	6.53	5.9	-	5.1	4.5	-
Critical Hdwy Stg 2	-	-	_	-	_	_	6.53	5.9	_	5.1	4.5	-
Follow-up Hdwy	2.2	_	_	2.236	_	-	3.527	4	3.327	3.5	4	3.3
Pot Cap-1 Maneuver	1466	-	_	1342	_	_	564	542	863	637	596	941
Stage 1	-	-	-	-	-	-	810	744	-	858	786	-
Stage 2	_	-	-	-	-	-	789	728	-	854	769	-
Platoon blocked, %		-	-		-	-						
Mov Cap-1 Maneuver	1461	-	-	1342	-	-	548	526	862	589	578	938
Mov Cap-2 Maneuver	-	-	-	-	-	-	548	526	-	589	578	-
Stage 1	-	-	-	-	-	-	808	743	-	854	764	-
Stage 2	-	-	-	-	-	-	763	708	-	807	767	-
Ŭ ²												
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0.1			1.5			11.4			10.9		
HCM LOS							В			В		
Minor Lane/Major Mvm	t	NBLn1 I	NBLn2	EBL	EBT	EBR	WBL	WBT	WBR	SBL _{n1}		
Capacity (veh/h)		547	862	1461	-	-	1342	-	-	613		
HCM Lane V/C Ratio		0.131	0.048	0.002	-	-	0.023	-	-	0.013		
HCM Control Delay (s)		12.6	9.4	7.5	0	-	7.7	0	-	10.9		
HCM Lane LOS		В	Α	Α	Α	-	Α	Α	-	В		
HCM 95th %tile Q(veh)		0.5	0.2	0	-	-	0.1	-	-	0		

Intersection						
Int Delay, s/veh	3.6					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations			₽		¥	
Traffic Vol, veh/h	42	128	160	14	67	52
Future Vol, veh/h	42	128	160	14	67	52
Conflicting Peds, #/hr	1	0	0	1	2	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage	э,# -	0	0	-	0	-
Grade, %	-	-3	1	-	-5	-
Peak Hour Factor	85	85	85	85	85	85
Heavy Vehicles, %	2	2	2	0	0	2
Mvmt Flow	49	151	188	16	79	61
Majar/Minar	Maiaut		10:00		Aire and	
	Major1		//ajor2		/linor2	407
Conflicting Flow All	205	0	-	0	448	197
Stage 1	-	-	-	-	197	-
Stage 2	-	-	-	-	251	-
Critical Hdwy	4.12	-	-	-	5.4	5.72
Critical Hdwy Stg 1	-	-	-	-	4.4	-
Critical Hdwy Stg 2	-	-	-	-	4.4	-
Follow-up Hdwy	2.218	-	-	-		3.318
Pot Cap-1 Maneuver	1366	-	-	-	648	868
Stage 1	-	-	-	-	888	-
Stage 2	-	_	-	-	853	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	1365	-	-	-	621	867
Mov Cap-2 Maneuver	-	-	-	-	621	-
Stage 1	-	-	-	-	852	-
Stage 2	-	-	-	-	852	-
Ü						
	-		1A/D		0.0	
Approach	EB		WB		SB	
HCM Control Delay, s	1.9		0		11.3	
HCM LOS					В	
Minor Lane/Major Mvn	nt	EBL	EBT	WBT	WBR :	SRI n1
Capacity (veh/h)		1365		****	-	709
HCM Lane V/C Ratio		0.036		-		0.197
HCM Control Delay (s	\	7.7		-	-	
HCM Lane LOS)		-	-		
	.\	A	-	-	-	B
HCM 95th %tile Q(veh)	0.1	-	-	-	0.7

-							
Intersection							
Int Delay, s/veh	1						
	EDI	EDT	WDT	WDD	CDI	CDD	
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	ሻ	150	210	0	<u>ነ</u>	77	
Traffic Vol, veh/h	5	159	210	2	11	27	
Future Vol, veh/h	5	159	210	2	11	27	
Conflicting Peds, #/hr		0	0	1	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-		-	None	
Storage Length	75	-	-	-	0	50	
Veh in Median Storag		0	0	-	0	-	
Grade, %	-	-5	3	-	0	-	
Peak Hour Factor	85	85	85	85	85	85	
Heavy Vehicles, %	0	3	2	0	0	0	
Mvmt Flow	6	187	247	2	13	32	
Major/Minor	Major1	N	Major2	ı	Minor2		
Conflicting Flow All	250	0	-	0	448	249	
Stage 1	-	-	_	-	249	-	
Stage 2	_	_	_	_	199	-	
Critical Hdwy	4.1	-	-	_	6.4	6.2	
Critical Hdwy Stg 1	-	_	_	_	5.4	-	
Critical Hdwy Stg 2	-	-	-	_	5.4	_	
Follow-up Hdwy	2.2	_	_	_	3.5	3.3	
Pot Cap-1 Maneuver	1327	-	-	_	572	795	
Stage 1	-	_	_	-	797	-	
Stage 2	_	-	_	_	839	-	
Platoon blocked, %		_	_	_	- 555		
Mov Cap-1 Maneuver	1326	_	_	_	568	794	
Mov Cap-2 Maneuver		_	_	_	568	-	
Stage 1	_	_	_	_	792	_	
Stage 2	<u>-</u>	<u>-</u>	_	_	838	_	
Clago 2					300		
Approach	EB		WB		SB		
HCM Control Delay, s	0.2		0		10.2		
HCM LOS					В		
Minor Lane/Major Mv	mt	EBL	EBT	WBT	WRR	SBLn1	SRI n2
	iiic	1326	LUI	וטיי	VVDIC	568	794
Capacity (veh/h) HCM Lane V/C Ratio		0.004	-	-	-	0.023	0.04
HCM Control Delay (s	-1	7.7	-				9.7
HCM Lane LOS)		-		-	11.5 B	
	h)	A	-	-	_		A
HCM 95th %tile Q(vel	n)	0	-	-	-	0.1	0.1

Intersection												
Int Delay, s/veh	5.9											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			सी	7	ች	^	7		^	
Traffic Vol, veh/h	2	1	4	98	1	139	2	370	77	86	501	2
Future Vol, veh/h	2	1	4	98	1	139	2	370	77	86	501	2
Conflicting Peds, #/hr	0	0	0	0	0	0	4	0	1	1	0	4
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	100	-	0	90	-	130	225	-	-
Veh in Median Storage,	, # -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	-2	-	-	4	-	-	2	-	-	3	-
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90
Heavy Vehicles, %	0	0	0	1	0	2	0	3	4	1	4	0
Mvmt Flow	2	1	4	109	1	154	2	411	86	96	557	2
Major/Minor N	/linor2			Minor1			Major1		<u> </u>	Major2		
Conflicting Flow All	964	1256	284	887	1171	207	563	0	0	498	0	0
Stage 1	754	754	-	416	416	-	-	-	-	-	-	-
Stage 2	210	502	-	471	755	-	-	-	-	-	-	-
Critical Hdwy	7.1	6.1	6.7	8.32	7.3	7.34	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.1	5.1	-	7.32	6.3	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.1	5.1	-	7.32	6.3	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4	3.3	3.51	4	3.32	2.2	-	-	2.21	-	-
Pot Cap-1 Maneuver	237	199	730	197	150	781	1019	-	-	1069	-	-
Stage 1	404	457	-	535	543	-	-	-	-	-	-	-
Stage 2	797	577	-	491	355	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	175	180	728	181	136	780	1016	-	-	1068	-	-
Mov Cap-2 Maneuver	175	180	-	181	136	-	-	-	-	-	-	-
Stage 1	402	414	-	533	541	-	-	-	-	-	-	-
Stage 2	637	575	-	443	322	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	16.9			28			0			1.3		
HCM LOS	С			D								
Minor Lane/Major Mvm	t	NBL	NBT	NBR I	EBLn1V	VBLn1V	VBLn2	SBL	SBT	SBR		
Capacity (veh/h)		1016	-	-	311	180	780	1068	-	-		
HCM Lane V/C Ratio		0.002	_	_		0.611			_	_		
HCM Control Delay (s)		8.6	_	_	16.9	52.2	10.8	8.7	_	-		
HCM Lane LOS		A	-	-	С	F	В	A	_	-		
HCM 95th %tile Q(veh)		0	-	-	0.1	3.4	0.7	0.3	-	-		

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Intersection												
Int Delay, s/veh	2.1											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			ĵ.		ች	^	1		^	
Traffic Vol, veh/h	10	1	17	33	1	38	15	401	15	41	556	6
Future Vol, veh/h	10	1	17	33	1	38	15	401	15	41	556	6
Conflicting Peds, #/hr	0	0	0	0	0	0	5	0	0	0	0	5
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	0	-	-	150	-	135	110	-	-
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	5	-	-	3	-	-	4	-	-	-2	-
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90
Heavy Vehicles, %	0	0	0	0	0	5	0	3	0	0	3	0
Mvmt Flow	11	1	19	37	1	42	17	446	17	46	618	7
Major/Minor N	1inor2		N	Minor1		ľ	Major1			Major2		
Conflicting Flow All	977	1216	318	882	1202	223	630	0	0	463	0	0
Stage 1	719	719	-	480	480		-	-	-	-	-	-
Stage 2	258	497	-	402	722	-	-	-	_	-	-	-
Critical Hdwy	8.5	7.5	7.4	8.1	7.1	7.3	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	7.5	6.5	-	7.1	6.1	-	-	-	-	-	-	-
Critical Hdwy Stg 2	7.5	6.5	-	7.1	6.1	-	_	-	-	-	-	-
Follow-up Hdwy	3.5	4	3.3	3.5	4	3.35	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	159	130	654	211	152	757	962	-	-	1109	-	-
Stage 1	320	357	-	499	515	-	-	-	-	-	-	-
Stage 2	679	477	-	562	385	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	142	122	651	194	143	757	958	-	-	1109	-	-
Mov Cap-2 Maneuver	142	122	-	194	143	-	-	-	-	-	-	-
Stage 1	313	341	-	490	506	-	-	-	-	-	-	-
Stage 2	628	468	-	521	368	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	20.3			18.5			0.3			0.6		
HCM LOS	С			С								
Minor Lane/Major Mvmt		NBL	NBT	NBR E	EBLn1V	VBLn1V	VBLn2	SBL	SBT	SBR		
Capacity (veh/h)		958	_	_	267	194	682	1109	_	_		
HCM Lane V/C Ratio		0.017	_	_		0.189			_	_		
HCM Control Delay (s)		8.8	-	-	20.3	27.8	10.6	8.4	_	-		
HCM Lane LOS		A	_	_	C	D	В	A	_	_		
HCM 95th %tile Q(veh)		0.1	-	-	0.4	0.7	0.2	0.1	-	-		
// (1011)		J. ,			7.1	V.	7.2	J .,				

Intersection												
Int Delay, s/veh	8.8											
• •	EBL	EBT	EBR	\\/DI	WDT	WDD	NDI	NDT	NDD	CDI	CDT	SBR
Movement				WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	
Lane Configurations	\	↑	164	أ	}	0.5	ሻ	^	77	<u> </u>	^	100
Traffic Vol, veh/h	96	61	164	43	27	25	76	310	77	7	493	106
Future Vol, veh/h	96	61	164	43	27	25	76	310	77	7	493	106
Conflicting Peds, #/hr	6	0	0	0	0	6	0	0	3	3	0	_ 0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	Yield	-	-	None	-	-	None	-	-	None
Storage Length	100	-	230	0	-	-	160	-	175	160	-	125
Veh in Median Storage,	, # -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	3	-	-	-3	-
Peak Hour Factor	91	91	91	91	91	91	91	91	91	91	91	91
Heavy Vehicles, %	2	0	1	0	0	0	1	3	0	0	4	1
Mvmt Flow	105	67	180	47	30	27	84	341	85	8	542	116
Major/Minor N	/linor2		N	Minor1		N	Major1			Major2		
Conflicting Flow All	918	1155	271	833	1186	180	658	0	0	429	0	0
Stage 1	558	558		512	512	-	-	-	-		-	-
Stage 2	360	597	_	321	674	_	_	_	_	_	_	_
Critical Hdwy	7.54	6.5	6.92	7.5	6.5	6.9	4.12	-	-	4.1	-	-
Critical Hdwy Stg 1	6.54	5.5	-	6.5	5.5	-		_	_	-	_	_
Critical Hdwy Stg 2	6.54	5.5	-	6.5	5.5	-	-	-	_	-	-	-
Follow-up Hdwy	3.52	4	3.31	3.5	4	3.3	2.21	_	_	2.2	_	_
Pot Cap-1 Maneuver	227	199	730	265	190	838	932	_	_	1141	-	-
Stage 1	482	515	-	518	540	-	-	_	_	-	_	_
Stage 2	631	495	_	671	457	_	_	_	_	_	_	_
Platoon blocked, %	30 1	.00		VI 1	.01			_	_		_	_
Mov Cap-1 Maneuver	176	179	730	131	171	832	932	_	_	1138	_	_
Mov Cap-2 Maneuver	176	179	-	131	171	- 002	-	_	_	-	_	_
Stage 1	439	511	_	470	490	_	_	_	_	_	_	_
Stage 2	519	449	_	436	454	_	_	_	_	_	_	_
Olugo Z	010	770		700	707							
A I				14/0			NE			0.0		
Approach	EB			WB			NB			SB		
HCM Control Delay, s	28.4			33			1.5			0.1		
HCM LOS	D			D								
Minor Lane/Major Mvm	t	NBL	NBT	NBR I	EBLn1	EBLn2 E	EBLn3V	VBLn1V	VBLn2	SBL	SBT	SBR
Capacity (veh/h)		932	-	-	176	179	730	131	277	1138	_	-
HCM Lane V/C Ratio		0.09	-	_	0.599	0.374				0.007	-	-
HCM Control Delay (s)		9.2	-	-	52.1	36.7	11.5	47.2	21.3	8.2	-	-
HCM Lane LOS		A	_	_	F	E	В	E	С	A	_	_
HCM 95th %tile Q(veh)		0.3	-	-	3.3	1.6	1	1.5	0.8	0	-	-

G.	Background	Development	t and Roadwa	y Improvement	Excerpts



TOWN OF WARRENTON CAPITAL IMPROVEMENT PROGRAM

2023 - 2028

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- f. Stormwater & Utilities (U)

Mission Statement

In Cooperation With, And For Our Citizens...

...The Mayor, Town Council and the Staff of Warrenton are dedicated to providing public safety, economic opportunity, and quality public services in an attractive, well-planned community with historic character for the benefit, enjoyment and accessibility of all.

Affirmed by Town Council August 28, 2018

Vision and Value Statement

To Achieve Our Mission, We Strive To...

•••

Provide high level services in a cost-effective manner; display honesty, respectfulness, and fairness in all relationships; support the health and economic well-being of our citizens and businesses; preserve our historic small-town character; encourage opportunities, services and infrastructure that allow people of all means to live, work and visit here; and address public concerns and opportunities promptly and effectively.

We recognize our Mission can be achieved only by the exchange of information and that through teamwork we can maintain an environment in which we can maximize our potential.

Affirmed by Town Council August 28, 2018

INTRODUCTION

The Capital Improvement Program (CIP) provides for an orderly implementation of short and long range plans for construction of Capital Improvement Projects and Land Acquisition. It further provides for the scheduling of the associated expenditures over a period of many years. The first year of the program represents the proposed Capital Budget for the Fiscal Year. In addition, consideration is given to the project's relations to other improvements and plans, and the Town's current and anticipated financial capabilities. The CIP is updated annually, at which time the schedule and the projects reevaluated, new or deferred projects are added, and the time frame is extended by one additional fiscal year.

The Town of Warrenton continues to enhance the structure of the budget and provide a greater understanding of funding commitments. Projects are presented under topical categories to help the community understand the investments that are being proposed and the tie in to priorities of the Town. Next, a Capital Asset Replacement Program (CARP) includes projects that cover standard operating and maintenance items. Unlike items listed in the capital project and acquisition program, these are items necessary for the ongoing operations of the Town and its facilities. Finally, the Town created dedicated Utilities and Stormwater Funds. These modifications to the CIP help move it towards a clearer document that works in conjunction with the budget and stated needs of the community.

POLICY

The following policies guide the development of the CIP:

- 1. The CIP should be realistic relative to the projected source of revenue.
- 2. A reserve fund should be established, as required, to reduce the fiscal impact of major projects in a single year.
- 3. Projects undertaken in the Enterprise Fund and Stormwater Fund are to be considered separate from the general Fund.

BENEFITS

A carefully planned CIP will enable the Town to realize several benefits:

- 1. Major improvements can be anticipated in advance, rather than addressed at the time the need arises.
- 2. The implementation strategy of the Comprehensive Plan is used as a guide for future needs and investments.
- 3. The Town Council and Planning Commission are better able to evaluate the needs of the entire community, instead of special projects.
- 4. Projects can be scheduled when revenue is available and when the community's anticipated ability to finance is determined.
- 5. Capital programming improves the Town's ability to vitalize state and federal aid. Applications can be timed to fit the development schedule.

DEFINING CAPITAL IMPROVEMENT PROJECTS

A capital improvement is defined as a major expenditure, beyond maintenance and operating costs, for the acquisition or construction of a needed facility. Salaries, supplies and other overhead expenditures are considered maintenance and operating costs, not provided for the CIP. Capital improvements include such things as utility systems, public buildings, land acquisitions, streets and sidewalks. The improvements are items that will have a significant impact on the community and are too expensive to be financed in the annual operating budget. Cost and frequency are two criteria that will be used to distinguish between a capital expenditure and a capital asset.

- 1. COST A capital improvement project shall be \$10,000 or more.
- 2. FREQUENCY Capital improvement projects should be non-recurring. An interval of three years between expenditures is recommended.

DEFINING CAPITAL ASSET REPLACEMENT PROGRAM (CARP)

Capital assets, which include property, plant, equipment, and infrastructure assets, are assets with an initial, individual cost of more than \$5,000 and a useful life of more than one year. Infrastructure assets capitalized have an original cost of \$25,000 or more. Such assets are recorded at historical cost or estimated historical cost if purchased or constructed. Donated capital assets are recorded at acquisition value at the date of donation. The costs of normal maintenance and repairs that do not add to the value of the asset or materially extend asset lives are not capitalized.

* Development of planning and regulatory documents are typically captured in a budget's operating expense; however, Warrenton recognizes these types of documents here as they do not occur annually and can have a substantial impact on the budget.

CATEGORIES

Starting the FY22, CIP projects are being classified around stated priorities of the Town. Projects are numbered under specific topical areas. The CIP further states how projects meet the Comprehensive Plan goals and objectives within the individual project sheets. Below is a general description of the categories.

The CIP programs are coded using the following information:

Economic Development and Tourism (E) – Economic development and tourism projects position Warrenton to leverage and promote the location of jobs, revenue-generating businesses, and attracting tourism through complementary place-based economic development that encourages local economic growth.

General Government (G) – General government projects relate to ensuring the efficiency and needs to run a government that meets the needs of its citizens in a responsive, safe, and transparent fashion.

Public Safety (P) - Public safety projects relate to the Town of Warrenton's Police Department and Warrenton Volunteer Fire Company needs to ensure the ongoing safety and security of the community.

Recreation and Quality of Life (R) – Recreation and quality of life projects are recognized as opportunities for additional cultural, arts, and recreational activities in the Town. These type of investments are an important factor for long term economic sustainability.

Transportation and Walkability (T) – Transportation and walkability projects provide for improved multimodal safety by enacting access management strategies, incorporating pedestrian and bike friendly strategies, and deconflicting through-travel and local traffic movements.

Utilities and Stormwater (U) – Utilities and stormwater projects locate, maintain, and build community facilities to ensure the service needs of the Town and Federal and state mandates are met.

EXAMPLE PROJECT NUMBER



The CIP is a planning and scheduling document. It does not represent authorization to expend Town funds. It does provide an orderly implementation of proposed short and long range plans for land acquisition and construction. Projects are authorized for implementation only after Town Council adopts and appropriates the Capital Budget. The impact of FY23 capital projects, for both improvement and asset projects, on the Town of Warrenton General Fund is \$1,281,289. The impact of FY23 capital projects, for both improvement and asset projects, on the Town of Warrenton Water and Sewer Fund is \$4,111,102. The impact of the FY23 capital projects on the Stormwater Utility Fund is \$94,918. The Town is also using \$976,500 in ARPA funds on projects in FY23. The CIP is an annual process and requires close review by both the Planning Commission and the Town Council.

CAPITAL IMPROVEMENT PROJECTS

PROJECT SHEETS

TRANSPORTATION & WALKABILITY

PROJECT NUMBER: T-28-003	PROJECT TITLE: Inters. Ir	ov.: Broadview/W. Lee Hwy/Winchester					
CATEGORY (check one):		PROGRAM TYPE (check one):					
Economic Development & Tourism (E)	Recreation & Quality of Life (R)	CARP					
General Government (G)	Stormwater & Utilities (U)	✓ CIP					
Public Safety (P)							

PROGRAM DESCRIPTION

The Town of Warrenton is interested in creating an improvement plan for this important transportation connection between two key arterial corridors. It is also key to the economic development potential of the surrounding area. Therefore, the Town is working with VDOT on a "pipeline project" for the Lee Highway corridor. This project will be updated upon completion of the study in spring 2022.

GOAL ADDRESSED

Plan Warrenton 2040 Transportation and Circulation Near Turn Recommendations page 38.



ESTIMATED COSTS	FY23 2022-23	FY24 2023-24	FY25 2024-25	FY26 2025-26	FY27 2026-27	FY28 & Beyond	Total
Land Acquisition						\$2,325,000	\$2,325,000
Architecture/Engineering						\$1,299,486	\$1,299,486
Construction/Purchase						\$3,641,809	\$3,641,809
Other							\$0
TOTAL	\$0	\$0	\$0	\$0	\$0	\$7,266,295	\$7,266,295
FUNDING SOURCES							
General Fund						\$7,266,295	\$7,266,295
Water and Sewer Fund							\$0
Stormwater Fund							\$0
ARPA							\$0
Grant- Federal							\$0
Proffer							\$0
Other							\$0
TOTAL	\$0	\$0	\$0	\$0	\$0	\$7,266,295	\$7,266,295
OPERATING IMPACT							
Ongoing maintenance							\$0
Other							\$0
TOTAL	\$0	\$0	\$0	\$0	\$0	\$ 0	\$0

FY2023-2028 60 Town of Warrenton

PROJECT NUMBER: T-28-004	PROJECT TITLE: Route 17 ((Broadview) Roebling Roundabout
CATEGORY (check one):		PROGRAM TYPE (check one):
Economic Development & Tourism (E)	Recreation & Quality of Life (R)	CARP
General Government (G)	Stormwater & Utilities (U)	✓ CIP
Public Safety (P)	✓ Transportation & Walkability (T)	

PROGRAM DESCRIPTION

The intersection at Route 17 (Broadview Avenue) and Roebling Street is subjected to safety issues. As the area around it redevelops, the intersection will need improvements. In 2020 the Town applied for an unsuccessful VDOT Smartscale grant. This application included an assessment of costs associated with a roundabout included below. Therefore, the Town is working with VDOT on a "pipeline project" for the Lee Higway corridor. This project will be updated upon completion of the study in spring of 2022.

GOAL ADDRESSED

Plan Warrenton 2040 Transportation and Circulation Near Turn Recommendations page 38.



ESTIMATED COSTS	FY23 2022-23	FY24 2023-24	FY25 2024-25	FY26 2025-26	FY27 2026-27	FY28 & Beyond	Total
Land Acquisition						\$1,987,500	\$1,987,500
Architecture/Engineering						\$1,291,020	\$1,291,020
Construction/Purchase						\$3,921,045	\$3,921,045
Other							\$0
TOTAL	\$0	\$0	\$0	\$0	\$0	\$7,199,565	\$7,199,565
FUNDING SOURCES							
General Fund						\$7,199,565	\$7,199,565
Water and Sewer Fund							\$0
Stormwater Fund							\$0
ARPA							\$0
Grant- Commonwealth							\$0
Proffer							\$0
Other							\$0
TOTAL	\$0	\$0	\$0	\$0	\$0	\$7,199,565	\$7,199,565
OPERATING IMPACT							
Ongoing maintenance							\$0
Other							\$0
TOTAL	\$0	\$0	\$0	\$0	\$0	\$0	\$0

FY2023-2028 61 Town of Warrenton

PROJECT NUMBER: T-28-005	PROJECT TITLE: Bear W	allow Road/ Roebling Intersection
CATEGORY (check one):		PROGRAM TYPE (check one):
Economic Development & Tourism (E)	Recreation & Quality of Life (R)	CARP
General Government (G)	Stormwater & Utilities (U)	✓ CIP
Public Safety (P)	✓ Transportation & Walkability (T)	

PROGRAM DESCRIPTION

The intersection at Bear Wallow Road and Roebling Street is subjected to safety issues and an awkward configuration. As the area around it redevelops, the intersection will need improvements. In 2020 the Town applied for an unsuccessful VDOT Smartscale grant. This application included an assessment of costs associated with a roundabout included below.



GOAL ADDRESSED

Plan Warrenton 2040 Transportation and Circulation Near Turn Recommendations page 38.

ESTIMATED COSTS	FY23 2022-23	FY24 2023-24	FY25 2024-25	FY26 2025-26	FY27 2026-27	FY28 & Beyond	Total
Land Acquisition						\$1,200,000	\$1,200,000
Architecture/Engineering						\$1,200,000	\$1,200,000
Construction/Purchase						\$3,600,000	\$3,600,000
Other							\$0
TOTAL	\$0	\$0	\$0	\$0	\$0	\$6,000,000	\$6,000,000
FUNDING SOURCES							
General Fund						\$6,000,000	\$6,000,000
Water and Sewer Fund							\$0
Stormwater Fund							\$0
ARPA							\$0
Grant- Commonwealth							\$0
Proffer							\$0
Other							\$0
TOTAL	\$0	\$0	\$0	\$0	\$0	\$6,000,000	\$6,000,000
OPERATING IMPACT							
Ongoing maintenance							\$0
Other							\$0
TOTAL	\$0	\$0	\$0	\$0	\$0	\$0	\$0

FY2023-2028 62 Town of Warrenton

https://www.fauquiernow.com/news/business/warrenton-town-council-greenlights-mixed-use-development-next-to-obriens-pub/article_5e6c8aca-611c-11ed-8421-2751bb1fb016.html

FEATURED

Warrenton Town Council greenlights mixed-use development next to O'Brien's Pub

James Jarvis, jjarvis@FauquierNow.com Nov 10, 2022



Rendering of a proposed mixed-use development, dubbed Waterloo Junction, that would be built between Broadview Avenue and Bear Wallow Road.

Farrish Properties & Acquisitions LLC

The Warrenton Town Council voted unanimously Wednesday to approve the construction of a mixed-use development -- including 47 townhomes, six apartments, one retail building and a small park -- on the corner of Lee Highway and Broadview Avenue.

The 4.81-acre development, dubbed Waterloo Junction, will consist of 47 1,800-square-foot townhomes, 3,600 square feet of new retail space, six apartments, parking and a small park with a community play area and benches. One townhome and five apartments – 10% of the proposed units – will be designated as affordable housing for individuals or families whose gross annual income does not exceed 80% of the current Fauquier County area median family income.



Rendering of proposed 47 townhomes that could be built as part of the Waterloo Junction development. Each townhome would be 1,800 square-feet and 45 feet high.

Dan Ryan Builders

According to the application, the townhomes will not exceed the town's zoning ordinance of 45 feet. They'll be priced somewhere between \$400,000 and \$500,000.

For the project to move forward, the council had to approve a zoning map amendment, special-use permit and Comprehensive Plan amendment.

The Warrenton Planning Commission previously <u>voted 5–1 recommending the</u> <u>council approve the project</u>. Commissioner Ali Zarabi cast the only dissenting vote, noting concerns about traffic mitigation, among other issues.

During the council meeting, Ward 2 representative William Semple urged his colleagues to delay the project. Semple said that while he supported the creation of more affordable housing, he argued it may create a "precedent" in which other developers would be incentivized to propose similar projects along Broadview Avenue that do not align with the 2040 Comprehensive Plan guidelines which the council approved in April 2021.

"I think that we should consider those issues before we adopt this one, because this is going to be what I call the lead horse in a variety of potential development down the road," Semple said.

The Comprehensive Plan states the Experience Broadview District "will allow for mixed-use residential at lower density, but nodal development with mixed-use anchors and improved edges to adjacent single-family neighborhoods. Current commercial uses will be maintained."

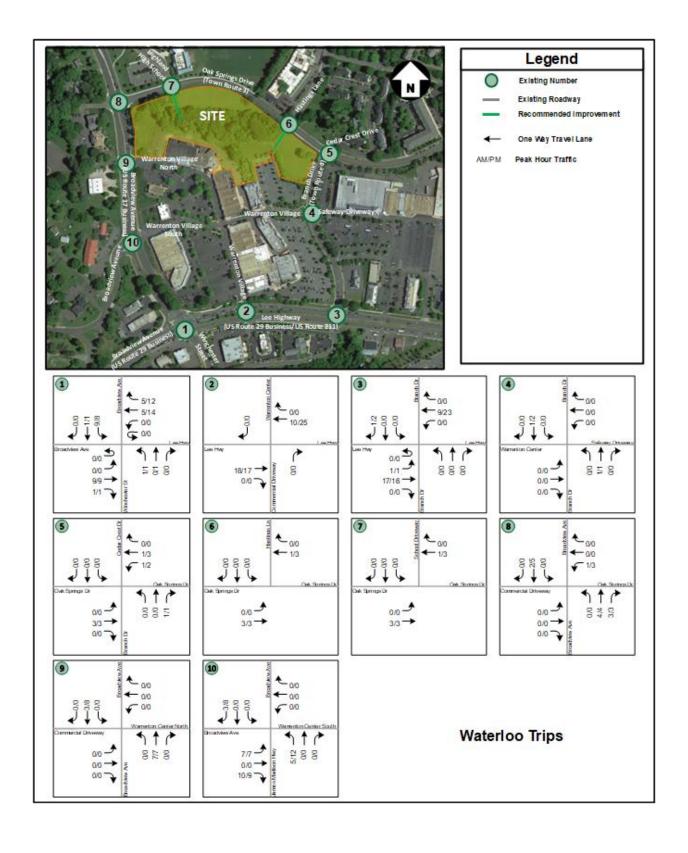
Semple moved to table the project, but it was rejected 6-1, with Semple casting the only supporting vote.

The rest of the council, including Mayor Carter Nevill, praised the project, saying it will be a positive addition to the town.

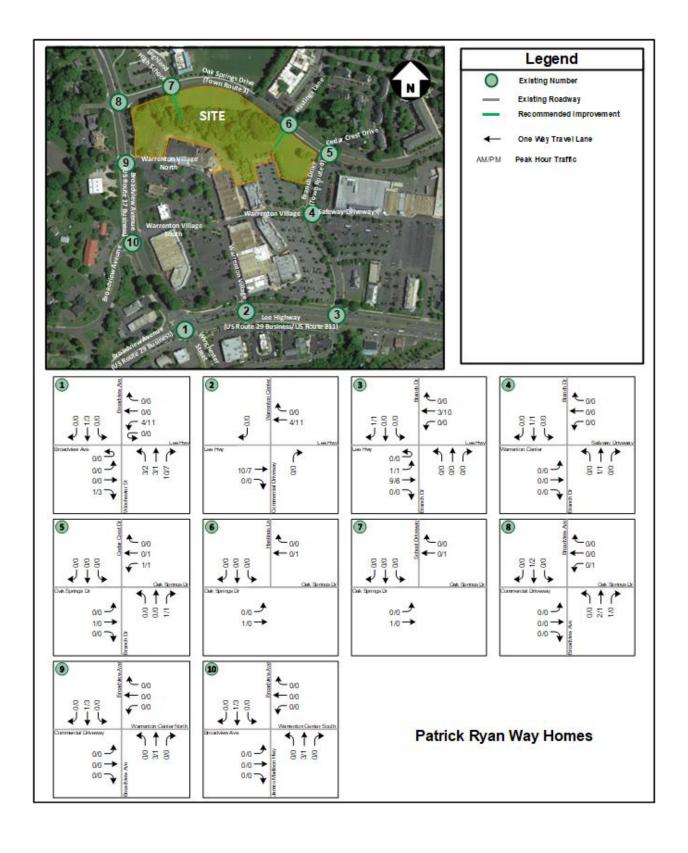
"I think this has been pointed out that the importance of ... bringing people into residential spaces that are close to commercial and entertainment spaces ... it recreates the same sense of community that you see in downtown, where you have people ... walking to restaurants, walking to shops, and I think the more we are able to bring that closer to our neighborhoods, the better we create our built environment to better serve the well-being of our residents," Nevill said.

The renovation of O'Brien's and the apartments above the restaurant currently vacant – is estimated to take four months. The townhome construction could be completed within 18 months.

James Jarvis







H. 2027 Future	Conditions with	out Developmen	t – Capacity A	nalysis Worksheet

LANE LEVEL OF SERVICE

Lane Level of Service

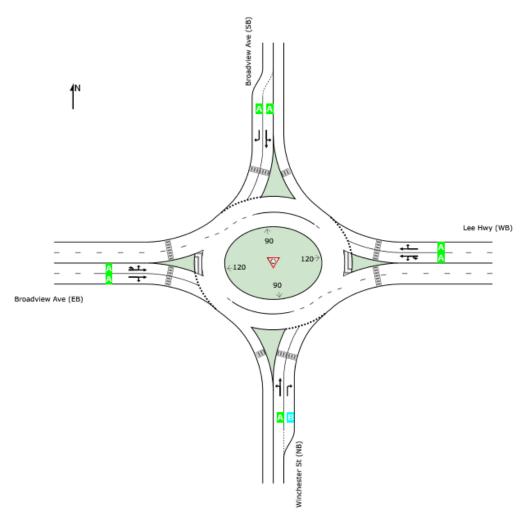
Site: 101 [Broadview/Winchester/Lee - 2027 FB AM (Site Folder:

General)]

Output produced by SIDRA INTERSECTION Version: 9.1.2.202

Warrenton Village Center 2027 Future Background Condtions AM Peak Hour Site Category: (None) Roundabout

		Approaches								
	South	East	North	West	Intersection					
LOS	Α	Α	Α	Α	Α					



Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

SIDRA INTERSECTION 9.1 | Copyright © 2000-2022 Akcelik and Associates Pty Ltd | sidrasolutions.com Organisation: GOROVE SLADE | Licence: PLUS / 1PC | Processed: Monday, February 12, 2024 2:04:14 AM Project: U:\3243\001. Warrenton Village Center\Analysis\Sidra\2nd Submission\2027 TF.sip9

LANE SUMMARY

▼ Site: 101 [Broadview/Winchester/Lee - 2027 FB AM (Site Folder:

General)]

Output produced by SIDRA INTERSECTION Version: 9.1.2.202

Warrenton Village Center 2027 Future Background Condtions AM Peak Hour Site Category: (None) Roundabout

Lane Use	and P	erforn	nance												
	Demand		Arrival		Сар.	Deg. Satn	Lane Util.	Aver. Delay	Level of Service	95% B Que	eue	Lane Config	Lane Length	Cap. F Adj. E	
	veh/h	нv ј %	veh/h	пv ј %	veh/h	v/c	%	sec		[Veh	Dist] ft		ft	%	%
South: Wir	nchester	St (NB	3)												
Lane 1 ^d	199	4.5	199	4.5	664	0.300	100	9.2	LOS A	1.4	35.5	Full	1600	0.0	0.0
Lane 2	87	4.0	87	4.0	475	0.183	100	10.2	LOS B	0.7	18.8	Short	250	0.0	NA
Approach	286	4.4	286	4.4		0.300		9.5	LOS A	1.4	35.5				
East: Lee	Hwy (WE	3)													
Lane 1	430	7.2	430	7.2	1024	0.420	100	8.0	LOS A	3.0	78.4	Full	1600	0.0	0.0
Lane 2 ^d	504	6.5	504	6.5	1201	0.420	100	7.2	LOS A	3.1	80.8	Full	1600	0.0	0.0
Approach	934	6.8	934	6.8		0.420		7.6	LOS A	3.1	80.8				
North: Bro	adview A	Ave (SE	3)												
Lane 1 ^d	240	3.7	240	3.7	750	0.320	100	8.6	LOS A	1.5	39.3	Short	215	0.0	NA
Lane 2	234	3.0	234	3.0	682	0.343	100	9.7	LOS A	1.7	42.6	Full	1600	0.0	0.0
Approach	474	3.4	474	3.4		0.343		9.1	LOS A	1.7	42.6				
West: Broa	adview A	ve (EB	3)												
Lane 1	448	4.1	448	4.1	1048	0.427	100	8.0	LOS A	3.1	79.7	Full	1600	0.0	0.0
Lane 2 ^d	523	3.9	523	3.9	1224	0.427	100	7.2	LOS A	3.2	82.8	Full	1600	0.0	0.0
Approach	971	4.0	971	4.0		0.427		7.6	LOS A	3.2	82.8				
All Vehicles	2664	4.9	2664	4.9		0.427		8.1	LOSA	3.2	82.8				

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

d Dominant lane on roundabout approach

Approach Lane Flows (veh/h)										
South: Wincl	hester St (NB)								
Mov.	L2	T1	R2	Total	%HV			Lane Prob.		
From S						Cap.		Util. SL Ov.		
To Exit:	W	Ν	E			veh/h	v/c	% %	No.	

Lane 1	84	115	-	199	4.5		664	0.300	100	NA	NA	
Lane 2	-	-	87	87	4.0		475	0.183	100	0.0	1	
Approach	84	115	87	286	4.4			0.300				
East: Lee Hw	y (WB)											
Mov.	U	L2	T1	R2	Total	%HV		Deg.		Prob.	Ov.	
From E	_						Cap. veh/h	Satn v/c	Util. %	SL Ov.	Lane No.	
To Exit:	Е	S	W	N			veii/ii	٧/٥	/0			
Lane 1	3	38	389	-	430	7.2			100	NA	NA	
Lane 2	-	-	313	191	504	6.5	1201	0.420	100	NA	NA	
Approach	3	38	701	191	934	6.8		0.420				
North: Broady	view Ave	(SB)										
Mov.	L2	T1	R2	Total	%HV			Deg.	Lane	Prob.	Ov.	
From N							Сар.	Satn	Util.	SL Ov.	Lane	
To Exit:	E	S	W				veh/h	v/c	%	%	No.	
Lane 1	137	103	-	240	3.7		750	0.320	100	0.0	2	
Lane 2	-	-	234	234	3.0		682	0.343	100	NA	NA	
Approach	137	103	234	474	3.4			0.343				
West: Broadv	riour Avo	/ED\										
Mov.	lew Ave	(EB) L2	T1	R2	Total	%HV		Dog	Lane	Prob.	Ov.	
From W		LZ		- K2	Total	-70 □ V	Cap.	Deg. Satn		SL Ov.	Lane	
To Exit:	W	N	Е	S			veh/h	v/c	%	%	No.	
Lane 1	5	62	380	-	448	4.1	1048	0.427	100	NA	NA	
Lane 2	-	-	487	36	523	3.9		0.427	100	NA	NA	
Approach	5	62	867	36	971	4.0	1227	0.427		1471	1 17 1	
, , , , , , , , , , , , , , , , , , , ,					971	7.0		J. 727				
	Total	%HV [Deg.Sat	n (v/c)								
All Vehicles	2664	4.9		0.427								

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

Merge Analysis								
Exit	Short	Percent Opposing	Critical	Follow-up Lane	Capacity	Deg.	Min.	Merge
Lane	Lane	Opng in Flow Rate	Gap	Headway Flow		Satn	Delay	Delay
Number	Length	Lane		Rate				
	ft	% veh/h pcu/h	sec	sec veh/h	veh/h	v/c	sec	sec
There are no Exit Short Lane	s for Mer	ge Analysis at this Site	•					

Variable Demand	Analysis			
	Initial Queued Demand	Residual Queued Demand	Time for Residual Demand to Clear	Duration of Oversatn
	veh	veh	sec	sec
South: Winchester S	t (NB)			
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0
East: Lee Hwy (WB)				
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0
North: Broadview Av	e (SB)			
Lane 1	0.0	0.0	0.0	0.0

Lane 2	0.0	0.0	0.0	0.0
West: Broadview	Ave (EB)			
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0

SIDRA INTERSECTION 9.1 | Copyright © 2000-2022 Akcelik and Associates Pty Ltd | sidrasolutions.com Organisation: GOROVE SLADE | Licence: PLUS / 1PC | Processed: Monday, February 12, 2024 2:04:14 AM Project: U:\3243\001. Warrenton Village Center\Analysis\Sidra\2nd Submission\2027 TF.sip9

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202	7 Fu	iture F	3acko	around

Intersection												
Int Delay, s/veh	0.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		† †	7		^	7			7			7
Traffic Vol, veh/h	0	944	63	0	839	31	0	0	29	0	0	20
Future Vol, veh/h	0	944	63	0	839	31	0	0	29	0	0	20
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	110	-	-	300	-	-	0	-	-	0
Veh in Median Storage	,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	1	-	-	3	-	-	3	-	-	-11	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	4	3	0	7	0	0	0	3	0	0	0
Mvmt Flow	0	1026	68	0	912	34	0	0	32	0	0	22
Major/Minor N	Major1		<u> </u>	Major2			Minor1		N	/linor2		
Conflicting Flow All	-	0	0	-	-	0	-	-	513	-	-	456
Stage 1	-	-	-	-	-	-	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-	-	-	-	-	-	-
Critical Hdwy	-	-	-	-	-	-	-	-	7.26	-	-	5.8
Critical Hdwy Stg 1	-	-	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2	-	-	-	-	-	-	-	-	-	-	-	-
Follow-up Hdwy	-	-	-	-	-	-	-	-	3.33	-	-	3.3
Pot Cap-1 Maneuver	0	-	-	0	-	-	0	0	483	0	0	640
Stage 1	0	-	-	0	-	-	0	0	-	0	0	-
Stage 2	0	-	-	0	-	-	0	0	-	0	0	-
Platoon blocked, %		-	-		-	-						
Mov Cap-1 Maneuver	-	-	-	-	-	-	-	-	483	-	-	640
Mov Cap-2 Maneuver	-	-	-	-	-	-	-	-	-	-	-	-
Stage 1	-	-	-	-	-	-	-	-	-	-	-	-
Stage 2	_	_	_	_	_	_	_	_	_	_	_	_
-												
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			0			13			10.8		
HCM LOS	_						В			В		
Minor Lane/Major Mvm	t N	NBLn1	EBT	EBR	WBT	WBR S	SBLn1					
Capacity (veh/h)		483				-						
HCM Lane V/C Ratio		0.065	_	_	_		0.034					
HCM Control Delay (s)		13	_	_	_	_						
HCM Lane LOS		В	<u>-</u>	<u>-</u>	_	<u>-</u>	В					
HCM 95th %tile Q(veh)		0.2	_	_	_		0.1					
How Jour Joure Q(Veri)		0.2					0.1					

3: BRANCH DR & LEE HWY

	ၨ	-	•	•	←	•	†	~	↓	4	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBT	NBR	SBT	SBR	
Lane Group Flow (vph)	42	1015	1	48	871	55	23	41	46	57	
v/c Ratio	0.37	0.43	0.00	0.41	0.39	0.05	0.15	0.16	0.40	0.29	
Control Delay	71.3	17.3	0.0	72.4	16.0	0.1	57.5	1.4	71.9	3.6	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	71.3	17.3	0.0	72.4	16.0	0.1	57.5	1.4	71.9	3.6	
Queue Length 50th (ft)	39	246	0	44	198	0	21	0	43	0	
Queue Length 95th (ft)	80	485	0	88	400	0	44	0	86	0	
Internal Link Dist (ft)		457			1504		131		565		
Turn Bay Length (ft)	240		330	150		150		60			
Base Capacity (vph)	199	2364	1143	227	2281	1124	279	352	185	248	
Starvation Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.21	0.43	0.00	0.21	0.38	0.05	0.08	0.12	0.25	0.23	
Intersection Summary											

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		٠	-	*	•	—	•	1	†	/	/	↓
Movement	EBU	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT
Lane Configurations		ă	^↑	7	ሻ		7		र्स	7		ની
Traffic Volume (vph)	7	31	934	1	44	801	51	10	11	38	34	8
Future Volume (vph)	7	31	934	1	44	801	51	10	11	38	34	8
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Grade (%)			-4%			2%			0%			-1%
Total Lost time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.0	6.0		7.5
Lane Util. Factor		1.00	0.95	1.00	1.00	0.95	1.00		1.00	1.00		1.00
Frt		1.00	1.00	0.85	1.00	1.00	0.85		1.00	0.85		1.00
Flt Protected		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (prot)		1793	3541	1647	1752	3372	1599		1856	1615		1792
Flt Permitted		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (perm)		1793	3541	1647	1752	3372	1599		1856	1615		1792
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	8	34	1015	1	48	871	55	11	12	41	37	9
RTOR Reduction (vph)	0	0	0	0	0	0	20	0	0	38	0	0
Lane Group Flow (vph)	0	42	1015	1	48	871	35	0	23	3	0	46
Heavy Vehicles (%)	14%	0%	4%	0%	2%	6%	0%	0%	0%	0%	3%	0%
Turn Type	Prot	Prot	NA	Perm	Prot	NA	Perm	Split	NA	Perm	Split	NA
Protected Phases	1	1	6		5	2		4	4		3	3
Permitted Phases			07.0	6	0.4	00.7	2		40.0	4		7.0
Actuated Green, G (s)		7.7	87.8	87.8	8.1	88.7	88.7		10.2	10.2		7.9
Effective Green, g (s)		7.7	87.8	87.8	8.1	88.7	88.7		10.2	10.2		7.9
Actuated g/C Ratio		0.06	0.63	0.63	0.06	0.63	0.63		0.07	0.07		0.06
Clearance Time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.0	6.0		7.5
Vehicle Extension (s)		3.0	3.0	3.0	3.0	3.0	3.0		3.0	3.0		3.0
Lane Grp Cap (vph)		98	2220	1032	101	2136	1013		135	117		101
v/s Ratio Prot		0.02	c0.29	0.00	c0.03	0.26	0.00		c0.01	0.00		c0.03
v/s Ratio Perm		0.40	0.40	0.00	0.40	0.44	0.02		0.47	0.00		0.40
v/c Ratio		0.43	0.46	0.00	0.48	0.41	0.03		0.17	0.03		0.46
Uniform Delay, d1		64.0	13.6	9.7	63.9	12.7	9.6		60.9	60.3		64.0
Progression Factor		1.00	1.00 0.7	1.00	1.00 3.5	1.00 0.6	1.00		1.00 0.6	1.00		1.00 3.2
Incremental Delay, d2 Delay (s)		67.0	14.3	9.7	67.4	13.3	9.7		61.5	60.4		67.2
Level of Service		67.0 E	14.3 B	9.7 A	_				61.5 E	_		67.2 E
Approach Delay (s)			16.4	A	E	15.7	А		60.8	E		64.7
Approach LOS			В			В			00.0 E			04. <i>1</i>
			ь			Ь						
Intersection Summary												
HCM 2000 Control Delay			19.7	Н	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capacit	y ratio		0.43		•							
Actuated Cycle Length (s)			140.0		um of lost				26.0			
Intersection Capacity Utilization	n		58.4%	IC	CU Level	ot Service)		В			
Analysis Period (min)			15									

c Critical Lane Group



Movement	SBR
Lane Configurations	7
Traffic Volume (vph)	52
Future Volume (vph)	52
Ideal Flow (vphpl)	1900
Grade (%)	
Total Lost time (s)	7.5
Lane Util. Factor	1.00
Frt	0.85
Flt Protected	1.00
Satd. Flow (prot)	1375
Flt Permitted	1.00
Satd. Flow (perm)	1375
Peak-hour factor, PHF	0.92
	57
Adj. Flow (vph)	
RTOR Reduction (vph)	54
Lane Group Flow (vph)	3
Heavy Vehicles (%)	18%
Turn Type	Perm
Protected Phases	
Permitted Phases	3
Actuated Green, G (s)	7.9
Effective Green, g (s)	7.9
Actuated g/C Ratio	0.06
Clearance Time (s)	7.5
Vehicle Extension (s)	3.0
Lane Grp Cap (vph)	77
v/s Ratio Prot	
v/s Ratio Perm	0.00
v/c Ratio	0.04
Uniform Delay, d1	62.5
Progression Factor	1.00
	0.2
Incremental Delay, d2	
Delay (s)	62.7
Level of Service	Е
Approach Delay (s)	
Approach LOS	
Intersection Summary	
mo. socion caminary	

HCM 6th Edition methodology expects strict NEMA phasing.

HCM 6th TWSC 4: BRANCH DR & WARRENTON VILLAGE CENTER/SAFEWAY DRIVEWAY2027 Future Background

Intersection												
Int Delay, s/veh	4.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			414			414	
Traffic Vol, veh/h	6	15	38	14	11	14	23	67	7	18	69	5
Future Vol, veh/h	6	15	38	14	11	14	23	67	7	18	69	5
Conflicting Peds, #/hr	0	0	2	2	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	_	-	-	-
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	-8	-	-	-2	-	-	1	_	-	-1	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	0	0	0	9	0	0	0	0	0	13	0
Mvmt Flow	7	16	41	15	12	15	25	73	8	20	75	5
Major/Minor M	linor2		ı	Minor1			Major1		N	/lajor2		
Conflicting Flow All	211	249	42	215	247	41	80	0	0	81	0	0
Stage 1	118	118	-	127	127	-	-	-	-	-	-	-
Stage 2	93	131	-	88	120	-	-	-	-	-	-	-
Critical Hdwy	5.9	4.9	6.1	7.1	6.28	6.7	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	4.9	3.9	-	6.1	5.28	-	-	-	-	-	-	-
Critical Hdwy Stg 2	4.9	3.9	-	6.1	5.28	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4	3.3	3.5	4.09	3.3	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	805	734	1036	746	656	1030	1531	-	-	1529	-	-
Stage 1	927	845	-	882	785	-	-	-	-	-	-	-
Stage 2	948	839	-	925	790	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	763	711	1034	686	636	1030	1531	-	-	1529	-	-
Mov Cap-2 Maneuver	763	711	-	686	636	-	-	-	-	-	-	-
Stage 1	911	833	-	867	772	-	-	-	-	-	-	-
Stage 2	904	825	-	857	779	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	9.3			10			1.8			1.4		
HCM LOS	Α			В								
Minor Lane/Major Mvmt		NBL	NBT	NBR I	EBLn1V		SBL	SBT	SBR			
Capacity (veh/h)		1531	-	-	898	760	1529	-	-			
HCM Lane V/C Ratio		0.016	-	-		0.056		-	-			
HCM Control Delay (s)		7.4	0	-	9.3	10	7.4	0	-			
HCM Lane LOS		Α	Α	-	Α	В	Α	Α	-			
HCM 95th %tile Q(veh)		0.1	-	-	0.2	0.2	0	-	-			

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Intersection												
Int Delay, s/veh	3											
		EDT		WDI	WDT	WDD	NDI	NDT	NDD	ODI	ODT	000
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4		40	4		70	-4	7		4	
Traffic Vol, veh/h	1	80	75	16	107	1	73	1	14	1	1	1
Future Vol, veh/h	1	80	75	16	107	1	73	1	14	1	1	1
Conflicting Peds, #/hr	_ 4	_ 0	_ 1	_ 1	_ 0	_ 4	0	0	2	2	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	0	-	-	-
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	1	-	-	2	-	-	-5	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	1	11	7	1	0	0	0	0	0	0	0
Mvmt Flow	1	87	82	17	116	1	79	1	15	1	1	1
Major/Minor N	1ajor1			Major2		N	Minor1		N	/linor2		
Conflicting Flow All	121	0	0	170	0	0	283	286	131	295	327	121
Stage 1	-	-	-	-	-	-	131	131	-	155	155	-
Stage 2	_	_	_	_	_	_	152	155	_	140	172	_
Critical Hdwy	4.1	_	_	4.17	_	-	7.5	6.9	6.4	6.1	5.5	5.7
Critical Hdwy Stg 1	-	-	_	-	_	_	6.5	5.9	-	5.1	4.5	-
Critical Hdwy Stg 2	_	_	_	-	-	-	6.5	5.9	-	5.1	4.5	_
Follow-up Hdwy	2.2	_	_	2.263	_	_	3.5	4	3.3	3.5	4	3.3
Pot Cap-1 Maneuver	1479	_	_	1378	-	-	652	607	917	718	651	952
Stage 1	-	_	_	-	_	_	865	780	-	890	807	-
Stage 2	-	_	_	-	-	-	841	760	-	902	797	_
Platoon blocked, %		_	_		_	_	- V 1 1				. •	
Mov Cap-1 Maneuver	1474	_	_	1377	-	-	643	596	915	694	639	949
Mov Cap-2 Maneuver	-	_	_	-	_	_	643	596	-	694	639	-
Stage 1	-	_	_	-	-	-	863	778	-	886	794	_
Stage 2	_	_	_	_	_	_	828	748	_	883	795	_
5.0.g5 L							520	0		500	. 00	
A	FF			WD			ND			0.0		
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			1			11			9.9		
HCM LOS							В			Α		
Minor Lane/Major Mvmt		NBLn11	NBLn2	EBL	EBT	EBR	WBL	WBT	WBR S	SBLn1		
Capacity (veh/h)		642	915		-		1377	-	-	739		
HCM Lane V/C Ratio				0.001	_		0.013	_	_	0.004		
HCM Control Delay (s)		11.4	9	7.4	0	-	7.6	0	-	9.9		
HCM Lane LOS		В	A	A	A	_	A	A	_	A		
HCM 95th %tile Q(veh)		0.4	0.1	0	-	-	0	-	-	0		
		J. r	3.1				- 3					

Intersection							
Int Delay, s/veh	1.9						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	T T	<u> </u>	<u>₩</u>	וטייי	JDL Š	7	
Traffic Vol, veh/h	38	160	153	51	31	19	
Future Vol, veh/h	38	160	153	51	31	19	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-		-	None	
Storage Length	75	-	-	-	0	50	
Veh in Median Storage	, # -	0	0	-	0	-	
Grade, %	-	-5	3	-	0	-	
Peak Hour Factor	92	92	92	92	92	92	
Heavy Vehicles, %	0	4	1	0	0	0	
Mvmt Flow	41	174	166	55	34	21	
Major/Minor N	Major1	N	Major2	N	Minor2		
Conflicting Flow All	221	0	-	0	450	194	
Stage 1	-	-	-	-	194	-	
Stage 2	-	-	-	-	256	-	
Critical Hdwy	4.1	-	-	-	6.4	6.2	
Critical Hdwy Stg 1	-	-	-	-	5.4	-	
Critical Hdwy Stg 2	-		-	-	5.4	-	
Follow-up Hdwy	2.2	-	-	-	3.5	3.3	
Pot Cap-1 Maneuver	1360	-	-	-	571	853	
Stage 1	-	-	-	-	844	-	
Stage 2	-	-	-	-	791	-	
Platoon blocked, %	1000	-	-	-			
Mov Cap-1 Maneuver	1360	-	-	-	554	853	
Mov Cap-2 Maneuver	-	-	-	-	554	-	
Stage 1	-	-	-	-	819	-	
Stage 2	-	-	-	-	791	-	
Approach	EB		WB		SB		
HCM Control Delay, s	1.5		0		10.9		
HCM LOS					В		
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR :	SBLn1 S	BLn2
Capacity (veh/h)		1360				554	853
HCM Lane V/C Ratio		0.03	_	_	_	0.061	
HCM Control Delay (s)		7.7	-	-	_	11.9	9.3
HCM Lane LOS		Α	-	-	-	В	Α
HCM 95th %tile Q(veh))	0.1	-	-	-	0.2	0.1

Intersection												
Int Delay, s/veh	3.8											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			र्स	7	ች	^	1	ች	^	
Traffic Vol, veh/h	1	1	1	65	1	106	1	413	102	95	358	1
Future Vol, veh/h	1	1	1	65	1	106	1	413	102	95	358	1
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	100	-	0	90	-	130	225	-	-
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	-2	-	-	4	-	-	2	-	-	3	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	0	0	0	0	1	0	6	1	5	5	0
Mvmt Flow	1	1	1	71	1	115	1	449	111	103	389	1
Major/Minor N	/linor2		N	Minor1			Major1		N	/lajor2		
Conflicting Flow All	823	1158	195	852	1047	225	390	0	0	560	0	0
Stage 1	596	596	-	451	451	-	-	-	-	-	-	-
Stage 2	227	562	_	401	596	-	_	-	_	-	-	-
Critical Hdwy	7.1	6.1	6.7	8.3	7.3	7.32	4.1	-	-	4.2	_	_
Critical Hdwy Stg 1	6.1	5.1	-	7.3	6.3	-	-	-	_	-	-	-
Critical Hdwy Stg 2	6.1	5.1	_	7.3	6.3	_	_	_	-	_	_	_
Follow-up Hdwy	3.5	4	3.3	3.5	4	3.31	2.2	-	_	2.25	-	-
Pot Cap-1 Maneuver	295	225	829	212	182	762	1180	-	-	987	-	-
Stage 1	494	529	-	509	520	-	-	-	-	-	-	-
Stage 2	780	546	-	551	434	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	229	201	829	194	163	762	1180	-	-	987	-	-
Mov Cap-2 Maneuver	229	201	-	194	163	-	-	-	-	-	-	-
Stage 1	494	474	-	508	519	-	-	-	-	-	-	-
Stage 2	660	545	-	492	389	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	17.8			19.7			0			1.9		
HCM LOS	С			С								
Minor Lane/Major Mvmt	t	NBL	NBT	NBR	EBLn1V	VBLn1V	VBLn2	SBL	SBT	SBR		
Capacity (veh/h)		1180			284	193	762	987				
HCM Lane V/C Ratio		0.001	-	_		0.372			_	_		
HCM Control Delay (s)		8.1	_	_	17.8	34.3	10.6	9.1	_	_		
HCM Lane LOS		Α	-	-	C	D	В	Α	_	_		
HCM 95th %tile Q(veh)		0	_	_	0	1.6	0.5	0.3	_	_		
7000 4(1011)						1.0	5.5	5.5				

2027 FB AM Synchro 11 Report Page 16 GS

Intersection												
Int Delay, s/veh	0.6											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4		ሻ	€		ች	^	7		^	
Traffic Vol, veh/h	1	1	3	5	1	18	13	498	10	15	405	3
Future Vol, veh/h	1	1	3	5	1	18	13	498	10	15	405	3
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	0	-	-	150	-	135	110	-	-
Veh in Median Storage,	,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	5	-	-	3	-	-	4	-	-	-2	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	0	0	0	0	6	0	5	0	0	4	0
Mvmt Flow	1	1	3	5	1	20	14	541	11	16	440	3
Major/Minor N	/linor2		ı	Minor1		ı	Major1		N	Major2		
Conflicting Flow All	773	1054	222	822	1044	271	443	0	0	552	0	0
Stage 1	474	474		569	569		-	-	_	-	_	-
Stage 2	299	580	_	253	475	-	-	_	_	_	-	_
Critical Hdwy	8.5	7.5	7.4	8.1	7.1	7.32	4.1	_	_	4.1	_	-
Critical Hdwy Stg 1	7.5	6.5	-	7.1	6.1	-	-	_	_	-	-	_
Critical Hdwy Stg 2	7.5	6.5	_	7.1	6.1	_	-	_	_	_	_	-
Follow-up Hdwy	3.5	4	3.3	3.5	4	3.36	2.2	_	_	2.2	-	_
Pot Cap-1 Maneuver	236	170	764	235	194	699	1128	_	-	1028	_	-
Stage 1	478	492	-	436	463	-	_	_	_	-	-	-
Stage 2	636	428	-	704	518	-	_	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	223	165	764	228	189	699	1128	-	-	1028	-	-
Mov Cap-2 Maneuver	223	165	-	228	189	-	-	-	-	-	-	-
Stage 1	472	484	-	431	457	-	-	-	-	-	-	-
Stage 2	609	423	-	689	510	-	-	-	-	-	-	-
-												
Approach	EB			WB			NB			SB		
HCM Control Delay, s	15.6			13.2			0.2			0.3		
HCM LOS	С			В								
Minor Lane/Major Mvmt	l _	NBL	NBT	NBR E	EBLn1V	VBLn1V	VBLn2	SBL	SBT	SBR		
Capacity (veh/h)		1128	-	-	346	228	612	1028	-	-		
HCM Lane V/C Ratio		0.013	-	-	0.016	0.024	0.034	0.016	-	-		
HCM Control Delay (s)		8.2	-	-	15.6	21.2	11.1	8.6	-	-		
HCM Lane LOS		Α	-	-	С	С	В	Α	-	-		
HCM 95th %tile Q(veh)		0	-	-	0	0.1	0.1	0	-	-		

Intersection												
Int Delay, s/veh	6.8											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	<u></u>	7	ሻ	4		ሻ	^	7	ሻ	^	7
Traffic Vol. veh/h	126	17	81	2	3	3	116	392	31	7	353	53
Future Vol, veh/h	126	17	81	2	3	3	116	392	31	7	353	53
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	<u> </u>	Yield	-	-	None	-	-	None	-	-	None
Storage Length	100	-	230	0	-	-	160	-	175	160	-	125
Veh in Median Storage	, # -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	_	0	-	-	0	-	-	3	-	-	-3	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	2	0	3	0	0	33	1	5	0	0	3	8
Mvmt Flow	137	18	88	2	3	3	126	426	34	8	384	58
Major/Minor N	/linor2		ľ	Minor1		ı	Major1			Major2		
Conflicting Flow All	867	1112	192	895	1136	213	442	0	0	460	0	0
Stage 1	400	400	-	678	678	-	_	-	-	-	-	-
Stage 2	467	712	-	217	458	-	-	-	-	_	-	-
Critical Hdwy	7.54	6.5	6.96	7.5	6.5	7.56	4.12	-	-	4.1	-	-
Critical Hdwy Stg 1	6.54	5.5	-	6.5	5.5	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.5	-	6.5	5.5	-	_	-	-	-	-	-
Follow-up Hdwy	3.52	4	3.33	3.5	4	3.63	2.21	-	-	2.2	-	-
Pot Cap-1 Maneuver	247	211	814	239	204	705	1122	-	_	1112	_	_
Stage 1	597	605	-	413	455	_		-	-	_	-	-
Stage 2	545	439	-	771	570	-	_	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	221	186	814	179	180	705	1122	-	-	1112	-	-
Mov Cap-2 Maneuver	221	186	-	179	180	-	-	-	-	-	-	-
Stage 1	530	601	-	367	404	-	-	-	-	-	-	-
Stage 2	478	390	-	662	566	-	-	-	-	-	-	-
-												
Approach	EB			WB			NB			SB		
HCM Control Delay, s	30.7			19.7			1.9			0.1		
HCM LOS	D			С								
Minor Lane/Major Mvm	t	NBL	NBT	NBR I	EBLn1	EBLn2 l	EBLn3V	VBLn1V	VBLn2	SBL	SBT	SBR
Capacity (veh/h)		1122	-	-	221	186	814	179	287	1112	-	-
HCM Lane V/C Ratio		0.112	-	-	0.62	0.099	0.108	0.012	0.023	0.007	-	-
HCM Control Delay (s)		8.6	-	-	44.6	26.5	10	25.4	17.8	8.3	-	-
HCM Lane LOS		Α	-	-	Е	D	В	D	С	Α	-	-
HCM 95th %tile Q(veh)		0.4	-	-	3.6	0.3	0.4	0	0.1	0	-	-
•												

LANE SUMMARY

▼ Site: 101 [Broadview/Winchester/Lee - 2027 FB PM (Site Folder:

General)]

Output produced by SIDRA INTERSECTION Version: 9.1.2.202

Warrenton Village Center 2027 Future Background Conditions PM Peak Hour Site Category: (None) Roundabout

Lane Use	and Pe	erform	nance												
	Demand				Сар.	Deg. Satn	Lane Util.	Aver. Delay	Level of Service	95% Ba Que	eue	Lane Config	Lane Length	Cap. F Adj. B	
	[Total veh/h	HV] %	[Total veh/h	пv ј %	veh/h	v/c	%	sec		[Veh	Dist] ft		ft	%	%
South: Wir	nchester	St (NB	3)												
Lane 1 ^d	223	0.5	223	0.5	570	0.391	100	12.2	LOS B	2.2	55.7	Full	1600	0.0	0.0
Lane 2	77	0.0	77	0.0	376	0.205	100	13.0	LOS B	0.9	22.4	Short	250	0.0	NA
Approach	300	0.3	300	0.3		0.391		12.4	LOS B	2.2	55.7				
East: Lee	Hwy (WE	3)													
Lane 1	625	1.7	625	1.7	888	0.703	100	16.2	LOS B	10.0	252.3	Full	1600	0.0	0.0
Lane 2 ^d	758	2.0	758	2.0	1078	0.703	100	14.0	LOS B	10.5	267.5	Full	1600	0.0	0.0
Approach	1382	1.9	1382	1.9		0.703		15.0	LOS B	10.5	267.5				
North: Bro	adview A	Ave (SE	3)												
Lane 1	340	0.7	340	0.7	435	0.780	100	35.1	LOS D	6.4	161.1	Short	215	0.0	NA
Lane 2 ^d	402	4.0	402	4.0	498	0.808	100	34.4	LOS C	7.4	190.7	Full	1600	0.0	0.0
Approach	742	2.5	742	2.5		0.808		34.7	LOS C	7.4	190.7				
West: Broa	adview A	ve (EB	3)												
Lane 1	538	2.5	538	2.5	923	0.583	100	11.9	LOS B	6.2	158.2	Full	1600	0.0	0.0
Lane 2 ^d	652	1.9	652	1.9	1118	0.583	100	10.4	LOS B	6.2	158.3	Full	1600	0.0	0.0
Approach	1191	2.1	1191	2.1		0.583		11.1	LOS B	6.2	158.3				
All Vehicles	3615	2.0	3615	2.0		0.808		17.6	LOS B	10.5	267.5				

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

d Dominant lane on roundabout approach

Approach	Lane Flo	ws (ve	h/h)							
South: Wincl	hester St (NB)								
Mov.	L2	T1	R2	Total	%HV			Lane Prob.		
From S						Cap.		Util. SL Ov.		
To Exit:	W	Ν	E			veh/h	v/c	% %	No.	

Lane 1	122	101	_	223	0.5		570	0.391	100	NA	NA	
Lane 2	-	-	77	77	0.0		376	0.205	100	0.0	1	
Approach	122	101	77	300	0.3			0.391				
East: Lee Hw	y (WB)											
Mov.	U	L2	T1	R2	Total	%HV	C = 12	Deg.		Prob.	Ov.	
From E To Exit:	Е	S	W	N			Cap. veh/h	Satn v/c	Util. %	SL Ov.	Lane No.	
Lane 1	10	70	544		625	1.7	888	0.703	100	NA	NA	
Lane 2	-	-	635	123	758	2.0	1078		100	NA	NA	
Approach	10	70	1179	123	1382	1.9		0.703				
North: Broad	view Ave	(SB)										
Mov.	L2	T1	R2	Total	%HV			Deg.	Lane	Prob.	Ov.	
From N							Cap.	Satn		SL Ov.	Lane	
To Exit:	Е	S	W				veh/h	v/c	%	%	No.	
Lane 1	249	91	-	340	0.7		435	0.780	100	0.0	2	
Lane 2	-	-	402	402	4.0		498	0.808	100	NA	NA	
Approach	249	91	402	742	2.5			0.808				
West: Broady	iew Ave	(EB)										
Mov.	U	L2	T1	R2	Total	%HV		Deg.	Lane	Prob.	Ov.	
From W	201		_				Cap. veh/h	Satn v/c	Util. %	SL Ov.	Lane No.	
To Exit:	W	N	Е	S								
Lane 1	2	273	263	-	538	2.5	923	0.583	100	NA	NA	
Lane 2	-	-	606	46	652	1.9	1118	0.583	100	NA	NA	
Approach	2	273	870	46	1191	2.1		0.583				
	Total	%HV I	Deg.Sat	n (v/c)								
All Vehicles	3615	2.0		0.808								

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

Merge Analysis								
Exit	Short	Percent Opposing	Critical	Follow-up Lane	Capacity	Deg.	Min.	Merge
Lane	Lane	Opng in Flow Rate	Gap	Headway Flow		Satn	Delay	Delay
Number	Length	Lane		Rate				
	ft	% veh/h pcu/h	sec	sec veh/h	veh/h	v/c	sec	sec
There are no Exit Short Lane	s for Mer	ge Analysis at this Site	•					

Variable Deman	d Analysis			
	Initial Queued Demand	Residual Queued Demand	Time for Residual Demand to Clear	Duration of Oversatn
	veh	veh	sec	sec
South: Winchester	St (NB)			
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0
East: Lee Hwy (WI	3)			
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0
North: Broadview A	Ave (SB)			
Lane 1	0.0	0.0	0.0	0.0

Lane 2	0.0	0.0	0.0	0.0
West: Broadview	Ave (EB)			
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0

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LANE LEVEL OF SERVICE

Lane Level of Service

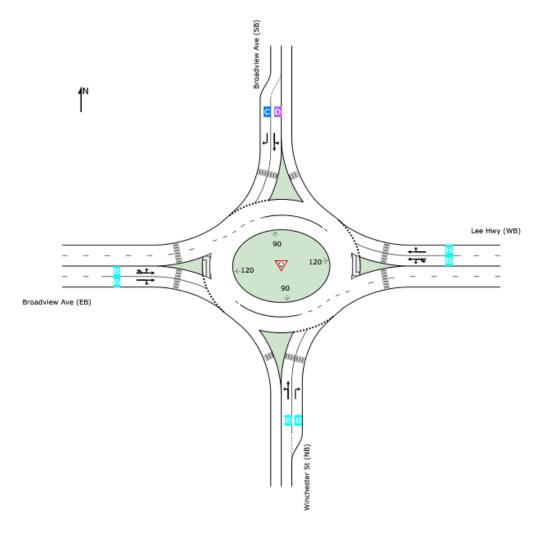
▼ Site: 101 [Broadview/Winchester/Lee - 2027 FB PM (Site Folder:

General)]

Output produced by SIDRA INTERSECTION Version: 9.1.2.202

Warrenton Village Center 2027 Future Background Conditions PM Peak Hour Site Category: (None) Roundabout

		Appro	aches		Intersection
	South	East	North	West	Intersection
LOS	В	В	С	В	В



Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

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Intersection												
Int Delay, s/veh	0.6											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		^	7		^	7			7			7
Traffic Vol, veh/h	0	1075	83	0	1247	102	0	0	25	0	0	79
Future Vol, veh/h	0	1075	83	0	1247	102	0	0	25	0	0	79
Conflicting Peds, #/hr	0	0	0	0	0	4	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	<u> </u>	-	None
Storage Length	-	-	110	-	-	300	-	-	0	-	-	0
Veh in Median Storage	, # -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	<u>-</u>	1	-	-	3	-	-	3	-	-	-11	-
Peak Hour Factor	93	93	93	93	93	93	93	93	93	93	93	93
Heavy Vehicles, %	0	2	0	0	2	0	0	0	4	0	0	0
Mvmt Flow	0	1156	89	0	1341	110	0	0	27	0	0	85
Major/Minor N	Major1		I	Major2			Minor1		N	Minor2		
Conflicting Flow All	-	0	0	_	-	0	-	-	578	-	-	675
Stage 1	_	-	-	_	_	-	-	-		-	-	
Stage 2	_	_	_	-	_	_	_	_	_	_	_	_
Critical Hdwy	-	-	-	-	-	-	-	-	7.28	-	-	5.8
Critical Hdwy Stg 1	_	-	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2	-	-	-	-	-	-	-	-	-	-	-	-
Follow-up Hdwy	-	-	-	-	-	-	-	-	3.34	-	-	3.3
Pot Cap-1 Maneuver	0	-	-	0	-	-	0	0	433	0	0	493
Stage 1	0	-	-	0	-	-	0	0	-	0	0	-
Stage 2	0	-	-	0	-	-	0	0	-	0	0	-
Platoon blocked, %		-	-		-	-						
Mov Cap-1 Maneuver	-	-	-	-	-	-	-	-	433	-	-	491
Mov Cap-2 Maneuver	-	-	-	-	-	-	-	-	-	-	-	-
Stage 1	-	-	-	-	_	-	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-	-	-	-	-	-	-
, and the second												
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			0			13.9			13.9		
HCM LOS							В			В		
Minor Lane/Major Mvm	it N	NBLn1	EBT	EBR	WBT	WBR S	SBLn1					
Capacity (veh/h)		433	-	_	_	_	491					
HCM Lane V/C Ratio		0.062	_	_	<u>-</u>	_	0.173					
HCM Control Delay (s)		13.9	_	_	-	-	400					
HCM Lane LOS		В	_	_	_	_	В					
HCM 05th %tile O(veh)	ı	0.2					0.6					

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0.6

HCM 95th %tile Q(veh)

0.2

3: BRANCH DR & LEE HWY

	•	→	\rightarrow	•	←	•	†	/	ļ	4	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBT	NBR	SBT	SBR	
Lane Group Flow (vph)	149	1006	2	68	1241	88	36	79	165	152	
v/c Ratio	0.72	0.47	0.00	0.54	0.67	0.10	0.31	0.30	0.76	0.45	
Control Delay	82.8	20.6	0.0	82.0	30.0	0.2	72.2	3.0	85.8	10.8	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	82.8	20.6	0.0	82.0	30.0	0.2	72.2	3.0	85.8	10.8	
Queue Length 50th (ft)	148	310	0	68	475	0	36	0	164	0	
Queue Length 95th (ft)	224	441	0	123	675	0	73	0	249	58	
Internal Link Dist (ft)		457			1504		131		565		
Turn Bay Length (ft)	240		330	150		150		60			
Base Capacity (vph)	260	2159	993	157	1850	906	202	327	250	363	
Starvation Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.57	0.47	0.00	0.43	0.67	0.10	0.18	0.24	0.66	0.42	
Intersection Summary											

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		۶	→	•	•	•	•	•	†	/	/	
Movement	EBU	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT
Lane Configurations		ă	^	7	ሻ	^	7		ર્ન	7		4
Traffic Volume (vph)	9	133	956	2	65	1179	84	17	17	75	139	18
Future Volume (vph)	9	133	956	2	65	1179	84	17	17	75	139	18
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Grade (%)			-4%			2%			0%			-1%
Total Lost time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.6	6.6		7.5
Lane Util. Factor		1.00	0.95	1.00	1.00	0.95	1.00		1.00	1.00		1.00
Frpb, ped/bikes		1.00	1.00	0.97	1.00	1.00	0.98		1.00	1.00		1.00
Flpb, ped/bikes		1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00
Frt		1.00	1.00	0.85	1.00	1.00	0.85		1.00	0.85		1.00
Flt Protected		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (prot)		1807	3682	1602	1787	3504	1558		1854	1615		1813
Flt Permitted		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (perm)		1807	3682	1602	1787	3504	1558		1854	1615		1813
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	9	140	1006	2	68	1241	88	18	18	79	146	19
RTOR Reduction (vph)	0	0	0	1	0	0	41	0	0	74	0	0
Lane Group Flow (vph)	0	149	1006	1	68	1241	47	0	36	5	0	165
Confl. Peds. (#/hr)			,,,,,	2			2	-			•	
Heavy Vehicles (%)	0%	2%	0%	0%	0%	2%	1%	0%	0%	0%	1%	0%
Turn Type	Prot	Prot	NA	Perm	Prot	NA	Perm	Split	NA	Perm	Split	NA
Protected Phases	1	1	6	1 01111	5	2	1 01111	4	4	1 01111	3	3
Permitted Phases	•	•	J	6	•	=	2	•	•	4	•	J
Actuated Green, G (s)		17.2	86.7	86.7	9.3	79.3	79.3		9.5	9.5		17.9
Effective Green, g (s)		17.2	86.7	86.7	9.3	79.3	79.3		9.5	9.5		17.9
Actuated g/C Ratio		0.11	0.58	0.58	0.06	0.53	0.53		0.06	0.06		0.12
Clearance Time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.6	6.6		7.5
Vehicle Extension (s)		3.0	3.0	3.0	3.0	3.0	3.0		3.0	3.0		3.0
Lane Grp Cap (vph)		207	2128	925	110	1852	823		117	102		216
v/s Ratio Prot		c0.08	0.27	320	0.04	c0.35	020		c0.02	102		c0.09
v/s Ratio Perm		60.00	0.21	0.00	0.04	00.00	0.03		00.02	0.00		00.03
v/c Ratio		0.72	0.47	0.00	0.62	0.67	0.06		0.31	0.05		0.76
Uniform Delay, d1		64.1	18.4	13.4	68.6	25.8	17.2		67.1	66.0		64.0
Progression Factor		1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00
Incremental Delay, d2		11.4	0.8	0.0	9.9	1.00	0.1		1.5	0.2		14.8
Delay (s)		75.4	19.1	13.4	78.5	27.8	17.3		68.6	66.2		78.8
Level of Service		75.4 E	В	13. 4 B	70.5 E	C C	17.3 B		60.0 E	60.2 E		70.0 E
Approach Delay (s)		<u> </u>	26.4	U	<u> </u>	29.6	U		67.0	<u> </u>		69.3
Approach LOS			20.4 C			23.0 C			67.0 E			03.5 E
Intersection Summary									_			_
			24.0	1.1	CM 2000	l aval af	Comileo					
HCM 2000 Control Delay			34.0	H	CIVI 2000	Level of	Service		С			
HCM 2000 Volume to Capacit	y ratio		0.66	^	() .	1 than 1 1 1			00.0			
Actuated Cycle Length (s)	_		150.0		um of los				26.6			
Intersection Capacity Utilization	n		76.1%	IC	U Level	of Service			D			
Analysis Period (min)			15									
c Critical Lane Group												



Movement	SBR
Lane Configurations	7
Traffic Volume (vph)	144
Future Volume (vph)	144
Ideal Flow (vphpl)	1900
Grade (%)	
Total Lost time (s)	7.5
Lane Util. Factor	1.00
Frpb, ped/bikes	1.00
Flpb, ped/bikes	1.00
Frt	0.85
Flt Protected	1.00
Satd. Flow (prot)	1607
Flt Permitted	1.00
Satd. Flow (perm)	1607
Peak-hour factor, PHF	0.95
Adj. Flow (vph)	152
RTOR Reduction (vph)	134
Lane Group Flow (vph)	18
Confl. Peds. (#/hr)	10
Heavy Vehicles (%)	1%
Turn Type	Perm
Protected Phases	
Permitted Phases	3
Actuated Green, G (s)	17.9
Effective Green, g (s)	17.9
Actuated g/C Ratio	0.12
Clearance Time (s)	7.5
Vehicle Extension (s)	3.0
Lane Grp Cap (vph)	191
v/s Ratio Prot	
v/s Ratio Perm	0.01
v/c Ratio	0.09
Uniform Delay, d1	58.8
Progression Factor	1.00
Incremental Delay, d2	0.2
Delay (s)	59.1
Level of Service	Е
Approach Delay (s)	
Approach LOS	
Intersection Summary	

HCM 6th Edition methodology expects strict NEMA phasing.

HCM 6th TWSC 4: BRANCH DR & WARRENTON VILLAGE CENTER/SAFEWAY DRIVEWAY2027 Future Background

Intersection												
Int Delay, s/veh	8.9											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			र्नी			र्सी	
Traffic Vol, veh/h	17	77	116	45	50	41	94	45	12	48	42	32
Future Vol, veh/h	17	77	116	45	50	41	94	45	12	48	42	32
Conflicting Peds, #/hr	0	0	14	14	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	-8	-	-	-2	-	-	1	-	-	-1	-
Peak Hour Factor	96	96	96	96	96	96	96	96	96	96	96	96
Heavy Vehicles, %	0	0	2	0	2	5	0	2	0	0	3	0
Mvmt Flow	18	80	121	47	52	43	98	47	13	50	44	33
Major/Minor N	linor2		N	/linor1			Major1			/lajor2		
Conflicting Flow All	407	417	53	426	427	30	77	0	0	60	0	0
Stage 1	161	161	-	250	250	-	_	-	-	-	-	-
Stage 2	246	256	-	176	177	_	_	-	-	_	_	_
Critical Hdwy	5.9	4.9	6.14	7.1	6.14	6.8	4.1	_	-	4.1	_	_
Critical Hdwy Stg 1	4.9	3.9	-	6.1	5.14	-	-	-	-	-	-	-
Critical Hdwy Stg 2	4.9	3.9	-	6.1	5.14	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4	3.32	3.5	4.02	3.35	2.2	_	_	2.2	_	_
Pot Cap-1 Maneuver	639	637	1015	542	544	1030	1535	-	-	1556	-	-
Stage 1	893	826	-	759	718	-	-	-	-	-	-	-
Stage 2	827	784	-	831	767	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	521	575	1003	390	491	1030	1535	-	-	1556	-	-
Mov Cap-2 Maneuver	521	575	-	390	491	-	-	-	-	-	-	-
Stage 1	834	798	-	709	671	-	-	-	-	-	-	-
Stage 2	683	732	-	628	741	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	11.8			14.3			4.7			2.9		
HCM LOS	В			В								
	_											
Minor Lane/Major Mvmt		NBL	NBT	NBR I	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		1535	-	_	744	529	1556	-	-			
HCM Lane V/C Ratio		0.064	_	_		0.268		_	_			
HCM Control Delay (s)		7.5	0	-	11.8	14.3	7.4	0	_			
HCM Lane LOS		A	A	_	В	В	A	A	_			
HCM 95th %tile Q(veh)		0.2	-	_	1.2	1.1	0.1	-	-			

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Intersection												
Int Delay, s/veh	3.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			स	7		4	
Traffic Vol. veh/h	3	109	86	31	116	2	62	2	39	1	5	1
Future Vol, veh/h	3	109	86	31	116	2	62	2	39	1	5	1
Conflicting Peds, #/hr	4	0	0	0	0	4	0	0	2	2	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	_	_	None	-	_	None	_	_	None	_	_	None
Storage Length	_	_	-	-	_	-	_	_	0	-	_	_
Veh in Median Storage,	# -	0	_	-	0	-	_	0	_	_	0	_
Grade, %	_	0	-	-	1	_	-	2	_	-	-5	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	3	0	4	1	0	3	0	3	0	0	0
Mvmt Flow	3	118	93	34	126	2	67	2	42	1	5	1
Major/Minor N	/lajor1			Major2		N	Minor1		N	/linor2		
Conflicting Flow All	132	0	0	211	0	0	369	371	167	394	416	131
Stage 1	-	-	-	-	-	-	171	171	-	199	199	-
Stage 2	_	_	_	_	_	_	198	200	<u>-</u>	195	217	_
Critical Hdwy	4.1	_	_	4.14	_	_	7.53	6.9	6.43	6.1	5.5	5.7
Critical Hdwy Stg 1	7.1	<u>-</u>	_		_	<u>-</u>	6.53	5.9	- 0.43	5.1	4.5	J.1 -
Critical Hdwy Stg 2	_			_	_	_	6.53	5.9	_	5.1	4.5	_
Follow-up Hdwy	2.2	<u>-</u>	_	2.236	_		3.527	4	3.327	3.5	4	3.3
Pot Cap-1 Maneuver	1466	_	_	1348	_	_	562	539	867	635	595	941
Stage 1	-	<u>-</u>	_	-	_	_	813	747	-	853	782	-
Stage 2	_	_	_	_	_	_	784	723	_	857	772	_
Platoon blocked, %		_	_		_	_	.01	. 20		001		
Mov Cap-1 Maneuver	1461	-	-	1348	_	-	545	522	866	585	576	938
Mov Cap-2 Maneuver	-	_	_	-	_	_	545	522	-	585	576	-
Stage 1	_	-	-	_	_	-	811	746	-	849	759	_
Stage 2	-	_	_	_	_	_	756	701	_	810	770	_
										•		
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0.1			1.6			11.4			11		
HCM LOS	•						В			В		
Minor Lane/Major Mvm	t	NBLn1 I	NBLn2	EBL	EBT	EBR	WBL	WBT	WBR S	SBLn1		
Capacity (veh/h)		544	866	1461		_	1348			611		
HCM Lane V/C Ratio			0.049	0.002	_	-	0.025	_	_	0.012		
HCM Control Delay (s)		12.6	9.4	7.5	0	_	7.7	0	_	11		
HCM Lane LOS		12.0	A	Α	A	_	Α.	A	_	В		
HCM 95th %tile Q(veh)		0.4	0.2	0	-	_	0.1	-	-	0		
		U. I	0.2				J. 1					

Intersection						
Int Delay, s/veh	3.5					
	EBL	EBT	\\/DT	WBR	CDI	SBR
Movement	ERF		WBT	WBK	SBL	SRK
Lane Configurations	40	121	164	1.1	67	E0
Traffic Vol, veh/h	42	131	164	14	67	52
Future Vol, veh/h	42	131	164	14	67	52
Conflicting Peds, #/hr	1	0	0	1	2	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	110110	-		-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage		0	0	-	0	-
Grade, %	-	-3	1	-	-5	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	0	0	2
Mvmt Flow	46	142	178	15	73	57
Major/Minor I	Major1	N	Major2	N	Minor2	
Conflicting Flow All	194	0	- -	0	423	187
Stage 1	-	_	_	-	187	-
Stage 2	_	_	_	<u>-</u>	236	_
Critical Hdwy	4.12	_	-	_	5.4	5.72
Critical Hdwy Stg 1	4.12	_	_	_	4.4	5.12
Critical Hdwy Stg 2			_	_	4.4	
Follow-up Hdwy	2.218	-	_	-		3.318
Pot Cap-1 Maneuver	1379		-	-	665	878
	13/9	-	_	-	895	- 070
Stage 1	-		-		863	-
Stage 2	-	-	-	-	000	-
Platoon blocked, %	4070	-	-	-	C40	077
Mov Cap-1 Maneuver	1378	-	-	-	640	877
Mov Cap-2 Maneuver	-	-	-	-	640	-
Stage 1	-	-	-	-	862	-
Stage 2	-	-	-	-	862	-
Approach	EB		WB		SB	
HCM Control Delay, s	1.9		0		11	
HCM LOS	1.0				В	
TIOM EGG						
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR S	SBLn1
Capacity (veh/h)		1378	-	-	-	726
HCM Lane V/C Ratio		0.033	-	-	-	0.178
HCM Control Delay (s)		7.7	-	-	-	11
HCM Lane LOS		Α	-	-	-	В
HCM 95th %tile Q(veh))	0.1	-	-	-	0.6

Intersection							
Int Delay, s/veh	1						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	EDL Š	<u>EDI</u>	VVD1	אסא	SBL T	SBR 7	
Traffic Vol, veh/h	5	T 162	T 214	2	11	27	
Future Vol, veh/h	5	162	214	2	11	27	
Conflicting Peds, #/hr	1	0	0	1	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-		-	None	
Storage Length	75	-	-	-	0	50	
Veh in Median Storage	e, # -	0	0	-	0	-	
Grade, %	-	-5	3	-	0	-	
Peak Hour Factor	92	92	92	92	92	92	
Heavy Vehicles, %	0	3	2	0	0	0	
Mvmt Flow	5	176	233	2	12	29	
Major/Minor N	Major1	N	Major2	N	Minor2		
Conflicting Flow All	236	0	-	0	421	235	
Stage 1	-	-	-	-	235	-	
Stage 2	-	-	-	-	186	-	
Critical Hdwy	4.1	-	-	-	6.4	6.2	
Critical Hdwy Stg 1	-	-	-	-	5.4	-	
Critical Hdwy Stg 2	-	-	-	-	5.4	-	
Follow-up Hdwy	2.2	-	-	-	3.5	3.3	
Pot Cap-1 Maneuver	1343	-	-	-	593	809	
Stage 1	-	-	-	-	809	-	
Stage 2	-	-	-	-	851	-	
Platoon blocked, %	4040	-	-	-	F00	000	
Mov Cap-1 Maneuver	1342	-	-	-	589	808	
Mov Cap-2 Maneuver	-	-	-	-	589	-	
Stage 1	-	-	-	-	805 850	=	
Stage 2	-	-	-	-	000	-	
Approach	EB		WB		SB		
HCM Control Delay, s	0.2		0		10.1		
HCM LOS					В		
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR S	SBLn1 S	BLn2
Capacity (veh/h)		1342	-	-	-	589	808
HCM Lane V/C Ratio		0.004	-	-	_	0.02	
HCM Control Delay (s)		7.7	-	-	-	11.2	9.6
HCM Lane LOS		Α	-	-	-	В	Α
HCM 95th %tile Q(veh))	0	-	-	-	0.1	0.1
-							

Intersection												
Int Delay, s/veh	5.9											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4	7	ሻ	^	7	ሻ	^	02.1
Traffic Vol, veh/h	2	1	4	102	1	139	2	375	80	86	508	2
Future Vol, veh/h	2	1	4	102	1	139	2	375	80	86	508	2
Conflicting Peds, #/hr	0	0	0	0	0	0	4	0	1	1	0	4
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	_	_	-	100	_	0	90	_	130	225	_	-
Veh in Median Storage,	# -	0	_	-	0	-	-	0	-	-	0	_
Grade, %	-	-2	_	_	4	_	_	2	_	_	3	_
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	0	0	1	0	2	0	3	4	1	4	0
Mvmt Flow	2	1	4	111	1	151	2	408	87	93	552	2
Major/Minor M	1inor2		ı	Minor1		-	Major1		N	Major2		
Conflicting Flow All	952	1243	281	876	1157	205	558	0	0	496	0	0
Stage 1	743	743	201	413	413	205	550	-	U	730	-	U
Stage 2	209	500	_	463	744	_		_	_	_	_	
Critical Hdwy	7.1	6.1	6.7	8.32	7.3	7.34	4.1		<u>-</u>	4.12	-	-
Critical Hdwy Stg 1	6.1	5.1	0.7	7.32	6.3	1.04	7.1	_	_	7.12	_	_
Critical Hdwy Stg 2	6.1	5.1	-	7.32	6.3	-	_	_	_	_		_
Follow-up Hdwy	3.5	4	3.3	3.51	4	3.32	2.2	_	_	2.21	_	_
Pot Cap-1 Maneuver	241	202	733	201	153	784	1023	<u>-</u>	<u>-</u>	1071	-	-
Stage 1	410	461	- 100	538	545	104	1023			1071		_
Stage 2	798	578		497	360	-	-	<u>-</u>	<u>-</u>	<u>-</u>	-	-
Platoon blocked, %	130	310		731	300			_	_		_	
Mov Cap-1 Maneuver	180	183	731	185	139	783	1020	_		1070		
Mov Cap-2 Maneuver	180	183	-	185	139		- 1020	_	_	-	_	_
Stage 1	408	420	_	536	543	_	_	_	_	_	_	_
Stage 2	641	576	<u>-</u>	450	328	_	_	_	_	_	_	_
		3.0		.00	320							
Annroach	EB			WB			NB			SB		
Approach												
HCM Control Delay, s HCM LOS	16.6 C			27.9 D			0			1.3		
I IOIVI LUO	U			U								
N. 1 (2.1)		ND	NET	NIDD.	-DL (1/DL 4:	VDL C	051	057	000		
Minor Lane/Major Mvmt		NBL	NBT			VBLn1V		SBL	SBT	SBR		
Capacity (veh/h)		1020	-	-	011	184	783	1070	-	-		
HCM Lane V/C Ratio		0.002	-	-		0.608			-	-		
HCM Control Delay (s)		8.5	-	-	16.6	51	10.7	8.7	-	-		
HCM Lane LOS		A	-	-	С	F	В	A	-	-		
HCM 95th %tile Q(veh)		0	-	-	0.1	3.4	0.7	0.3	-	-		

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Intersection												
Int Delay, s/veh	2.1											
• •		- CDT		WDI	WDT	WDD	NDI	NDT	NDD	ODI	ODT	000
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	40	4	4-	\	- î	00	ች	^	7	7	^	•
Traffic Vol, veh/h	10	1	17	33	1	38	15	409	15	41	567	6
Future Vol, veh/h	10	1	17	33	1	38	15	409	15	41	567	6
Conflicting Peds, #/hr	0	0	0	0	0	0	_ 5	_ 0	_ 0	_ 0	_ 0	_ 5
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	0	-	-	150	-	135	110	-	-
Veh in Median Storage,	,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	5	-	-	3	-	-	4	-	-	-2	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	0	0	0	0	5	0	3	0	0	3	0
Mvmt Flow	11	1	18	36	1	41	16	445	16	45	616	7
Major/Minor N	/linor2		N	Minor1		_	Major1		N	Major2		
Conflicting Flow All	970	1208	317	876	1195	223	628	0	0	461	0	0
Stage 1	715	715	-	477	477		-	-	_	-	-	-
Stage 2	255	493	_	399	718	_	_	_	_	_	_	_
Critical Hdwy	8.5	7.5	7.4	8.1	7.1	7.3	4.1	_	_	4.1	_	_
Critical Hdwy Stg 1	7.5	6.5	, . .	7.1	6.1	- 1.0	- -	_	_	- '	_	_
Critical Hdwy Stg 2	7.5	6.5	-	7.1	6.1	_	-	_	_	_	_	_
Follow-up Hdwy	3.5	4	3.3	3.5	4	3.35	2.2	_	_	2.2	_	_
Pot Cap-1 Maneuver	161	132	655	213	154	757	964	_	_	1111	_	_
Stage 1	322	359	-	502	517	-	-	_	_	-	_	_
Stage 2	683	480	_	565	387	_	_		_		_	_
Platoon blocked, %	000	100		- 000	501			_	_		_	_
Mov Cap-1 Maneuver	144	124	652	197	145	757	960	_	_	1111	_	_
Mov Cap-2 Maneuver	144	124	-	197	145	-	-	_	_	-	_	_
Stage 1	315	343	_	493	508		_					
Stage 2	634	472	_	525	370	_	_	_	_	_	_	_
Olugo Z	007	714		020	310							
Approach	EB			WB			NB			SB		
HCM Control Delay, s	20			18.3			0.3			0.6		
HCM LOS	С			С								
Minor Lane/Major Mvmt	l	NBL	NBT	NBR E	EBLn1V	VBLn1V	VBLn2	SBL	SBT	SBR		
Capacity (veh/h)		960	_	_	270	197	683	1111	_	_		
HCM Lane V/C Ratio		0.017	_					0.04	_	_		
HCM Control Delay (s)		8.8	_	_	20	27.3	10.6	8.4	_	_		
HCM Lane LOS		A	_	_	C	D	В	A	_	_		
HCM 95th %tile Q(veh)		0.1	_	_	0.4	0.6	0.2	0.1	_	_		
HOW JOHN JUNE Q(VEII)		0.1			0.7	0.0	0.2	0.1				

Intersection												
Int Delay, s/veh	9.8											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	↑	7	ሻ	1		ሻ	^	7	<u> </u>	^	7
Traffic Vol, veh/h	103	61	173	43	27	25	88	311	77	7	496	114
Future Vol, veh/h	103	61	173	43	27	25	88	311	77	7	496	114
Conflicting Peds, #/hr	6	0	0	0	0	6	0	0	3	3	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	- Clop	- Olop	Yield	-	-	None	-	-	None	-	-	None
Storage Length	100	_	230	0	_	-	160	_	175	160	_	125
Veh in Median Storage,		0	-	-	0	_	-	0	-	-	0	-
Grade, %	" -	0	_	_	0	_	_	3	_	_	-3	_
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	2	0	1	0	0	0	1	3	0	0	4	1
Mvmt Flow	112	66	188	47	29	27	96	338	84	8	539	124
WATER TOWN	112	- 00	100	71	23	LI	- 50	000	U-7	- 0	000	127
N.A' (N.A.'	ı			1' 4		_	1.1.4			\4.:C		
	linor2	44-5		Minor1	10:5		Major1			Major2		
Conflicting Flow All	937	1172	270	852	1212	178	663	0	0	425	0	0
Stage 1	555	555	-	533	533	-	-	-	-	-	-	-
Stage 2	382	617	-	319	679	-	-	-	-	-	-	-
Critical Hdwy	7.54	6.5	6.92	7.5	6.5	6.9	4.12	-	-	4.1	-	-
Critical Hdwy Stg 1	6.54	5.5	-	6.5	5.5	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.5	-	6.5	5.5	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4	3.31	3.5	4	3.3	2.21	-	-	2.2	-	-
Pot Cap-1 Maneuver	219	194	731	256	184	841	928	-	-	1145	-	-
Stage 1	484	516	-	503	528	-	-	-	-	-	-	-
Stage 2	612	484	-	673	454	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	167	172	731	122	164	835	928	-	-	1142	-	-
Mov Cap-2 Maneuver	167	172	-	122	164	-	-	-	-	-	-	-
Stage 1	434	512	-	450	473	-	-	-	-	-	-	-
Stage 2	495	433	-	432	451	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	31.9			35.5			1.7			0.1		
HCM LOS	D			E						7. 1		
				_								
Minor Lane/Major Mvmt		NBL	NBT	NRP	-RI n1	FRI n2 l	=RI n3\	VBLn1V	VRI n2	SBL	SBT	SBR
Capacity (veh/h)		928	ND1	NDN I	167	172	731	122	267	1142	301	אמט
HCM Lane V/C Ratio		0.103						0.383				-
			-	-							-	-
HCM Long LOS		9.3	-	-	62	38.5	11.6	51.8	22.1	8.2	-	-
HCM Of the O(voh)		A	-	-	F	E	В	F	С	A	-	-
HCM 95th %tile Q(veh)		0.3	-	-	3.9	1.7	1	1.6	0.8	0	-	-

I. 2027 Future Con	ditions with Deve	lopment – Cap	pacity Analysis	Worksheets

LANE SUMMARY

♥ Site: 101 [Broadview/Winchester/Lee - 2027 TF AM (Site Folder:

General)]

Output produced by SIDRA INTERSECTION Version: 9.1.2.202

Warrenton Village Center 2027 Future with Development AM Peak Hour Site Category: (None) Roundabout

Lane Use	and Po	erform	nance												
	Demand				Сар.	Deg. Satn	Lane Util.	Aver. Delay	Level of Service	95% Ba	eue	Lane Config	Lane Length	Cap. F Adj. E	
	[Total veh/h	HV J %	[Total veh/h	нv ј %	veh/h	v/c	%	sec		[Veh	Dist] ft		ft	%	%
South: Wir	chester	St (NB	5)												
Lane 1 ^d	203	4.5	203	4.5	569	0.357	100	11.5	LOS B	1.8	46.7	Full	1600	0.0	0.0
Lane 2	87	4.0	87	4.0	397	0.219	100	12.7	LOS B	0.9	22.9	Short	250	0.0	NA
Approach	290	4.3	290	4.3		0.357		11.9	LOS B	1.8	46.7				
East: Lee I	Hwy (WE	3)													
Lane 1	418	7.2	418	7.2	813	0.514	100	11.4	LOS B	4.4	115.6	Full	1600	0.0	0.0
Lane 2 ^d	517	6.5	517	6.5	1005	0.514	100	9.8	LOS A	4.5	117.1	Full	1600	0.0	0.0
Approach	935	6.8	935	6.8		0.514		10.5	LOS B	4.5	117.1				
North: Broa	adview A	ve (SE	3)												
Lane 1 ^d	253	3.6	253	3.6	717	0.353	100	9.5	LOS A	1.8	47.0	Short	215	0.0	NA
Lane 2	251	3.0	251	3.0	653	0.385	100	10.8	LOS B	2.1	52.8	Full	1600	0.0	0.0
Approach	504	3.3	504	3.3		0.385		10.1	LOS B	2.1	52.8				
West: Broa	adview A	ve (EB)												
Lane 1	549	4.5	549	4.5	1025	0.535	100	10.0	LOS A	4.3	111.1	Full	1600	0.0	0.0
Lane 2 ^d	646	3.9	646	3.9	1207	0.535	100	8.9	LOS A	4.5	115.6	Full	1600	0.0	0.0
Approach	1195	4.2	1195	4.2		0.535		9.4	LOS A	4.5	115.6				
All Vehicles	2924	4.9	2924	4.9		0.535		10.1	LOS B	4.5	117.1				

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

d Dominant lane on roundabout approach

Approach	Lane Flo	ws (ve	h/h)							
South: Wincl	hester St (NB)								
Mov.	L2	T1	R2	Total	%HV			Lane Prob.		
From S						Cap.		Util. SL Ov.		
To Exit:	W	Ν	E			veh/h	v/c	% %	No.	

Lane 1	84	120	-	203	4.5		569	0.357	100	NA	NA	
Lane 2	-	-	87	87	4.0		397	0.219	100	0.0	1	
Approach	84	120	87	290	4.3			0.357				
East: Lee Hw	y (WB)											
Mov.	U	L2	T1	R2	Total	%HV		Deg.		Prob.	Ov.	
From E	_		107				Cap. veh/h	Satn v/c	Util. %	SL Ov. %	Lane No.	
To Exit:	Е	S	W	N								
Lane 1	3	38	377	-	418	7.2		0.514	100	NA	NA	
Lane 2	-	-	326	191	517	6.5	1005	0.514	100	NA	NA	
Approach	3	38	702	191	935	6.8		0.514				
North: Broady	view Ave	(SB)										
Mov.	L2	T1	R2	Total	%HV			Deg.	Lane	Prob.	Ov.	
From N							Сар.	Satn	Util.	SL Ov.	Lane	
To Exit:	Е	S	W				veh/h	v/c	%	%	No.	
Lane 1	137	116	-	253	3.6		717	0.353	100	0.0	2	
Lane 2	-	-	251	251	3.0		653	0.385	100	NA	NA	
Approach	137	116	251	504	3.3			0.385				
West: Broady	ιίονι Δια	(ER)										
Mov.	U	L2	T1	R2	Total	%HV	_	Deg.	Lane	Prob.	Ov.	_
From W	U	LZ		112	Iotai	701 I V	Сар.	Satn		SL Ov.	Lane	
To Exit:	W	N	Е	S			veh/h	v/c	%	%	No.	
Lane 1	5	286	257	-	549	4.5	1025	0.535	100	NA	NA	
Lane 2	_		610	36	646	3.9		0.535	100	NA	NA	
Approach	5	286	867	36	1195	4.2		0.535				
• • •												
	Total	%HV [Deg.Sat	n (v/c)								
All Vehicles	2924	4.9		0.535								

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

Merge Analysis								
Exi	Short	Percent Opposing	Critical	Follow-up Lane	e Capacity	Deg.	Min.	Merge
Lane		Opng in Flow Rate	Gap	Headway Flov		Satn E	Delay	Delay
Numbe	Length	Lane		Rate				
	ft	% veh/h pcu/h	sec	sec veh/l	n veh/h	v/c	sec	sec
There are no Exit Short Lar	es for Mer	ge Analysis at this Site						

Variable Demar	nd Analysis			
	Initial Queued Demand	Residual Queued Demand	Time for Residual Demand	Duration of Oversatn
	veh	veh	to Clear sec	sec
South: Wincheste	r St (NB)			
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0
East: Lee Hwy (W	/B)			
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0
North: Broadview	Ave (SB)			
Lane 1	0.0	0.0	0.0	0.0

Lane 2	0.0	0.0	0.0	0.0
West: Broadview	Ave (EB)			
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0

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LANE LEVEL OF SERVICE

Lane Level of Service

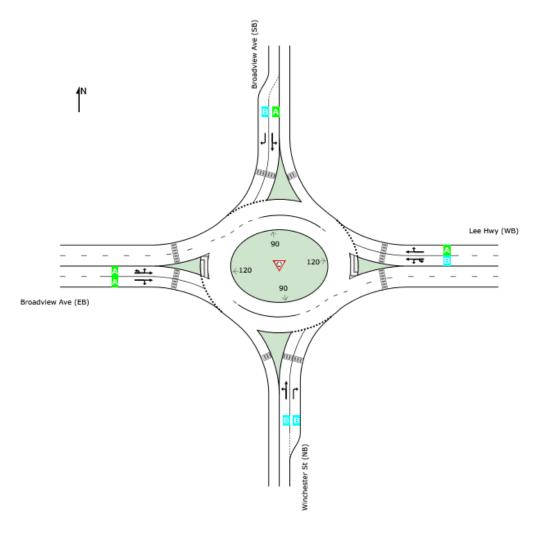
▼ Site: 101 [Broadview/Winchester/Lee - 2027 TF AM (Site Folder:

General)]

Output produced by SIDRA INTERSECTION Version: 9.1.2.202

Warrenton Village Center 2027 Future with Development AM Peak Hour Site Category: (None) Roundabout

		Appro	aches		Intersection
	South	East	North	West	Intersection
LOS	В	В	В	Α	В



Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

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Intersection												
Int Delay, s/veh	0.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		^	7		^	7			7			7
Traffic Vol, veh/h	0	944	63	0	839	32	0	0	29	0	0	21
Future Vol, veh/h	0	944	63	0	839	32	0	0	29	0	0	21
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	_	_	None	-	-	None	-	-	None	-	-	None
Storage Length	_	_	110	-	-	300	_	-	0	-	_	0
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	_	0	-
Grade, %	-	1	-	-	3	-	-	3	-	-	-11	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	4	3	0	7	0	0	0	3	0	0	0
Mvmt Flow	0	1026	68	0	912	35	0	0	32	0	0	23
Major/Minor NA	laiar1			laier?		A	/linor1			liner?		
	lajor1	^		//ajor2						/linor2		450
Conflicting Flow All	-	0	0	-	-	0	-	-	513	-	-	456
Stage 1	-	-	-	-	-	-	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-	-	-	7 26	-	-	- E 0
Critical Hdwy	-	-	-	-	-	-	-	-	7.26	-	-	5.8
Critical Hdwy Stg 1	-	-	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2 Follow-up Hdwy	-	-	-	-		-	-	-	3.33	- -	-	3.3
Pot Cap-1 Maneuver	0	-	-	0	-	-	0	0	483	0	0	640
Stage 1	0	_	-	0	-	-	0	0	403	0	0	040
Stage 1	0	-	-	0	-	-	0	0	-	0	0	-
Platoon blocked, %	U	-	_	U	_	_	U	U	_	U	U	-
Mov Cap-1 Maneuver	_	-	-	_		-	_	_	483		_	640
Mov Cap-1 Maneuver	_	_	_	_	_	_	-	_	-1 00	_	_	040
Stage 1	-	-	_	_			-	<u>-</u>	_	_		-
Stage 2	_	_	_	_	_	_	_	_	_	_	_	_
Olago Z	_		_	_	_	-	-		_	_		
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			0			13			10.8		
HCM LOS							В			В		
Minor Lane/Major Mvmt	N	NBLn1	EBT	EBR	WBT	WBR S	SBLn1					
Capacity (veh/h)		483	-	-	-	-	640					
HCM Lane V/C Ratio		0.065	_	_	_	_	0.036					
HCM Control Delay (s)		13	-	-	-	-	10.8					
HCM Lane LOS		В	-	-	_	_	В					
HCM 95th %tile Q(veh)		0.2	-	-	-	_	0.1					
2000 2(1011)							J.,					

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3: BRANCH DR & LEE HWY

	۶	→	\rightarrow	•	←	•	†	/	ļ	4	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBT	NBR	SBT	SBR	
Lane Group Flow (vph)	42	1015	1	48	872	75	23	41	110	57	
v/c Ratio	0.37	0.47	0.00	0.41	0.42	0.07	0.17	0.17	0.62	0.23	
Control Delay	71.3	19.4	0.0	72.4	18.1	0.1	60.7	1.6	74.9	2.2	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	71.3	19.4	0.0	72.4	18.1	0.1	60.7	1.6	74.9	2.2	
Queue Length 50th (ft)	39	273	0	44	221	0	21	0	102	0	
Queue Length 95th (ft)	80	485	0	88	400	0	47	0	163	0	
Internal Link Dist (ft)		457			1504		131		565		
Turn Bay Length (ft)	240		330	150		150		60			
Base Capacity (vph)	199	2178	1063	227	2104	1047	261	338	200	259	
Starvation Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.21	0.47	0.00	0.21	0.41	0.07	0.09	0.12	0.55	0.22	
Intersection Summary											

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	•	٠	→	•	•	•	•	1	†	/	/	
Movement	EBU	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT
Lane Configurations		Ä	^	7	ň	^	7		4	7		4
Traffic Volume (vph)	7	31	934	1	44	802	69	10	11	38	93	8
Future Volume (vph)	7	31	934	1	44	802	69	10	11	38	93	8
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Grade (%)			-4%			2%			0%			-1%
Total Lost time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.0	6.0		7.5
Lane Util. Factor		1.00	0.95	1.00	1.00	0.95	1.00		1.00	1.00		1.00
Frt		1.00	1.00	0.85	1.00	1.00	0.85		1.00	0.85		1.00
Flt Protected		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (prot)		1793	3541	1647	1752	3372	1599		1856	1615		1777
Flt Permitted		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (perm)		1793	3541	1647	1752	3372	1599		1856	1615		1777
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	8	34	1015	1	48	872	75	11	12	41	101	9
RTOR Reduction (vph)	0	0	0	0	0	0	30	0	0	38	0	0
Lane Group Flow (vph)	0	42	1015	1	48	872	45	0	23	3	0	110
Heavy Vehicles (%)	14%	0%	4%	0%	2%	6%	0%	0%	0%	0%	3%	0%
Turn Type	Prot	Prot	NA	Perm	Prot	NA	Perm	Split	NA	Perm	Split	NA
Protected Phases	1	1	6	•	5	2	0	4	4		3	3
Permitted Phases		7.7	00.0	6	0.4	00.0	2		0.0	4		44.0
Actuated Green, G (s)		7.7	83.0	83.0	8.1	83.9	83.9		8.9	8.9		14.0
Effective Green, g (s)		7.7	83.0	83.0	8.1	83.9	83.9		8.9	8.9		14.0
Actuated g/C Ratio		0.06	0.59	0.59	0.06	0.60	0.60		0.06	0.06		0.10
Clearance Time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.0	6.0		7.5
Vehicle Extension (s)		3.0	3.0	3.0	3.0	3.0	3.0		3.0	3.0		3.0
Lane Grp Cap (vph)		98	2099	976	101	2020	958		117	102		177
v/s Ratio Prot		0.02	c0.29	0.00	c0.03	0.26	0.02		c0.01	0.00		c0.06
v/s Ratio Perm v/c Ratio		0.43	0.48	0.00	0.48	0.43	0.03 0.05		0.20	0.00		0.62
		64.0	16.3	11.6	63.9	15.2	11.6		62.2	61.5		0.62 60.5
Uniform Delay, d1 Progression Factor		1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00
Incremental Delay, d2		3.0	0.8	0.0	3.5	0.7	0.1		0.8	0.1		6.6
Delay (s)		67.0	17.1	11.6	67.4	15.8	11.7		63.0	61.6		67.1
Level of Service		67.0 E	В	В	07.4 E	В	В		03.0 E	01.0 E		_
Approach Delay (s)		_	19.0	D	_	18.0	D		62.1	_		63.7
Approach LOS			В			В			E			E
Intersection Summary												
HCM 2000 Control Delay			23.1	HCM 2000 Level of Service					С			
HCM 2000 Volume to Capacity ratio			0.48									
Actuated Cycle Length (s)			140.0	S	um of los	t time (s)			26.0			
Intersection Capacity Utilization			59.7%		CU Level)		В			
Analysis Period (min)			15									
o Critical Lang Croup												

c Critical Lane Group



Movement	SBR
Lane Configurations	7
Traffic Volume (vph)	52
Future Volume (vph)	52
Ideal Flow (vphpl)	1900
Grade (%)	
Total Lost time (s)	7.5
Lane Util. Factor	1.00
Frt	0.85
Flt Protected	1.00
Satd. Flow (prot)	1375
Flt Permitted	1.00
Satd. Flow (perm)	1375
Peak-hour factor, PHF	0.92
Adj. Flow (vph)	57
RTOR Reduction (vph)	51
Lane Group Flow (vph)	6
Heavy Vehicles (%)	18%
Turn Type	Perm
Protected Phases	Fellii
Permitted Phases	3
Actuated Green, G (s)	14.0
Effective Green, g (s)	14.0
Actuated g/C Ratio	0.10
Clearance Time (s)	7.5
Vehicle Extension (s)	3.0
Lane Grp Cap (vph)	137
v/s Ratio Prot	
v/s Ratio Perm	0.00
v/c Ratio	0.04
Uniform Delay, d1	56.9
Progression Factor	1.00
Incremental Delay, d2	0.1
Delay (s)	57.1
Level of Service	E
Approach Delay (s)	
Approach LOS	
Intersection Summary	
intersection Summary	

HCM 6th Edition methodology expects strict NEMA phasing.

Intersection												
Int Delay, s/veh	3.7											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			414			414	
Traffic Vol, veh/h	6	15	44	14	11	14	24	84	7	18	122	5
Future Vol, veh/h	6	15	44	14	11	14	24	84	7	18	122	5
Conflicting Peds, #/hr	0	0	2	2	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	_	-	None	_	_	None	-	_		_	_	None
Storage Length	_	_	_	-	_	-	-	_	_	-	_	-
Veh in Median Storage,	# -	0	-	-	0	_	-	0	-	-	0	-
Grade, %	-	-8	-	-	-2	-	-	1	-	-	-1	_
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	0	0	0	9	0	0	0	0	0	13	0
Mvmt Flow	7	16	48	15	12	15	26	91	8	20	133	5
Major/Minor N	1inor2		ľ	Minor1			Major1		Į.	Major2		
Conflicting Flow All	280	327	71	264	325	50	138	0	0	99	0	0
Stage 1	176	176	-	147	147	-	-	-	-	-	-	-
Stage 2	104	151	-	117	178	-	-	-	-	-	-	-
Critical Hdwy	5.9	4.9	6.1	7.1	6.28	6.7	4.1	-	-	4.1	-	_
Critical Hdwy Stg 1	4.9	3.9	-	6.1	5.28	-	-	-	-	-	-	-
Critical Hdwy Stg 2	4.9	3.9	-	6.1	5.28	-	-	-	-	-	-	_
Follow-up Hdwy	3.5	4	3.3	3.5	4.09	3.3	2.2	-	_	2.2	-	-
Pot Cap-1 Maneuver	743	688	999	693	597	1017	1458	_	-	1507	-	_
Stage 1	881	819	-	860	770	-		_	_	-	_	-
Stage 2	939	830	_	892	749	_	-	_	-	-	-	_
Platoon blocked, %								_	_		-	-
Mov Cap-1 Maneuver	702	665	997	630	577	1017	1458	-	-	1507	-	_
Mov Cap-2 Maneuver	702	665	-	630	577	_	-	-	-	-	-	-
Stage 1	864	808	-	844	755	_	-	-	-	-	-	_
Stage 2	893	814	-	819	739	_	-	_	_	-	-	-
Ŭ.												
Approach	EB			WB			NB			SB		
HCM Control Delay, s	9.5			10.4			1.6			0.9		
HCM LOS	Α			В								
Minor Lane/Major Mvmt	<u> </u>	NBL	NBT	NBR I	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		1458	-	-	864	708	1507	-	-			
HCM Lane V/C Ratio		0.018	-	-	0.082		0.013	-	-			
HCM Control Delay (s)		7.5	0	-	9.5	10.4	7.4	0	-			
HCM Lane LOS		Α	Α	-	Α	В	Α	Α	-			
HCM 95th %tile Q(veh)		0.1	-	-	0.3	0.2	0	-	-			

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Intersection												
Int Delay, s/veh	3.1											
	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Movement Long Configurations	EDL		EDK	VVDL		WDK	INDL		NBK	ODL		אמט
Lane Configurations Traffic Vol, veh/h	1	♣ 91	128	16	♣ 111	1	90	ન 1	14	1	♣	1
Future Vol, veh/h	1	91	128	16	111	1	90	1	14	1	1	1
Conflicting Peds, #/hr	4	0	120	10	0	4	0	0	2	2	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	- Otop	- Olop	None	- Olop	-	None
Storage Length	<u>-</u>	_	-	_	_	-	_	_	0	_	_	-
Veh in Median Storage,		0	_	_	0	_	_	0	-	_	0	_
Grade, %	_	0	_	_	1	_	_	2	_	_	-5	_
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	1	11	7	1	0	0	0	0	0	0	0
Mvmt Flow	1	99	139	17	121	1	98	1	15	1	1	1
Major/Minor N	1ajor1			Major2		ı	Minor1		N	/linor2		
Conflicting Flow All	126	0	0	239	0	0	329	332	172	341	401	126
Stage 1	120	-	-	200	-	-	172	172	-	160	160	120
Stage 2	_	_	_	_	_	_	157	160	<u>-</u>	181	241	<u>-</u>
Critical Hdwy	4.1	_	_	4.17	_	_	7.5	6.9	6.4	6.1	5.5	5.7
Critical Hdwy Stg 1	-	_	_	-	-	-	6.5	5.9	-	5.1	4.5	-
Critical Hdwy Stg 2	-	-	-	-	-	-	6.5	5.9	-	5.1	4.5	_
Follow-up Hdwy	2.2	_	_	2.263	-	_	3.5	4	3.3	3.5	4	3.3
Pot Cap-1 Maneuver	1473	-	-	1299	-	-	606	570	869	678	604	946
Stage 1	-	-	-	-	-	-	819	746	-	885	804	-
Stage 2	_	-	_	-	-	-	835	756	-	868	759	-
Platoon blocked, %		-	-		-	-						
Mov Cap-1 Maneuver	1468	-	-	1298	-	-	597	559	867	654	593	943
Mov Cap-2 Maneuver	-	-	-	-	-	-	597	559	-	654	593	-
Stage 1	-	-	-	-	-	-	817	745	-	881	790	-
Stage 2	-	-	-	-	-	-	821	743	-	849	757	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			1			11.8			10.2		
HCM LOS							В			В		
Minor Lane/Major Mvmt	- 1	NBLn11	VBI n2	EBL	EBT	EBR	WBL	WBT	WBR S	SBI n1		
Capacity (veh/h)	<u> </u>	597	867	1468	-		1298	-	-	702		
HCM Lane V/C Ratio				0.001	_		0.013	_		0.005		
HCM Control Delay (s)		12.2	9.2	7.5	0	_	7.8	0	_			
HCM Lane LOS		В	Α.2	Α.5	A	_	Α.	A	<u>-</u>	В		
HCM 95th %tile Q(veh)		0.6	0.1	0	-	-	0	-	-	0		

Intersection												
Int Delay, s/veh	3.8											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			4			4	
Traffic Vol. veh/h	83	170	1	2	156	44	5	1	2	47	1	67
Future Vol, veh/h	83	170	1	2	156	44	5	1	2	47	1	67
Conflicting Peds, #/hr	1	0	0	0	0	1	0	0	0	0	0	2
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-		-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage	e,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	-3	-	-	1	-	-	0	-	-	-5	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	6	1	2	2	1	0	2	2	2	17	2	0
Mvmt Flow	90	185	1	2	170	48	5	1	2	51	1	73
Major/Minor I	Major1			Major2			Minor1			Minor2		
Conflicting Flow All	219	0	0	186	0	0	603	589	186	566	565	197
Stage 1	-	-	_	-	-	-	366	366	-	199	199	-
Stage 2	-	-	-	-	-	-	237	223	-	367	366	-
Critical Hdwy	4.16	-	-	4.12	-	-	7.12	6.52	6.22	6.27	5.52	5.7
Critical Hdwy Stg 1	-	-	-	-	-	-	6.12	5.52	-	5.27	4.52	-
Critical Hdwy Stg 2	-	-	-	-	-	-	6.12	5.52	-	5.27	4.52	-
Follow-up Hdwy	2.254	-	-	2.218	-	-	3.518			3.653	4.018	3.3
Pot Cap-1 Maneuver	1327	-	-	1388	-	-	411	421	856	483	508	873
Stage 1	-	-	-	-	-	-	653	623	-	813	778	-
Stage 2	-	-	-	-	-	-	766	719	-	690	689	-
Platoon blocked, %		-	-		-	-						
Mov Cap-1 Maneuver	1326	-	-	1388	-	-	353	388	856	452	468	871
Mov Cap-2 Maneuver	-	-	-	-	-	-	353	388	-	452	468	-
Stage 1	-	-	-	-	-	-	603	576	-	750	776	-
Stage 2	-	-	-	-	-	-	698	717	-	635	637	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	2.6			0.1			13.8			12.2		
HCM LOS							В			В		
Minor Lane/Major Mvm	nt 1	NBLn1	EBL	EBT	EBR	WBL	WBT	WBR	SBLn1			
Capacity (veh/h)		419	1326	-	_	1388	_	_	628			
HCM Lane V/C Ratio			0.068	-	_	0.002	-	-	0.199			
HCM Control Delay (s)		13.8	7.9	0	-	7.6	0	-	12.2			
HCM Lane LOS		В	Α	A	_	Α	A	-	В			
HCM 95th %tile Q(veh))	0.1	0.2	-	-	0	-	-	0.7			
	,											

Int Delay, s/veh	Intersection												
Traffic Vol, veh/h 38 161 6 19 158 51 20 1 62 31 1 19		3.5											
Lane Configurations	Movement	FBL	FBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Traffic Vol, veh/h													
Future Vol, veh/h 38 161 6 19 158 51 20 1 62 31 1 19				6	19		51	20		62	31		
Conflicting Peds, #/hr O O O O O O O O O	· ·								1				
Sign Control Free Stop Stop Stop Stop Stop RT Channelized - - None Storage Length 75 - - - 0 - - 0 - - 0 - -	<u>'</u>												
RT Channelized		Free	Free	Free	Free		Free	Stop	Stop	Stop	Stop	Stop	Stop
Storage Length 75													
Veh in Median Storage, # 0 - 0 0 - 0 0 - 0 0 1 4 1 2 0 0 1 1 0 0 1 0 <td>Storage Length</td> <td>75</td> <td>-</td> <td></td> <td>-</td> <td>-</td> <td></td> <td>-</td> <td>-</td> <td></td> <td>-</td> <td>-</td> <td></td>	Storage Length	75	-		-	-		-	-		-	-	
Grade, % - -5 - - 3 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 2 92		# -	0	-	-	0	-	-	0	-	-	0	-
Heavy Vehicles, %			-5	-	-	3	-	-	0	-	-	0	-
Mynt Flow 41 175 7 21 172 55 22 1 67 34 1 21 Major/Minor Major1 Major2 Minor1 Minor2 Conflicting Flow All 227 0 0 182 0 0 514 530 179 537 506 200 Stage 1 - - - - - 261 261 - 242 242 - Stage 2 - - - - - 253 269 - 295 264 - Critical Hdwy 4.1 - - 4.12 - - 7.12 6.52 6.22 7.1 6.52 6.2 Critical Hdwy Stg 1 - - - - 6.12 5.52 - 6.1 5.52 - Critical Hdwy Stg 2 - - - - 6.12 5.52 - 6.1 5.52	Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Major/Minor Major1 Major2 Minor1 Minor2 Conflicting Flow All 227 0 0 182 0 0 514 530 179 537 506 200 Stage 1 - - - - - 261 261 - 242 242 - Stage 2 - - - - - 253 269 - 295 264 - Critical Hdwy 4.1 - - 4.12 - - 7.12 6.52 6.22 7.1 6.52 6.2 Critical Hdwy Stg 1 - - - - - 6.12 5.52 - 6.1 5.52 - Critical Hdwy Stg 2 - - - - 6.12 5.52 - 6.1 5.52 - Follow-up Hdwy 2.2 - - 2.218 - 3.518 4.018 3.318 3.5 4	Heavy Vehicles, %	0	4	2	2	1	0	2	2	2	0	2	0
Conflicting Flow All 227 0 0 182 0 0 514 530 179 537 506 200 Stage 1 - - - - - - 261 - 242 242 - Stage 2 - - - - - 253 269 - 295 264 - Critical Hdwy 4.1 - - 4.12 - - 7.12 6.52 6.22 7.1 6.52 6.2 Critical Hdwy Stg 1 - - - - - 6.12 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52<	Mvmt Flow	41	175	7	21	172	55	22	1	67	34	1	21
Conflicting Flow All 227 0 0 182 0 0 514 530 179 537 506 200 Stage 1 - - - - - - 261 261 - 242 242 - Stage 2 - - - - - 253 269 - 295 264 - Critical Hdwy 4.1 - - 4.12 - - 7.12 6.52 6.22 7.1 6.52 6.2 Critical Hdwy Stg 1 - - - - - 6.12 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 </td <td></td>													
Conflicting Flow All 227 0 0 182 0 0 514 530 179 537 506 200 Stage 1 - - - - - - 261 - 242 242 - Stage 2 - - - - - 253 269 - 295 264 - Critical Hdwy 4.1 - - 4.12 - - 7.12 6.52 6.22 7.1 6.52 6.2 Critical Hdwy Stg 1 - - - - - 6.12 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52 - 6.1 5.52<	Major/Minor M	ajor1		ı	Major2			Minor1			Minor2		
Stage 1 - - - - 261 261 - 242 242 - Stage 2 - - - - - 253 269 - 295 264 - Critical Hdwy 4.1 - - 4.12 - - 7.12 6.52 6.22 7.1 6.52 6.2 Critical Hdwy Stg 1 - - - - 6.12 5.52 - 6.1 5.52 - Critical Hdwy Stg 2 - - - - 6.12 5.52 - 6.1 5.52 - Follow-up Hdwy 2.2 - - 2.218 - 3.518 4.018 3.318 3.5 4.018 3.3 Pot Cap-1 Maneuver 1353 - 1393 - 471 455 864 458 469 846 Stage 2 - - - - - 715 687 - 718 690 - Platoon blocked, % - - -		_	0			0			530			506	200
Stage 2 - - - - 253 269 - 295 264 - Critical Hdwy 4.1 - - 4.12 - 7.12 6.52 6.22 7.1 6.52 6.2 Critical Hdwy Stg 1 - - - - - 6.12 5.52 - 6.1 5.52 - Critical Hdwy Stg 2 - - - - - 6.12 5.52 - 6.1 5.52 - Follow-up Hdwy 2.2 - 2.218 - 3.518 4.018 3.318 3.5 4.018 3.3 Pot Cap-1 Maneuver 1353 - 1393 - 471 455 864 458 469 846 Stage 2 - - - - - 751 687 - 718 690 - Platoon blocked, % - - - - - - - - - - 442 434 864 406 447 846				-									
Critical Hdwy Stg 1 4.12 - 7.12 6.52 6.22 7.1 6.52 6.2 Critical Hdwy Stg 1 6.12 5.52 - 6.1 5.52 - Critical Hdwy Stg 2 6.12 5.52 - 6.1 5.52 - Endlow-up Hdwy 2.2 - 2.218 - 3.518 4.018 3.318 3.5 4.018 3.3 Pot Cap-1 Maneuver 1353 - 1393 - 471 455 864 458 469 846 Stage 1 744 692 - 766 705 - Stage 2 751 687 - 718 690 - Platoon blocked, % 751 687 - 718 690 - Platoon blocked, % 442 434 864 406 447 846 Mov Cap-2 Maneuver 442 434 864 406 447 - Stage 1 722 671 - 743 693 - Stage 2 719 675 - 641 669 - Stage 2 719 675 - 641 669 - Stage 2 719 675 - 641 669 - 180 - 18	•	_	_	_	_	_	_			_			_
Critical Hdwy Stg 1 6.12 5.52 - 6.1 5.52 - Critical Hdwy Stg 2 6.12 5.52 - 6.1 5.52 - Ellow-up Hdwy 2.2 2.218 3.518 4.018 3.318 3.5 4.018 3.3 Pot Cap-1 Maneuver 1353 - 1393 - 471 455 864 458 469 846 Stage 1 744 692 - 766 705 - Stage 2 751 687 - 718 690 - Platoon blocked, % 751 687 - 718 690 - Platoon blocked, % 442 434 864 406 447 846 Mov Cap-2 Maneuver 1353 - 1393 - 442 434 864 406 447 - Stage 1 722 671 - 743 693 - Stage 2 719 675 - 641 669 - Stage 2 719 675 - 641 669		4.1	_	-	4.12	-	_			6.22			6.2
Critical Hdwy Stg 2 6.12 5.52 - 6.1 5.52 - Follow-up Hdwy 2.2 - 2.218 - 3.518 4.018 3.318 3.5 4.018 3.3 Pot Cap-1 Maneuver 1353 - 1393 - 471 455 864 458 469 846 Stage 1 744 692 - 766 705 - Stage 2 751 687 - 718 690 - Platoon blocked, % Wov Cap-1 Maneuver 1353 - 1393 - 442 434 864 406 447 846 Mov Cap-2 Maneuver 442 434 864 406 447 - Stage 1 722 671 - 743 693 - Stage 2 719 675 - 641 669	•	_	-	_		_	-			_			
Follow-up Hdwy 2.2 2.218 3.518 4.018 3.318 3.5 4.018 3.3 Pot Cap-1 Maneuver 1353 - 1393 - 471 455 864 458 469 846 Stage 1 744 692 - 766 705 - Stage 2 751 687 - 718 690 - Platoon blocked, % Mov Cap-1 Maneuver 1353 - 1393 - 442 434 864 406 447 846 Mov Cap-2 Maneuver 442 434 864 406 447 - Stage 1 722 671 - 743 693 - Stage 2 719 675 - 641 669 719 675 - 641 669 719 675 - 641 669 719 675 - 641 669 719 675 - 641 669 719 675 - 641 669 719 675 - 719 675 - 719 675 - 719 675 - 641 669		-	-	-	-	-	-			-			-
Pot Cap-1 Maneuver 1353 1393 471 455 864 458 469 846	, ,	2.2	-	-	2.218	-	-		4.018	3.318	3.5	4.018	3.3
Stage 1 - - - - 744 692 - 766 705 - Stage 2 - - - - 751 687 - 718 690 - Platoon blocked, % -		1353	-	-	1393	-	-	471	455		458	469	846
Stage 2 - - - - 751 687 - 718 690 - Platoon blocked, % - <t< td=""><td></td><td>-</td><td>-</td><td>-</td><td>-</td><td>-</td><td>-</td><td>744</td><td>692</td><td>-</td><td>766</td><td>705</td><td>-</td></t<>		-	-	-	-	-	-	744	692	-	766	705	-
Mov Cap-1 Maneuver 1353 - - 1393 - - 442 434 864 406 447 846 Mov Cap-2 Maneuver - - - - - 442 434 - 406 447 - Stage 1 - - - - - 722 671 - 743 693 - Stage 2 - - - - - 719 675 - 641 669 - Approach EB WB NB SB HCM Control Delay, s 1.4 0.6 10.9 12.7		-	-	-	-	-	-	751	687	-	718	690	-
Mov Cap-2 Maneuver - - - - 442 434 - 406 447 - Stage 1 - - - - - 722 671 - 743 693 - Stage 2 - - - - - 719 675 - 641 669 - Approach EB WB NB SB HCM Control Delay, s 1.4 0.6 10.9 12.7	Platoon blocked, %		-	-		-	-						
Stage 1 - - - - 722 671 - 743 693 - Stage 2 - - - - - 719 675 - 641 669 - Approach EB WB NB SB HCM Control Delay, s 1.4 0.6 10.9 12.7	Mov Cap-1 Maneuver	1353	-	-	1393	-	-	442	434	864	406	447	846
Stage 2 - - - - 719 675 - 641 669 - Approach EB WB NB SB HCM Control Delay, s 1.4 0.6 10.9 12.7	Mov Cap-2 Maneuver	-	-	-	-	-	-	442	434	-	406	447	-
Approach EB WB NB SB HCM Control Delay, s 1.4 0.6 10.9 12.7	Stage 1	-	-	-	-	-	-			-			-
HCM Control Delay, s 1.4 0.6 10.9 12.7	Stage 2	-	-	-	-	-	-	719	675	-	641	669	-
HCM Control Delay, s 1.4 0.6 10.9 12.7													
HCM Control Delay, s 1.4 0.6 10.9 12.7	Approach	EB			WB			NB			SB		
,													
					3.0								
Minor Lane/Major Mvmt NBLn1 EBL EBT EBR WBL WBT WBR SBLn1 SBLn2	Minor Lane/Major Mumt	N	JRI n1	FRI	FRT	FRR	WRI	WRT	WRR	SRI n1	SRI n2		
Capacity (veh/h) 696 1353 1393 407 846		ľ				LDIX			WDI				
HCM Lane V/C Ratio 0.13 0.031 0.015 0.085 0.024						-			-				
HCM Control Delay (s) 10.9 7.7 - 7.6 0 - 14.7 9.4						-							
HCM Lane LOS B A A A - B A						-							
HCM 95th %tile Q(veh) 0.4 0.1 0 0.3 0.1						-							
110/01 00th 70th 0 4(VCH) 0.1 0 0.0 0.1	How John Johne Q(Ven)		0.4	0.1	<u>-</u>	_	U	_	_	0.3	0.1		

Intersection												
Int Delay, s/veh	4.5											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4	7	ሻ	^	7	ሻ	^	
Traffic Vol, veh/h	1	1	1	80	1	116	1	415	107	97	359	1
Future Vol, veh/h	1	1	1	80	1	116	1	415	107	97	359	1
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	100	-	0	90	-	130	225	-	-
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	-2	-	-	4	-	-	2	-	-	3	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	0	0	0	0	1	0	6	1	5	5	0
Mvmt Flow	1	1	1	87	1	126	1	451	116	105	390	1
Major/Minor N	1inor2		N	Minor1			Major1		N	Major2		
Conflicting Flow All	829	1170	196	859	1054	226	391	0	0	567	0	0
Stage 1	601	601	-	453	453	-	-	-	_	-	-	-
Stage 2	228	569	_	406	601	-	_	_	_	_	_	_
Critical Hdwy	7.1	6.1	6.7	8.3	7.3	7.32	4.1	-	-	4.2	_	-
Critical Hdwy Stg 1	6.1	5.1	-	7.3	6.3	-	-	-	_	-	-	-
Critical Hdwy Stg 2	6.1	5.1	-	7.3	6.3	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4	3.3	3.5	4	3.31	2.2	-	-	2.25	-	-
Pot Cap-1 Maneuver	292	222	828	209	180	761	1179	-	-	981	-	-
Stage 1	491	527	-	507	518	-	-	-	-	-	-	-
Stage 2	779	542	-	546	431	-	-	-	-	-	-	-
Platoon blocked, %								-	_		-	-
Mov Cap-1 Maneuver	223	198	828	191	161	761	1179	-	-	981	-	-
Mov Cap-2 Maneuver	223	198	-	191	161	-	-	-	-	-	-	-
Stage 1	491	471	-	506	517	-	-	-	-	-	-	-
Stage 2	648	541	-	486	385	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	18.1			22.3			0			1.9		
HCM LOS	C			22.3 C			U			1.0		
TIOWI LOO	J			J								
N.C		ND	NDT	NDD	-DI 4	MDI 41	A/DL C	051	057	000		
Minor Lane/Major Mvmt		NBL	NBT		EBLn1V			SBL	SBT	SBR		
Capacity (veh/h)		1179	-	-	279	191	761	981	-	-		
HCM Lane V/C Ratio		0.001	-	-			0.166		-	-		
HCM Control Delay (s)		8.1	-	-	18.1	39	10.7	9.1	-	-		
HCM Lane LOS		A	-	-	С	Е	В	A	-	-		
HCM 95th %tile Q(veh)		0	-	-	0	2.2	0.6	0.4	-	-		

2027 TF AM Synchro 11 Report Page 16 GS

Intersection												
Int Delay, s/veh	0.9											
		EDT	EDD	WDL	MOT	MPP	NDI	NET	NDD	ODL	ODT	ODB
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4		7	ĵ,		<u>ነ</u>	^	7	<u>ነ</u>	^	
Traffic Vol, veh/h	1	1	3	17	1	20	13	503	14	16	420	3
Future Vol, veh/h	1	1	3	17	1	20	13	503	14	16	420	3
Conflicting Peds, #/hr	0	0	0	0	0	0	_ 0	_ 0	_ 0	_ 0	_ 0	_ 0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length		-	-	0	-	-	150	-	135	110	-	-
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	5	-	-	3	-	-	4	-	-	-2	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	0	0	0	0	6	0	5	0	0	4	0
Mvmt Flow	1	1	3	18	1	22	14	547	15	17	457	3
Major/Minor M	linor2		N	Minor1		ı	Major1		N	Major2		
Conflicting Flow All	795	1083	230	838	1069	274	460	0	0	562	0	0
Stage 1	493	493	-	575	575		-	-	-		-	-
Stage 2	302	590	_	263	494	_	_	_	_	_	_	_
Critical Hdwy	8.5	7.5	7.4	8.1	7.1	7.32	4.1	_	-	4.1	-	_
Critical Hdwy Stg 1	7.5	6.5	- '	7.1	6.1	- 1.02	- '	_	_	-	_	_
Critical Hdwy Stg 2	7.5	6.5	-	7.1	6.1	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4	3.3	3.5	4	3.36	2.2	_	_	2.2	_	-
Pot Cap-1 Maneuver	226	162	754	228	187	696	1112	-	-	1019	-	-
Stage 1	464	480	-	432	460	-	_	_	_	-	_	_
Stage 2	633	423	-	694	506	-	-	-	-	-	-	-
Platoon blocked, %								_	_		_	-
Mov Cap-1 Maneuver	213	157	754	221	181	696	1112	-	-	1019	-	-
Mov Cap-2 Maneuver	213	157	-	221	181	-	-	_	_	-	_	-
Stage 1	458	472	-	426	454	-	-	-	-	-	-	-
Stage 2	604	418	_	678	497	_	_	_	_	_	_	_
				5.0								
Approach	ED			MD			ND			CD		
Approach	EB			WB			NB			SB		
HCM Control Delay, s	16			16.3			0.2			0.3		
HCM LOS	С			С								
Minor Lane/Major Mvmt		NBL	NBT	NBR I	EBLn1V	VBLn1V	VBLn2	SBL	SBT	SBR		
Capacity (veh/h)		1112	-	-	332	221	613	1019	_	_		
HCM Lane V/C Ratio		0.013	-	-		0.084			-	-		
HCM Control Delay (s)		8.3	-	-	16	22.8	11.1	8.6	-	-		
HCM Lane LOS		Α	-	_	C	C	В	Α	_	-		
HCM 95th %tile Q(veh)		0	-	-	0.1	0.3	0.1	0.1	-	-		

Intersection												
Int Delay, s/veh	7.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	<u></u>	7	ኘ	1		ሻ	^	7	<u> </u>	^	7
Traffic Vol, veh/h	126	17	81	3	3	3	116	401	32	7	380	53
Future Vol, veh/h	126	17	81	3	3	3	116	401	32	7	380	53
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	Yield	-	-	None	-	-	None	-	-	None
Storage Length	100	_	230	0	_	-	160	_	175	160	_	125
Veh in Median Storage,		0	-	_	0	_	-	0		-	0	-
Grade, %	-	0	_	_	0	_	_	3	_	_	-3	_
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	2	0	3	0	0	33	1	5	0	0	3	8
Mvmt Flow	137	18	88	3	3	3	126	436	35	8	413	58
								.00				- 55
Major/Minor N	/linor2		N	Minor1			Major1			Major2		
Conflicting Flow All	901	1152	207	920	1175	218	471	0		471	0	0
<u> </u>		429		688					0	4/1		U
Stage 1	429 472		-		688 487	-	-	-	-	-	-	-
Stage 2 Critical Hdwy	7.54	723 6.5	- 6.06	232			4.12	-	-	11	-	-
•			6.96	7.5 6.5	6.5	7.56	4.12	-	-	4.1	-	-
Critical Hdwy Stg 1	6.54	5.5 5.5	-		5.5	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54		2 22	6.5	5.5	2 62	2 24	-	-	-	-	-
Follow-up Hdwy	3.52	4	3.33	3.5	4	3.63	2.21	-	-	2.2	-	-
Pot Cap-1 Maneuver	233	199	796	229	193	699	1094	-	-	1101	-	-
Stage 1	574	587	-	407	450	-	-	-	-	-	-	-
Stage 2	542	434	-	756	554	-	-	-	-	-	-	-
Platoon blocked, %	207	175	700	170	170	600	1004	-	-	1101	-	-
Mov Cap-1 Maneuver	207	175	796	170	170	699	1094	-	-	1101	-	-
Mov Cap-2 Maneuver	207	175	-	170	170	-	-	-	-	-	-	-
Stage 1	508	583	-	360	398	-	-	-	-	-	-	-
Stage 2	473	384	-	646	550	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	34.5			21.2			1.8			0.1		
HCM LOS	D			С								
Minor Lane/Major Mvmt	t	NBL	NBT	NBR I	EBLn1	EBLn2 I	EBLn3\	VBLn1V	VBLn2	SBL	SBT	SBR
Capacity (veh/h)		1094	-	-	207	175	796	170	273	1101	-	-
HCM Lane V/C Ratio		0.115	-	_		0.106					-	-
HCM Control Delay (s)		8.7	_	_	51	28	10.1	26.6	18.5	8.3	_	_
HCM Lane LOS		Α	-	-	F	D	В	D	С	Α	-	-
HCM 95th %tile Q(veh)		0.4	-	-	4	0.3	0.4	0.1	0.1	0	-	-

LANE LEVEL OF SERVICE

Lane Level of Service

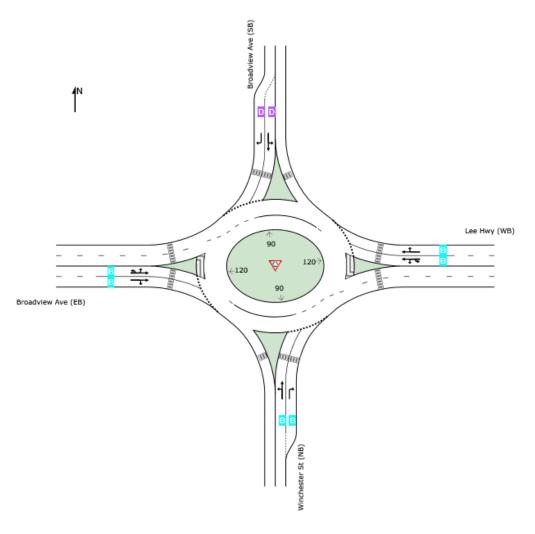
▼ Site: 101 [Broadview/Winchester/Lee - 2027 TF PM (Site Folder:

General)]

Output produced by SIDRA INTERSECTION Version: 9.1.2.202

Warrenton Village Center 2027 Future with Development PM Peak Hour Site Category: (None) Roundabout

		Appro	aches		Intersection
	South	East	North	West	Intersection
LOS	В	В	D	В	В



Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

SIDRA INTERSECTION 9.1 | Copyright © 2000-2022 Akcelik and Associates Pty Ltd | sidrasolutions.com Organisation: GOROVE SLADE | Licence: PLUS / 1PC | Processed: Monday, February 12, 2024 1:51:53 AM Project: U:\3243\001. Warrenton Village Center\Analysis\Sidra\2nd Submission\2027 TF.sip9

LANE SUMMARY

♥ Site: 101 [Broadview/Winchester/Lee - 2027 TF PM (Site Folder:

General)]

Output produced by SIDRA INTERSECTION Version: 9.1.2.202

Warrenton Village Center 2027 Future with Development PM Peak Hour Site Category: (None) Roundabout

Lane Use	and Pe	erform	nance												
	Demand				Сар.	Deg. Satn	Lane Util.	Aver. Delay	Level of Service	95% B Que	eue	Lane Config	Lane Length	Cap. F Adj. E	
	[Total veh/h	нv ј %	[Total veh/h	пv ј %	veh/h	v/c	%	sec		[Veh	Dist] ft		ft	%	%
South: Wir	nchester	St (NB	3)												
Lane 1 ^d	235	0.5	235	0.5	556	0.423	100	13.2	LOS B	2.5	62.1	Full	1600	0.0	0.0
Lane 2	77	0.0	77	0.0	361	0.214	100	13.7	LOS B	0.9	23.2	Short	250	0.0	NA
Approach	313	0.4	313	0.4		0.423		13.3	LOS B	2.5	62.1				
East: Lee	Hwy (WE	3)													
Lane 1	623	1.7	623	1.7	857	0.726	100	17.7	LOS B	10.7	271.5	Full	1600	0.0	0.0
Lane 2 ^d	761	2.0	761	2.0	1047	0.726	100	15.3	LOS B	11.5	291.4	Full	1600	0.0	0.0
Approach	1383	1.9	1383	1.9		0.726		16.3	LOS B	11.5	291.4				
North: Bro	adview A	ve (SE	3)												
Lane 1	347	0.7	347	0.7	426	0.815	100	39.5	LOS D	7.1	177.8	Short	215	0.0	NA
Lane 2 ^d	413	4.0	413	4.0	487	0.848	100	39.7	LOS D	8.4	216.0	Full	1600	0.0	0.0
Approach	759	2.5	759	2.5		0.848		39.6	LOS D	8.4	216.0				
West: Broa	adview A	ve (EB	i)												
Lane 1	547	2.5	547	2.5	913	0.599	100	12.4	LOS B	6.7	169.7	Full	1600	0.0	0.0
Lane 2 ^d	664	1.9	664	1.9	1108	0.599	100	10.8	LOS B	6.8	171.5	Full	1600	0.0	0.0
Approach	1210	2.2	1210	2.2		0.599		11.5	LOS B	6.8	171.5				
All Vehicles	3666	2.0	3666	2.0		0.848		19.3	LOS B	11.5	291.4				

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

d Dominant lane on roundabout approach

Approach	Lane Flo	ws (vel	h/h)							
South: Wincl	hester St (NB)								
Mov.	L2	T1	R2	Total	%HV		Deg.	Lane Prob.		
From S						Cap.		Util. SL Ov.		
To Exit:	W	Ν	Ε			veh/h	v/c	% %	No.	

Lane 1	122	114	-	235	0.5		556	0.423	100	NA	NA	
Lane 2	-	-	77	77	0.0		361	0.214	100	0.0	1	
Approach	122	114	77	313	0.4			0.423				
East: Lee Hw	y (WB)											
Mov.	U	L2	T1	R2	Total	%HV		Deg.		Prob.	Ov.	
From E							Cap. veh/h	Satn v/c	Util. %	SL Ov.	Lane No.	
To Exit:	Е	S	W	N			ven/m	۷/С	70	70	INU.	
Lane 1	10	70	543	-	623	1.7	857	0.726	100	NA	NA	
Lane 2	-	-	638	123	761	2.0	1047	0.726	100	NA	NA	
Approach	10	70	1180	123	1383	1.9		0.726				
North: Broad	view Ave	(SB)										
Mov.	L2	T1	R2	Total	%HV			Deg.	Lane	Prob.	Ov.	
From N							Cap.	Satn		SL Ov.	Lane	
To Exit:	Е	S	W				veh/h	v/c	%	%	No.	
Lane 1	249	98	-	347	0.7		426	0.815	100	0.0	2	
Lane 2	-	-	413	413	4.0		487	0.848	100	NA	NA	
Approach	249	98	413	759	2.5			0.848				
West: Broady	view Ave	(EB)										
Mov.	U	L2	T1	R2	Total	%HV		Deg.	Lane	Prob.	Ov.	
From W							Cap.	Satn		SL Ov.	Lane	
To Exit:	W	N	Е	S			veh/h	v/c	%	%	No.	
Lane 1	2	293	252	-	547	2.5	913	0.599	100	NA	NA	
Lane 2	-	-	618	46	664	1.9	1108	0.599	100	NA	NA	
Approach	2	293	870	46	1210	2.2		0.599				
	Total	%HV I	Deg.Sat	n (v/c)								
All Vehicles	3666	2.0		0.848								

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

Merge Analysis								
Exi	Short	Percent Opposing	Critical	Follow-up Lane	e Capacity	Deg.	Min.	Merge
Lane		Opng in Flow Rate	Gap	Headway Flov		Satn E	Delay	Delay
Numbe	Length	Lane		Rate				
	ft	% veh/h pcu/h	sec	sec veh/l	n veh/h	v/c	sec	sec
There are no Exit Short Lar	es for Mer	ge Analysis at this Site						

Variable Demand	Analysis			
	Initial Queued Demand	Residual Queued Demand	Time for Residual Demand to Clear	Duration of Oversatn
	veh	veh	sec	sec
South: Winchester S	t (NB)			
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0
East: Lee Hwy (WB)				
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0
North: Broadview Av	e (SB)			
Lane 1	0.0	0.0	0.0	0.0

Lane 2	0.0	0.0	0.0	0.0
West: Broadview	Ave (EB)			
Lane 1	0.0	0.0	0.0	0.0
Lane 2	0.0	0.0	0.0	0.0

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Intersection												
Int Delay, s/veh	0.6											
	EDI	CDT	EDD	WDI	WDT	WDD	NDI	NDT	NDD	CDI	CDT	CDD
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	0	^	7	0	^	104	^	^	7	^	^	7
Traffic Vol, veh/h	0	1075	83	0	1247	104	0	0	25	0	0	80
Future Vol, veh/h	0	1075	83	0	1247	104	0	0	25	0	0	80
Conflicting Peds, #/hr	_ 0	0	0	0	0	4	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	110	-	-	300	-	-	0	-	-	0
Veh in Median Storage,		0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	1	-	-	3	-	-	3	-	-	-11	-
Peak Hour Factor	93	93	93	93	93	93	93	93	93	93	93	93
Heavy Vehicles, %	0	2	0	0	2	0	0	0	4	0	0	0
Mvmt Flow	0	1156	89	0	1341	112	0	0	27	0	0	86
Major/Minor M	ajor1		N	Major2		N	/linor1		N	/linor2		
Conflicting Flow All	-	0	0	-	-	0	-	-	578	-	-	675
Stage 1	-	-	-	-	_	-	-	_	-	-	_	-
Stage 2	_	_	_	_	_	-	_	_	_	_	_	_
Critical Hdwy	-	_	_	-	-	-	-	_	7.28	-	_	5.8
Critical Hdwy Stg 1	_	_	_	_	_	-	_	_	-	_	_	-
Critical Hdwy Stg 2	-	_	_	-	-	-	-	_	-	-	_	_
Follow-up Hdwy	_	_	_	-	_	-	-	_	3.34	-	_	3.3
Pot Cap-1 Maneuver	0	_	_	0	_	-	0	0	433	0	0	493
Stage 1	0	_	_	0	_	-	0	0	-	0	0	-
Stage 2	0	-	-	0	_	-	0	0	-	0	0	_
Platoon blocked, %		_	_		_	_						
Mov Cap-1 Maneuver	-	-	-	_	-	-	-	-	433	-	-	491
Mov Cap-2 Maneuver	_	_	_	_	_	_	_	_	-	_	_	-
Stage 1	-	-	-	_	-	-	-	-	-	-	-	-
Stage 2	-	_	_	_	_	_	_	_	_	_	_	_
Annroach	EB			WB			NB			SB		
Approach												
HCM LOS	0			0			13.9			13.9		
HCM LOS							В			В		
Minor Lane/Major Mvmt	1	NBLn1	EBT	EBR	WBT	WBR S	SBLn1					
Capacity (veh/h)		433	-	-	-	-	491					
HCM Lane V/C Ratio		0.062	-	-	-	-	0.175					
HCM Control Delay (s)		13.9	-	-	-	-	13.9					
HCM Lane LOS		В	-	-	-	-	В					
HCM 95th %tile Q(veh)		0.2	-	-	-	-	0.6					

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	۶	→	\rightarrow	•	•	•	†	/	ļ	4	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBT	NBR	SBT	SBR	
Lane Group Flow (vph)	149	1006	2	68	1243	151	36	79	204	152	
v/c Ratio	0.72	0.48	0.00	0.54	0.70	0.17	0.31	0.30	0.80	0.41	
Control Delay	82.8	22.5	0.0	82.0	32.7	2.3	72.2	3.0	83.9	9.8	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	82.8	22.5	0.0	82.0	32.7	2.3	72.2	3.0	83.9	9.8	
Queue Length 50th (ft)	148	333	0	68	508	0	36	0	201	0	
Queue Length 95th (ft)	224	441	0	123	675	28	73	0	#344	58	
Internal Link Dist (ft)		457			1504		131		565		
Turn Bay Length (ft)	240		330	150		150		60			
Base Capacity (vph)	260	2078	960	157	1773	876	202	327	268	377	
Starvation Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.57	0.48	0.00	0.43	0.70	0.17	0.18	0.24	0.76	0.40	

Intersection Summary
95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

		۶	→	•	•	←	•	1	†	/	/	+
Movement	EBU	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT
Lane Configurations		ă	^	7	ሻ	^	7		ર્ન	7		्
Traffic Volume (vph)	9	133	956	2	65	1181	143	17	17	75	176	18
Future Volume (vph)	9	133	956	2	65	1181	143	17	17	75	176	18
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Grade (%)			-4%			2%			0%			-1%
Total Lost time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.6	6.6		7.5
Lane Util. Factor		1.00	0.95	1.00	1.00	0.95	1.00		1.00	1.00		1.00
Frpb, ped/bikes		1.00	1.00	0.97	1.00	1.00	0.98		1.00	1.00		1.00
Flpb, ped/bikes		1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00
Frt		1.00	1.00	0.85	1.00	1.00	0.85		1.00	0.85		1.00
Flt Protected		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (prot)		1807	3682	1602	1787	3504	1558		1854	1615		1810
Flt Permitted		0.95	1.00	1.00	0.95	1.00	1.00		0.98	1.00		0.96
Satd. Flow (perm)		1807	3682	1602	1787	3504	1558		1854	1615		1810
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	9	140	1006	2	68	1243	151	18	18	79	185	19
RTOR Reduction (vph)	0	0	0	1	0	0	74	0	0	74	0	0
Lane Group Flow (vph)	0	149	1006	1	68	1243	77	0	36	5	0	204
Confl. Peds. (#/hr)				2		1_10	2	•			•	_0.
Heavy Vehicles (%)	0%	2%	0%	0%	0%	2%	1%	0%	0%	0%	1%	0%
Turn Type	Prot	Prot	NA	Perm	Prot	NA	Perm	Split	NA	Perm	Split	NA
Protected Phases	1	1	6	1 01111	5	2	1 01111	4	4	1 01111	3	3
Permitted Phases	•	•	•	6	•	=	2	•	•	4	•	J
Actuated Green, G (s)		17.2	83.4	83.4	9.3	76.0	76.0		9.5	9.5		21.2
Effective Green, g (s)		17.2	83.4	83.4	9.3	76.0	76.0		9.5	9.5		21.2
Actuated g/C Ratio		0.11	0.56	0.56	0.06	0.51	0.51		0.06	0.06		0.14
Clearance Time (s)		6.4	5.7	5.7	6.8	5.6	5.6		6.6	6.6		7.5
Vehicle Extension (s)		3.0	3.0	3.0	3.0	3.0	3.0		3.0	3.0		3.0
Lane Grp Cap (vph)		207	2047	890	110	1775	789		117	102		255
v/s Ratio Prot		c0.08	0.27	000	0.04	c0.35	700		c0.02	102		c0.11
v/s Ratio Perm		60.00	0.21	0.00	0.04	00.00	0.05		00.02	0.00		00.11
v/c Ratio		0.72	0.49	0.00	0.62	0.70	0.10		0.31	0.05		0.80
Uniform Delay, d1		64.1	20.3	14.8	68.6	28.3	19.2		67.1	66.0		62.3
Progression Factor		1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00
Incremental Delay, d2		11.4	0.8	0.0	9.9	2.3	0.2		1.5	0.2		16.3
Delay (s)		75.4	21.2	14.8	78.5	30.6	19.4		68.6	66.2		78.6
Level of Service		75.4 E	C C	14.0 B	70.5 E	C	В		60.0 E	60.2 E		70.0 E
Approach Delay (s)		<u> </u>	28.2	U	<u> </u>	31.7	U		67.0	<u> </u>		69.1
Approach LOS			20.2 C			C C			67.0 E			03.1 E
Intersection Summary									_			_
HCM 2000 Control Delay			36.0	Н	CM 2000	Level of	Sarvica		D			
HCM 2000 Volume to Capacit	v ratio		0.69	1 1'	CIVI ZUUU	Level OI	OCI VICE		U			
Actuated Cycle Length (s)	y TallO		150.0	C.	um of los	t time (c)			26.6			
	'n		76.2%			t time (s) of Service			20.0 D			
Intersection Capacity Utilizatio	71.1		15	IC	o Level (or service			U			
Analysis Period (min)			15									
c Critical Lane Group												



Movement	SBR
Lane Configurations	7
Traffic Volume (vph)	144
Future Volume (vph)	144
Ideal Flow (vphpl)	1900
Grade (%)	
Total Lost time (s)	7.5
Lane Util. Factor	1.00
Frpb, ped/bikes	1.00
Flpb, ped/bikes	1.00
Frt	0.85
Flt Protected	1.00
Satd. Flow (prot)	1607
Flt Permitted	1.00
Satd. Flow (perm)	1607
Peak-hour factor, PHF	0.95
Adj. Flow (vph)	152
RTOR Reduction (vph)	131
Lane Group Flow (vph)	21
Confl. Peds. (#/hr)	Z1
Heavy Vehicles (%)	1%
	Perm
Turn Type Protected Phases	Perm
Protected Phases Permitted Phases	3
Actuated Green, G (s)	21.2
Effective Green, g (s)	21.2
Actuated g/C Ratio	0.14
Clearance Time (s)	7.5
Vehicle Extension (s)	3.0
Lane Grp Cap (vph)	227
v/s Ratio Prot	
v/s Ratio Perm	0.01
v/c Ratio	0.09
Uniform Delay, d1	56.0
Progression Factor	1.00
Incremental Delay, d2	0.2
Delay (s)	56.2
Level of Service	Е
Approach Delay (s)	
Approach LOS	
Interception Cummer	
Intersection Summary	

HCM 6th Edition methodology expects strict NEMA phasing.

Intersection												
Int Delay, s/veh	8.4											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	LDL	4	LDK	WDL	₩	WDK	NDL	1 DN	אטוז	ODL	100 41h	אמט
Traffic Vol, veh/h	17	77	120	45	50	41	97	101	12	48	4 P	32
Future Vol, veh/h	17	77	120	45	50	41	97	101	12	48	75	32
Conflicting Peds, #/hr	0	0	14	14	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	_	_	-	-	_	-	_	-	-	_	-	-
Veh in Median Storage,	# -	0	_	_	0	_	_	0	-	_	0	_
Grade, %	_	-8	-	-	-2	-	_	1	_	-	-1	_
Peak Hour Factor	96	96	96	96	96	96	96	96	96	96	96	96
Heavy Vehicles, %	0	0	2	0	2	5	0	2	0	0	3	0
Mvmt Flow	18	80	125	47	52	43	101	105	13	50	78	33
Major/Minor N	linor2			Minor1			Major1		N	Major2		
Conflicting Flow All	476	515	70	507	525	59	111	0	0	118	0	0
Stage 1	195	195	-	314	314	-	-	-	-	-	-	-
Stage 2	281	320	-	193	211	-	-	-	-	-	-	-
Critical Hdwy	5.9	4.9	6.14	7.1	6.14	6.8	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	4.9	3.9	-	6.1	5.14	-	-	-	-	-	-	-
Critical Hdwy Stg 2	4.9	3.9	-	6.1	5.14	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4	3.32	3.5	4.02	3.35	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	589	586	994	479	483	988	1492	-	-	1483	-	-
Stage 1	866	810	-	701	678	-	-	-	-	-	-	-
Stage 2	802	756	-	813	744	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	471	524	982	336	432	988	1492	-	-	1483	-	-
Mov Cap-2 Maneuver	471	524	-	336	432	-	-	-	-	-	-	-
Stage 1	803	781	-	650	629	-	-	-	-	-	-	-
Stage 2	652	701	-	607	717	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	12.5			16			3.6			2.4		
HCM LOS	В			С								
Minor Lane/Major Mvmt		NBL	NBT	NBR I	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		1492	-	-		467	1483	-				
HCM Lane V/C Ratio		0.068	_			0.303		_	<u>-</u>			
HCM Control Delay (s)		7.6	0.1	_	12.5	16	7.5	0.1	-			
HCM Lane LOS		A	A	_	В.	C	A	A	_			
HCM 95th %tile Q(veh)		0.2	-	_	1.4	1.3	0.1	-	-			

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Warrenton Village Center 2027 Total Future

Intersection												
Int Delay, s/veh	4.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4		1,00	4	1,5,1		4	7	UDL	4	UDIK
Traffic Vol, veh/h	3	116	119	31	128	2	118	2	39	1	5	1
Future Vol, veh/h	3	116	119	31	128	2	118	2	39	1	5	1
Conflicting Peds, #/hr	4	0	0	0	0	4	0	0	2	2	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	Stop -	Stop -	None	Slop -	Stop -	None
Storage Length	_	_	110116	_	_	-	_	_	0	_		TAOHE
Veh in Median Storage,	# -	0	_	<u>-</u>	0	<u>-</u>	_	0	-	<u>-</u>	0	<u>-</u> -
Grade, %	# - -	0	_	-	1	<u>-</u>	_	2	<u>-</u>	_	-5	_
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	3	0	4	1	0	3	0	3	0	0	0
Mymt Flow	3	126	129	34	139	2	128	2	42	1	5	1
IVIVIIIL FIOW	3	120	129	34	139		120		42	I	3	I
Major/Minor M	1ajor1			Major2			Minor1		<u> </u>	Minor2		
Conflicting Flow All	145	0	0	255	0	0	408	410	193	433	473	144
Stage 1	-	-	-	-	-	-	197	197	-	212	212	-
Stage 2	-	-	-	-	-	-	211	213	-	221	261	-
Critical Hdwy	4.1	-	-	4.14	-	-	7.53	6.9	6.43	6.1	5.5	5.7
Critical Hdwy Stg 1	-	-	-	-	-	-	6.53	5.9	-	5.1	4.5	-
Critical Hdwy Stg 2	-	-	_	-	-	_	6.53	5.9	-	5.1	4.5	-
Follow-up Hdwy	2.2	-	-	2.236	_	-	3.527		3.327	3.5	4	3.3
Pot Cap-1 Maneuver	1450	-	-	1298	-	_	527	511	837	605	562	927
Stage 1	-	-	-	-	_	-	785	726	-	843	775	-
Stage 2	-	-	_	_	_	_	771	713	-	836	748	-
Platoon blocked, %		-	_		_	-						
Mov Cap-1 Maneuver	1445	-	-	1298	_	-	511	494	836	557	543	924
Mov Cap-2 Maneuver	-	_	_	-	_	_	511	494	-	557	543	-
Stage 1	-	_	_	_	_	_	783	725	-	839	751	-
Stage 2	_	_	_	_	_	_	743	691	_	788	747	_
Jugo L								30 1		. 00		
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0.1			1.5			13.2			11.3		
HCM LOS							В			В		
Minor Lane/Major Mvmt		NBLn11	VRI n2	EBL	EBT	EBR	WBL	WBT	WBR S	SRI n1		
		511	836	1445	LDI	LDIX	1298	WDI	יוטויי	579		
Capacity (veh/h) HCM Lane V/C Ratio			0.051		-			_	-			
					- 0	-	0.026	-		0.013		
HCM Long LOS		14.4	9.5	7.5	0	-	7.8	0	-			
HCM C5th 0(tile O(tob)		В	A	A	Α	-	Α	Α	-	В		
HCM 95th %tile Q(veh)		1	0.2	0	-	-	0.1	-	-	0		

Intersection												
Int Delay, s/veh	3.3											
		EDT		MDI	MOT	WDD	NDI	NDT	NDD	ODI	ODT	000
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	40	4	_	•	4	4.4	•	4		07	4	
Traffic Vol, veh/h	42	170	5	6	226	14	3	1	1	67	1	52
Future Vol, veh/h	42	170	5	6	226	14	3	1	1	67	1	52
Conflicting Peds, #/hr	1	0	0	0	0	1	0	0	0	2	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage	, # -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	-3	-	-	1	-	-	0	-	-	-5	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	0	2	2	2	0	2	2
Mvmt Flow	46	185	5	7	246	15	3	1	1	73	1	57
Major/Minor N	Major1			Major2			Minor1		N	/linor2		
Conflicting Flow All	262	0	0	190	0	0	577	556	190	552	551	255
Stage 1	- 202	-	-	-	-	-	280	280	-	269	269	200
Stage 2	_			_	_		297	276	<u>-</u>	283	282	_
Critical Hdwy	4.12			4.12	_		7.12	6.52	6.22	6.1	5.52	5.72
Critical Hdwy Stg 1	7.12			7.12	_		6.12	5.52	- 0.22	5.1	4.52	J.12 -
Critical Hdwy Stg 2				_	_		6.12	5.52	_	5.1	4.52	_
Follow-up Hdwy	2.218			2.218	_		3.518	4.018		3.5	4.018	3.318
Pot Cap-1 Maneuver	1302			1384	_		428	439	852	522	515	812
Stage 1	1002	_		100-1	_		727	679	- 002	799	740	- 012
Stage 2				_	_		712	682	_	788	733	_
Platoon blocked, %					_	_	112	002		700	100	
Mov Cap-1 Maneuver	1301			1384	_	_	383	418	851	501	491	811
Mov Cap-1 Maneuver	1301			1304	_	_	383	418	-	501	491	-
Stage 1	-	-	-	<u>-</u>	<u>-</u>	-	698	652		766	735	-
Stage 2			_	_	_		657	677	<u>-</u>	753	704	_
Glaye Z	_	_	-	<u>-</u>	_	_	001	011	<u>-</u>	100	104	<u>-</u>
Approach	EB			WB			NB			SB		
HCM Control Delay, s	1.5			0.2			13.3			12.7		
HCM LOS							В			В		
Minor Lane/Major Mvm	nt l	NBLn1	EBL	EBT	EBR	WBL	WBT	WBR	SBI n1			
Capacity (veh/h)		439	1301			1384	-	-	600			
HCM Lane V/C Ratio		0.012	0.035	-		0.005	<u>-</u>		0.217			
HCM Control Delay (s)		13.3	7.9	0	-	7.6	0	-	12.7			
HCM Lane LOS		13.3 B	7.9 A	A	_	7.0 A	A	-	12. <i>1</i>			
HCM 95th %tile Q(veh)	\	0	0.1		-	0	- -		0.8			
How som whe Q(ven)		U	U. I	-	-	U	-	-	0.0			

Intersection	6 -											
Int Delay, s/veh	2.7											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	f)			4			4			ર્ન	7
Traffic Vol, veh/h	5	167	22	62	217	2	12	1	39	11	1	27
Future Vol, veh/h	5	167	22	62	217	2	12	1	39	11	1	27
Conflicting Peds, #/hr	1	0	0	0	0	1	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	75	-	-	-	-	-	-	-	-	-	-	50
Veh in Median Storage	, # -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	-5	-	-	3	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	3	2	2	2	0	2	2	2	0	2	0
Mvmt Flow	5	182	24	67	236	2	13	1	42	12	1	29
Major/Minor N	/lajor1			Major2			Minor1			Minor2		
Conflicting Flow All	239	0	0	206	0	0	590	577	194	598	588	238
Stage 1	200	-	-		-	-	204	204	-	372	372	200
Stage 2	_	<u> </u>	_	_	_	_	386	373	_	226	216	_
Critical Hdwy	4.1	_	_	4.12	_	_	7.12	6.52	6.22	7.1	6.52	6.2
Critical Hdwy Stg 1	- '-	_	_	- 1.12	_	_	6.12	5.52	-	6.1	5.52	-
Critical Hdwy Stg 2	_	_	_	-	_	_	6.12	5.52	-	6.1	5.52	-
Follow-up Hdwy	2.2	_	_	2.218	_	_	3.518	4.018	3.318	3.5	4.018	3.3
Pot Cap-1 Maneuver	1340	-	_	1365	_	_	419	427	847	417	421	806
Stage 1	-	_	_	-	_	_	798	733	-	653	619	-
Stage 2	_	-	-	_	-	-	637	618	_	704	724	-
Platoon blocked, %		_	_		_	-						
Mov Cap-1 Maneuver	1339	-	-	1365	-	-	384	401	847	377	395	805
Mov Cap-2 Maneuver	-	-	_	-	-	-	384	401	-	377	395	-
Stage 1	-	-	-	-	-	-	795	730	-	650	583	-
Stage 2	-	-	-	-	-	-	578	582	-	738	721	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0.2			1.7			11			11.2		
•	0.2			1.7			В					
HCM LOS							B			В		
Minor Lane/Major Mvm	t I	NBLn1	EBL	EBT	EBR	WBL	WBT	WBR	SBLn1			
Capacity (veh/h)		652	1339	-	-	1365	-	-	378	805		
HCM Lane V/C Ratio			0.004	-	-	0.049	-	-	0.035			
HCM Control Delay (s)		11	7.7	-	-	7.8	0	-	14.9	9.6		
HCM Lane LOS		В	Α	-	-	Α	Α	-	В	Α		
HCM 95th %tile Q(veh)		0.3	0	-	-	0.2	-	-	0.1	0.1		

Intersection												
Int Delay, s/veh	7.2											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4	7	ች	^	7	*	^	
Traffic Vol, veh/h	2	1	4	111	1	145	2	376	96	97	510	2
Future Vol, veh/h	2	1	4	111	1	145	2	376	96	97	510	2
Conflicting Peds, #/hr	0	0	0	0	0	0	4	0	1	1	0	4
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	_	_	None	-	-	None	-	-	None
Storage Length	-	-	-	100	-	0	90	-	130	225	-	-
Veh in Median Storage	,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	-2	-	-	4	-	-	2	-	-	3	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	0	0	1	0	2	0	3	4	1	4	0
Mvmt Flow	2	1	4	121	1	158	2	409	104	105	554	2
Major/Minor N	Minor2		ľ	Minor1			Major1		N	Major2		
Conflicting Flow All	978	1287	282	902	1184	206	560	0	0	514	0	0
Stage 1	769	769	-	414	414	-	-	-	-	-	-	-
Stage 2	209	518	-	488	770	-	-	-	-	-	-	-
Critical Hdwy	7.1	6.1	6.7	8.32	7.3	7.34	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.1	5.1	-	7.32	6.3	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.1	5.1	-	7.32	6.3	-	-	-	-	-	-	_
Follow-up Hdwy	3.5	4	3.3	3.51	4	3.32	2.2	-	-	2.21	-	-
Pot Cap-1 Maneuver	232	191	732	192	147	782	1021	-	-	1055	-	-
Stage 1	397	450	-	537	544	-	-	-	-	-	-	-
Stage 2	798	568	-	478	348	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	169	171	730	175	132	781	1018	-	-	1054	-	-
Mov Cap-2 Maneuver	169	171	-	175	132	-	-	-	-	-	-	-
Stage 1	395	404	-	535	542	-	-	-	-	-	-	-
Stage 2	634	566	-	427	312	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	17.2			33.7			0			1.4		
HCM LOS	С			D								
Minor Lane/Major Mvm	t	NBL	NBT	NRR	EBLn1V	VBI n1V	VRI n2	SBL	SBT	SBR		
Capacity (veh/h)		1018	-	-	302	174	781	1054	ODT	ODIX		
HCM Lane V/C Ratio		0.002	-		0.025		0.202	0.1	-	-		
HCM Control Delay (s)		8.5	-	-	17.2	63.4	10.8	8.8				
HCM Lane LOS		6.5 A	-		17.2 C	63.4 F	10.6 B	0.0 A	<u>-</u>	-		
HCM 95th %tile Q(veh)		0		-	0.1	4.2	0.8	0.3				
HOW JOHN JOHN Q(VEII)		U		_	0.1	7.2	0.0	0.0				

2027 TF PM Synchro 11 Report Page 16 GS

Intersection												
Int Delay, s/veh	2.3											
• •		EST	ED5	14/51	VAIDT	MES	ND	NOT	NDD	051	057	000
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	40	4	4=	\	ĵ,	20	<u>ነ</u>	^	7	<u> </u>	^	•
Traffic Vol, veh/h	10	1	17	40	1	39	15	425	28	43	576	6
Future Vol, veh/h	10	1	17	40	1	39	15	425	28	43	576	6
Conflicting Peds, #/hr	0	0	0	0	0	0	_ 5	0	_ 0	0	0	_ 5
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	0	-	-	150	-	135	110	-	-
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	5	-	-	3	-	-	4	-	-	-2	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	0	0	0	0	0	5	0	3	0	0	3	0
Mvmt Flow	11	1	18	43	1	42	16	462	30	47	626	7
Major/Minor N	1inor2		N	Minor1			Major1		N	Major2		
Conflicting Flow All	993	1253	322	902	1226	231	638	0	0	492	0	0
Stage 1	729	729	-	494	494	-	-	-	-	-	-	-
Stage 2	264	524	-	408	732	-	-	-	-	-	-	-
Critical Hdwy	8.5	7.5	7.4	8.1	7.1	7.3	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	7.5	6.5	-	7.1	6.1	-	-	-	-	-	-	-
Critical Hdwy Stg 2	7.5	6.5	-	7.1	6.1	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4	3.3	3.5	4	3.35	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	154	123	650	203	147	748	956	-	-	1082	-	-
Stage 1	314	352	-	489	506	-	-	-	-	-	-	-
Stage 2	673	461	-	557	380	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	137	115	647	187	138	748	952	-	-	1082	-	-
Mov Cap-2 Maneuver	137	115	-	187	138	-	-	-	-	-	-	-
Stage 1	307	335	-	481	497	-	-	-	-	-	-	-
Stage 2	623	453	-	516	362	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
	20.7			20.3			0.3			0.6		
HCM Control Delay, s HCM LOS	20.7 C			20.3 C			0.0			0.0		
I IOWI LOG	U			U								
Minor Lane/Major Mvmt		NBL	NBT	NBR I		VBLn1V		SBL	SBT	SBR		
Capacity (veh/h)		952	-	-	259	187	674	1082	-	-		
HCM Lane V/C Ratio		0.017	-	-		0.233		0.043	-	-		
HCM Control Delay (s)		8.8	-	-	20.7	30	10.7	8.5	-	-		
HCM Lane LOS		Α	-	-	С	D	В	Α	-	-		
HCM 95th %tile Q(veh)		0.1	-	-	0.4	0.9	0.2	0.1	-	-		

Intersection												
Int Delay, s/veh	10.7											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ኝ	<u></u>	7	ሻ	1	TTDIX.	ሻ	^	7	<u> </u>	^	7
Traffic Vol, veh/h	103	61	173	44	27	25	88	340	79	7	512	114
Future Vol, veh/h	103	61	173	44	27	25	88	340	79	7	512	114
Conflicting Peds, #/hr	6	0	0	0	0	6	0	0	3	3	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	_	Yield	-	_	None	_	-	None	-	-	None
Storage Length	100	-	230	0	_	-	160	_	175	160	-	125
Veh in Median Storage,	,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	3	-	-	-3	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	2	0	1	0	0	0	1	3	0	0	4	1
Mvmt Flow	112	66	188	48	29	27	96	370	86	8	557	124
Major/Minor N	/linor2		I	Minor1			Major1			Major2		
Conflicting Flow All	971	1224	279	893	1262	194	681	0	0	459	0	0
Stage 1	573	573		565	565	-	-	_	-	-	_	-
Stage 2	398	651	-	328	697	-	_	-	_	_	-	-
Critical Hdwy	7.54	6.5	6.92	7.5	6.5	6.9	4.12	-	-	4.1	-	-
Critical Hdwy Stg 1	6.54	5.5	-	6.5	5.5	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.5	-	6.5	5.5	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4	3.31	3.5	4	3.3	2.21	-	-	2.2	-	-
Pot Cap-1 Maneuver	207	181	721	239	171	821	914	-	-	1113	-	-
Stage 1	472	507	-	482	511	-	-	-	-	-	-	-
Stage 2	599	468	-	664	446	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	155	161	721	110	152	815	914	-	-	1110	-	-
Mov Cap-2 Maneuver	155	161	-	110	152	-	-	-	-	-	-	-
Stage 1	422	503	-	430	456	-	-	-	-	-	-	-
Stage 2	482	418	-	423	443	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	35.9			40.7			1.6			0.1		
HCM LOS	E			E			1.5			7. 1		
	_			_								
Minor Lane/Major Mvm	t	NBL	NBT	NBR	-Bl n1	FBI n2 I	=BI n3\/	VBLn1V	VBI n2	SBL	SBT	SBR
Capacity (veh/h)		914	-	-	155	161	721	110	250	1110		
HCM Lane V/C Ratio		0.105	_					0.435				_
HCM Control Delay (s)		9.4	_		72.8	42.2	11.7	60.8	23.6	8.3	_	_
HCM Lane LOS		9.4 A	_	_	72.0 F	42.2 E	В	60.6 F	23.0 C	Α	_	_
HCM 95th %tile Q(veh)		0.3	_	_	4.3	1.8	1	1.9	0.8	0	_	_
TOW JOHN JOHN Q(VEII)		0.0			7.0	1.0		1.5	0.0			

J. Turn Lane Warrant Tables and Charts

Left Turn Lane Warrant Assessment

Two-Lane Highways

Based on AASHTO / VDOT RDM Appendix F

Background:

Warrants for left-turn storage lanes on two-lane highways at unsignalized intersections are based on Figure 3-4 to Figure 3-21 in Appendix F of the Virginia Department of Transportation's (VDOT) *Road Design Manual* (RDM). The figures provide a graphical representation for determining the necessity of a left turn lane by comparing the advancing volumes of a given approach and the respective opposing volumes and are differentiated by design speed and percent left turning volume.

Project Information:

Project: Project ID: Warrenton Village

Intersection(s) and Movement(s):

6 - Oak Springs Drive at Hastings Lane / Future Access (WB) 7 - Oak Springs Drive at High School Driveway / Future Garage Access (WB)

Scenario: 2027 Future Conditions with Development

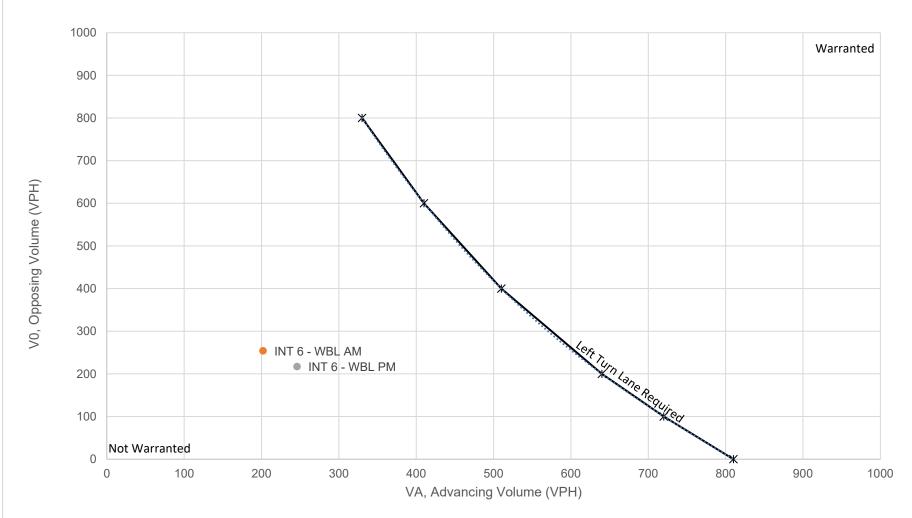
Analysis: Gorove Slade

Design Speed (mph): 40 (40, 50, or 60?)

Assessment Summary:

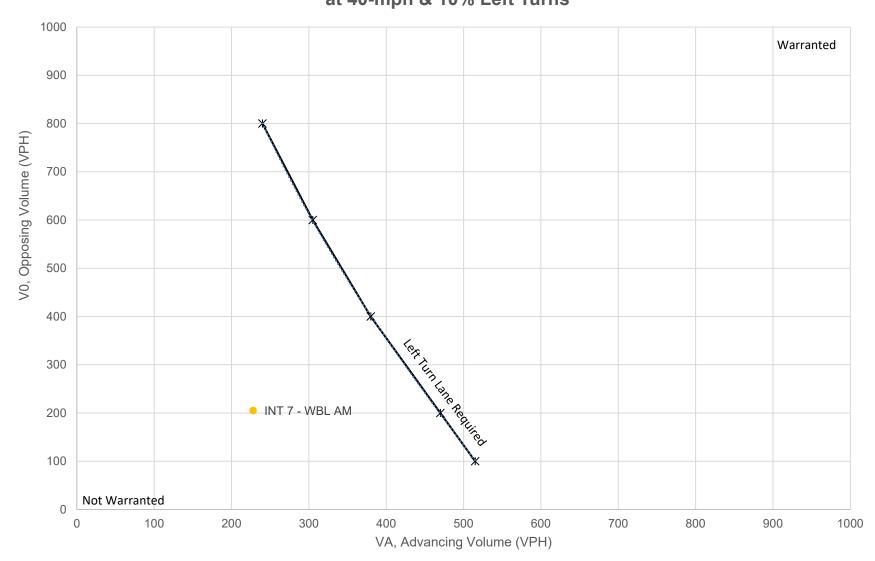
Ir	nput			VDOT Calculated Thesholds						
Study Scenario	Opposing Vol. (VPH)	Advancing Vol. (VPH)	Left Turn Vol. (VPH)	Left Turn %	Minimum Opposing Threshold (VPH)	VDOT RDM F Figure	Treatment			
INT 6 - WBL AM	254	202	2	0.99%	1,208	Fig. 3-4	Not Warranted			
INT 6 - WBL PM	217	246	6	2.44%	1,054	Fig. 3-4	Not Warranted			
INT 7 - WBL AM	205	228	19	8.33%	841	Fig. 3-5	Not Warranted			
INT 7 - WBL PM	194	281	62	22.06%	274	Fig. 3-8	Not Warranted			





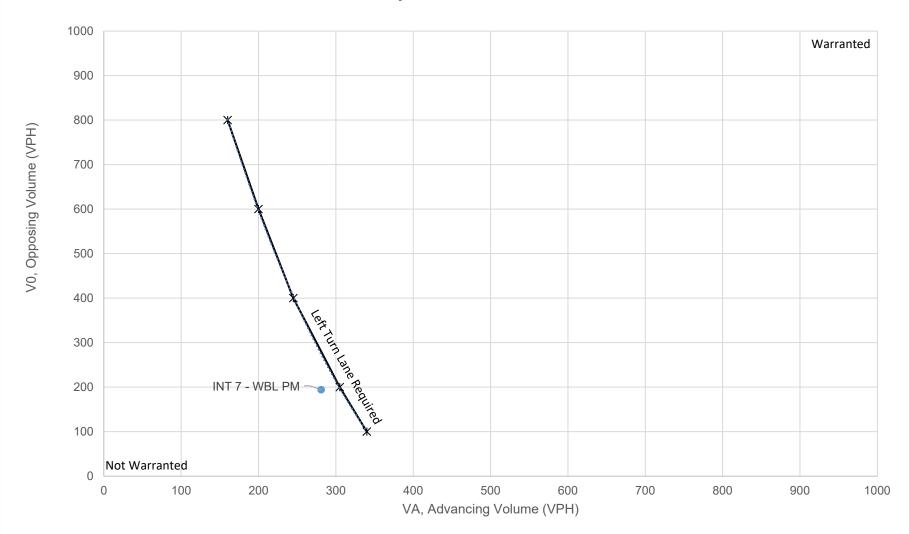
 $y = -2E-06x^3 + 0.0053x^2 - 5.5692x + 2132.8$ $R^2 = 1$





 $y = -6E-06x^3 + 0.0094x^2 - 6.8063x + 1981.6$ $R^2 = 1$

VDOT RDM-F Figure 3-8
Warrant for Left Turn Storage Lanes on 2-Lane Highways at 40-mph & 30% Left Turns



 $y = -8E-06x^3 + 0.0143x^2 - 9.4443x + 1979.9$ $R^2 = 0.9999$

Left Turn Lane Warrant Assessment

Four-Lane Highways

Background:

Warrants for left-turn storage lanes on four-lane highways at unsignalized intersections are based on Figure 3-3 in Appendix F of the Virginia Department of Transportation's (VDOT) *Road Design Manual* (RDM). The figure provides a graphical representation for determining the necessity of a left turn lane for divided and undivided roadway conditions by comparing the left turning volumes of a given approach and the respective opposing traffic volume.

Project Information:

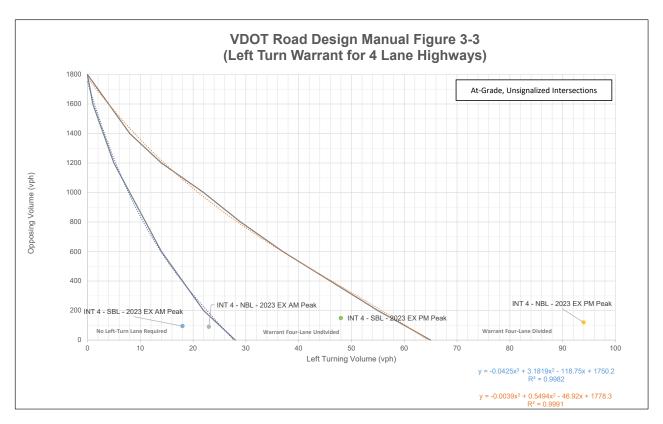
Project: Project ID:

Intersection(s) and Movement(s): 4 - Branch Drive at Warrenton Village Center Driveway / Safeway Driveway (NBL & SBL)

Scenario: 2023 Existing Conditions
Analysis: Gorove Slade

Assessment Summary:

Ir	nput			Result			
Study Scenario	Opposing Vol. (VPH)	Advancing Vol. (VPH)	Left Turning Vol. (VPH)	Left Turn %	Treatment		
INT 4 - NBL - 2023 EX AM Peak	90	95	23	24.2%	Not Warranted		
INT 4 - NBL - 2023 EX PM Peak	119	149	94	63.1%	Full-width Turn Lane and Taper Warranted (for Undivided and Divided)		
INT 4 - SBL - 2023 EX AM Peak	95	90	18	20.0%	Not Warranted		
INT 4 - SBL - 2023 EX PM Peak	149	119	48	40.3%	Full-width Turn Lane and Taper Warranted (for Undivided)		



Left Turn Lane Warrant Assessment

Four-Lane Highways

Background:

Warrants for left-turn storage lanes on four-lane highways at unsignalized intersections are based on Figure 3-3 in Appendix F of the Virginia Department of Transportation's (VDOT) *Road Design Manual* (RDM). The figure provides a graphical representation for determining the necessity of a left turn lane for divided and undivided roadway conditions by comparing the left turning volumes of a given approach and the respective opposing traffic volume.

Project Information:

Project: Warrenton Village Center

Project ID:

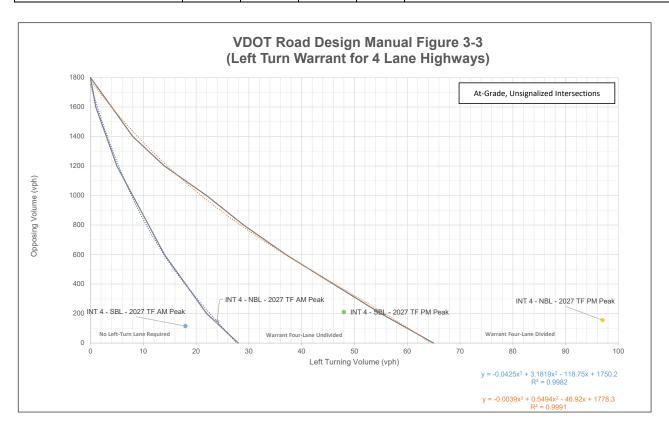
Intersection(s) and Movement(s): 4 - Branch Drive at Warrenton Village Center Driveway / Safeway Driveway (NBL & SBL)

Scenario: 2027 Future Conditions with Development

Analysis: Gorove Slade

Assessment Summary:

	Input			Result			
Study Scenario	Opposing Vol. (VPH)	Advancing Vol. (VPH)	Left Turning Vol. (VPH)	Left Turn %	Treatment		
INT 4 - NBL - 2027 TF AM Peak	145	115	24	20.9%	Not Warranted		
INT 4 - NBL - 2027 TF PM Peak	155	210	97	46.2%	Full-width Turn Lane and Taper Warranted (for Undivided and Divided)		
INT 4 - SBL - 2027 TF AM Peak	115	145	18	12.4%	Not Warranted		
INT 4 - SBL - 2027 TF PM Peak	210	155	48	31.0%	Full-width Turn Lane and Taper Warranted (for Undivided)		



Right Turn Lane Warrant Assessment

Two-Lane Highways

Based on NCHRP Report 279 / VDOT RDM Appendix F
"Intersection Channelization Guide"

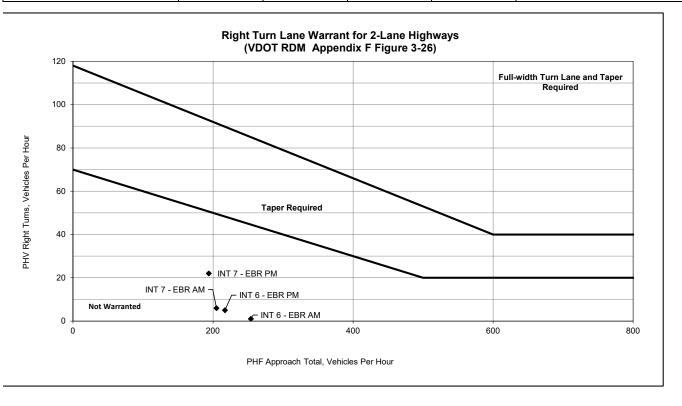
Background:

Warrants for right-turn storage lanes on two-lane highways at unsignalized intersections are based on Figure 3-26 in Appendix F of the Virginia Department of Transportation's (VDOT) *Road Design Manual* (RDM). This figure provides a graphical representation for determining the necessity of a right turn lane and / or taper by comparing the total volumes of a given approach with their respective right turn volumes.

Project Information:

Project:	Warrenton Village Center
Project ID:	
Intersection(s) and Movement(s):	6 - Oak Springs Drive at Hastings Lane / Future Access (EB)
	7 - Oak Springs Drive at High School Driveway / Future Garage Access (EB)
Scenario:	2027 Future Condtitions with Development
Analyst:	Gorove Slade

Study Scenario	Approach Volume	Right Turn Volume	Minimum Right Turn Taper Threshold	Minimum Right Turn Full Lane Threshold	Treatment
INT 6 - EBR AM	254	1	45	85	Not Warranted
INT 6 - EBR PM	217	5	48	90	Not Warranted
INT 7 - EBR AM	205	6	50	91	Not Warranted
INT 7 - EBR PM	194	22	51	93	Not Warranted



Right Turn Lane Warrant Assessment

Four-Lane Highways

Based on NCHRP Report 279 / VDOT RDM Appendix F
"Intersection Channelization Guide"

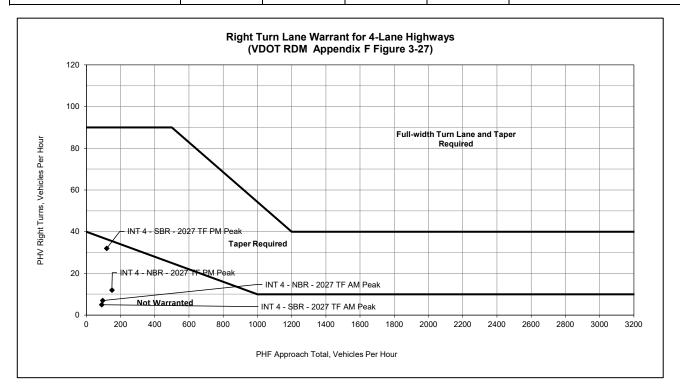
Background:

Warrants for right-turn storage lanes on four-lane highways at unsignalized intersections are based on Figure 3-27 in Appendix F of the Virginia Department of Transportation's (VDOT) *Road Design Manual* (RDM). This figure provides a graphical representation for determining the necessity of a right turn lane and / or taper by comparing the total volumes of a given approach with their respective right turn volumes.

Project Information:

Project:	
Project ID:	
Intersection(s) and Movement(s):	4 -Branch Drive at Warrenton Village Center Driveway / Safeway Driveway (NBR & SBR)
Scenario:	2027 Future Conditions with Development
Analyst:	Gorove Slade

Study Scenario	Approach Volume	Right Turn Volume	Minimum Right Turn Taper Threshold	Minimum Right Turn Full Lane Threshold	Treatment
INT 4 - NBR - 2027 TF AM Peak	95	7	37	90	Not Warranted
INT 4 - NBR - 2027 TF PM Peak	149	12	36	90	Not Warranted
INT 4 - SBR - 2027 TF AM Peak	90	5	37	90	Not Warranted
INT 4 - SBR - 2027 TF PM Peak	119	32	36	90	Not Warranted



K. MUTCD 4-Hour Warrant

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CHAPTER 4C. TRAFFIC CONTROL SIGNAL NEEDS STUDIES

Section 4C.01 Studies and Factors for Justifying Traffic Control Signals

Standard:

An engineering study of traffic conditions, pedestrian characteristics, and physical characteristics of the location shall be performed to determine whether installation of a traffic control signal is justified at a particular location.

The investigation of the need for a traffic control signal shall include an analysis of factors related to the existing operation and safety at the study location and the potential to improve these conditions, and the applicable factors contained in the following traffic signal warrants:

Warrant 1, Eight-Hour Vehicular Volume

Warrant 2, Four-Hour Vehicular Volume

Warrant 3. Peak Hour

Warrant 4, Pedestrian Volume

Warrant 5, School Crossing

Warrant 6, Coordinated Signal System

Warrant 7, Crash Experience

Warrant 8, Roadway Network

Warrant 9, Intersection Near a Grade Crossing

The satisfaction of a traffic signal warrant or warrants shall not in itself require the installation of a traffic control signal.

Support:

- Sections 8C.09 and 8C.10 contain information regarding the use of traffic control signals instead of gates and/ or flashing-light signals at highway-rail grade crossings and highway-light rail transit grade crossings, respectively. *Guidance:*
- A traffic control signal should not be installed unless one or more of the factors described in this Chapter are met.
- A traffic control signal should not be installed unless an engineering study indicates that installing a traffic control signal will improve the overall safety and/or operation of the intersection.
- A traffic control signal should not be installed if it will seriously disrupt progressive traffic flow.
- The study should consider the effects of the right-turn vehicles from the minor-street approaches.

 Engineering judgment should be used to determine what, if any, portion of the right-turn traffic is subtracted from the minor-street traffic count when evaluating the count against the signal warrants listed in Paragraph 2.
- Engineering judgment should also be used in applying various traffic signal warrants to cases where approaches consist of one lane plus one left-turn or right-turn lane. The site-specific traffic characteristics should dictate whether an approach is considered as one lane or two lanes. For example, for an approach with one lane for through and right-turning traffic plus a left-turn lane, if engineering judgment indicates that it should be considered a one-lane approach because the traffic using the left-turn lane is minor, the total traffic volume approaching the intersection should be applied against the signal warrants as a one-lane approach. The approach should be considered two lanes if approximately half of the traffic on the approach turns left and the left-turn lane is of sufficient length to accommodate all left-turn vehicles.
- Similar engineering judgment and rationale should be applied to a street approach with one through/left-turn lane plus a right-turn lane. In this case, the degree of conflict of minor-street right-turn traffic with traffic on the major street should be considered. Thus, right-turn traffic should not be included in the minor-street volume if the movement enters the major street with minimal conflict. The approach should be evaluated as a one-lane approach with only the traffic volume in the through/left-turn lane considered.
- At a location that is under development or construction and where it is not possible to obtain a traffic count that would represent future traffic conditions, hourly volumes should be estimated as part of an engineering study for comparison with traffic signal warrants. Except for locations where the engineering study uses the satisfaction of Warrant 8 to justify a signal, a traffic control signal installed under projected conditions should have an engineering study done within 1 year of putting the signal into stop-and-go operation to determine if the signal is justified. If not justified, the signal should be taken out of stop-and-go operation or removed.
- For signal warrant analysis, a location with a wide median, even if the median width is greater than 30 feet, should be considered as one intersection.

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Option:

At an intersection with a high volume of left-turn traffic from the major street, the signal warrant analysis may be performed in a manner that considers the higher of the major-street left-turn volumes as the "minor-street" volume and the corresponding single direction of opposing traffic on the major street as the "major-street" volume.

- For signal warrants requiring conditions to be present for a certain number of hours in order to be satisfied, any four sequential 15-minute periods may be considered as 1 hour if the separate 1-hour periods used in the warrant analysis do not overlap each other and both the major-street volume and the minor-street volume are for the same specific one-hour periods.
- For signal warrant analysis, bicyclists may be counted as either vehicles or pedestrians.

Support:

When performing a signal warrant analysis, bicyclists riding in the street with other vehicular traffic are usually counted as vehicles and bicyclists who are clearly using pedestrian facilities are usually counted as pedestrians.

Option:

- Engineering study data may include the following:
 - A. The number of vehicles entering the intersection in each hour from each approach during 12 hours of an average day. It is desirable that the hours selected contain the greatest percentage of the 24-hour traffic volume.
 - B. Vehicular volumes for each traffic movement from each approach, classified by vehicle type (heavy trucks, passenger cars and light trucks, public-transit vehicles, and, in some locations, bicycles), during each 15-minute period of the 2 hours in the morning and 2 hours in the afternoon during which total traffic entering the intersection is greatest.
 - C. Pedestrian volume counts on each crosswalk during the same periods as the vehicular counts in Item B and during hours of highest pedestrian volume. Where young, elderly, and/or persons with physical or visual disabilities need special consideration, the pedestrians and their crossing times may be classified by general observation.
 - D. Information about nearby facilities and activity centers that serve the young, elderly, and/or persons with disabilities, including requests from persons with disabilities for accessible crossing improvements at the location under study. These persons might not be adequately reflected in the pedestrian volume count if the absence of a signal restrains their mobility.
 - E. The posted or statutory speed limit or the 85th-percentile speed on the uncontrolled approaches to the location.
 - F. A condition diagram showing details of the physical layout, including such features as intersection geometrics, channelization, grades, sight-distance restrictions, transit stops and routes, parking conditions, pavement markings, roadway lighting, driveways, nearby railroad crossings, distance to nearest traffic control signals, utility poles and fixtures, and adjacent land use.
 - G. A collision diagram showing crash experience by type, location, direction of movement, severity, weather, time of day, date, and day of week for at least 1 year.
- The following data, which are desirable for a more precise understanding of the operation of the intersection, may be obtained during the periods described in Item B of Paragraph 17:
 - A. Vehicle-hours of stopped time delay determined separately for each approach.
 - B. The number and distribution of acceptable gaps in vehicular traffic on the major street for entrance from the minor street.
 - C. The posted or statutory speed limit or the 85th-percentile speed on controlled approaches at a point near to the intersection but unaffected by the control.
 - D. Pedestrian delay time for at least two 30-minute peak pedestrian delay periods of an average weekday or like periods of a Saturday or Sunday.
 - E. Queue length on stop-controlled approaches.

Section 4C.02 Warrant 1, Eight-Hour Vehicular Volume

Support:

- The Minimum Vehicular Volume, Condition A, is intended for application at locations where a large volume of intersecting traffic is the principal reason to consider installing a traffic control signal.
- The Interruption of Continuous Traffic, Condition B, is intended for application at locations where Condition A is not satisfied and where the traffic volume on a major street is so heavy that traffic on a minor intersecting street suffers excessive delay or conflict in entering or crossing the major street.
- It is intended that Warrant 1 be treated as a single warrant. If Condition A is satisfied, then Warrant 1 is satisfied and analyses of Condition B and the combination of Conditions A and B are not needed. Similarly, if Condition B is satisfied, then Warrant 1 is satisfied and an analysis of the combination of Conditions A and B is not needed.

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Standard:

The need for a traffic control signal shall be considered if an engineering study finds that one of the following conditions exist for each of any 8 hours of an average day:

- A. The vehicles per hour given in both of the 100 percent columns of Condition A in Table 4C-1 exist on the major-street and the higher-volume minor-street approaches, respectively, to the intersection; or
- B. The vehicles per hour given in both of the 100 percent columns of Condition B in Table 4C-1 exist on the major-street and the higher-volume minor-street approaches, respectively, to the intersection.

In applying each condition the major-street and minor-street volumes shall be for the same 8 hours. On the minor street, the higher volume shall not be required to be on the same approach during each of these 8 hours.

Option:

If the posted or statutory speed limit or the 85th-percentile speed on the major street exceeds 40 mph, or if the intersection lies within the built-up area of an isolated community having a population of less than 10,000, the traffic volumes in the 70 percent columns in Table 4C-1 may be used in place of the 100 percent columns. *Guidance:*

The combination of Conditions A and B is intended for application at locations where Condition A is not satisfied and Condition B is not satisfied and should be applied only after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems.

Standard:

- The need for a traffic control signal shall be considered if an engineering study finds that both of the following conditions exist for each of any 8 hours of an average day:
 - A. The vehicles per hour given in both of the 80 percent columns of Condition A in Table 4C-1 exist on the major-street and the higher-volume minor-street approaches, respectively, to the intersection; and
 - B. The vehicles per hour given in both of the 80 percent columns of Condition B in Table 4C-1 exist on the major-street and the higher-volume minor-street approaches, respectively, to the intersection.

These major-street and minor-street volumes shall be for the same 8 hours for each condition; however, the 8 hours satisfied in Condition A shall not be required to be the same 8 hours satisfied in Condition B. On the minor street, the higher volume shall not be required to be on the same approach during each of the 8 hours.

Table 4C-1. Warrant 1, Eight-Hour Vehicular Volume

Condition A—Minimum Vehicular Volume

Number of lar traffic on each			r on majo approach		Vehicles per hour on higher-volume minor-street approach (one direction only)				
Major Street	Minor Street	100% ^a 80% ^b 70% ^c 56% ^d				100%ª	80% ^b	70%°	56% ^d
1	1	500	400	350	280	150	120	105	84
2 or more	1	600	480	420	336	150	120	105	84
2 or more	2 or more	600	480	420	336	200	160	140	112
1	2 or more	500	400	350	280	200	160	140	112

Condition B—Interruption of Continuous Traffic

	nes for moving ch approach	Vehicle (tot	s per hou al of both	ır on majo approach	r street nes)	Vehicles per hour on higher-volume minor-street approach (one direction only)			
Major Street	Minor Street	100%ª	100%a 80%b 70%c 56%d				80% ^b	70%°	56% ^d
1	1	750	600	525	420	75	60	53	42
2 or more	1	900	720	630	504	75	60	53	42
2 or more	2 or more	900	720	630	504	100	80	70	56
1	2 or more	750	600	525	420	100	80	70	56

a Basic minimum hourly volume

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^b Used for combination of Conditions A and B after adequate trial of other remedial measures

^c May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000

^d May be used for combination of Conditions A and B after adequate trial of other remedial measures when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000

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Option:

If the posted or statutory speed limit or the 85th-percentile speed on the major street exceeds 40 mph, or if the intersection lies within the built-up area of an isolated community having a population of less than 10,000, the traffic volumes in the 56 percent columns in Table 4C-1 may be used in place of the 80 percent columns.

Section 4C.03 Warrant 2, Four-Hour Vehicular Volume

Support:

The Four-Hour Vehicular Volume signal warrant conditions are intended to be applied where the volume of intersecting traffic is the principal reason to consider installing a traffic control signal.

Standard:

The need for a traffic control signal shall be considered if an engineering study finds that, for each of any 4 hours of an average day, the plotted points representing the vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the higher-volume minor-street approach (one direction only) all fall above the applicable curve in Figure 4C-1 for the existing combination of approach lanes. On the minor street, the higher volume shall not be required to be on the same approach during each of these 4 hours.

Option:

If the posted or statutory speed limit or the 85th-percentile speed on the major street exceeds 40 mph, or if the intersection lies within the built-up area of an isolated community having a population of less than 10,000, Figure 4C-2 may be used in place of Figure 4C-1.

Section 4C.04 Warrant 3, Peak Hour

Support:

The Peak Hour signal warrant is intended for use at a location where traffic conditions are such that for a minimum of 1 hour of an average day, the minor-street traffic suffers undue delay when entering or crossing the major street.

Standard:

- This signal warrant shall be applied only in unusual cases, such as office complexes, manufacturing plants, industrial complexes, or high-occupancy vehicle facilities that attract or discharge large numbers of vehicles over a short time.
- The need for a traffic control signal shall be considered if an engineering study finds that the criteria in either of the following two categories are met:
 - A. If all three of the following conditions exist for the same 1 hour (any four consecutive 15-minute periods) of an average day:
 - 1. The total stopped time delay experienced by the traffic on one minor-street approach (one direction only) controlled by a STOP sign equals or exceeds: 4 vehicle-hours for a one-lane approach or 5 vehicle-hours for a two-lane approach; and
 - 2. The volume on the same minor-street approach (one direction only) equals or exceeds 100 vehicles per hour for one moving lane of traffic or 150 vehicles per hour for two moving lanes; and
 - 3. The total entering volume serviced during the hour equals or exceeds 650 vehicles per hour for intersections with three approaches or 800 vehicles per hour for intersections with four or more approaches.
 - B. The plotted point representing the vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the higher-volume minor-street approach (one direction only) for 1 hour (any four consecutive 15-minute periods) of an average day falls above the applicable curve in Figure 4C-3 for the existing combination of approach lanes.

Option:

- If the posted or statutory speed limit or the 85th-percentile speed on the major street exceeds 40 mph, or if the intersection lies within the built-up area of an isolated community having a population of less than 10,000, Figure 4C-4 may be used in place of Figure 4C-3 to evaluate the criteria in the second category of the Standard.
- If this warrant is the only warrant met and a traffic control signal is justified by an engineering study, the traffic control signal may be operated in the flashing mode during the hours that the volume criteria of this warrant are not met.

Guidance:

If this warrant is the only warrant met and a traffic control signal is justified by an engineering study, the traffic control signal should be traffic-actuated.

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500 2 OR MORE LANES & 2 OR MORE LANES 400 2 OR MORE LANES & 1 LANE MINOR 1 LANE & 1 LANE STREET 300 HIGHER-**VOLUME** 200 APPROACH -**VPH** 115* 100 80* 300 400 500 600 700 800 900 1000 1100 1200 1300 1400 MAJOR STREET—TOTAL OF BOTH APPROACHES— VEHICLES PER HOUR (VPH)

Figure 4C-1. Warrant 2, Four-Hour Vehicular Volume

*Note: 115 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 80 vph applies as the lower threshold volume for a minor-street approach with one lane.

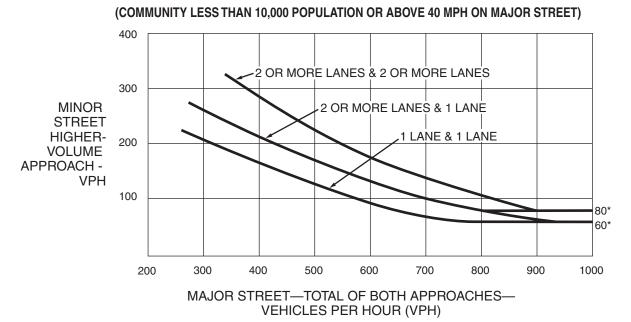


Figure 4C-2. Warrant 2, Four-Hour Vehicular Volume (70% Factor)

*Note: 80 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 60 vph applies as the lower threshold volume for a minor-street approach with one lane.

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