

STRUCTURAL CIVIL SURVEY

To: City of Mills
Attn: Casey Coates
Re: Wyoming Classical Academy Site Review
Location: 6389 Poison Spider Ln., Mills, WY 82604

Dear Casey,

Based on the review received dated 9/28/2026, the following changes have been made to the above-mentioned drawings. You will find an itemized list which addresses each comment individually. You will find the original comments followed by our response in bold.

Parking Lot

1. Stall size per Table 40.10-2 details that 90-degree parking requires (Stall Width of 10'/Stall Depth of 24').

1 Response: The proposed parking lot has been redesigned to accommodate with city stall size requirements. As a result of the increased stall size, the number of stalls in the new parking lot has been reduced to 149 stalls. This brings the overall site parking to 247 stalls still over the total parking required for the entire school campus per 40.10-1. See sheets C200 and C201 with updated grading on sheet C300 and C301.

2. Stall depth may be reduced to 21.5 ft where permanent curb stops are installed 40.10(3)(a)(iii).

2 Response: All curb facing stalls around the perimeter of the parking lot utilize this depth reduction. Stalls within the center parking island are sized for a 24-ft depth. See sheet C201.

3. Accessible parking is calculated per parking facility (IBC 1106.1). The new 176-stall lot requires 6 accessible stalls, including 1 van-accessible; 3 are shown.

3 Response: With the reduction of the new parking lot, 5 accessible stalls are provided within the 149 stall lot. All 5 ADA stalls are 10-ft wide adjoined by a 10-ft wide accessible aisle. See sheets C200 and C201.

Traffic Study

1. The study assumes a traffic signal will be installed, and that the car lines will operate in a double-stacked fashion. This must occur for the study to have merit; the way things operate now, only half of the car line is used, and the remaining half is blocked.

1 Response: The school plans on utilizing both stacking lanes for pick-up and drop-off. See the new traffic circulation plan for more information.

2. Show the double-stacked car line on the site plan (lane striping, merge point, signage, and staff direction locations). (Designate the central access as parking lot access, separate from the car line, and show this on the site plan).

2 Response: Included in the updated civil set is a traffic circulation plan detailing the recommendations from the traffic study. See sheet C202.

STRUCTURAL CIVIL SURVEY

3. Provide a written commitment to staggered start and dismissal times, to be included in the Development Plan Agreement.

3 Response: Owner intends to comply and will provide this when available.

4. Provide a queue analysis at the 650-student build-out enrollment (the study modeled 610).

4 Response: Per email from Josh Gibbons on 9-30-26, The study's reference to the 610 student model was a report typo. The queueing analysis conducted in the report was run for the full 650 student enrollment. The revised Traffic Impact Study is included in this response.

5. The applicant will be required to contribute a proportionate share toward the Poison Spider Lane / Robertson Road signal per 10.40(7)(f).

5 Response:

Fire Hydrants

1. Per discussion with our fire chief and based on the 1700 GPM flow rate, two hydrants will be needed for the new school. Please confirm with Brett's report. The fire chief would like to see the additional hydrant on the NW corner in front of the addition.

1 Response: The updated utility plans propose relocating the existing hydrant in the new parking lot to the NW corner of the front of the addition. See sheets C400 and C401.

2. Mills Engineering Comment – C400/Upsize the C900 size to 8" to accommodate fire flows related to line length, remove the 45 bends, and install a 6" tee to the fire hydrant; blind flange the end of the 8" to accommodate future needs of the school from the 8".

2 Response: The C-900 fire line supplying the proposed fire hydrant has been upsized to 8-in. The 45 bends have been removed, and the utility sheets include a callout to install a tee at the hydrant with a blind flange on the west connection for future needs. See sheets C400 and C401.

Landscape Plan

1. Please include a tree and shrub in every island. The landscape plan must indicate irrigation and existing vegetation.

1 Response: Noted and see revised plan. Also note there are gas lines through the parking lot and islands that will impact the plantings.

2. Update L1.0 to the 8/28/26 layout. Remove the "Preliminary" label and correct the location to Mills.

2 Response: Plan updated and corrected.

3. Show planting and irrigation for the 5-ft strip on C500. It is labeled only as "park strip", with no surface or plantings specified.

3 Response: Revised accordingly. Irrigation notes on the plans and design will be completed during the construction phase with the contractor.

STRUCTURAL CIVIL SURVEY

Lighting Plan

1. Update the lighting plan and photometrics to match the revised 8/28/26 parking layout.

1 Response:

2. Extend the photometric grid to 5 ft beyond all property lines to show light levels do not exceed 0.2 foot-candles 40.35(3)(d). If this can't be met along Poison Spider Lane, request a Director exception.

2 Response:

3. Include all exterior fixtures in the photometric calculations, including the play-area poles and building wall packs.

3 Response:

4. Clarify pole height and base height separately. Within 150 ft of residential, poles may not exceed 15 ft, and fixtures may not be mounted above 17 ft 40.35(5)(a).

4 Response:

5. Show house-side shielding and aiming for fixtures facing residential properties to the north and west 40.35(5)(b).

5 Response:

6. Show timer or photocell controls for the site lighting 40.35(3)(a).

6 Response:

7. Provide manufacturer cut sheets for all exterior fixtures 40.35(4)(a)(ii).

7 Response:

8. Provide a brief written narrative describing the lighting objectives 40.35(4)(a)(v).

8 Response:

9. The play-area fixtures (A3, about 57,500 lumens each). Justify lighting level or reduce them 40.35(3)(b), (i).

9 Response:

10. Provide a photometric calculation summary (average, maximum, minimum, and max/min ratio).

10 Response:**Drainage**

1. Show how gutter flow from the new curb and gutter on Poison Spider Lane will be conveyed to the ditch (curb cuts, inlets, or rundowns).

1 Response: Runoff collected in the new Poison Spider curb and gutter will be conveyed to the existing drainage ditch by curb cuts allowing overland flow into the ditch. See new detail 2/C500.

STRUCTURAL CIVIL SURVEY

2. The drainage study does not evaluate the Poison Spider Lane ditch or culvert capacity. Provide pre- and post-development peak flows to the ditch, and demonstrate capacity including the new M1 inlet and the new curb and gutter.

2 Response: The drainage study now shows the existing impact on the swale and the proposed impact after the development is finished. The new M1 inlet allows water to be retained until the full capacity of the 24" culvert is needed. This increases the amount of water the system can handle. See updated report included in this response.

3. Provide pond routing demonstrating adequate capacity and freeboard with the 16" outlet restriction.

3 Response: We have updated the pond and the drainage area to match the most up to date plan. The 16" outlet restriction was removed.

Fire Access

1. The fire access to the rear of the school will be sufficient; however, the existing hard surfacing will need to be striped to indicate its use as the fire lane. The fire lane shall remain unobstructed during car line operations.

1 Response: A striping diagram for the fire lane behind the school is included on the updated site plan. Notes are also included to ensure proper signage is posted on all gates to always keep the fire lane clear. See sheets C200 and C201.

Submittal

1. Provide one consolidated plan set.

1 Response: All plans that are being resubmitted are combined into one set.

2. Provide consent from the pipeline operators (Sinclair, Black Hills Energy) for improvements over their lines.

2 Response: We are coordinating with Raelynn Saxton, Sinclair Right of Way Specialist. We will provide the approved consent once received.

3. Note on the plans that the gym, track, field, bleachers, and concessions are future phases subject to separate approval.

3 Response: This note is included on all civil site plans.

4. Replat recording before building permit issuance. Without it, the 20-acre minimum lot size isn't met.

4 Response: This has been submitted and is currently in process.

5. Building elevations. These are a required submittal, and they tie into the lighting narrative if the building is lit.

5 Response: See attached Building elevations included with this response.



Wyoming Classical Academy

Storm Water Drainage Study -Wyoming Classical Academy

PREPARED FOR: Casey Coates, City of Mills
PREPARED BY: Robert Bennett, CEPI
Austin Luers, CEPI
DATE: October 2, 2026



Introduction

Wyoming Classical Academy is looking to begin construction on Phase II of the charter school. Phase II will consist of the addition of the 7th grade to 12th grade building that will attach to the existing building. This phase will also consist of the construction of the parking lot, roads, and sports fields. The City of Mills has observed the existing ditch along Poison Spider over flowing during significant moisture events.

Historic Flows

In reference to the original drainage study, October 25, 2023 prepared by ECS Engineers, both Phase I and Phase II are located in sub-basin C. Sub-base C has an area of 56.73 acres. The school takes up roughly 20 acres and the rural housing development takes the other 36.73 acres. The drainage study prepared by ECS Engineers shows the average percentage of land impervious to be 40.8% which would increase the detention required to 226,494 cf. The detention pond was over designed and has an as-built volume of 260,955 cubic feet with 1 foot of free board retained. Leaving the basin with excess of by 34,461 cubic feet. Within the school's 20 acres, 9.67 acres drain directly to the drainage swale along Poison Spider Road. The existing impact on the swale is contributing 13.6 cfs to the swale at peak flow during a 100 year moisture event. The other 10.33 acres and the subdivision's 36.73 acres drain into a 57,112 cf retention pond prior to entering the drainage swale along Poison Spider Rd.

Projected Flows

With the new layout of Phase II, the new average area of land that is impervious is 42.9% for the 56.73 acres of sub-basin C. this makes the required detention of sub-basin C, 230,672 cf. The Post development Flows from the school's property to the drainage swale along Poison Spider Road for the 100-year moisture event is 26.9 cfs.

Storm Water Detention

The existing detention pond in the North West Corner of Sub-Basin C has the capacity to hold the additional 4,178 cf required and still have an additional 30,283 cf of storage. This change has little to no effect of the drainage system and will have no negative impact for the swale on Poison Spider, there should be a 13" M1 inlet drain installed on the culvert on the East Side of the North West access of the school's property. This will allow the water to slow down until the major moisture event where the full capacity of the 24-Inch culvert is needed.

STORMWATER DRAINAGE STUDY

For

Construction of the

WCA Phase 2 SWALE ON POISON SPIDER

CEPI Project No. 26-014



October 2026

FOR INFORMATION REGARDING
THIS PROJECT CONTACT:
ROBERT BENNETT
CEPI
6080 Enterprise Drive
CASPER, WYOMING 82609
307.266.4346

WCA Phase 2 SWALE ON POISON SPIDER

EXISTING CONDITIONS

October 2026

Time of Concentration

$$T_c = 1.87 \frac{(1.1 - C \times C_f)(L^{0.5})}{S^{0.33}} \quad (\text{Eq. 1 - Sheet Flow})$$

$$T_c = \frac{L}{(1.49/n)((d/4)^{0.66})(S^{0.5})} \quad (\text{Eq. 2 - Pipe Flow})$$

Table 1 - Sheet Flow

C	L (ft)	S (%)	C _{f,100YR}	CxC _f	T _{CX} (10yr)	T _{CX} (100yr)
0.39	1050	2.1	1.25	0.49	33.6	29.0
			1.25			
			1.25			
			1.25			

Table 2 - Pipe Flow

d (in)	n*	L (ft)	S (%)	T _{CX} (10yr/100yr)

* 0.01 for PVC
0.013 for RCP

T_{C,10YR} = 33.6 min

T_{C,100YR} = 29.0 min

Rainfall Intensity

$$i = \frac{a}{(b + D)^n} \quad (\text{Eq. 3 - Rainfall Intensity})$$

a_{10YR} = 36.69421 b_{10YR} = 9.85 D_{10YR} = 33.6 min n_{10YR} = 0.81962
a_{100YR} = 60.87626 b_{100YR} = 10.154 D_{100YR} = 29.0 min n_{100YR} = 0.83098

i_{10YR} = 1.7 in/hr

i_{100YR} = 2.9 in/hr

Flow

$$Q = C_f C \times i \times A \quad (\text{Eq. 4 - Peak Flow})$$

Area (acres)	C	A*C
9.67	0.39	3.771

A_{TOTAL} = 9.67

C = 0.39

C_{f,100yr} = 1.25

CxC_f = 0.488

Q_{10YR} = 6.3 cfs

Q_{100YR} = 13.6 cfs

WCA Phase 2 SWALE ON POISON SPIDER DEVELOPED CONDITIONS

October 2026

Time of Concentration

$$T_c = 1.87 \frac{(1.1 - C \times C_f)(L^{0.5})}{S^{0.33}} \quad (\text{Eq. 1 - Sheet Flow})$$

$$T_c = \frac{L}{(1.49/n)((d/4)^{0.66})(S^{0.5})} \quad (\text{Eq. 2 - Pipe Flow})$$

Table 1 - Sheet Flow

C	L (ft)	S (%)	C _{f,100YR}	CxC _f	T _{CX} (10yr)	T _{CX} (100yr)
0.58	1050	2.1	1.25	0.73	24.6	17.7
			1.25			
			1.25			
			1.25			

Table 2 - Pipe Flow

d (in)	n*	L (ft)	S (%)	T _{CX} (10yr/100yr)

* 0.01 for PVC
0.013 for RCP

T_{C,10YR} = 24.6 min

T_{C,100YR} = 17.7 min

Rainfall Intensity

$$i = \frac{a}{(b + D)^n} \quad (\text{Eq. 3 - Rainfall Intensity})$$

a_{10YR} = 36.69421 b_{10YR} = 9.85 D_{10YR} = 24.6 min n_{10YR} = 0.81962
a_{100YR} = 60.87626 b_{100YR} = 10.154 D_{100YR} = 17.7 min n_{100YR} = 0.83098

i_{10YR} = 2.0 in/hr

i_{100YR} = 3.8 in/hr

Flow

$$Q = C_f C \times i \times A \quad (\text{Eq. 4 - Peak Flow})$$

Area (acres)	C	A*C
9.67	0.58	5.61

A_{TOTAL} = 9.67

C = 0.58

C_{f,100yr} = 1.25

CxC_f = 0.725

Q_{10YR} = 11.3 cfs

Q_{100YR} = 26.9 cfs

WCA Phase 2 SWALE ON POISON SPIDER
STORAGE
October 2026

10-YR EVENT

Rainfall Duration (min)	Intensity (in/hr)	Peak Runoff (cfs)	Storm Runoff Volume (cf)	Release Flow Volume (cfs)	Req. Storage Volume (cfs)	Critical Volume
15	2.64	14.8	13306	5660	7646	
16	2.55	14.3	13742	6038	7704	
17	2.47	13.9	14153	6415	7738	
18	2.40	13.5	14543	6792	7751	<==
19	2.33	13.1	14914	7170	7744	
20	2.27	12.7	15266	7547	7720	
21	2.21	12.4	15603	7924	7678	

Required Volume = 7751 cf

$$Volume = H \frac{A_{BOTTOM} + A_{TOP}}{2}$$

(Eq. 5 - Volume of Pond)

$$\begin{aligned} A_{BOTTOM} &= 190 \text{ sf} \\ A_{TOP} &= 1020 \text{ sf} \\ H &= 4 \text{ ft} \end{aligned}$$

Volume of Pond = 2420 cf

FALSE <-Storage Amount OKAY?

100-YR EVENT (FOR INFORMATION PURPOSES ONLY)

Rainfall Duration	Intensity (in/hr)	Peak Runoff (cfs)	Storm Runoff Volume (cf)	Release Flow Volume (cfs)	Req. Storage Volume (cfs)	Critical Volume
50	2.02	14.2	42540	40885	1655	<==
51	2.00	14.0	42801	41703	1098	
52	1.97	13.8	43056	42521	535	
53	1.94	13.6	43305	43338	-33	
54	1.92	13.4	43550	44156	-606	
55	1.89	13.3	43790	44974	-1183	
56	1.87	13.1	44026	45791	-1766	

WCA Phase 2 SWALE ON POISON SPIDER OUTFALL DESIGN

October 2026

Manning's "n" = 0.013
 L = 85 ft
 E_s = 5248.00 ft
 E_c = 5245.00 ft
 Q_{10YR,PRE-DEV} = 6.3 cfs

(Static Water Elevation)

(Pipe Centerline Elevation)

D (trial) = 13 in

<--Increase/Decrease to the diameter below
 Do not use less than 6"

$$K_p = 5087n^2 D^{-4/3}$$

(Eq. 6 - Pipe Friction Coefficient)

$$C = 0.456 + 0.047(K_p) - 0.0024(K_p)^2 + 0.00006(K_p)^3$$

(Eq. 7 - Minor Losses)

$$D = 12 \left(\frac{Q_{10YR,PREDEV}^5}{C(E_s - E_c)^{0.25}} \right)^{0.25}$$

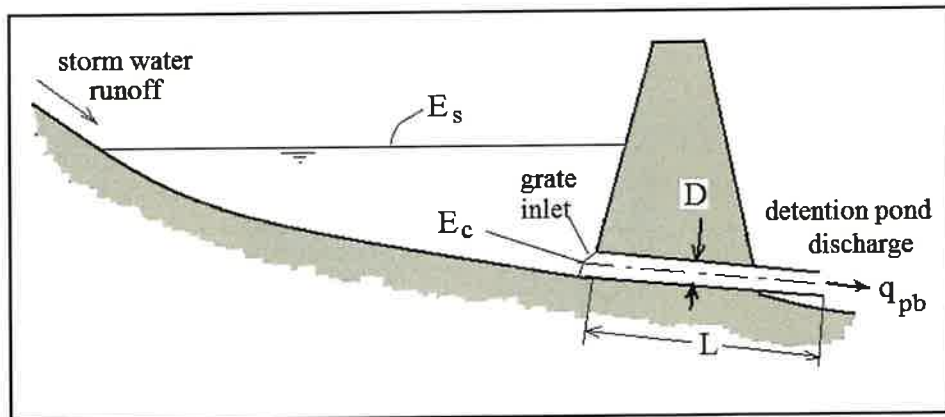
(Eq. 8 - Pipe Diameter)

K_p = 0.028

C = 0.555

D = 13 in

<--Insert value above



Storm Water Detention Pond with Pipe Outlet Control

STORMWATER DRAINAGE STUDY

For

Construction of the

WCA Phase 2 Detention Pond

CEPI Project No. 26-014



October 2026

FOR INFORMATION REGARDING
THIS PROJECT CONTACT:
ROBERT BENNETT
CEPI
6080 Enterprise Drive
CASPER, WYOMING 82609
307.266.4346

WCA Phase 2 Detention Pond EXISTING CONDITIONS

October 2026

Time of Concentration

$$T_c = 1.87 \frac{(1.1 - C \times C_f)(L^{0.5})}{S^{0.33}} \quad (\text{Eq. 1 - Sheet Flow})$$

$$T_c = \frac{L}{(1.49/n)((d/4)^{0.66})(S^{0.5})} \quad (\text{Eq. 2 - Pipe Flow})$$

Table 1 - Sheet Flow

C	L (ft)	S (%)	C _{f,100YR}	CxC _f	T _{CX} (10yr)	T _{CX} (100yr)
0.25	950	3	1.25	0.31	34.0	31.5
0.38	1300	3	1.25	0.48	33.7	29.2
			1.25			
			1.25			

Table 2 - Pipe Flow

d (in)	n*	L (ft)	S (%)	T _{CX} (10yr/100yr)
24	0.012	500	1	1.07

* 0.01 for PVC
0.013 for RCP

T_{C,10YR} = 68.7 min

T_{C,100YR} = 61.8 min

Rainfall Intensity

$$i = \frac{a}{(b + D)^n} \quad (\text{Eq. 3 - Rainfall Intensity})$$

$a_{10YR} = 36.69421$ $b_{10YR} = 9.85$ $D_{10YR} = 68.7 \text{ min}$ $n_{10YR} = 0.81962$
 $a_{100YR} = 60.87626$ $b_{100YR} = 10.154$ $D_{100YR} = 61.8 \text{ min}$ $n_{100YR} = 0.83098$

i_{10YR} = 1.0 in/hr

i_{100YR} = 1.7 in/hr

Flow

$$Q = C_f C \times i \times A \quad (\text{Eq. 4 - Peak Flow})$$

Area (acres)	C	A*C
10.33	0.25	2.583
36.73	0.38	13.96

A_{TOTAL} = 47.06

C = 0.351

C_{f,100yr} = 1.25

CxC_f = 0.439

Q_{10YR} = 17.0 cfs

Q_{100YR} = 36.1 cfs

WCA Phase 2 Detention Pond DEVELOPED CONDITIONS

October 2026

Time of Concentration

$$T_c = 1.87 \frac{(1.1 - C \times C_f)(L^{0.5})}{S^{0.33}} \quad (\text{Eq. 1 - Sheet Flow})$$

$$T_c = \frac{L}{(1.49/n)((d/4)^{0.66})(S^{0.5})} \quad (\text{Eq. 2 - Pipe Flow})$$

Table 1 - Sheet Flow

C	L (ft)	S (%)	C _{f,100YR}	CxC _f	T _{CX} (10yr)	T _{CX} (100yr)
0.25	950	3	1.25	0.31	34.0	31.5
0.38	1300	3	1.25	0.48	33.7	29.2
			1.25			
			1.25			

Table 2 - Pipe Flow

d (in)	n*	L (ft)	S (%)	T _{CX} (10yr/100yr)
24	0.012	500	1	1.07

* 0.01 for PVC
0.013 for RCP

T_{C,10YR} = 68.7 min

T_{C,100YR} = 61.8 min

Rainfall Intensity

$$i = \frac{a}{(b + D)^n} \quad (\text{Eq. 3 - Rainfall Intensity})$$

a_{10YR} = 36.69421 b_{10YR} = 9.85 D_{10YR} = 68.7 min n_{10YR} = 0.81962
a_{100YR} = 60.87626 b_{100YR} = 10.154 D_{100YR} = 61.8 min n_{100YR} = 0.83098

i_{10YR} = 1.0 in/hr

i_{100YR} = 1.7 in/hr

Flow

$$Q = C_f C \times i \times A \quad (\text{Eq. 4 - Peak Flow})$$

Area (acres)	C	A*C
10.33	0.25	2.58
36.73	0.38	13.96

A_{TOTAL} = 47.06

C = 0.351

C_{f,100yr} = 1.25

CxC_f = 0.439

Q_{10YR} = 17.0 cfs

Q_{100YR} = 36.1 cfs

WCA Phase 2 Detention Pond
STORAGE
 October 2026

10-YR EVENT

Rainfall Duration (min)	Intensity (in/hr)	Peak Runoff (cfs)	Storm Runoff Volume (cf)	Release Flow Volume (cfs)	Req. Storage Volume (cfs)	Critical Volume
15	2.64	43.6	39241	15279	23961	
16	2.55	42.2	40525	16298	24227	
17	2.47	40.9	41739	17316	24422	
18	2.40	39.7	42889	18335	24554	
19	2.33	38.6	43982	19354	24628	
20	2.27	37.5	45021	20372	24649	<==
21	2.21	36.5	46013	21391	24622	

Required Volume = 24649 cf

$$Volume = H \frac{A_{BOTTOM} + A_{TOP}}{2}$$

(Eq. 5 - Volume of Pond)

$$\begin{aligned} A_{BOTTOM} &= 8850 \text{ sf} \\ A_{TOP} &= 14000 \text{ sf} \\ H &= 5 \text{ ft} \end{aligned}$$

Volume of Pond = 57125 cf

TRUE <-Storage Amount OKAY?

100-YR EVENT (FOR INFORMATION PURPOSES ONLY)

Rainfall Duration	Intensity (in/hr)	Peak Runoff (cfs)	Storm Runoff Volume (cf)	Release Flow Volume (cfs)	Req. Storage Volume (cfs)	Critical Volume
50	2.02	41.8	125452	108159	17293	<==
51	2.00	41.2	126220	110322	15898	
52	1.97	40.7	126972	112486	14487	
53	1.94	40.2	127709	114649	13060	
54	1.92	39.6	128431	116812	11619	
55	1.89	39.1	129139	118975	10163	
56	1.87	38.6	129833	121138	8694	

WCA Phase 2 Detention Pond OUTFALL DESIGN

October 2026

Manning's "n" =	0.013	
L =	85	ft
E _s =	5248.00	ft
E _c =	5245.00	ft
Q _{10YR,PRE-DEV} =	17.0	cfs

(Static Water Elevation)

(Pipe Centerline Elevation)

D (trial) = 19 in

<--Increase/Decrease to the diameter below
Do not use less than 6"

$$K_p = 5087n^2 D^{-4/3} \quad (\text{Eq. 6 - Pipe Friction Coefficient})$$

$$C = 0.456 + 0.047 \times (LK_p) - 0.0024 \times (LK_p)^2 + 0.00006 \times (LK_p)^3 \quad (\text{Eq. 7 - Minor Losses})$$

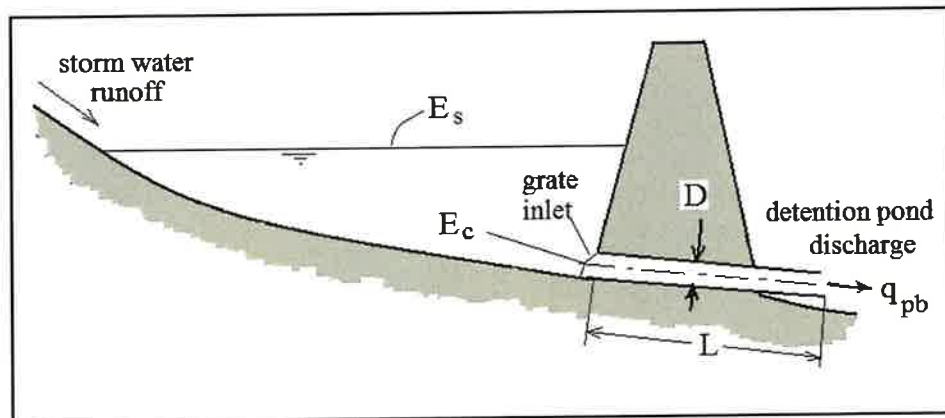
$$D = 12 \left(\frac{Q_{10YR,PRE-DEV}^5}{C} (E_s - E_c) \right)^{-0.25} \quad (\text{Eq. 8 - Pipe Diameter})$$

K_p = 0.017

C = 0.519

D = 19 in

<--Insert value above



Storm Water Detention Pond with Pipe Outlet Control



**ENGINEER'S WATER SUPPLY ANALYSIS
WYOMING CLASSICAL ACADEMY - ADDITION
SEPTEMBER 28, 2026**

This report contains an assessment of the water supply available at the proposed Addition for Wyoming Classical Academy located at 6389 Poison Spider Lane in Mills, Wyoming. This report is prepared at the direction of:

Mr. Logan Hammer
Silverpeak Engineering
177 East Antelope Drive, Suite B
Layton, Utah 84041

Prepared by:

Brett A. Jones
Protection Consultants, Inc.
1199 South Main Street, Suite 101
Centerville, Utah 84014

SUMMARY

The purpose of this report is to determine the water supply that is currently available for the proposed sprinkler system at the Wyoming Classical Academy - Addition to determine the available fire flow, and to determine the water supply available for this facility. The available water supply was determined by conducting a water flow test using existing fire hydrants located nearby the proposed Campus to measure available water flow while recording the static and residual pressures.

WATER FLOW TEST AND ANALYSIS

The water supply was determined by performing a water flow test. The test was performed at 10:00 AM on September 17, 2026, by Protection Consultants, Inc., and Casey Coates, Public Works Supervisor with the City of Mills. A pressure gauge was placed on a fire hydrant located in the parking area North of the existing school building. Discharge was then measured by flowing the steamer outlet on a hydrant located directly North of where the proposed building addition will occur. Refer to the attached water flow test report for the locations of the tested hydrants. The results of the water flow test are as follows:

WATER SUPPLY ANALYSIS

Wyoming Classical Academy - Addition
6389 Poison Spider Lane
Mills, Wyoming

Page 2

Static Pressure: 68 psi
Residual Pressure: 58 psi
Flow: 1,720 gpm

This water flow test represents the current pressures and volume available from the 8" water line which runs in the drop off loop of the Academy on the North side of the proposed and existing building. This test provides a good representation of the water pressures and volume that can be expected from this water system at this location during the year. Based on the results of this test PCI calculates a theoretical fire flow of 4,012 gpm at 20 psi.

Prior to the design of the fire sprinkler system for the proposed addition, the pressures should be adjusted to account for lower pressures that could be encountered during periods of peak demand and after further development if any of the immediate area. A 10% reduction in water pressures used for the fire sprinkler system design is recommended. The water supply that should be used for the design of the fire sprinkler system should be:

Static Pressure: 61 psi
Residual Pressure: 52 psi
Flow: 1,720 gpm

WATER SUPPLY ANALYSIS

Information about the City of Mills City Water System and how it operates was obtained from an interview with Casey Coates, Public Works Supervisor with the City of Mills. "The water storage tank feeding the school and the related subdivision has a total capacity of 2.4 million gallons. A second tank, which equalizes this tank has the capacity of 1.5 million gallons of storage. These tanks are serviced by a primary tank with a capacity of 600 thousand gallons. A set of pumps pulls water from the primary tank and sends water to each of the high volume tanks." The water supply comes from the water treatment plant which provides 1.5 million gallons per day to the city water system.

The results of our water flow test finds this portion of the water system **capable** of providing a theoretical fire flow of **approximately 4,012 gpm at 20 psi**. The Wyoming Classical Academy is a two level building. The breakdown of square footage for the building is as follows:

Existing Building

Main Level: 23,023 square feet
Upper Level: 13,841 square feet
Total: 36,864 Total existing square footage

WATER SUPPLY ANALYSIS

Wyoming Classical Academy - Addition
6389 Poison Spider Lane
Mills, Wyoming

Page 3

Addition to Existing Building

Main Level: 13,552 square feet
Upper Level: 12,595 square feet
Total: 26,147 square feet

The total square footage of this building including the existing and new areas will be 63,011 square feet. This building will be built utilizing type II-B construction. The required fire flow per Table B105.1 in the 2021 Edition of the International Fire Code (Attached) for a building of this size and construction type is **5,250 gpm** for a period of four hours. In accordance with the exception noted in IFC B105 (Attached) the required fire flow (up to 25% of the initial value but not less than 1,000 gpm) may be obtained through the installation of a fire sprinkler system in all areas of the building where approved by the Authority Having Jurisdiction. A reduction in the fire flow requirements for this building **WILL BE** required whereas the available fire flow of **4,012 gpm** is less than the required fire flow of **5,250 gpm**. Since a fire sprinkler system per NFPA 13 will be present throughout the Wyoming Classical Academy, the resultant required fire flow is $5,250 \text{ gpm} \times 0.25 = 1,313 \text{ gpm}$. The available fire flow of 4,012 gpm measured during the water flow test **EXCEEDS** the required fire flow of 1,313 gpm for the Academy. The water system can provide the required fire flow for the proposed improvement to the new and existing portions of the Academy building.

CONCLUSIONS AND RECOMMENDATIONS

The data collected for this analysis reflects the pressures and flows that are available in this water system at this time and throughout the year. Fluctuations in pressures and flows can be expected during periods of high demand. A reduction in the fire flow requirements for the Wyoming Classical Academy **WILL BE** required where the available fire flow of **4,012 gpm** is less than the required fire flow of **5,250 gpm**.

If there are any questions regarding this analysis please contact the author.

Brett A. Jones

Brett A. Jones
Protection Consultants, Inc.

PROTECTION CONSULTANTS, INC.

1199 SOUTH MAIN STREET, SUITE 101
CENTERVILLE, UTAH 84014

PAGE 1 OF 2

WATER FLOW TEST REPORT

PROJECT NAME: WYOMING CLASSICAL ACADEMY - ADDITION

STREET ADDRESS: 6389 POISON SPIDER LANE

CITY: MILLS

STATE: WYOMING

TESTED BY: MILLS WATER DEPARTMENT

WITNESSED BY: CASEY COATES - MILLS WATER DEPARTMENT

TEST DATE: 09/21/2026

TEST TIME: 10:00 AM

TEMPERATURE: 59°F

PROJECT ELEVATION: 5,263 FT.

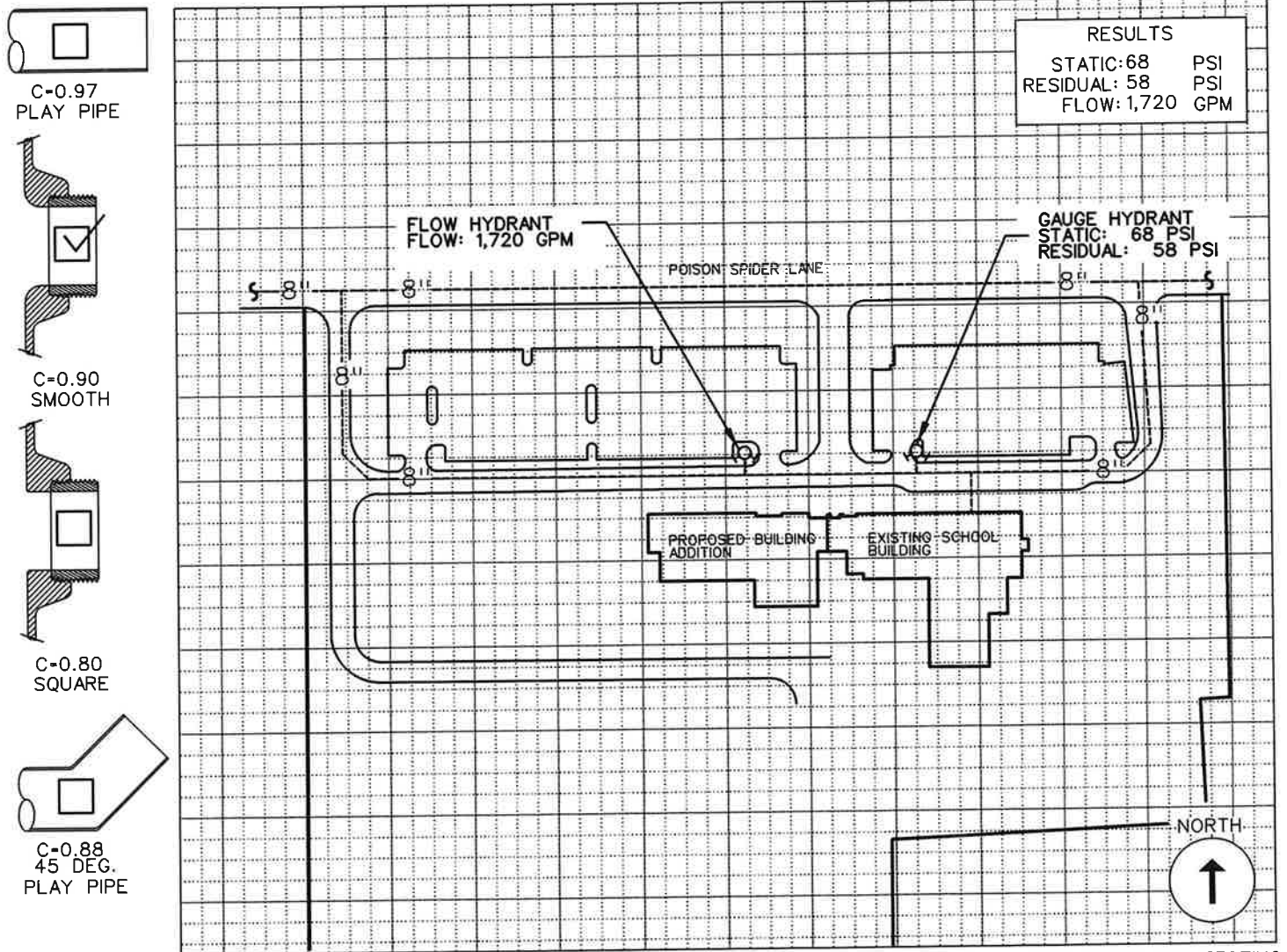
COMMENTS: FIRE FLOW: 4,012 GPM @ 20 PSI.

HYDRANT & FLOW DATA

TEST HYDRANT (GAUGED):	STATIC:	68	PSI	RESIDUAL:	58	PSI	ELEVATION:	5,263	FT.
FLOW OUTLET DIAMETER:	OUTLET 1:	2.500	INCHES	OUTLET 2:		INCHES			
FLOW OUTLET C-FACTOR:	OUTLET 1:	0.90		OUTLET 2:					
FLOW HYDRANT (PITOTED):	OUTLET 1:		PSI	OUTLET 2:		PSI			
WATER FLOW VOLUME:	OUTLET 1:	1,720	GPM	OUTLET 2:		GPM	TOTAL:	1,720	GPM

FORMULA: $Q = 29.83Cd^2\sqrt{P}$ Q: FLOW VOLUME d: OUTLET DIAMETER P: PITOT PRESSURE C: COEFFICIENT OF DISCHARGE

AREA MAP

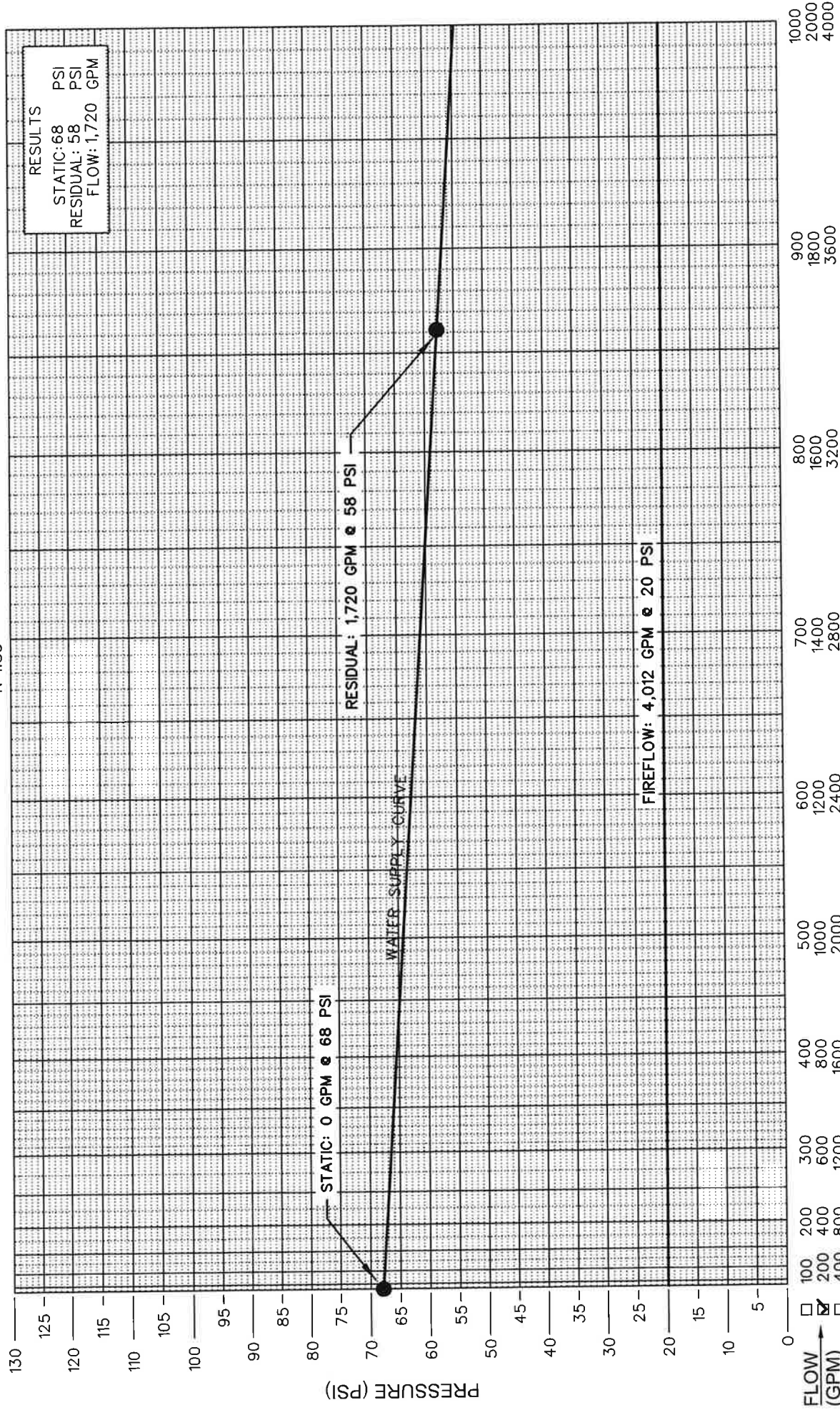


☒ FLOW TEST CONDUCTED IN ACCORDANCE WITH NFPA 291 "RECOMENDED PRACTICE FOR FIRE FLOW TESTING AND MARKING OF HYDRANTS"

PROTECTION CONSULTANTS, INC.

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CENTERVILLE, UTAH 84014

WATER FLOW GRAPH
N-1.85



EXPLAIN ANY VARIABLES IN OPERATION
OF WATER SYSTEM THAT WOULD AFFECT
EITHER STATIC PRESSURE OR FLOW
VOLUMES AT A DIFFERENT TIME OF
DAY OR DURING THE YEAR.

APPENDIX B—FIRE-FLOW REQUIREMENTS FOR BUILDINGS

TABLE B105.1(1)
REQUIRED FIRE FLOW FOR ONE- AND TWO-FAMILY DWELLINGS, GROUP R-3 AND R-4 BUILDINGS AND TOWNHOUSES

FIRE-FLOW CALCULATION AREA (square feet)	AUTOMATIC SPRINKLER SYSTEM (Design Standard)	MINIMUM FIRE FLOW (gallons per minute)	FLOW DURATION (hours)
0–3,600	No automatic sprinkler system	1,000	1
3,601 and greater	No automatic sprinkler system	Value in Table B105.1(2)	Duration in Table B105.1(2) at the required fire-flow rate
0–3,600	Section 903.3.1.3 of the <i>International Fire Code</i> or Section P2904 of the <i>International Residential Code</i>	500	1/2
3,601 and greater	Section 903.3.1.3 of the <i>International Fire Code</i> or Section P2904 of the <i>International Residential Code</i>	1/2 value in Table B105.1(2)	1

For SI: 1 square foot = 0.0929 m², 1 gallon per minute = 3.785 L/m.

TABLE B105.1(2)
REFERENCE TABLE FOR TABLES B105.1(1) AND B105.2

FIRE-FLOW CALCULATION AREA (square feet)					FIRE FLOW (gallons per minute) ^b	FLOW DURATION (hours)
Type IA and IB ^a	Type IIA and IIIA ^a	Type IV and V-A ^a	Type IIB and IIIB ^a	Type V-B ^a		
0–22,700	0–12,700	0–8,200	0–5,900	0–3,600	1,500	2
22,701–30,200	12,701–17,000	8,201–10,900	5,901–7,900	3,601–4,800	1,750	
30,201–38,700	17,001–21,800	10,901–12,900	7,901–9,800	4,801–6,200	2,000	
38,701–48,300	21,801–24,200	12,901–17,400	9,801–12,600	6,201–7,700	2,250	
48,301–59,000	24,201–33,200	17,401–21,300	12,601–15,400	7,701–9,400	2,500	
59,001–70,900	33,201–39,700	21,301–25,500	15,401–18,400	9,401–11,300	2,750	
70,901–83,700	39,701–47,100	25,501–30,100	18,401–21,800	11,301–13,400	3,000	3
83,701–97,700	47,101–54,900	30,101–35,200	21,801–25,900	13,401–15,600	3,250	
97,701–112,700	54,901–63,400	35,201–40,600	25,901–29,300	15,601–18,000	3,500	
112,701–128,700	63,401–72,400	40,601–46,400	29,301–33,500	18,001–20,600	3,750	
128,701–145,900	72,401–82,100	46,401–52,500	33,501–37,900	20,601–23,300	4,000	4
145,901–164,200	82,101–92,400	52,501–59,100	37,901–42,700	23,301–26,300	4,250	
164,201–183,400	92,401–103,100	59,101–66,000	42,701–47,700	26,301–29,300	4,500	
183,401–203,700	103,101–114,600	66,001–73,300	47,701–53,000	29,301–32,600	4,750	
203,701–225,200	114,601–126,700	73,301–81,100	53,001–58,600	32,601–36,000	5,000	
225,201–247,700	126,701–139,400	81,101–89,200	58,601–65,400	36,001–39,600	5,250	
247,701–271,200	139,401–152,600	89,201–97,700	65,401–70,600	39,601–43,400	5,500	
271,201–295,900	152,601–166,500	97,701–106,500	70,601–77,000	43,401–47,400	5,750	
295,901–Greater	166,501–Greater	106,501–115,800	77,001–83,700	47,401–51,500	6,000	
—	—	115,801–125,500	83,701–90,600	51,501–55,700	6,250	
—	—	125,501–135,500	90,601–97,900	55,701–60,200	6,500	
—	—	135,501–145,800	97,901–106,800	60,201–64,800	6,750	
—	—	145,801–156,700	106,801–113,200	64,801–69,600	7,000	
—	—	156,701–167,900	113,201–121,300	69,601–74,600	7,250	
—	—	167,901–179,400	121,301–129,600	74,601–79,800	7,500	
—	—	179,401–191,400	129,601–138,300	79,801–85,100	7,750	
—	—	191,401–Greater	138,301–Greater	85,101–Greater	8,000	

For SI: 1 square foot = 0.0929 m², 1 gallon per minute = 3.785 L/m, 1 pound per square inch = 6.895 kPa.

a. Types of construction are based on the *International Building Code*.

b. Measured at 20 psi residual pressure.

APPENDIX B-2

2021 INTERNATIONAL FIRE CODE®

APPENDIX B—FIRE-FLOW REQUIREMENTS FOR BUILDINGS

TABLE B105.2
REQUIRED FIRE FLOW FOR BUILDINGS OTHER THAN ONE- AND
TWO-FAMILY DWELLINGS, GROUP R-3 AND R-4 BUILDINGS AND TOWNHOUSES

AUTOMATIC SPRINKLER SYSTEM (Design Standard)	MINIMUM FIRE FLOW (gallons per minute)	FLOW DURATION (hours)
No automatic sprinkler system	Value in Table B105.1(2)	Duration in Table B105.1(2)
Section 903.3.1.1 of the <i>International Fire Code</i>	25% of the value in Table B105.1(2) ^a	Duration in Table B105.1(2) at the reduced flow rate
Section 903.3.1.2 of the <i>International Fire Code</i>	25% of the value in Table B105.1(2) ^b	Duration in Table B105.1(2) at the reduced flow rate

For SI: 1 gallon per minute = 3.785 L/m.

a. The reduced fire flow shall be not less than 1,000 gallons per minute.

b. The reduced fire flow shall be not less than 1,500 gallons per minute.

SECTION B106 REFERENCED STANDARDS

B106.1 General. See Table B106.1 for standards that are referenced in various sections of this appendix. Standards are listed by the standard identification with the effective date, standard title, and the section or sections of this appendix that reference the standard.

TABLE B106.1
REFERENCED STANDARDS

STANDARD ACRONYM	STANDARD NAME	SECTIONS HEREIN REFERENCED
IBC—21	<i>International Building Code</i>	B104.2
IRC—21	<i>International Residential Code</i>	Table B105.1(1)
IWUIC—21	<i>International Wildland-Urban Interface Code</i>	B103.3
NFPA 1142—17	<i>Standard on Water Supplies for Suburban and Rural Fire Fighting</i>	B103.3

WYOMING CLASSICAL ACADEMY

6389 POISON SPIDER LANE

MILLS, WYOMING 82604



PROJECT DIRECTORY

PROJECT	OWNER	ARCHITECT
WYOMING CLASSICAL ACADEMY	WYOMING CLASSICAL ACADEMY	WYOMING CLASSICAL ACADEMY
6389 POISON SPIDER LANE	6389 POISON SPIDER LANE	6389 POISON SPIDER LANE
MILLS, WYOMING 82604	MILLS, WYOMING 82604	MILLS, WYOMING 82604
PROJECT NO. 1000000000	PROJECT NO. 1000000000	PROJECT NO. 1000000000

DEFERRED SUBMITTALS & SPECIAL INSPECTIONS

1. SPECIAL INSPECTIONS SHALL BE PROVIDED BY THE ARCHITECT. THE ARCHITECT SHALL BE RESPONSIBLE FOR THE SPECIAL INSPECTIONS. THE ARCHITECT SHALL BE RESPONSIBLE FOR THE SPECIAL INSPECTIONS. THE ARCHITECT SHALL BE RESPONSIBLE FOR THE SPECIAL INSPECTIONS.

SHEET INDEX

NO.	DESCRIPTION	DATE
001	COVER SHEET	01/15/2020
002	GENERAL NOTES	01/15/2020
003	FOUNDATION	01/15/2020
004	FIRST FLOOR	01/15/2020
005	SECOND FLOOR	01/15/2020
006	THIRD FLOOR	01/15/2020
007	MECHANICAL	01/15/2020
008	ELECTRICAL	01/15/2020
009	PLUMBING	01/15/2020
010	PAINTING	01/15/2020
011	LANDSCAPE	01/15/2020
012	EXTERIOR	01/15/2020
013	INTERIOR	01/15/2020
014	MECHANICAL	01/15/2020
015	ELECTRICAL	01/15/2020
016	PLUMBING	01/15/2020
017	PAINTING	01/15/2020
018	LANDSCAPE	01/15/2020
019	EXTERIOR	01/15/2020
020	INTERIOR	01/15/2020
021	MECHANICAL	01/15/2020
022	ELECTRICAL	01/15/2020
023	PLUMBING	01/15/2020
024	PAINTING	01/15/2020
025	LANDSCAPE	01/15/2020
026	EXTERIOR	01/15/2020
027	INTERIOR	01/15/2020
028	MECHANICAL	01/15/2020
029	ELECTRICAL	01/15/2020
030	PLUMBING	01/15/2020
031	PAINTING	01/15/2020
032	LANDSCAPE	01/15/2020
033	EXTERIOR	01/15/2020
034	INTERIOR	01/15/2020
035	MECHANICAL	01/15/2020
036	ELECTRICAL	01/15/2020
037	PLUMBING	01/15/2020
038	PAINTING	01/15/2020
039	LANDSCAPE	01/15/2020
040	EXTERIOR	01/15/2020
041	INTERIOR	01/15/2020
042	MECHANICAL	01/15/2020
043	ELECTRICAL	01/15/2020
044	PLUMBING	01/15/2020
045	PAINTING	01/15/2020
046	LANDSCAPE	01/15/2020
047	EXTERIOR	01/15/2020
048	INTERIOR	01/15/2020
049	MECHANICAL	01/15/2020
050	ELECTRICAL	01/15/2020
051	PLUMBING	01/15/2020
052	PAINTING	01/15/2020
053	LANDSCAPE	01/15/2020
054	EXTERIOR	01/15/2020
055	INTERIOR	01/15/2020
056	MECHANICAL	01/15/2020
057	ELECTRICAL	01/15/2020
058	PLUMBING	01/15/2020
059	PAINTING	01/15/2020
060	LANDSCAPE	01/15/2020
061	EXTERIOR	01/15/2020
062	INTERIOR	01/15/2020
063	MECHANICAL	01/15/2020
064	ELECTRICAL	01/15/2020
065	PLUMBING	01/15/2020
066	PAINTING	01/15/2020
067	LANDSCAPE	01/15/2020
068	EXTERIOR	01/15/2020
069	INTERIOR	01/15/2020
070	MECHANICAL	01/15/2020
071	ELECTRICAL	01/15/2020
072	PLUMBING	01/15/2020
073	PAINTING	01/15/2020
074	LANDSCAPE	01/15/2020
075	EXTERIOR	01/15/2020
076	INTERIOR	01/15/2020
077	MECHANICAL	01/15/2020
078	ELECTRICAL	01/15/2020
079	PLUMBING	01/15/2020
080	PAINTING	01/15/2020
081	LANDSCAPE	01/15/2020
082	EXTERIOR	01/15/2020
083	INTERIOR	01/15/2020
084	MECHANICAL	01/15/2020
085	ELECTRICAL	01/15/2020
086	PLUMBING	01/15/2020
087	PAINTING	01/15/2020
088	LANDSCAPE	01/15/2020
089	EXTERIOR	01/15/2020
090	INTERIOR	01/15/2020
091	MECHANICAL	01/15/2020
092	ELECTRICAL	01/15/2020
093	PLUMBING	01/15/2020
094	PAINTING	01/15/2020
095	LANDSCAPE	01/15/2020
096	EXTERIOR	01/15/2020
097	INTERIOR	01/15/2020
098	MECHANICAL	01/15/2020
099	ELECTRICAL	01/15/2020
100	PLUMBING	01/15/2020

WYOMING CLASSICAL ACADEMY
6389 POISON SPIDER LANE
MILLS, WYOMING 82604

SILVERPEAK
ENGINEERING



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STRUCTURAL CIVIL SURVEY WWW.SILVERPEAKENG.COM

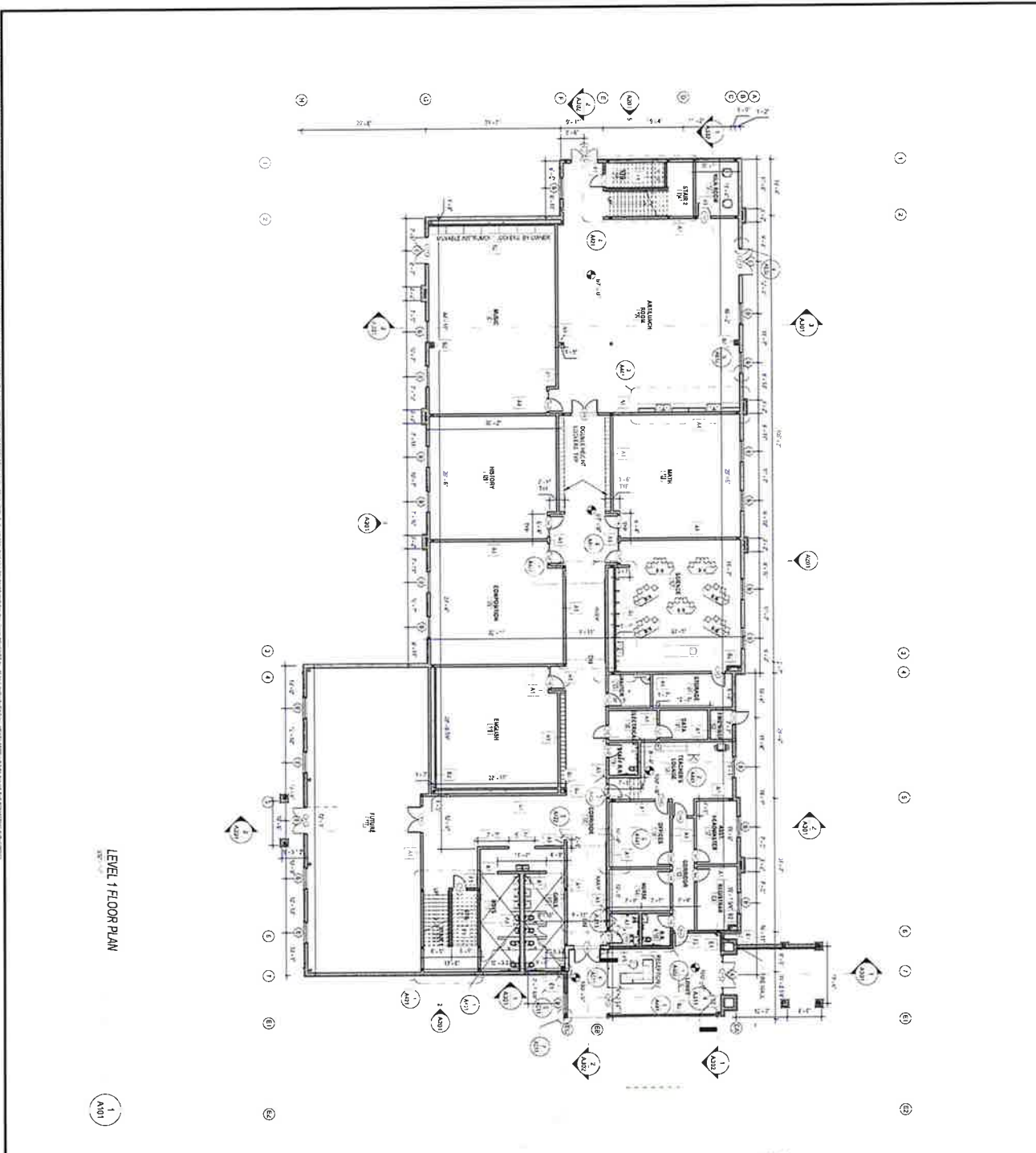
SHEET NUMBER
G001

COVER SHEET



DATE: 01/15/2020
DRAWN BY: [Signature]
CHECKED BY: [Signature]

WYOMING CLASSICAL ACADEMY, 6389 POISON SPIDER LANE, MILLS, WYOMING 82604. PROJECT NO. 1000000000. SHEET NO. G001. DATE: 01/15/2020. DRAWN BY: [Signature]. CHECKED BY: [Signature].



LEVEL 1 FLOOR PLAN

1
ANSI

BUILDING AREA - PHASE 1	
DATE: 10/10/10	10/10/10
PROJECT: 10/10/10	10/10/10
DESIGNER: 10/10/10	10/10/10
CONTRACTOR: 10/10/10	10/10/10

BUILDING AREA - PHASE 2	
DATE: 10/10/10	10/10/10
PROJECT: 10/10/10	10/10/10
DESIGNER: 10/10/10	10/10/10
CONTRACTOR: 10/10/10	10/10/10

GENERAL NOTES

1. ALL WORK SHALL BE IN ACCORDANCE WITH THE LATEST EDITIONS OF THE WYOMING BUILDING CODE AND ALL APPLICABLE LOCAL ORDINANCES.
2. THE DESIGNER HAS CONDUCTED VISUAL GENERAL VERIFICATION OF THE EXISTING CONDITIONS AND HAS NOT CONDUCTED A DETAILED SURVEY OF THE EXISTING CONDITIONS.
3. THE DESIGNER HAS CONDUCTED VISUAL GENERAL VERIFICATION OF THE EXISTING CONDITIONS AND HAS NOT CONDUCTED A DETAILED SURVEY OF THE EXISTING CONDITIONS.
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9. THE DESIGNER HAS CONDUCTED VISUAL GENERAL VERIFICATION OF THE EXISTING CONDITIONS AND HAS NOT CONDUCTED A DETAILED SURVEY OF THE EXISTING CONDITIONS.
10. THE DESIGNER HAS CONDUCTED VISUAL GENERAL VERIFICATION OF THE EXISTING CONDITIONS AND HAS NOT CONDUCTED A DETAILED SURVEY OF THE EXISTING CONDITIONS.

FLOOR PLAN LEGEND

SYMBOL	DESCRIPTION
	WALL - 1/2" THICK CONCRETE
	DOOR - 1/2" THICK CONCRETE
	WINDOW - 1/2" THICK CONCRETE

WYOMING CLASSICAL ACADEMY
 6389 POISON SPIDER LANE
 MILLS, WYOMING 82604



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STRUCTURAL CIVIL SURVEY WWW.SILVERPEAKENG.COM

DATE: 10/10/10

PROJECT: 10/10/10

DESIGNER: 10/10/10

CONTRACTOR: 10/10/10

10/10/10

10/10/10

10/10/10

10/10/10

LEVEL 1 FLOOR PLAN

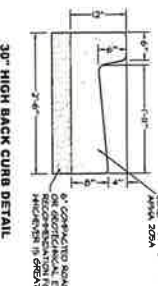
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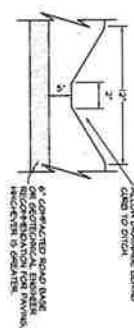
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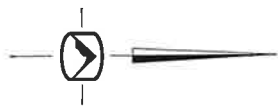
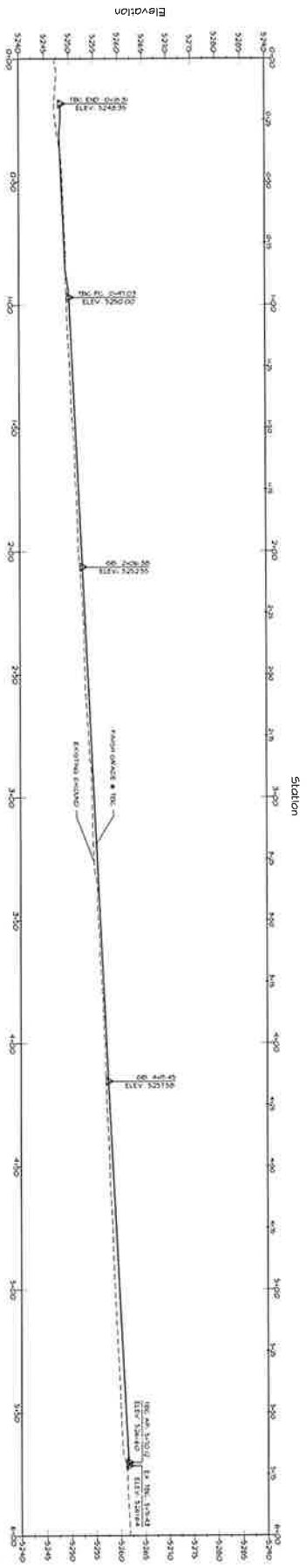


POISON SPIDER LANE IMPROVEMENTS



TYPICAL CURB CUT DETAIL
NOT TO SCALE

DEVELOPMENT NOTE: THE PLANNED 6TH / 7TH FLOOR ADDITION, TRACK, FIELD, BLEACHERS, AND CONCESSIONS ARE FUTURE PHASES SUBJECT TO SEPARATE CITY OF MILLS APPROVAL

[illegible]**POISON SPIDER LANE
IMPROVEMENT PLAN**

SHEET NUMBER
C500

WYOMING CLASSICAL ACADEMY
6389 POISON SPIDER LN
MILLS, WYOMING

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WYOMING CLASSICAL ACADEMY



ALIVE DIFFERENCE FROM THE STOOD SYSTEM



MAINTENANCE: REMOVE A CLEAN CARPET LOS DEDUCTIBLY EACH WEEK OR AFTER A STORM THAT CAUSE MAJOR WEAR. STOPS IN PREVENT STAINING

I USE 1/2" BALL BEARING BALL TO PROTECT THE CATCH BEAM IN
SEPARATION.



NOTES

2. TAPED FROM VERTICAL AND SURFACE SOUNDS, PICKED UP, AND DISPOSED OF PROPERLY.



- 1.
- Working in Robert Smith of audience and other artists in 1970-75 and*

INSPECTION AND MAINTENANCE SHALL BEGIN WITH THE INSTALLATION OF THE FIRST BAR AND CONTINUE UNTIL THE

- SELDING AND PARTNER SHALL BE CONSIDERED COMPLETE WHEN TWO OF PARTNERS ARE ESTABLISHED

A. PROHIBITION ON MOST NON-STORM WATER DISCHARGES

STIMULATION FACTORS' (TAP'S)

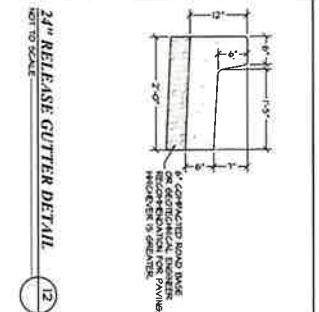
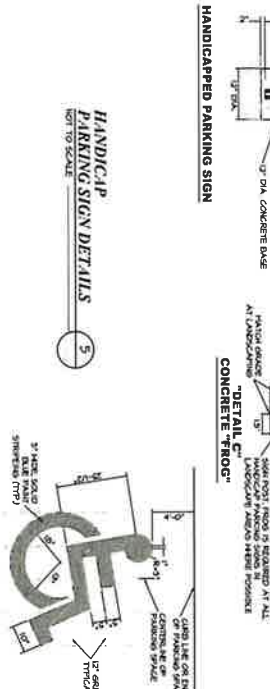
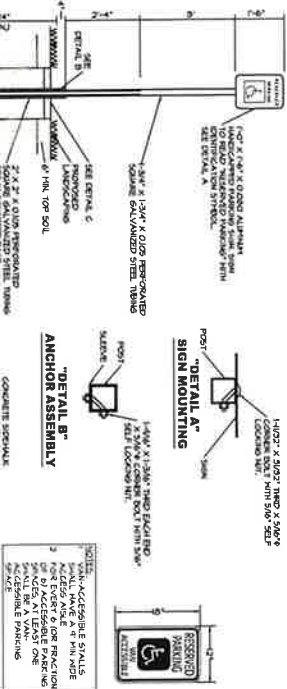
1. *Pharmaceutical industry*



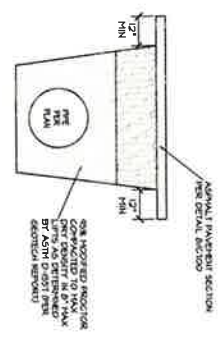
CUT/DPD A/OTES



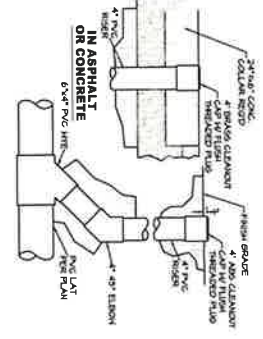
ANT CONSTRUCTION



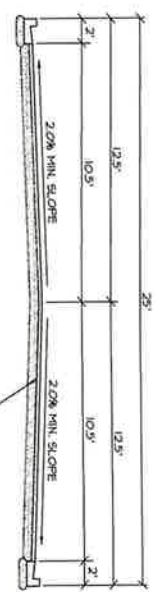
6" CONCRETE BASE
12" CONCRETE BLOCK
1" BRICK VENEER



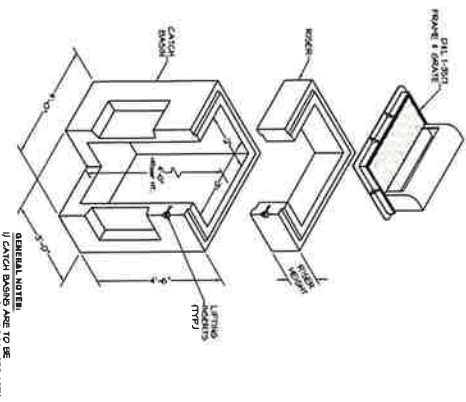
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NOT TO SCALE



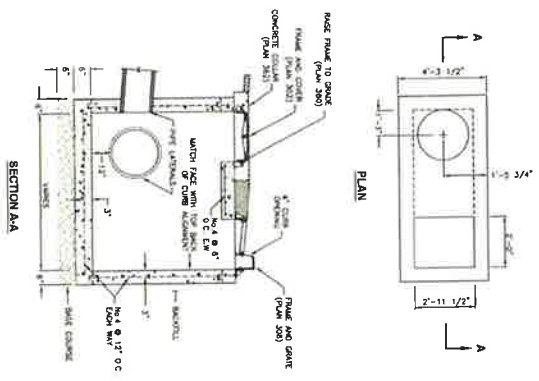
SANITARY SEWER CLEANOUT
NOT TO SCALE



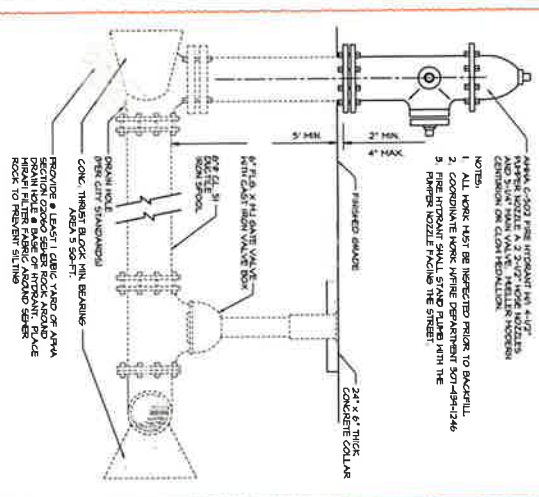
SOUTH DRIVE LANE X-SECTION
NOT TO SCALE



STORM DRAIN CATCH BASIN (SDCB)
NOT TO SCALE



STORM DRAIN CONDUIT BOX
NOT TO SCALE



FIRE HYDRANT ASSEMBLY
NOT TO SCALE

SITE PLAN CHECKLIST

1. LEGAL DESCRIPTION, SEE VACATION AND REPLY OF LOT 1A MOUNTAIN
2. TITLE BLOCK, AS SHOWN
3. NAMES OF ALL ADJACENT PROPERTIES, SEE VACATION AND REPLY OF LOT 1A
4. SURROUNDING LAND USE, (RESIDENTIAL, URBAN, AG, LIGHT INDUSTRIAL)
5. ZONING, AS SHOWN
6. NORTH ARROW, PLAN SCALE AND DATE, AS SHOWN
7. LOT DIMENSIONS, AS SHOWN
8. LOCATION AND DIMENSIONS OF ALL PROPOSED OFF-STREET LOADING DOCK AREAS, AS SHOWN
9. ADVERTISING AND SIGN, AS SHOWN
10. ADVERTISING AND SIGN, AS SHOWN
11. ADVERTISING AND SIGN, AS SHOWN
12. ADVERTISING AND SIGN, AS SHOWN
13. ADVERTISING AND SIGN, AS SHOWN
14. ADVERTISING AND SIGN, AS SHOWN
15. EXISTING AND PROPOSED CURB CUTS AND SIDEWALKS, SEE SITE PLANS
16. EXISTING AND PROPOSED DRIVEWAYS AND SIDEWALKS, SEE SITE PLANS
17. CURBING LOCATION, SEE SITE PLANS
18. EXISTING AND PROPOSED DRIVEWAYS AND SIDEWALKS, SEE SITE PLANS
19. EXISTING AND PROPOSED DRIVEWAYS AND SIDEWALKS, SEE SITE PLANS
20. VIOLET MAP, AS SHOWN
21. GENERAL NOTES, AS SHOWN
22. BUILDING ADDITION, AS SHOWN
23. BUILDING ADDITION, AS SHOWN
24. BUILDING ADDITION, AS SHOWN
25. BUILDING ADDITION, AS SHOWN
26. BUILDING ADDITION, AS SHOWN
27. BUILDING ADDITION, AS SHOWN

