TRAFFIC IMPACT ANALYSIS

TULIP CREEK APARTMENT DEVELOPMENT LOCATED ALONG
NORTH EASON BOULEVARD, TUPELO, MS



PREPARED BY:

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1.0 INTRODUCTION

W. L. Burle Engineers, P.A. (BURLE) was retained by McCarty Architects, P.A. (McCARTY) in June of 2022 to conduct an engineering traffic analysis for a proposed development known as "Tulip Creek Apartments". The analysis was requested to determine any detrimental effects to North Eason Boulevard that could result from the generated traffic of this development. It should be noted that this development, according to the Tupelo Development Code (CODE), did not meet the minimum standards to require a traffic analysis due to the low amount of traffic projected to be generated. Section 12.5.3 of the CODE states:

"Unless exempted below, a traffic impact analysis (TIA) shall be required for zoning map changes utilizing a development plan, site plans, and preliminary plats that can be anticipated to generate at least 130 vehicle trips at the peak hour (as determined by Institute of Transportation Engineers Standards). Trips generated by separate developments meeting the criteria of Section 12.5.3, TIA Submission for Projects with Cumulative Impacts, shall be considered cumulatively" § 12.5.1.

As outlined later in this report, this particular development will produce far less than the 130 vehicle per hour threshold that is required as noted above. Instead, this analysis is being requested at the behest of the City of Tupelo Planning Commission. It is the goal of this report to resolve any concerns the Commission may have.

2.0 DEVELOPMENT DETAILS

The proposed site for the development is located along North Eason Boulevard approximately ¼ of a mile from the intersection with East Main Street. The current 14.5 acre site is undeveloped forest land that is bound by more undeveloped forest land to the north, two developed commercial sites to the east and west, and North Eason Boulevard to the south. The site is located in an existing mixed-use area in the north-eastern part of the city.

The proposed development will consist of 7 buildings, 6 of which will house 48 apartment units. Parking for the development will consist of 109 spaces that will be accessed via an access road that is approximately 500 feet in length. The access road will intersect with North Eason Boulevard at coordinates N34° 15' 42.92", W88° 39' 20.07". Site plan shown in Figure 2.1.



3.0 ANALYSIS DETAILS

As required by the CODE, this analysis utilized the latest editions of both the Trip Generation Manual (TGM) as published by the Institute of Transportation Engineers and the Highway Capacity Manual (HCM) as published by the Transportation Research Board. This analysis also utilizes information such as traffic counts, roadway dimensions, roadway geometry, travel speeds, and more that were determined from both in-field inspection and aerial imagery provided by Google Earth.

The purpose of this analysis was to establish the amount of future traffic that could be generated by this development and determine how this would affect the existing traffic conditions along North Eason Boulevard as well as determine the efficiency of both the proposed access road and its proposed intersection with North Eason Boulevard.

The future traffic generation for this development was determined using graphs/equations from the TGM. The TGM uses years of survey data to establish patterns of traffic use that is used to extrapolate traffic generation data for future developments based off of land use. This analysis relied on the ITETripGen web-based app (version 6.0.1) to come to its conclusions. The web-based app is based off of the most current edition (11th) of the TGM.

To determine effects on the existing traffic conditions, quantitative values for both existing and future conditions were determined for North Eason Boulevard. These quantitative values are known as the Levels of Service (LOS) and are determined using methodologies outlines in the HCM. Comparison of the two LOS values provides insight into how detrimental additional traffic could be to the existing traffic conditions.

The efficiency of the proposed access road was determined using LOS measures as outlined above for the existing traffic on North Eason Boulevard. The efficiency of the future intersection of the access road with North Eason Boulevard was determined using similar LOS analysis techniques but for intersections as outlined in the HCM. Since the proposed access road does not currently exist, analysis was performed only for the future traffic conditions. These future LOS estimates can be used to establish how effective the proposed traffic measures should be at moving traffic from one roadway to another.

Results were analyzed for both the A.M. and P.M. peak hours. These results are discussed in detail below. All calculations are provided with this report as Appendix A.

4.0 TRAFFIC COUNTS & GENERATION

4.1 EXISTING TRAFFIC

Existing traffic conditions were determined from an in-field traffic count. Results of the traffic count are provided in Figures 4.1 and 4.2 and discussed below. The traffic count was conducted on June 27, 2022 at a location approximately 500 feet north of the future intersection of North Eason Boulevard and the proposed access road.

The peak A.M. hour occurred from 7:00 to 8:00 with 496 vehicles per hour using the roadway. Traffic was split with approximately 35% of the traffic heading northbound and 65% of the traffic



heading southbound. It was also determined that approximately 16% of this traffic would be considered heavy truck traffic.

The peak P.M. hour occurred from 4:00 to 5:00 with 640 vehicles per hour using the roadway. Traffic was split with approximately 64% of the traffic heading northbound and 36% of the traffic heading southbound. It was also determined that approximately 7% of this traffic would be considered heavy truck traffic.

EXISTING	TRAFFIC	(A.M.)
N. EA	SON BLV	D.
PERIOD	N.B.	S.B.
6:00-6:15	37	63
6:15-6:30	37	83
6:30-6:45	49	88
6:45 - 7:00	46	80
TOTAL	169	314
7:00-7:15	37	63
7:15-7:30	55	114
7:30-7:45	39	27
7:45 - 8:00	41	120
TOTAL	172	324
8:00 - 8:15	32	80
8:15 – 8:30	39	70
8:30 - 8:45	47	55
8:45 – 9:00	49	59
TOTAL	167	264

Figure 4.1 -	- Existing Traffi	c Data for A.M.	(BURLE)

	` /
ASON BLV	D.
N.B.	S.B.
72	44
91	60
93	64
71	83
327	251
114	54
79	53
100	43
116	81
409	231
130	45
107	64
88	59
64	31
389	199
	72 91 93 71 327 114 79 100 116 409 130 107 88 64

Figure 4.2 – Existing Traffic Data for P.M. (BURLE)

4.2 FUTURE TRAFFIC GENERATION

Trip end generations were determined using the TGM section for Multifamily Housing (Low-Rise), Weekday, Peak Hour of Adjacent Street Traffic. During the peak A.M. hour, it was determined that an additional 38 vehicles per hour could be generated with 24% of those entering and 76% exiting the development. During the peak P.M. hour, it was determined that an additional 41 vehicles per hour could be generated with 63% entering and 37% exiting the development.

Other traffic measures for the future traffic, such as north/south directional split, were determined from the existing traffic patterns. Since this development is residential in use, it was determined that 0% of the future traffic generated could be considered heavy truck traffic.

5.0 ROADWAY GEOMETRY

5.1 NORTH EASON BOULEVARD

North Eason Boulevard is a local roadway owned and maintained by the City of Tupelo. It is



located in the southeastern portion of the city and connects Interstate I22 with East Main Street. It runs in a north-south fashion for approximately 2 miles and has roughly 13 access points per mile. It has one travel lane for each travel direction that is 12 feet in width. Most of the roadway has a shoulder that is approximately 6 feet in width. It has a level terrain with 100% no passing in the area where the development will be located. For purposes of this analysis, the roadway was considered to be a Two-Way Two-Lane Class II Highway as defined by the HCM.

5.2 PROPOSED ACCESS ROAD

The proposed access road, as shown in figure 2.1 above, will connect North Eason Boulevard with the parking area for the proposed development in an east/west fashion. It will be approximately 500 feet in length and will have 10 feet wide travel lanes, one for each direction. There will be no shoulder nor access points located along the roadway. The roadway will also not allow traffic to pass due to its short length. For purposes of this analysis, the roadway was considered to be a Two-Way Two-Lane Class II Highway as defined by the HCM.

5.3 PROPOSED INTERSECTION OF NORTH EASON BOULEVARD & THE ACCESS ROAD

The future intersection of North Eason Boulevard and the proposed access road will be stop controlled with one stop sign being placed so as to stop eastbound traffic prior to entering North Eason Boulevard. Traffic along North Eason Boulevard will not be required to stop or yield to traffic entering the roadway. Due to the low volume of expected traffic generation, no dedicated right or left turn lanes will be considered on either roadway. A concrete island will be used to separate traffic entering and existing the access road. See figure 2.1 above.

6.0 ROADWAY LEVEL-OF-SERVICE RESULTS

All roadways in this analysis were considered to be Two-Way Two-Lane Class II Highways and were evaluated as such. To determine the LOS for these types of roadways, an estimation of the percent time a vehicle can be expected to follow another vehicle was determined. This value is referred to as the Percent Time Spent Following (PTSF). The PTSF value is dependent upon the Passenger-Car Equivalent Flow Rate (Vp), the Base Percent Time Spent Following (BPTSF), and the percent of no passing zones. The Vp is determined using roadway geometry and traffic data about heavy and recreational vehicle use of the roadway. The BPTSF is determined using the Vp value. All terms are as defined by the HCM. Results for each are discussed below.

6.1 NORTH EASON BOULEVARD

6.1.1 PRE-CONSTRUCTION FOR A.M. PEAK HOUR

For the pre-construction A.M. peak hour period along North Eason Boulevard, it was determined that there were 496 vehicles per hour using the roadway with 16% of these being heavy trucks and 0% being recreational vehicles. From this data, it was determined that the roadway has a Vp of 752 vehicles per hour which results in a BPTSF of 48.4%. The PTSF was then calculated to be 73.0% which gives the roadway an existing LOS rating of "D".



6.1.2 PRE-CONSTRUCTION FOR P.M. PEAK HOUR

For the pre-construction P.M. peak hour period along North Eason Boulevard, it was determined that there were 640 vehicles per hour using the roadway with 7% of these being heavy trucks and 0% being recreational vehicles. From this data, it was determined that the roadway has a Vp of 827 vehicles per hour which results in a BPTSF of 51.6%. The PTSF was then calculated to be 76.2% which gives the roadway an existing LOS rating of "D".

6.1.3 POST-CONSTRUCTION FOR A.M. PEAK HOUR

For the post-construction A.M. peak hour period along North Eason Boulevard, it was determined that there would be an estimated 534 vehicles per hour using the roadway with 16% of these being heavy trucks and 0% being recreational vehicles. From this data, it was determined that the roadway would have an estimated Vp of 797 vehicles per hour which results in a BPTSF of 50.4%. The PTSF was then estimated to be 75.0% (a 2% increase) which will maintain the roadways existing LOS rating of "D".

6.1.4 POST-CONSTRUCTION FOR P.M. PEAK HOUR

For the post-construction P.M. peak hour period along North Eason Boulevard, it was determined that there would be an estimated 681 vehicles per hour using the roadway with 7% of these being heavy trucks and 0% being recreational vehicles. From this data, it was determined that the roadway would have an estimated Vp of 876 vehicles per hour which results in a BPTSF of 53.7%. The PTSF was then estimated to be 78.3% (a 2.1% increase) which will maintain the roadways existing LOS rating of "D".

6.2 PROPOSED ACCESS ROAD

6.2.1 POST-CONSTRUCTION FOR A.M. PEAK HOUR

For the post-construction A.M. peak hour period along the proposed access road, it was determined that there would be an estimated 38 vehicles per hour using the roadway with 0% of these being heavy trucks and 0% being recreational vehicles. From this data, it was determined that the roadway would have an estimated Vp of 47 vehicles per hour which results in a BPTSF of 4.0%. The PTSF was then estimated to be 28.6% which gives the roadway an estimated LOS rating of "A".

6.2.2 POST-CONSTRUCTION FOR P.M. PEAK HOUR

For the post-construction P.M. peak hour period along the proposed access road, it was determined that there would be an estimated 41 vehicles per hour using the roadway with 0% of these being heavy trucks and 0% being recreational vehicles. From this data, it was determined that the roadway would have an estimated Vp of 50 vehicles per hour which results in a BPTSF of 4.3%. The PTSF was then estimated to be 28.9% which gives the roadway an estimated LOS rating of "A".



7.0 INTERSECTION LEVEL-OF-SERVICE RESULTS

The intersection of interest for this analysis is considered a Two-Way Stop-Controlled Intersection as defined by the HCM. LOS for this type of intersection is determined from the Control Delay (CD) value, which is the time of delay in seconds that results from the intersection controls. There are several different factors that go into determining the CD value and deals largely with the traffic volume and the intersection's geometry. For this type of intersection, there are three conflicting traffic movements that control the CD value. See figure 7.1 below for movement definitions.

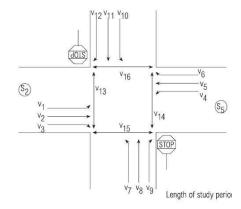


Figure 7.1 – Movement Definitions (HCM)

The three conflicting movements are the major left turn (1), minor right turn (12), and the minor left turn (10). There are two important values to calculate for each of these conflicting movements: the Critical Gap Time (Tc) and the Follow Up Time (Tf). From these values and using conflicting traffic impedance values as defined in the HCM, the Movement Capacity (Cm) and the Shared Lane Capacity (Csh) can be calculated. Using these values, the CD can then be calculated and the LOS value determined. All terms are defined in the HCM. Results are discussed below.

7.1 NORTH EASON BOULEVARD AND PROPOSED ACCESS ROAD

7.1.1 POST-CONSTRUCTION FOR A.M. PEAK HOUR

For post-construction A.M. peak hour period for the proposed intersection of North Eason Boulevard and the access road, the following values were estimated for movements 1, 12, and 10 respectively:

- Tc: 4.1, 6.2, and 6.4 seconds
- Tf: 2.2, 3.3, and 3.5 seconds
- Cm: 1,358, 824, and 642 vehicles per hour

From these values, the Csh was calculated to be 979 vehicles per hour with a 9 second control delay. This will give the intersection an estimated LOS value of "A".

7.1.2 POST-CONSTRUCTION FOR P.M. PEAK HOUR

For post-construction P.M. peak hour period for the proposed intersection of North Eason



Boulevard and the access road, the following values were estimated for movements 1, 12, and 10 respectively:

- Tc: 4.1, 6.2, and 6.4 seconds
- Tf: 2.2, 3.3, and 3.5 seconds
- Cm: 1,418, 881, and 489 vehicles per hour

From these values, the Csh was determined to be 641 vehicles per hour with an 11 second control delay. This will give the intersection an estimated LOS value of "B".

8.0 CONCLUSION

It is the consensus of this report that, based on the results of the traffic analysis, the Tulip Creek Apartment Development will have a minimal effect on the existing traffic conditions for North Eason Boulevard. As well, it is the consensus of this report that the current design of the proposed access road will efficiently convey traffic into and out of the development. Similarly, the current design of the proposed intersection of the access road with North Eason Boulevard should efficiently direct traffic from one roadway to another with minimal interruption.

It is also worth noting that current traffic patterns, heavy vehicle use, and existing geometry are all contributing factors to the poor LOS of North Eason Boulevard. The addition of this development will NOT cause any significant changes to the current condition of this roadway and will NOT affect health and safety of drivers in any meaningful way.



APPENDIX "A" TRAFFIC ANALYSIS CALCULATIONS

Calculations By: SWS
Traffic Count Location: 34° 15' 46.8" N
88° 39' 14.9" W Project Name: Tulip Creek Traffic Analysis
Project Number: 04717-1-0122
Date: 6/27/2022 WB Street: EB Street: ACCESS RD
EXISTING TRAFFIC COUNT NB Sreet: N EASON BLVD
SB Street: N EASON BLVD N/A ACCESS RD NORTH ESTIMATED FUTURE TRAFFIC COUNT (SB) 324 N EASON BLVD N EASON BLVD N EASON BLVD N EASON BLVD (NB) (NB) N/A N/A PEAK 8:30 AM - 8:45 AM 8:45 AM - 8:00 AM TOTALS 7:00 AM - 7:15 AM 7:15 AM - 7:30 AM 7:30 AM - 7:45 AM 7:45 AM - 8:00 AM 6:00 AM - 6:15 AM 6:15 AM - 6:30 AM 6:30 AM - 6:45 AM 7:15 AM - 7:30 AM 8:00 AM - 8:15 AM 8:15 AM - 8:30 AM 6:45 AM - 7:00 AM 7:00 AM - 7:15 AM 7:30 AM - 7:45 AM 7:45 AM - 8:00 AM Peak Time Frame Time Frame DIRECTIONAL SPLIT (A.M.): %WB Right Turn: N/A %NB Right Turn: 0% PERIOD TOTALS

N EASON BLVD TOTALS TOTALS PHF_{lane}: N EASON BLVD 0.78 PHF_{N/S}: <u>0.74</u> PHF_{N/S}: 0.73 0.78 35% %NB Left Turn: <u>0%</u> %WB Left Turn: <u>N/A</u> 0.00 65% FUTURE TRAFFIC GENERATION (A.M. PERIOD) 0.00 **EXISTING TRAFFIC COUNT (A.M. PERIOD)** N EASON BLVD (SB) 0.68 N EASON BLVD DIRECTIONAL SPLIT (A.M.): %SB Right Turn: <u>0%</u> %EB Right Turn: <u>N/A</u> 0.68 120 ACCESS RD 0.00 N/A PHF_{E/W}: N/A PHF_{E/W}: <u>0.73</u> Thru 0.00 0% ACCESS RD (WB) 0.00 N/A (WB) 0% %SB Left Turn: <u>0%</u> %EB Left Turn: <u>N/A</u> 1.00 0.00 ACCESS RD (EB) 1.00

TOTAL PERCENT RECREATIONAL (NORTH-SOUTH): 0%
TOTAL PERCENT RECREATIONAL (EAST-WEST): 0%

TOTAL PERCENT HEAVY (NORTH-SOUTH): 16% TOTAL TOTAL PERCENT HEAVY (EAST-WEST): 0% TO

ACCESS RD
NORTH
(SB)
19
0
(NB)
N/A

TRIP ENTER= $\frac{24\%}{2}$ What percentage of traffic will use this intersection? $\frac{100\%}{29}$ ENTER SB (VEH/HR)= $\frac{65\%}{6}$ EXIT SB (VEH/HR)= $\frac{65\%}{19}$ EXIT NB (VEH/HR)= $\frac{35\%}{19}$ EXIT NB (VEH/HR)= $\frac{35\%}{19}$

NO. OF UNTIS= $\underline{48}$ TRIP ENDS= $\underline{38}$

ST. LOCATION IN INTERSECTION (SINGLE LEG): WEST
TRIP GENERATION MANUAL, 10th ED.
SOURCE INFO: MULTIFAMILY HOUSING (LOW RISE)
WEEKDAY A.M. PEAK HOUR

TRIP END GENERATION CALCULATIONS (A.M. PERIOD)
STREET: NORTH ENTRANCE

Calculations By: SWS
Traffic Count Location: 34° 15' 46.8" N
88° 39' 14.9" W Project Name: Tulip Creek Traffic Analysis
Project Number: 04717-1-0122
Date: 6/27/2022 WB Street: NB Street: ACCESS RD
EXISTING TRAFFIC COUNT NB Sreet: N EASON BLVD
SB Street: N EASON BLVD N/A ACCESS RD NORTH ESTIMATED FUTURE TRAFFIC COUNT (SB) 231 N EASON BLVD N EASON BLVD N EASON BLVD N EASON BLVD (NB) (NB) N/A N/A PEAK 5:30 PM - 5:45 PM 5:45 PM - 6:00 PM TOTALS 4:15 PM - 4:30 PM 4:30 PM - 4:45 PM 4:45 PM - 5:00 PM 3:00 PM - 3:15 PM 3:15 PM - 3:30 PM 3:30 PM - 3:45 PM 4:15 PM - 4:30 PM 4:00 PM - 4:15 PM 5:15 PM - 5:30 PM 3:45 PM - 4:00 PM 4:45 PM - 5:00 PM 4:30 PM - 4:45 PM 5:00 PM - 5:15 PM 4:00 PM - 4:15 PM Peak Time Frame Time Frame %NB Right Turn: <u>0%</u> %WB Right Turn: <u>N/A</u> DIRECTIONAL SPLIT (P.M.): PERIOD TOTALS 0
N EASON BLVD TOTALS TOTALS PHF_{lane}: N EASON BLVD 0.88 PHF_{N/S}: 0.82 PHF_{N/S}: 0.81 0.88 64% %NB Left Turn: <u>0%</u> %WB Left Turn: <u>N/A</u> 0.00 36% 426 FUTURE TRAFFIC GENERATION (P.M. PERIOD) 0.00 **EXISTING TRAFFIC COUNT (P.M. PERIOD)** N EASON BLVD (SB) N EASON BLVD 0.71 DIRECTIONAL SPLIT (P.M.): %SB Right Turn: <u>0%</u> %EB Right Turn: <u>N/A</u> 0.71 ACCESS RD 0.00 N/A PHF_{E/W}: N/A PHF_{E/w}: <u>0.81</u> Thru 0.00 0% ACCESS RD (WB) 0.00 N/A (WB) 0% %SB Left Turn: <u>0%</u> %EB Left Turn: <u>N/A</u> 1.00 0.00 ACCESS RD (EB) 1.00

% HEAVY VEHICLES

% REC. VEHICLES TOTAL PERCENT HEAVY (NORTH-SOUTH): 7% TOTAL PERCENT HEAVY (EAST-WEST): 0% TOTAL PERCENT RECREATIONAL (NORTH-SOUTH): 0% TOTAL PERCENT RECREATIONAL (EAST-WEST): 0% 0%

0%

000000000000000000000000000000000000000	00000000000				#1 0 41 76 76 204 0 204 HEAVY VEHICLES 9 0 9 11 0 11 2 0 27 RECREATIONAL VEHICLES 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	94.0 0 2 HEAVY VEHICLES 9 0 0 11 0 0 227 0 0 5 0 0 6 0 0 7 REATIONAL VEHIC	441 7/6 20/4 HE 9 9 9 11 11 12 2 2 3 5 5 7 RECRE 0 0 0 0		394 394 1 1 1 1 1 0 0 0	000000000000000000000000000000000000000	110 394 2 2 2 1 1 1 1 0 0 0	000000000000000000000000000000000000000	4:30 PM - 4:15 PM 4:45 PM - 5:00 PM 4:45 PM - 4:15 PM 4:15 PM - 4:30 PM 4:30 PM - 4:45 PM 4:45 PM - 5:00 PM 70TALS 4:00 PM - 4:15 PM 4:15 PM - 5:00 PM 4:45 PM - 5:00 PM 4:45 PM - 5:00 PM	
0	0	0 0	0	0	42	0 0	42	0	78	0	78	0	4:15 PM - 4:30 PM	
0	0	0	0	0	45	0	45	0	112	0	112	0	4:00 PM - 4:15 PM	
					PASSENGER VEHICLES	FNGER V	PASS							_

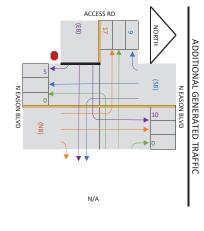
Peak Time Frame

HEAVY / RECREATIONAL VEHICLE CALCULATIONS

N EASON BLVD (SB)

ACCESS RD (WB)

ACCESS RD (EB)



What percentage of traffic will use this intersection? $\underline{100\%}$ TRIP ENTER= $\frac{63\%}{26}$ ENTER SB (VEH/HR)= $\frac{36\%}{9}$ EXIT SB (VEH/HR)= $\frac{36\%}{5}$ RIGHT TURN ENTER NB (VEH/HR)= $\frac{64\%}{17}$ EXIT NB (VEH/HR)= $\frac{64\%}{10}$ TRIP EXIT= $\frac{37\%}{15}$ LEFT TURN

NO. OF UNTIS= 48 TRIP ENDS= 41

ST. LOCATION IN INTERSECTION (SINGLE LEG): WEST TRIP GENERATION MANUAL, 10th ED.

SOURCE INFO: MULTIFAMILY HOUSING (LOW RISE)

WEEKDAY A.M. PEAK HOUR

STREET: NORTH ENTRANCE TRIP END GENERATION CALCULATIONS (P.M. PERIOD)

Project Number: <u>04717-1-0122</u>

Date: <u>6/27/2022</u>

Calculations By: <u>SWS</u>

Street of Interest: N EASON BLVD

Development Location: 34° 15' 72.92" N

88° 39' 20.07" W

GENERAL STREET INFORMATION

		$V_{\text{directional}}$ (veh/hr)= $\frac{172}{}$	V (veh/hr)= 496	Which direcd:
*Determined from Aerial Imagery	Access (Point/Mile)= $\frac{13}{}$	Terrain: <u>Level</u>	BFFS (mph)= <u>50</u>	Which direcdtion does the street run? NORTH-SOUTH
			*POSTED LIMIT	HTUOS
	Class: <u>II</u>	W_{sholder} (ft)= $\underline{6}$	PHF= <u>0.73</u>	
		W _{lane} (ft)=		
	Split:	t)= <u>12</u>	P _t (%)= 16%	This calculator uses I
	ω		16%	tor uses HCM 2
	35%	No Pass (%)= 100%	P _r (HCM 2000 Chapter
	65%	%)= 100%	P _r (%)= <u>0%</u>	20

TRAVEL SPEED CALCULATIONS

TRA	WEL SPEED	TRAVEL SPEED CALCULATIONS		PERCENT TIME FOLLO	PERCENT TIME FOLLOWING CALCULATIONS	
f _g = <u>1</u>	EXH. 20-7	$E_t = 1.7$	EXH. 20-9	$f_g = 1$ EXH. 20-8	-8 E _t = <u>1.1</u>	EXH. 20-10
$f_{hv} = 0.90$		E,= <u>1</u>	EXH. 20-9	$f_{hv} = 0.90$	E _r = <u>1</u>	EXH. 20-10
EQ: 1/[1+P _t	EQ: $1/[1+P_t(E_t-1)+P_r(E_r-1)]$)]		EQ: $1/[1+P_t(E_t-1)+P_r(E_r-1)]$	E _r -1)]	
V _p (veh/hr)= <u>752</u>	<u>752</u>	EQ: $v/[PHF*f_g*f_{hv}]$	<1,700 veh/hr	V_p (veh/hr)= 752	EQ: v/[PHF*fg*fhv]	
$V_{p-directional}$ (veh/hr)= 491	491	EQ: v _p *{MAX SPLIT}	<3,200 veh/hr	$V_{p-directional}$ (veh/hr)= 491	EQ: v _p *{MAX SPLIT}	
f_{ls} (mph)= 1.3	EXH. 20-5	f _{np} (mph)= <u>4</u>	EXH. 20-11	BPTSF (%)= <u>48.4</u>	EQ: 100(1-exp(-0.000879*v _p))	*v _p))
$f_A (mph) = \frac{7.5}{}$	EXH. 20-6	ATS (mph)= 31		$f_{d/np}$ (%)= 24.6	EXH. 20-12 *Interpo	*Interpolated Value
FFS (mph)= 41	EQ: BFFS-f _{Is} -f _A		EQ: FFS-0.00776*v _p -f _{np}	PTSF (%)= <u>73.0</u>	EQ: BPTSF+f _{d/np}	

	ľ	
PRE-CONSTRUCTION (A.M.) L.O.S. OF	D	WAS DETERMINED

					1INED	
*IISE EXH 20-3 FOR LOS CLASS I	ш	D	С	В	Α	LOS (CLASS II) PTSF
FOR LOS CLASS I	>85	>70-85	>55-70	>40-55	<=40	PTSF EXH. 20-4

Project Number: <u>04717-1-0122</u>

Calculations By: <u>SWS</u> Date: <u>6/27/2022</u>

Street of Interest: N EASON BLVD

Development Location: 34° 15' 72.92" N

88° 39' 20.07" W

GENERAL STREET INFORMATION

		$V_{\text{directional}}$ (veh/hr)= 409	V (veh/hr)= <u>640</u>	Which direcd:
*Determined from Aerial Imagery	Access (Point/Mile)= 13	Terrain: <u>Level</u>	BFFS (mph)= <u>50</u>	Which direcdtion does the street run? NORTH-SOUTH
	Class: <u>II</u>	W_{sholder} (ft)= <u>6</u>	*POSTED LIMIT PHF= 0.81	HTUC
		8		
	Split:	/ _{lane} (ft)= 12	P _t (%)	This calcul
	rt: <u>64%</u>		$o_{t}(\%) = \frac{7\%}{1}$	This calculator uses HCM 20
	_	No Pass (%)= 100%	P _r (%)= <u>0%</u>)00 Chapter 20
	36%	00%	%	

TRAVEL SPEED CALCULATIONS

TR	AVEL SPEED	TRAVEL SPEED CALCULATIONS		PERCENT TIME FC	PERCENT TIME FOLLOWING CALCULATIONS	
$f_g = 1$	EXH. 20-7	$E_t = 1.7$	EXH. 20-9	$f_g = 1$ EXH	EXH. 20-8 $E_t = \frac{1.1}{1.1}$	EXH. 20-10
$f_{hv} = 0.95$		E ₇ = <u>1</u>	EXH. 20-9	$f_{hv} = 0.95$	E _r = <u>1</u>	EXH. 20-10
EQ: 1/[1+P	EQ: $1/[1+P_t(E_t-1)+P_r(E_r-1)]$	[)]		EQ: $1/[1+P_t(E_{t}-1)+P_r(E_{r}-1)]$	$+P_r(E_r-1)$	
V _p (veh/hr)= <u>827</u>	= 827	EQ: $v/[PHF*f_g*f_{hv}]$	<1,700 veh/hr	$V_{p} (veh/hr) = 827$	EQ: v/[PHF*fg*fhv]	
$V_{p ext{-directional}}$ (veh/hr)= 528	= <u>528</u>	EQ: v _p *{MAX SPLIT}	<3,200 veh/hr	$V_{p-directional}$ (veh/hr)= 528	EQ: v _p *{MAX SPLIT}	
f _{Is} (mph)= <u>1.3</u>	EXH. 20-5	f_{np} (mph)= 4	EXH. 20-11	BPTSF (%)= <u>51.6</u>	5 EQ: 100(1-exp(-0.000879*ν _p))	v _p))
$f_A (mph) = 7.5$	EXH. 20-6	ATS (mph)= <u>31</u>		$f_{d/np}$ (%)= 24.6	EXH. 20-12	*Interpolated Value
FFS (mph)= <u>41</u>	EQ: BFFS-f _{Is} -f _A		EQ: FFS-0.00776*v _p -f _{np}	PTSF (%)= <u>76.2</u>	EQ: BPTSF+f _{d/np}	

LOS CALCULATIONS

D C

>70-85 >55-70 >40-55 <=40 LOS (CLASS II) PTSF

EXH. 20-4

*USE EXH. 20-3 FOR LOS CLASS I

Project Number: <u>04717-1-0122</u>

Calculations By: <u>SWS</u> Date: <u>6/27/2022</u>

Street of Interest: N EASON BLVD

Development Location: 34° 15' 72.92" N

88° 39' 20.07" W

GENERAL STREET INFORMATION

		$V_{\text{directional}}$ (veh/hr)= $\frac{185}{1}$	V (veh/hr)= <u>534</u>	Which direcd
*Determined from Aerial Imagery	Access (Point/Mile)= 13	Terrain: <u>Level</u>	BFFS (mph)= <u>50</u>	Which direcdtion does the street run? NORTH-SOUTH
	Class: <u>II</u>	W_{sholder} (ft)= $\underline{6}$	*POSTED LIMIT PHF= 0.74	HTUC
	Split:	W _{iane} (ft)= 12	P_{t} (%)= 16%	This calculator uses HCI
	35% \ 65%	No Pass (%)= 100%	P _r (%)= <u>0%</u>	M 2000 Chapter 20

TRAVEL SPEE	TRAVEL SPEED CALCULATIONS		PERCENT TIME FOLLOWING CALCULATIONS	WING CALCULATIONS	
$f_g = 1$ EXH. 20-7	7 $E_{t} = \frac{1.7}{1.7}$	EXH. 20-9	$f_g = 1$ EXH. 20-8	8 $E_{t} = \frac{1.1}{1.1}$	EXH. 20-10
f _{hv} = <u>0.90</u>	E _r = <u>1</u>	EXH. 20-9	$f_{hv} = 0.90$	E _r = <u>1</u>	EXH. 20-10
EQ: $1/[1+P_t(E_{t}-1)+P_r(E_{r}-1)]$	_{[r} -1)]		EQ: $1/[1+P_t(E_t-1)+P_r(E_r-1)]$	(-1)]	
$V_{p} (veh/hr) = 797$	EQ: $v/[PHF*f_g*f_{hv}]$	<1,700 veh/hr	V_p (veh/hr)= $\overline{797}$	EQ: $v/[PHF*f_g*f_{hv}]$	
$V_{p-directional}$ (veh/hr)= 521	EQ: v _p *{MAX SPLIT}	<3,200 veh/hr	$V_{p-directional}$ (veh/hr)= 521	EQ: v _p *{MAX SPLIT}	

BPTSF (%)= $\frac{50.4}{f_{d/np}}$ (%)= $\frac{24.6}{75.0}$	50.4 24.6 75.0
---	----------------------

LOS CALCULATIONS	LOS (CLASS II) PTSF	PTSF
POST-CONSTRUCTION (A.M.) L.O.S. OF D WAS DETERMINED	Α	<=40
	В	>40-55
	С	>55-70
	D	>70-85
	ш	>85
	*IISE EXH 20-3 EOR LOS CLASS I	OR LOS CLA

Project Number: <u>04717-1-0122</u>

Calculations By: <u>SWS</u> Date: <u>6/27/2022</u>

Street of Interest: N EASON BLVD

Development Location: 34° 15' 72.92" N

88° 39' 20.07" W

GENERAL STREET INFORMATION

		$V_{\text{directional}}$ (veh/hr)= 435	V (veh/hr)= <u>681</u>	Which direcd
*Determined from Aerial Imagery	Access (Point/Mile)= 13	Terrain: <u>Level</u>	BFFS (mph)= <u>50</u>	Which direcdtion does the street run? NORTH-SOUTH
			*POST	H-SOUTH
	Class: <u>I</u>	$W_{sholder}$ (ft)= <u>6</u>	*POSTED LIMIT PHF= 0.82	
	!—	10,).82	
		W _{lane} (ft)= 12		
	Split:	12	P_{t} (%)= $\frac{7\%}{1}$	This calculator uses HCM 2000 Chapter 20
	<u>64%</u>		<u> %</u>	r uses HCM 2
	/ %	No Pass (P _r (000 Chapte
	36%	No Pass (%)= 100%	P _r (%)= <u>0%</u>	r 20

TRAVEL SPEED CALCULATIONS

TR.	NEL SPEED	TRAVEL SPEED CALCULATIONS		PERCENT TIME FOLLOWING CALCULATIONS	VING CALCULATIONS	
$f_g = 1$	EXH. 20-7	$E_t = \frac{1.7}{1.7}$	EXH. 20-9	$f_g = 1$ EXH. 20-8	E _t = 1.1	EXH. 20-10
f _{hv} = <u>0.95</u>		E,= <u>1</u>	EXH. 20-9	$f_{hv} = 0.95$	E _r = <u>1</u>	EXH. 20-10
EQ: 1/[1+P ₁	EQ: $1/[1+P_t(E_{t}-1)+P_r(E_{r}-1)]$)]		EQ: $1/[1+P_t(E_{t}-1)+P_r(E_{r}-1)]$	-1)]	
$V_{p} (veh/hr) = 876$	= <u>876</u>	EQ: $v/[PHF*f_g*f_{hv}]$	<1,700 veh/hr	$V_{p} \text{ (veh/hr)= } 876$	EQ: v/[PHF*fg*fhv]	
$V_{p-directional}$ (veh/hr)= 560	= <u>560</u>	EQ: v _p *{MAX SPLIT}	<3,200 veh/hr	$V_{p-directional}$ (veh/hr)= 560	EQ: v _p *{MAX SPLIT}	
f_{ls} (mph)= 1.3	EXH. 20-5	f _{np} (mph)= 4	EXH. 20-11	BPTSF (%)= 53.7	EQ: 100(1-exp(-0.000879*v _p))	₉))
$f_A (mph) = \frac{7.5}{}$	EXH. 20-6	ATS (mph)= 30		$f_{d/np}$ (%)= 24.6	EXH. 20-12 *Interpolated Value	ted Value
FFS (mph)= <u>41</u>	EQ: BFFS-f _{IS} -f _A		EQ: FFS-0.00776*v _p -f _{np}	PTSF (%)= <u>78.3</u>	EQ: BPTSF+f _{d/np}	

					POST-CONSTRUCTION (P.M.) L.O.S. OF D WAS DETERMINED	LOS CALCULATIONS
*IISE FXH 20-3	ш	D	С	В	Þ	LOS (CLASS II) PTSF
XH 20-3 FOR LOS CLASS I	>85	>70-85	>55-70	>40-55	<=40	PTSF
ASSI						EXH. 20-4

Project Number: <u>04717-1-0122</u>

Calculations By: <u>SWS</u> Date: <u>6/27/2022</u>

Street of Interest: ACCESS RD

Development Location: 34° 15' 72.92" N

88° 39' 20.07" W

GENERAL STREET INFORMATION

		$V_{\text{directional}}$ (veh/hr)= 9	V (veh/hr)= <u>38</u>	Which direcdt
*Determined from Aerial Imagery	Access (Point/Mile)= 0	Terrain: <u>Level</u>	BFFS (mph)= <u>20</u>	Which direcdtion does the street run? EAST-WEST
	Class: <u>II</u>	$W_{sholder}$ (ft)= 0	*POSTED LIMIT PHF= 0.81	<u>EST</u>
	Split:	W_{lane} (ft)= 10	P _t (%)= <u>0%</u>	This calcula
	24%	No Pass (%)= 100%	P _r (%)= <u>0%</u>	This calculator uses HCM 2000 Chapter 20
	76%	00%	%	

TRA	VEL SPEED	TRAVEL SPEED CALCULATIONS		PERCENT TIME	PERCENT TIME FOLLOWING CALCULATIONS	CULATIONS	
$f_g = 1$	EXH. 20-7	$E_t = 1.7$	EXH. 20-9	$f_g = \underline{1}$	EXH. 20-8	$E_t = 1.1$	EXH. 20-10
$f_{hv} = 1.00$		E ₇ = <u>1</u>	EXH. 20-9	$f_{hv} = \frac{1.00}{1.00}$		E _r = <u>1</u>	EXH. 20-10
EQ: 1/[1+P _t	EQ: $1/[1+P_t(E_t-1)+P_r(E_r-1)]$)]		EQ: $1/[1+P_t(E_t-1)+P_r(E_r-1)]$	$[-1) + P_r(E_r-1)]$		
V_p (veh/hr)= 47	<u>47</u>	EQ: $v/[PHF*f_g*f_{hv}]$	<1,700 veh/hr	V_p (veh/hr)= 47		EQ: $v/[PHF*f_g*f_{hv}]$	
$V_{p ext{-directional}}$ (veh/hr)= 36	= <u>36</u>	EQ: v _p *{MAX SPLIT}	<3,200 veh/hr	$V_{p-directional}$ (veh/hr)= 36		EQ: v _p *{MAX SPLIT}	
f_{1s} (mph)= $\frac{5.28}{}$	EXH. 20-5	$f_{np} (mph) = 1.12$	EXH. 20-11	BPTSF (%)= <u>4.0</u>		EQ: 100(1-exp(-0.000879*v _p))	
$f_A (mph) = 0$	EXH. 20-6	ATS (mph)= <u>13</u>		$f_{d/np}$ (%)= 24.6	24.6 EXH. 20-12	0-12 *Interpolated Value	ed Value
FFS (mph)= <u>15</u>	EQ: BFFS-f _{Is} -f _A		EQ: FFS-0.00776*v _p -f _{np}	PTSF (%)= <u>28.6</u>		EQ: BPTSF+f _{d/np}	

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LOS CALCULATIONS

POST-CONSTRUCTION

TERMINED	LOS (CLASS II) PTSF	PTSF <=40	EXH. 20-4
	В	>40-55	
	С	>55-70	
	D	>70-85	
	ш	>85	
	*USE EXH. 20-3 FOR LOS CLASS I	OR LOS CLA	SS I

Project Number: <u>04717-1-0122</u>

Calculations By: <u>SWS</u> Date: <u>6/27/2022</u>

Street of Interest: ACCESS RD

Development Location: 34° 15' 72.92" N

88° 39' 20.07" W

GENERAL STREET INFORMATION

		$V_{\text{directional}}$ (veh/hr)= 26	V (veh/hr)= <u>41</u>	Which direcd
*Determined from Aerial Imagery	Access (Point/Mile)= $\underline{0}$	Terrain: <u>Level</u>	BFFS (mph)= <u>20</u>	Which direcdtion does the street run? EAST-WEST
	Class: <u>II</u>	W_{sholder} (ft)= $\underline{0}$	*POSTED LIMIT PHF= 0.81	<u>EST</u>
	Split:	W _{lane} (ft)= <u>10</u>	P _t (%)= <u>0%</u>	This calcula
	: 63%	No Pass (%)= 100%	P _r (%)= <u>0%</u>	This calculator uses HCM 2000 Chapter 20
	<u>37%</u>	= 100%	= 0%	0

TR	AVEL SPEED	TRAVEL SPEED CALCULATIONS		PERCENT TIME	PERCENT TIME FOLLOWING CALCULATIONS	CULATIONS	
f _g = <u>1</u>	EXH. 20-7	$E_t = 1.7$	EXH. 20-9	$f_g = 1$	EXH. 20-8	E _t = <u>1.1</u>	EXH. 20-10
$f_{hv} = 1.00$		E,= <u>1</u>	EXH. 20-9	$f_{hv} = 1.00$		E _r = <u>1</u>	EXH. 20-10
EQ: 1/[1+F	EQ: $1/[1+P_t(E_{t}-1)+P_r(E_{r}-1)]$)]		EQ: $1/[1+P_t(E_{t}-1)+P_r(E_{r}-1)]$	$_{t}$ -1)+ $P_{r}(E_{r}$ -1)]		
V _p (veh/hr)= <u>50</u>	<u>= 50</u>	EQ: $v/[PHF*f_g*f_{hv}]$	<1,700 veh/hr	V_p (veh/hr)= 50		EQ: v/[PHF*fg*fhv]	
$V_{p-directional}$ (veh/hr)= 32	= <u>32</u>	EQ: v _p *{MAX SPLIT}	<3,200 veh/hr	$V_{p-directional}$ (veh/hr)= 32		EQ: v _p *{MAX SPLIT}	
f_{ls} (mph)= $\frac{5.28}{}$	EXH. 20-5	$f_{np} (mph) = \frac{1.12}{1.12}$	EXH. 20-11	BPTSF (%)= <u>4.3</u>		EQ: 100(1-exp(-0.000879*v _p))	
f _A (mph)= <u>0</u>	EXH. 20-6	ATS (mph)= <u>13</u>		$f_{d/np}$ (%)= 24.6	24.6 EXH. 20-12	*Interpolated Value	d Value
FFS (mph)= <u>15</u>	EQ: BFFS-f _{ls} -f _A		EQ: FFS-0.00776*v _p -f _{np}	PTSF (%)= <u>28.9</u>	28.9 EQ: BPTSF+f _{d/np}	SF+f _{d/np}	

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					CONSTRUCTION (P.M.) L.O.S. OF A	LOS CALCULATIONS
					WAS DETERMINED	
*USE EXH. 20-3 FOR LOS CLASS	ш	D	С	В	Þ	LOS (CLASS II) PTSF
FOR LOS CLASS I	>85	>70-85	>55-70	>40-55	<=40	PTSF EXH. 20-4

Project Number: <u>04717-1-0122</u>

Date: <u>6/27/2022</u>

Calculations By: <u>SWS</u>

Development Location: 34° 15' 72.92" N

Intersection of Interest: N EASON BLVD & ACCESS RD

88° 39' 20.07" W

Which direction is the primary street running? NORTH-SOUTH

VEHICLE VOLUME CALCULATIONS

0%	13%	0%	0%	22%	0%	0%	0%	0%	0%	0%	0%	P _{hv} (%):
19	0	10	0	0	0	4	219	0	0	134	2	V _{hourly} (veh/hr):
1.00	0.00	1.00	0.00	0.00	0.00	0.68	0.68	0.00	0.00	0.78	0.78	PHF:
19	0	10	0	0	0	9	324	0	0	172	3	V (veh/hr):
12	11	10	9	8	7	9	5	4	3	2	1	Movement:

PEDESTRIAN VOLUME CALCULATIONS

/lovement:	13	14	15	16
x (ped/hr):	0	0	0	0
W _{lane} (ft): N/A		N/A	N/A	N/A
S _p (ft/sec): N/A		N/A	N/A	N/A
f _p (%): N/A		N/A	N/A	N/A

MOVEMENT KEY

Questions from Exhibit 17-4

Saturation (veh/hr)= 1,900

[a] / [c] Does major st. have dedicated right turn lane? NO

[b] How many thru lanes does the major street have? 1

[d] Does major street have multiple lanes? [This is for STAGE II movement of 7 and 10 if applicable] NO

[e] Is right turning traffic on minor st seperated by island and/or minor street multi-lane? $\frac{NO}{NO}$

 $v_{12}^{e} = 19$

CRITICAL GAP CALCULATIONS

$^{-}$ 5 for V_4 and V_1	for V_9 and V_{12} ; EQ. 17-5 for V_4 and V_1	EQ. 17-5 for V_9	\setminus		0.998	0.000	0.977	0.000	$P_{0,x}$:
10	642 EQ. 17-4; EQ. 17-7 for V_7 and V_{10}	EQ. 17-4; EQ. 1	642	0	1,358	0	824	0	c _{m,x} (s):
		0.998 EQ. 17-13	0.998	0.000	\setminus	\setminus	\setminus	\setminus	f _x .
		1 EQ. 17-12	1	1	1	1	₽	1	P _{p,x} :
		643 EQ. 17-3	643	0	1,358	0	824	0	$C_{p,x}$ (s):
$^*\mbox{V}_7$ and \mbox{V}_{10} are set up for signle stage equation	$^* extsf{V}_7$ and $ extsf{V}_{10}$ are se	360 EXH. 17-4	360	0	223	0	221	0	$V_{c,x}$ (veh/hr):
			Minor LT	N/A	Major LT	N/A	Minor RT	N/A	
			IK 3	RANK 3		IK 2	RANK 2		
			V_{10}	V ₇	V_1	V_4	V ₁₂	V ₉	
					ULATIONS	IMPEDANCE AND CAPACITY CALCULATIONS	ANCE AND C	IMPED	
3.5 EQ: tf,base+tf,HV*PHV	3.5	0	0	0	3.3	0	0	2.2	t _f (s):
0.9 *0.9 FOR 2-LN; 1 FOR 4-LN	0.9				0.9			0.9	t _{f,hv} (s):
3.5 EXH. 17-5	3.5				3.3			2.2	t _{f, base} (s):
				IONS	FOLLOW UP TIME CALCULATIONS	OLLOW UP TI	77		
6.4 EQ: $t_{c,x}=t_{c,base}+t_{c,HV}*PHV+t_{c,G}*G-t_{c,T}-t_{3,LT}$		0	0	0	6.2	0	0	4.1	$t_c(s)$ {single stage}:
0 *1 1 st /2 nd stage; 0 for 1 stage	0	0	0	0	\setminus	\setminus	\setminus	\setminus	$t_{c,T}$ (s) {single stage}:
0.7 *Note on PG 17-7	0.7					0	0		t _{3,LT} (s):
0 EQ: %Grade/100	0	0	0	0	0	0	0	0	Grade:
0.2 *SET VALUES		0.2	0.2	0.2	0.1	0.1			$t_{c,G}(s)$:
	0%	0%	13%	22%	0%	0%	0%	0%	P _{hv} (%):
1 *1 FOR 2-LN; 2 FOR 4-LN	1				1			1	$t_{c,hv}$ (s):
7.1 EXH. 17-5	7.1				6.2			4.1	t _{c,base} (s):
	10	7	11	8	12	9	4	1	Movement:

0.000

SHARED-LANE CAPACITY CALCULATIONS

0; 1	10; 1	1 (10; 11; 12)		3 (7	2 (7	1 (7	LANE										LANE
3 (10; 11; 12)	2 (10; 11; 12)	1; 12)		3 (7; 8; 9)	2 (7; 8; 9)	1 (7; 8; 9)			3	2	1		3	2	1		
		29				0	V (veh/hr)				10	mv10			0	mv7	
		979				0	V (veh/hr) C _m (veh/hr) v/c					mv11				mv8	v (veh/hr)
		0.030				0.000 N/A	v/c	CONTROI			19	mv12			0	mv9	
		-158.98436				N/A	Que (<2)	. DELAY/QUE			642	mv10			0	mv7	
						N/A	CD (sec/veh) LOS	LENGTH, LOS				mv11				mv8	c _m (veh/hr)
		9 A					LOS	CONTROL DELAY/QUE LENGTH, LOS CALCULATIONS			1,358	mv12			0	mv9	
								S			0.016	mv10			0.000	mv7	
											0.000	mv11			0.000	mv8	v/C _m
											0.014	mv12			0.000	mv9	
	" "	Ш	D	С	В	Α	LOS	EXH 17-2			979)		C _{SH} (veh/hr)

t= 0.25

Project Number: <u>04717-1-0122</u>

Date: <u>6/27/2022</u> Calculations By: <u>SWS</u>

Intersection of Interest: N EASON BLVD & ACCESS RD Development Location: 34° 15' 72.92" N

88° 39' 20.07" W

Which direction is the primary street running? NORTH-SOUTH

VEHICLE VOLUME CALCULATIONS

0%	13%	0%	0%	4%	0%	0%	0%	0%	0%	0%	0%	P _{hv} (%):
00/	100	20/				20/					/00	D (0/)-
5	0	10	0	0	0	7	165	0	0	361	15	V _{hourly} (veh/hr):
1.00	0.00	1.00	0.00	0.00	0.00	0.71	0.71	0.00	0.00	0.88	0.88	PHF:
5	0	10	0	0	0	9	231	0	0	409	17	V (veh/hr):
12	11	10	9	8	7	6	. 5	4	3	2	1	Movement:

PEDESTRIAN VOLUME CALCULATIONS

Movement:	13	14	15	16
V_{x} (ped/hr):	0	0	0	0
W _{lane} (ft): N/A		N/A	N/A	N/A
S _p (ft/sec): N/A		N/A	N/A	N/A
f _p (%): N/A		N/A	N/A	N/A

Questions from Exhibit 17-4

Saturation (veh/hr)= 1,900

[a] / [c] Does major st. have dedicated right turn lane? $\frac{NO}{NO}$

3 = 0

[b] How many thru lanes does the major street have? $\frac{1}{2}$

1 $v_5^b = 16$

 $v_2^{=} = 361$

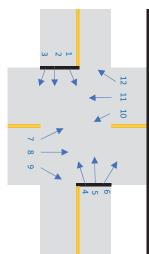
[d] Does major street have multiple lanes? [This is for STAGE II movement of 7 and 10 if applicable] NO

 $rac{1}{2} = 0$ $rac{d}{6} = 7$

[e] Is right turning traffic on minor st seperated by island and/or minor street multi-lane? $\frac{NO}{NO}$

 $V_9^{e} = 0$

V₁₂ e= !



MOVEMENT KEY

CRITICAL GAP CALCULATIONS

							UA) A
EQ. 17-16	EQ	\	0.989	0.000	/	/	P _{0v v*} :
EQ. 17-5 for $\rm V_9$ and $\rm V_{12}$; EQ. 17-5 for $\rm V_4$ and $\rm V_1$	EQ		0.990	0.000	0.994	0.000	P _{0,x} :
489 EQ. 17-4; EQ. 17-7 for V_7 and V_{10}	489 EQ	0	1,418	0	881	0	c _{m,x} (s):
17-13	0.990 EQ. 17-13	0.000		\setminus			f_x :
1 EQ. 17-12	1 EQ	1	1	1	1	1	P _{p,x} :
17-3	494 EQ. 17-3	0	1,418	0	881	0	$C_{p,x}(s)$:
H. $17-4$ *V_7 and V_{10} are set up for signle stage equation	558 EXH. 17-4	0	171	0	168	0	$V_{C,X}$ (veh/hr):
	Minor LT	N/A	Major LT	N/A	Minor RT	N/A	
	JK 3	RANK 3		IK 2	RANK 2		

V9

IMPEDANCE AND CAPACITY CALCULATIONS

V₁₀

3 (10; 11; 12)	2 (10; 11; 12)	1 (10; 11; 12)		3 (7; 8; 9)	2 (7; 8; 9)	1 (7; 8; 9)	LANE										LANE	
)) 15)) 0	V (veh/hr)		ω	2	1 10	mv10	ω	2	0	mv7		
		641				0	V (veh/hr) C _m (veh/hr) v/c					mv11				mv8	v (veh/hr)	
		0.024					v/c	CONTRO				mv12				mv9		
		4 -180.56911				0.000 N/A	Que (<2)	I DELAY/QUE			5 489	mv10			0	mv7		SHARED-L
		1 11				N/A	CD (sec/veh)	CONTROL DELAY/QUE LENGTH, LOS CALCULATIONS			9	mv11			0	mv8	c _m (veh/hr)	SHARED-LANE CAPACITY CALCULATIONS
		1 B					LOS	CALCULATION			1,418	mv12				mv9		Y CALCULATIO
								SN			8 0.020	mv10			0.000	mv7		SNC
											0.000	mv11			0.000	mv8	v/C _m	
											0.004	mv12			0.000	mv9		
	T	П	D	С	В	Α	LOS	EXH			1 641				0		C _{SH} (veh/hr)	
	>50	>35-50	>25-35	>15-25	>10-15	: 0-10	CD	EXH 17-2			1		<u> </u>		0			J

t = 0.25

Multifamily Housing (Low-Rise)

Not Close to Rail Transit (220)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

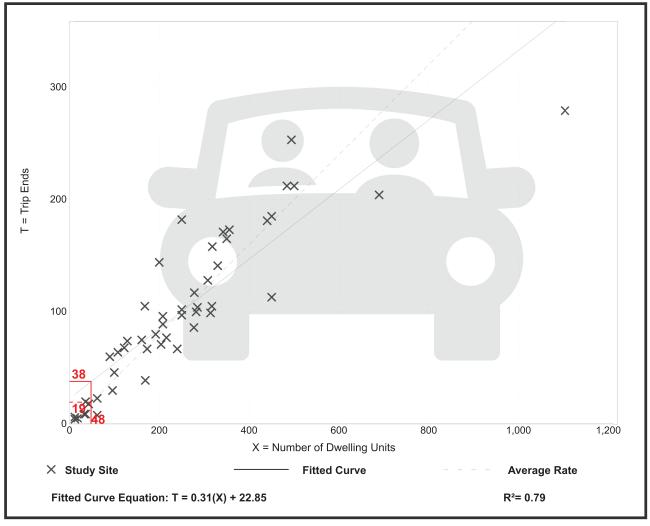
Number of Studies: 49 Avg. Num. of Dwelling Units: 249

Directional Distribution: 24% entering, 76% exiting

Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.40	0.13 - 0.73	0.12

Data Plot and Equation



Multifamily Housing (Low-Rise)

Not Close to Rail Transit (220)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

Number of Studies: 59 Avg. Num. of Dwelling Units: 241

Directional Distribution: 63% entering, 37% exiting

Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.51	0.08 - 1.04	0.15

Data Plot and Equation

