

PRELIMINARY STORM WATER MANAGEMENT CALCULATIONS
FOR
1220 10th STREET

Lake Park, Florida
MMA #24-004

May 22, 2024
Revised:
N/A

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5/22/2024

Date

PRELIMINARY STORM WATER MANAGEMENT CALCULATIONS

Project Name: 1220 10th STREET
Project #: MMA #24-004

Engineer: TNM

Date: 05/22/24

Revised: N/A

LAND USE BREAKDOWN

EXISTING

Site Area = 2.74 ac

Basin Area = 2.74 ac

	Acres	%	Grading	
			From	To
Impervious Area				
Existing Building	0.46 ac	(17%)	13.18	
Pavement & Concrete	1.20 ac	(44%)	10.70	13.00
Pervious Area				
Green Space	1.08 ac	(39%)	10.50	14.00
Subtotal Impervious Areas	1.66 ac	(61%)		
Subtotal Pervious Areas	1.08 ac	(39%)		

Find Curve Number:

Avg. Pervious Ground El. = 12.25

Control Elevation = 7.00

Depth to Water Table = 5.25

Soil Type = Coastal

Soil Storage Table

(SFWMD's Vol. IV, Basis of Review, page E-2)

Depth to W.T. (ft)	Coastal Storage (in)	Flatwoods Storage (in)	Depression Storage (in)
1.0	0.6	0.6	0.6
2.0	2.5	2.5	2.1
3.0	6.6	5.4	4.4
4.0	10.9	9.0	6.8

Pervious Area = 1.08 ac

Storage from Table = 8.18 in (w/ 25% compaction)

Available Soil Storage = 0.74 af

Soil Moisture Storage (S) = 3.22 in

Curve Number = 76

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LAND USE BREAKDOWN

PROPOSED

Site Area = **2.74 ac**

Basin Area = **2.74 ac**

	Acres	%	Grading	
			From	To
Impervious Area				
Building	0.66 ac	(24%)	13.20	
Pavement	1.10 ac	(40%)	10.70	13.00
Pervious Area				
Green Space	0.92 ac	(34%)	10.50	14.00
Dry Retention Bottom	0.02 ac	(1%)	8.50	
Retention Banks	0.04 ac	(1%)	8.50	11.50
Subtotal Impervious Areas	1.76 ac	(64%)		
Subtotal Pervious Areas	0.98 ac	(36%)		

Find Curve Number:

Avg. Pervious Ground El. = 12.08
 Control EL. = **7.00**
 Depth to Water Table = **5.08**
 Soil Type = Coastal

Soil Storage Table

(SFWMMD's Vol. IV, Basis of Review, page E-2)

Depth to W.T. (ft)	Coastal Storage (in)	Flatwoods Storage (in)	Depression Storage (in)
1.0	0.6	0.6	0.6
2.0	2.5	2.5	2.1
3.0	6.6	5.4	4.4
4.0	10.9	9.0	6.8

Pervious Area = 0.98 ac
 Storage from Table = **8.18 in** (w/ 25% compaction)
 Avail Soil Storage = 0.67 af
 Soil Moisture Storage (S) = **2.92 in**
 Curve Number = **77**

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STAGE -STORAGE CALCULATIONS

PROPOSED

Starting Stage	7.00
Ending Stage	13.50
Stage Increment	0.50

Name	Pavement	Green Space	Dry Retention Bottom	Retention Banks	Trench	
Area	1.10	0.92	0.02	0.04	0.21 (AF)	
Start Elev	10.70	10.50	8.50	8.50	7.00	
End Elev	13.00	14.00	0.00	11.50	10.50	
Stage Feet	Linear Storage	Linear Storage	Vert Storage	Linear Storage	Linear Storage	Total Storage
NAVD	Ac-ft	Ac-ft	Ac-ft	Ac-ft	Ac-ft	Ac-ft
7.00	0.00	0.00	0.00	0.00	0.00	0.00
7.50	0.00	0.00	0.00	0.00	0.03	0.03
8.00	0.00	0.00	0.00	0.00	0.06	0.06
8.50	0.00	0.00	0.00	0.00	0.09	0.09
9.00	0.00	0.00	0.01	0.00	0.12	0.13
9.50	0.00	0.00	0.02	0.01	0.15	0.18
10.00	0.00	0.00	0.03	0.02	0.18	0.23
10.50	0.00	0.00	0.04	0.03	0.21	0.28
11.00	0.02	0.03	0.05	0.04	0.21	0.36
11.50	0.15	0.13	0.06	0.06	0.21	0.61
12.00	0.40	0.30	0.07	0.08	0.21	1.06
12.50	0.77	0.53	0.08	0.10	0.21	1.69
13.00	1.27	0.82	0.09	0.12	0.21	2.51
13.50	1.82	1.18	0.10	0.14	0.21	3.45

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RUNOFF (ZERO DISCHARGE) CALCULATIONS

Soil Moisture Storage (S_{exist})	3.22 in
Soil Moisture Storage (S_{prop})	2.92 in

25 Year, 3 Day Rainfall Amount (P):	13.0 in	Figure C-8
100 Year, 3 Day Rainfall Amount (P):	15.5 in	Figure C-9

PRE/POST RUNOFF: 25-YEAR, 3-DAY RUNOFF CALCULATIONS:

Existing:

$$Q = (P - (0.2XS))^2 / (P + (0.8 \cdot S))$$

$$= 9.8 \text{ in}$$

$$\text{Volume} = Q \times \text{Site Area} \times 1\frac{1}{12}"$$

$$= 9.8 \text{ in} \times 2.74 \times 1\frac{1}{12}" = 2.24 \text{ AF}$$

Proposed:

$$Q = (P - (0.2XS))^2 / (P + (0.8 \cdot S))$$

$$= 10.0 \text{ in}$$

$$\text{Volume} = Q \times \text{Site Area} \times 1\frac{1}{12}"$$

$$= 10.0 \text{ in} \times 2.74 \times 1\frac{1}{12}" = 2.29 \text{ AF}$$

Pre- vs. Post- = **0.06 AF** of storage required
0.33 AF Provided at Elev. **11.5** Ft NAVD

FINISHED FLOORS: 100-YEAR, 3-DAY RUNOFF CALCULATIONS:

Proposed:

$$Q = (P - (0.2XS))^2 / (P + (0.8 \cdot S))$$

$$= 12.5 \text{ in}$$

$$\text{Volume} = Q \times \text{Site Area} \times 1\frac{1}{12}"$$

$$= 12.5 \text{ in} \times 2.74 \times 1\frac{1}{12}" = 2.85 \text{ AF}$$

2.90 AF Provided at Elev. **13.20** Ft NAVD

Storm Event	Rainfall (in)	Peak Stage (ft-NAVD)	Peak Discharge (cfs)	Design Criteria	Prop Stage (ft-NAVD)
25-yr, 3-day =	13.0	12.85	N/A	Allowable Discharge / Pre vs. Post	N/A
100-yr, 3-day =	15.5	13.15	n/a	Finished Floors	13.20

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WATER QUALITY CALCULATIONS

1-inch Over the Project Area

$$\begin{array}{ccccccc} \text{(Treated Volume)} & 1\text{-inch} & * & 1\text{-ft/12-in} & * & \frac{2.74}{\text{PROJECT AREA (AC)}} & = \frac{0.23}{\text{TREATED VOLUME}} \text{ ac-ft} \end{array}$$

2.5-inches Times the Percent Impervious

$$\begin{array}{l} \text{(Site Area)} \quad \frac{2.74}{\text{PROJECT AREA (AC)}} - \left(\frac{0.00}{\text{LAKES (AC)}} + \frac{0.66}{\text{ROOFS (AC)}} \right) = \frac{2.08}{\text{SITE AREA}} \text{ ac} \\ \\ \text{(Impervious Area)} \quad \frac{2.08}{\text{SITE AREA (AC)}} - \frac{0.98}{\text{PERVIOUS AREA (AC)}} = \frac{1.10}{\text{IMPERVIOUS AREA}} \text{ ac} \\ \\ \text{(\% Impervious)} \quad \frac{\text{IMPERVIOUS AREA} * 100\%}{\text{SITE AREA (AC)}} = \frac{52.88\%}{\text{SITE AREA (AC)}} \\ \\ \text{(2.5-in * \% Imp.)} \quad 2.5\text{-inches} * \frac{52.88\%}{\text{PERCENT IMPERVIOUS}} = \frac{1.32}{\text{INCHES TO BE TREATED}} \text{ in} \\ \\ \text{(Treated Volume)} \quad \frac{1.32}{\text{TREATED (IN)}} * 1\text{-ft/12-in} * \frac{2.74}{\text{PROJECT AREA - LAKES (AC)}} = \frac{0.31}{\text{TREATED VOLUME}} \text{ ac-ft} \end{array}$$

THEREFORE 2.5-INCHES X %IMP GOVERNS

$$\text{Required WQ Treatment} = 0.31 \text{ ac-ft}$$

$$\text{Provided WQ Treatment (Via Exfil Trench \& Retention @ EL. 11.5)} = 0.33 \text{ ac-ft}$$

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EXFILTRATION TRENCH DESIGN: ONSITE

(All elevations shown in NAVD 1988 datum)

Minimum Ground Elevation = 12.00

Weir Elevation = 11.50

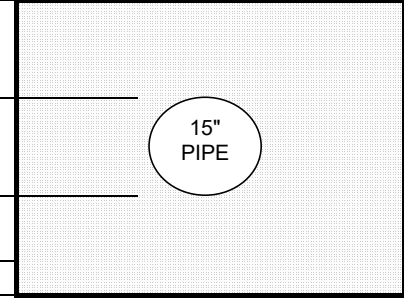
Trench Top Elevation = 10.50

Pipe Overt Elevation = 9.25

Pipe Invert Elevation = 8.00

CWE (Per Soils Report) = 7.00 ▽

Trench Bottom Elevation = 7.00



Standard Formula

$$V = L \cdot (K(H_2 \cdot W + 2 \cdot H_2 \cdot Du - Du^2 + 2 \cdot H_2 \cdot Ds) + (1.39 \cdot 10^{-4}) \cdot W \cdot Du)$$

<=== INPUT ONLY IN GRAY CELLS

L _{WQ}	Length of Trench Provided for Water Quality	190
W	Trench Width (feet)	6
K	Hydraulic Conductivity (cfs/ft ² -ft.head)	2.24E-04
H ₂	Depth to Water Table (feet)	4.5
Du	Non Saturated Trench Depth (feet)	3.5
Ds	Saturated Trench Depth (feet)	0

V_{WQ} Volume Treated (acre-in) 2.52

V_{WQ} Volume Treated (acre-ft) 0.21