# **Traffic Analysis**

FOR:

## 3 Tees, LLC

### **Horse Creek Quarry**

## **Commercial Entrance**

LOCATED ON:

3725 Sullivan Gardens Parkway

SULLIVAN COUNTY, TENNESSEE

DESIGNED BY:

Stephen E. Maxfield 1745 Roman Ridge Road Honaker, VA, 24260

March 23, 2024

#### **Executive Summary**

A commercial entrance has been designed for the proposed quarry at 3725 Sullivan Gardens Parkway, Kingsport Tennessee in accordance with American Association of State Highway and Transportation Officials (AASHTO) Policy on Geometric Design of Highways and Streets (Green Book) based on site conditions and a traffic analysis. No deceleration or acceleration lanes are proposed. Entrance shall accommodate WB-62 type trucks.

#### **Proposed Location**

The proposed location is at 3725 Sullivan Gardens Parkway (Route 93) between Regional Park Drive and Rock Springs Road. This entrance is approximately 1.8 miles South of Interstate 26. The purpose of this entrance is to provide access to the proposed 3 Tees, LLC Horse Creek Quarry.

#### Topography

Route 93 is an undivided five (5) lane Principal Urban Arterial Route, with a continuous center turn lane. The new commercial entrance will be a two (2) lane entrance leading into a rock quarry. The surrounding land use is primarily a combination of residential and farmland. In the vicinity of the proposed entrance, the Route 93 profile is nearly level, with no grades over 1% or crests or sags from vertical curves.

#### **Site Drainage**

There are no drainage structures within TDOT R.O.W. The entrance will be graded to direct the drainage away from Route 93. Therefore, the post development run-off on TDOT R.O.W. is less than or equal to the pre-development run-off.

#### **Sight Distance**

As noted above in the Topography Section, Route 93 is an undivided 5-lane highway, with a dedicated turn lane. In the location of the proposed entrance the road is nearly level and straight with no sags or crests. The sight distances were measured in accordance with the AASHTO criteria for eye level height, object height, and measuring location. All aspects of

sight distance at this location are well within the design criteria of the AASHTO Manual. The sight distances are summarized in the table below:

| Aspect             | Speed Limit | Grade      | Sight Distance | Min. Req'd |
|--------------------|-------------|------------|----------------|------------|
| Stopping Westbound | 45 mph      | 0.4 % up   | >1,000 ft      | 360 ft     |
| Stopping Eastbound | 45 mph      | 0.0 %      | 580 ft         | 360ft      |
| Left               | 45 mph      | 0.0 %      | 580 ft         | 565 ft     |
| Right              | 45 mph      | 0.4 % down | >1,000 ft      | 600 ft     |

The entrance is designed to accommodate WB-62 trucks; however, the majority of vehicles on Route 92 are passenger vehicles that must react to vehicles using the entrance. Therefore, minimum requirements are for passenger vehicles.

#### **Vehicle Volume**

Vehicle volumes for this section of Route 93 were acquired from 2023 Tennessee Department of Transportation (TDOT) Traffic Count Database System (TCDS). TDOT continuously collects traffic information on Tennessee's roadways as part of the Department's responsibility to monitor, collect, analyze, manage, and disseminate transportation data. Traffic data includes volume counts, vehicle classification counts, and speed data (see attached Appendix B). Annual Average Daily Traffic (AADT) volume is used throughout the Long-Range Planning process. TDOT collects Average Daily Traffic (ADT), which is based on a 24hour count. This information is transformed in AADT by using the raw traffic data, which is statistically corrected by a seasonal variation factor that considers time of year and day of the week, as well as adjustments for vehicle type, determined by seasonal and axle correction factors. The peak hour volume (PHV) was determined as follows: (AADT) x (K) x (Direction Factor); where, K is a factor is based on the 30th highest hour of the year and is used to compute design hour volumes. Directional factors (D-factor) are measures of the peak hour directionality. They are based on the average weekday peak hour.

PHV =  $(13,614) \times (0.10) \times (0.59) = 803 \text{ vpd} \div 8 \text{ hrs} \approx 100 \text{ vehicles per hour.}$ 

This value was used for traffic in both directions as worst case scenario for designing the entrance.

#### Vehicular Speeds

The Posted Speed Limit at this location on Route 93 is 45 MPH.

#### **Types of Vehicles**

The type of vehicle used for the worst case design would be a WB-62 Truck.

#### **Entrance Geometry**

The entrance has been designed to accommodate the WB-62 Truck. This is an Interstate Semi type truck. This is not the typical truck in and out of a quarry but would be an infrequent basis such as special shipment or delivery. The entrance design is a 3 centered compound curve, with radii of 200 ft, 50 ft, and 600 ft. from the AASHTO Design Manual. This design ensures that the path of the outer front wheel and the inner rear wheel of the vehicle are maintained in the designated paved lane.

#### **Pedestrian Movements**

No crosswalks are present at the proposed entrance location. Due to the nature of the entrance, few pedestrians are anticipated.

#### **Trip Generation**

The traffic generation of the proposed entrance was determined by assuming production/sales = 200,000 tpy or 770 tpd and 20 tons per truck; 770/20=39 trucks per day + employees, salesmans, etc. say 55 vpd. A maximum of 55 vehicles per day was determined. A total of 22 vehicles per peak hour were determined by the following: If all truck drivers and quarry employees were to arrive at the same time for work that day as well as any additional deliveries that may come in for that day, then that should be a maximum of 40% of the total daily vehicle trips; thus,  $(0.4) \times (55) = 22$ . Table 2 summarizes the estimated peak hour generation based on the proposed development.

Since 22 vph is the peak amount, and Interstate 26 is 1.8 miles north and Interstate 81 is 6.6 miles south, it is assumed that there are 80% of vehicles turning left into site and 20% turning right into site. Similarly, egress traffic will be 80% right turn onto 93 and 20% left onto 93.

| Table 2                     |               |         |  |  |  |  |  |  |
|-----------------------------|---------------|---------|--|--|--|--|--|--|
| Trip Generation Volumes for |               |         |  |  |  |  |  |  |
| the Proposed Entrance       |               |         |  |  |  |  |  |  |
| Parking Spaces              | Ample Parking |         |  |  |  |  |  |  |
| Period                      | Entering      | Exiting |  |  |  |  |  |  |
| Peak                        | 22            | 22      |  |  |  |  |  |  |
| Daily Total                 | 55            | 55      |  |  |  |  |  |  |

Highway 93, being a 5-lane undivided highway with a dedicated continuous center turn lane, no improvements will be necessary for traffic turning left into the quarry. As noted above, an estimated 20% of the traffic volume will turn right into the quarry. At the peak volume this would be 5 vph (20% of 22). According to AASHTO Design Manual, no left turn lanes or tapers are required (see attached Appendix). The entrance is proposed to be constructed to provide adequate site distance in both directions (+500 left and +1000 right).

#### Conclusion

The proposed commercial entrance will have a use of 55 vpd and have a peak hour volume of 22 vph, and will not require a right or left turn lane. There is adequate sight distance in both directions and an entrance geometry is proposed for larger trucks than will use the entrance.

PREPARED BY:

Stephen E. Maxfield, P. E. March 23, 2024

Start Africa

| Location ID    | 82000102                                | MPO ID      |       |
|----------------|---|-------------|-------|
| Туре           | SPOT                                    | HPMS ID     |       |
| On NHS         | Yes                                     | On HPMS     |       |
| LRS ID         | 82SR093001                              | LRS Loc Pt. | 5.961 |
| SF Group       | Urban Principal Arterial                | Route Type  |       |
| AF Group       | Region 1 Urban Other Principal Arterial | Route       |       |
| GF Group       | Sullivan                                | Active      | Yes   |
| Class Dist Grp | Region 1 Urban Other Principal Arterial | Category    | CC    |
| Seas Clss Grp  |   |             |       |
| WIM Group      |   |             | A     |
| QC Group       | Default                                 |             |       |
| Fnct'l Class   | Other Principal Arterial                | Milepost    |       |
| Located On     | SR093                                   |             |       |
| Loc On Alias   | SULLIVAN GARDENS PKWY.                  |             |       |
|                | S OF KINGSPORT                          |             |       |
| More Detail    |   |             |       |

### Directions: 2-WAY NB SB

| Year | AADT                 | DHV-30 | K % | D % | PA           | BC         | Src |
|------|----------------------|--------|-----|-----|--------------|------------|-----|
| 2023 | 13,614 <sup>12</sup> |        | 10  | 59  | 12,919 (95%) | 695 (5%)   |     |
| 2022 | 12,822 <sup>7</sup>  |        | 10  | 59  | 12,193 (95%) | 629 (5%)   |     |
| 2021 | 13,034               | 1,345  | 10  | 59  | 12,292 (94%) | 742 (6%)   |     |
| 2020 | 12,057               | 1,246  | 10  | 56  | 10,995 (91%) | 1,062 (9%) |     |
| 2019 | 12,898               |        | 11  | 56  |              |            |     |

| Travel Demand Model |               |               |        |        |        |        |        |        |        |        |  |
|---------------------|---------------|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--|
|                     | Model<br>Year | Model<br>AADT | AM PHV | AM PPV | MD PHV | MD PPV | PM PHV | PM PPV | NT PHV | NT PPV |  |

Stopping sight distances exceeding those shown in the table below should be used as basis for design wherever practical.

In computing and measuring stopping sight distances, the height of the driverce eye is estimated to be 3.5 feet and the height of the object to be seen by the driver is 2 feet, equivalent to the taillight height of a passenger car. The % Values+ shown are a coefficient by which the algebraic difference in grade may be multiplied to determine the length in feet of the vertical curve that will provide minimum sight distance. Crest vertical curves shall meet or exceed AASHTO design criteria for Stopping Sight Distance, not the "k" Values. Sag vertical curves shall meet or exceed the AASHTO design criteria for headlight sight distance and "k" Values.

| Height of Eye 3.5' Height of Object 2 |           |                  |                        |                               |                                      |   |  |   |  | t <b>2</b> '  |
|---------------------------------------|-----------|------------------|------------------------|-------------------------------|--------------------------------------|---|--|---|--|---|
| 25                                    | 30        | 35               | 40                     | <mark>45</mark>               | 50                                   | 55  | 60   | 65  | 70   | 75  |
| 155                                   | 200       | 250              | 305                    | <mark>360</mark>              | 425                                  | 495   | 570  | 645   | 730  | 820   |
| MINIMUM K VALUE FOR:                  |           |                  |                        |                               |                                      |   |  |   |  |   |
| 12                                    | 19        | 29               | 44                     | 61                            | 84                                   | 114   | 151  | 193   | 247  | 312   |
| 26                                    | 37        | 49               | 64                     | 79                            | 96                                   | 115   | 136  | 157   | 181  | 206   |
|                                       | 155<br>12 | 155 200<br>12 19 | 155 200 250   12 19 29 | 155 200 250 305   12 19 29 44 | 155 200 250 305 360   12 19 29 44 61 | 155   200   250   305   360   425     12   19   29   44   61   84 | 25303540455055155200250305360425495121929446184114 | 25     30     35     40     45     50     55     60       155     200     250     305     360     425     495     570       12     19     29     44     61     84     114     151 | 25     30     35     40     45     50     55     60     65       155     200     250     305     360     425     495     570     645       12     19     29     44     61     84     114     151     193 | 25     30     35     40     45     50     55     60     65     70       155     200     250     305     360     425     495     570     645     730       12     19     29     44     61     84     114     151     193     247 |

Source: 2011 AASHTO Green Book, Chapter 3, Section 3.2.2, page 3-4

#### **TABLE 2-5 STOPPING SIGHT DISTANCE**

When a highway is on a grade, the sight distances in the table below shall be used.

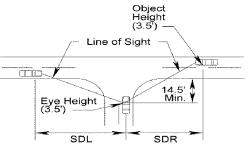
| Design      |     | Stopping Sight Distance on Grades |      |          |     |     |  |  |  |  |  |  |
|-------------|-----|-----------------------------------|------|----------|-----|-----|--|--|--|--|--|--|
| Speed       |     | Downgrades                        | S    | Upgrades |     |     |  |  |  |  |  |  |
| (mph)<br>** | 3%  | 6%                                | 9%   | 3%       | 6%  | 9%  |  |  |  |  |  |  |
| 15          | 80  | 82                                | 85   | 75       | 74  | 73  |  |  |  |  |  |  |
| 20          | 116 | 120                               | 126  | 109      | 107 | 104 |  |  |  |  |  |  |
| 25          | 158 | 165                               | 173  | 147      | 143 | 140 |  |  |  |  |  |  |
| 30          | 205 | 215                               | 227  | 200      | 184 | 179 |  |  |  |  |  |  |
| 35          | 257 | 271                               | 287  | 237      | 229 | 222 |  |  |  |  |  |  |
| 40          | 315 | 333                               | 354  | 289      | 278 | 269 |  |  |  |  |  |  |
| 45          | 378 | 400                               | 427  | 344      | 331 | 320 |  |  |  |  |  |  |
| 50          | 446 | 474                               | 507  | 405      | 388 | 375 |  |  |  |  |  |  |
| 55          | 520 | 553                               | 593  | 469      | 450 | 433 |  |  |  |  |  |  |
| 60          | 598 | 638                               | 686  | 538      | 515 | 495 |  |  |  |  |  |  |
| 65          | 682 | 728                               | 785  | 612      | 584 | 561 |  |  |  |  |  |  |
| 70          | 771 | 825                               | 891  | 690      | 658 | 631 |  |  |  |  |  |  |
| 75          | 866 | 927                               | 1003 | 772      | 736 | 704 |  |  |  |  |  |  |

TABLE 2-6 STOPPING SIGHT DISTANCE ON GRADES(See 2011 AASHTO Green Book, Chapter 3, Section 3.2.2, page 3-5)

#### Intersection Sight Distance

Т

The following table shows intersection sight distance requirements for various speeds along major roads:



SDR = Sight Distance Right (For a vehicle making a left turn) SDL = Sight Distance Left (For a vehicle making a right or left turn)

| Height of Eye 3.5' Height of Object                                  |       |     |     |     |     |     |                  |     |     |     | 3.5' |      |
|--|-------|-----|-----|-----|-----|-----|------------------|-----|-----|-----|------|------|
| Design Speed (mph)*  | *     | 20  | 25  | 30  | 35  | 40  | <mark>45</mark>  | 50  | 55  | 60  | 65   | 70   |
| <b>SDL=SDR</b> : 2 Lane Major<br>Road                                |       | 225 | 280 | 335 | 390 | 445 | 500              | 555 | 610 | 665 | 720  | 775  |
| <b>SDR</b> : 4 Lane Major Road<br>(Undivided) or 3 Lane              |       | 250 | 315 | 375 | 440 | 500 | 565              | 625 | 690 | 750 | 815  | 875  |
| <b>SDL</b> : 4 Lane Major Road<br>(Undivided) or 3 Lane              |       | 240 | 295 | 355 | 415 | 475 | 530              | 590 | 650 | 710 | 765  | 825  |
| <b>SDR</b> : 4 Lane Major Road (Divided . 18qMedian)                 |       | 275 | 340 | 410 | 480 | 545 | 615              | 680 | 750 | 820 | 885  | 955  |
| <b>SDL</b> : 4 Lane Major Road<br>(Divided . 18qMedian)              | eet   | 240 | 295 | 355 | 415 | 475 | 530              | 590 | 650 | 710 | 765  | 825  |
| <b>SDR</b> : 5 Lane Major Road<br>(continuous two-way turn-<br>lane) | In Fe | 265 | 335 | 400 | 465 | 530 | <mark>600</mark> | 665 | 730 | 800 | 860  | 930  |
| <b>SDL:</b> 5 Lane Major Road<br>(continuous two-way turn-<br>lane)  |       | 250 | 315 | 375 | 440 | 500 | <mark>565</mark> | 625 | 690 | 750 | 815  | 875  |
| <b>SDR</b> : 6 Lane Major Road (Divided . 18qMedian)                 |       | 290 | 360 | 430 | 505 | 575 | 645              | 720 | 790 | 860 | 935  | 1005 |
| <b>SDL</b> : 6 Lane Major Road<br>(Divided . 18qMedian)              |       | 250 | 315 | 375 | 440 | 500 | 565              | 625 | 690 | 750 | 815  | 875  |
| <b>SDL</b> : (Where left turns are physically restricted)            |       | 210 | 260 | 310 | 365 | 415 | 465              | 515 | 566 | 620 | 670  | 725  |

#### **TABLE 2-7 INTERSECTION SIGHT DISTANCE**

Source: AASHTO Green Book, Chapter 9, Section 9.5.3, page 9-37 thru 9-52, \* Table 9-5 thru 9-14

\*\*For all tables, use design speed if available, if not use legal speed.

<sup>\*</sup> Rev. 1/14

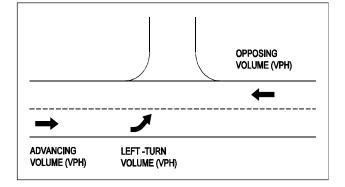
#### Warrants for Left Turn Storage Lanes on Two-Lane Highways

Advancing volume and opposing volumes (VPH), speed and percent left turns are used to determine whether a left turn storage lane is warranted on two-lane highways.

The warrants in table below are taken from the 2011 AASHTO Green Book, Chapter 9, Section 9.7.3, Page 9-132, Table 9-23. They were derived from Highway Research Report No. 211, Figures 2 through 19, for required storage length determinations.

| VPH                | ADVANCING VOLUME     |                   |                     |     |  |  |  |  |  |  |
|--------------------|----------------------|-------------------|---------------------|-----|--|--|--|--|--|--|
| OPPOSING<br>VOLUME | 5%<br>LEFT TURNS     | 10%<br>LEFT TURNS | 30%<br>S LEFT TURNS |     |  |  |  |  |  |  |
|                    | 40-MPH DESIGN SPEED* |                   |                     |     |  |  |  |  |  |  |
| 800                | 330                  | 240               | 180                 | 160 |  |  |  |  |  |  |
| 600                | 410                  | 305               | 225                 | 200 |  |  |  |  |  |  |
| 400                | 510                  | 380               | 275                 | 245 |  |  |  |  |  |  |
| 200                | 640                  | 470               | 350                 | 305 |  |  |  |  |  |  |
| 100                | 720                  | 515               | 390                 | 340 |  |  |  |  |  |  |
|                    | 50-MPH DESIGN SPEED* |                   |                     |     |  |  |  |  |  |  |
| 800                | 280                  | 210               | 165                 | 135 |  |  |  |  |  |  |
| 600                | 350                  | 280               | 195                 | 170 |  |  |  |  |  |  |
| 400                | 430                  | 320               | 240                 | 210 |  |  |  |  |  |  |
| 200                | 550                  | 400               | 300                 | 270 |  |  |  |  |  |  |
| 100                | 615                  | 445               | 335                 | 295 |  |  |  |  |  |  |
|                    |                      | 60-MPH DE         | SIGN SPEE           | D*  |  |  |  |  |  |  |
| 800                | 230                  | 170               | 125                 | 115 |  |  |  |  |  |  |
| 600                | 290                  | 210               | 160                 | 140 |  |  |  |  |  |  |
| 400                | 365                  | 270               | 200                 | 175 |  |  |  |  |  |  |
| 200                | 450                  | 330               | 250                 | 215 |  |  |  |  |  |  |
| 100                | 505                  | 370               | 275                 | 240 |  |  |  |  |  |  |

#### WARRANTS FOR LEFT TURN LANES ON TWO-LANE HIGHWAYS



Example:

Two-lane highway with 40-MPH operating speed

Opposing Volume (VPH) - 600 Advancing Volume (VPH) - 440 Left-Turn Volume (VPH) - 44 or 10% of Advancing Volume

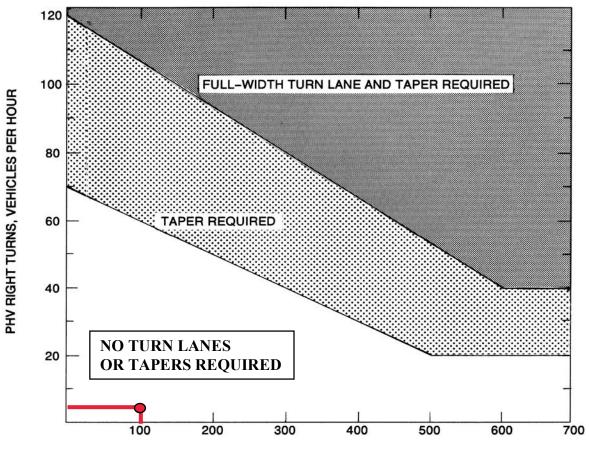
With opposing volume (VPH) of 600 and 10% of advancing volume (VPH) making left turns, and advancing volume (VPH) of 305 or more will warrant a left-turn lane.

When the Average Running Speed on an existing facility is available, the corresponding Design Speed may be obtained from Appendix A, Section A-1.

#### TABLE 3-1

Source: Adapted from 2011 AASHTO Green Book, Chapter 9, Section 9.7.3, Page 9-132, Table 9-23

\* USE DESIGN SPEED IF AVAILABLE, IF NOT USE LEGAL SPEED LIMIT.\*



PHV APPROACH TOTAL, VEHICLES PER HOUR

Appropriate Radius required at all Intersections and Entrances (Commercial or Private).

#### **LEGEND**

PHV - Peak Hour Volume (also Design Hourly Volume equivalent)

#### Adjustment for Right Turns

For posted speeds at or under 45 mph, PHV right turns > 40, and PHV total < 300. Adjusted right turns = PHV Right Turns - 20

If PHV is not known use formula:  $PHV = ADT \times K \times D$ 

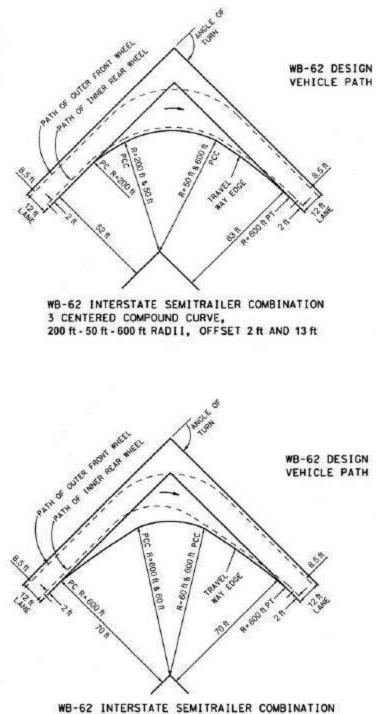
K = the percent of AADT occurring in the peak hour

D = the percent of traffic in the peak direction of flow

Note: An average of 11% for K x D will suffice.

When right turn facilities are warranted, see Figure 3-1 for design criteria.\*

#### FIGURE 3-26 WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)



3 CENTERED COMPOUND CURVE, 600 ft - 60 ft - 600 ft RADII, OFFSET 10 ft

#### **US** Customary

Exhibit 9-26. Minimum Edge-of-Traveled-Way Designs (WB-19 [WB-62] Design Vehicle Path) (Continued)