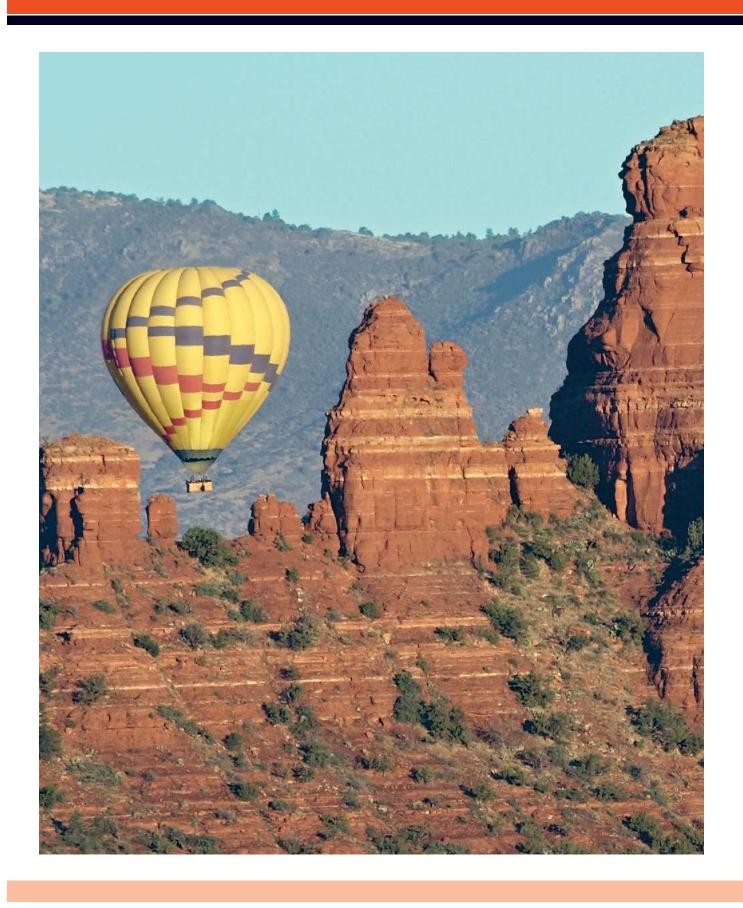
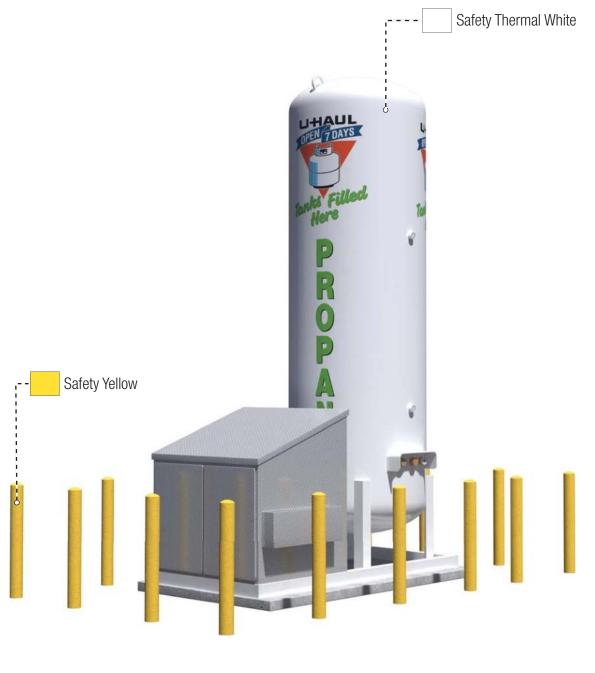


ELEVATION



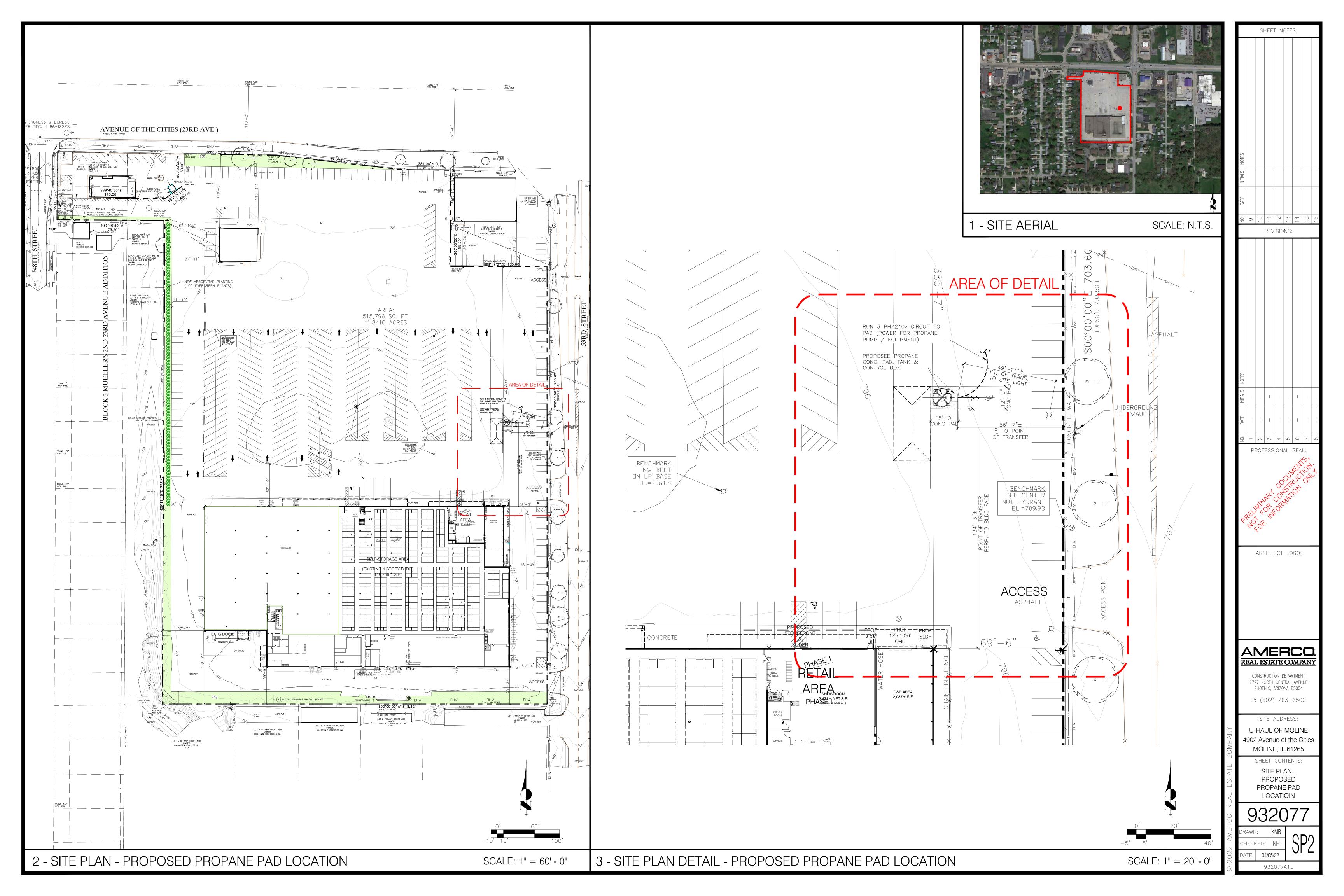






SITE MAP





EMERGENCY RELIEF

EMERGENCY RELIEF

IN THE WAKE OF A HURRICANE



Storm Prep Reminder: Check Propane before Nate Arrives

PHOENIX, Ariz. (Oct. 6, 2017) — U-Haul International and its many propane suppliers are reminding people to fill their propane generators and additional propane cylinders prior to the onset of major storms during the ongoing hurricane season.

Tropical Storm Nate has already been blamed for multiple fatalities in Central America, and the storm is expected to gain strength and become a hurricane as it heads north through the Gulf of Mexico toward the U.S. Officials in Louisiana have declared a state of emergency and ordered some evacuations in coastal areas.

U-Haul, the largest retailer of propane in U.S., has kept a constantly stocked supply of propane at its full-service facilities before and after Hurricanes Harvey and Irma brought massive flooding to Texas, Florida and other regions in and around the Gulf Coast. Propane is again well stocked in anticipation of Nate's arrival.

Find U-Haul propane locations at https://www.uhaul.com/Propane/.

"It's important for people to consider their propane supply in preparing for Nate and other major storms that approach the U.S.," said John Barnett, U-Haul propane program manager. "You don't want to run out of a primary power source. If the flooding and damage from a storm is severe, getting to a propane location after a storm may be difficult."

Propane is important to have in the aftermath of storms in order to power generators, heaters, stoves and grills for cooking, propane-fueled refrigerators, and machinery used for recovery efforts. As a clean-burning fuel, propane is among the most dependable energy sources during weather-related crises. Power outages nullify electric generators, while generators requiring gas and oil can create gunk and stall. Propane is also optimal for performing under temperature swings that high winds can cause.

U-Haul is offering 30 days of free self-storage at 36 facilities across Louisiana, Mississippi and Alabama to anyone who stands to be impacted by Nate. Find a list of participating facilities here.

In addition to its 30 days free self-storage disaster relief program, U-Haul is proud to be at the forefront of aiding communities in times of need as an official American Red Cross Disaster Responder.

About U-Haul

Since 1945, U-Haul has been the No. 1 choice of do-it-yourself movers, with a network of more than 21,000 locations across all 50 states and 10 Canadian provinces. U-Haul Truck Share 24/7 now offers customers access to U-Haul trucks every hour of every day through the self-service options on their internet-connected mobile devices. U-Haul customers' patronage has enabled the U-Haul fleet to grow to more than 150,000 trucks, 112,000 trailers and 40,000 towing devices. U-Haul offers more than 581,000 rooms and more than 51 million square feet of self-storage space at owned and managed facilities throughout North America. U-Haul is the largest

installer of permanent trailer hitches in the automotive aftermarket industry and is the largest retailer of propane in the U.S.

Contact:

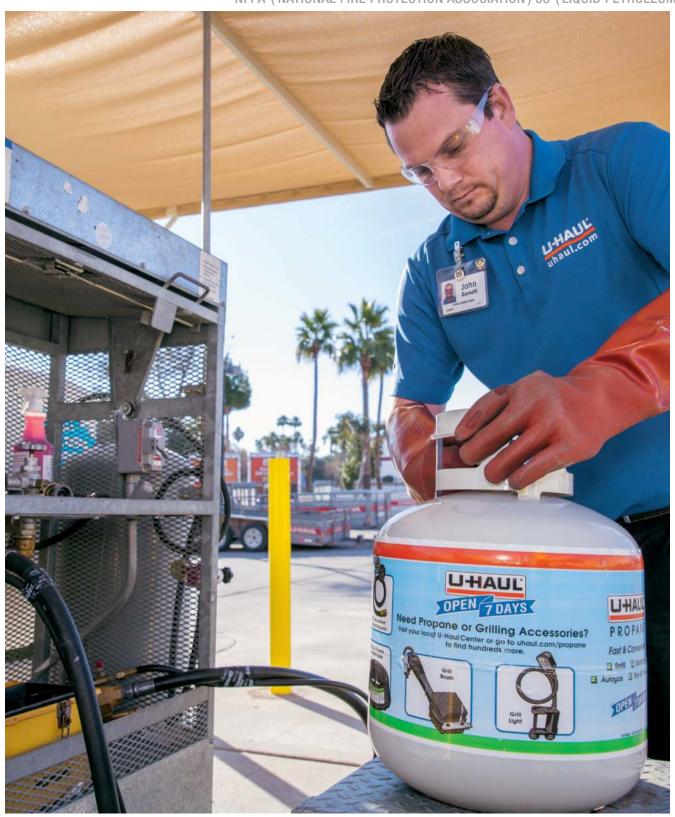
Jeff Lockridge Sebastien Reyes

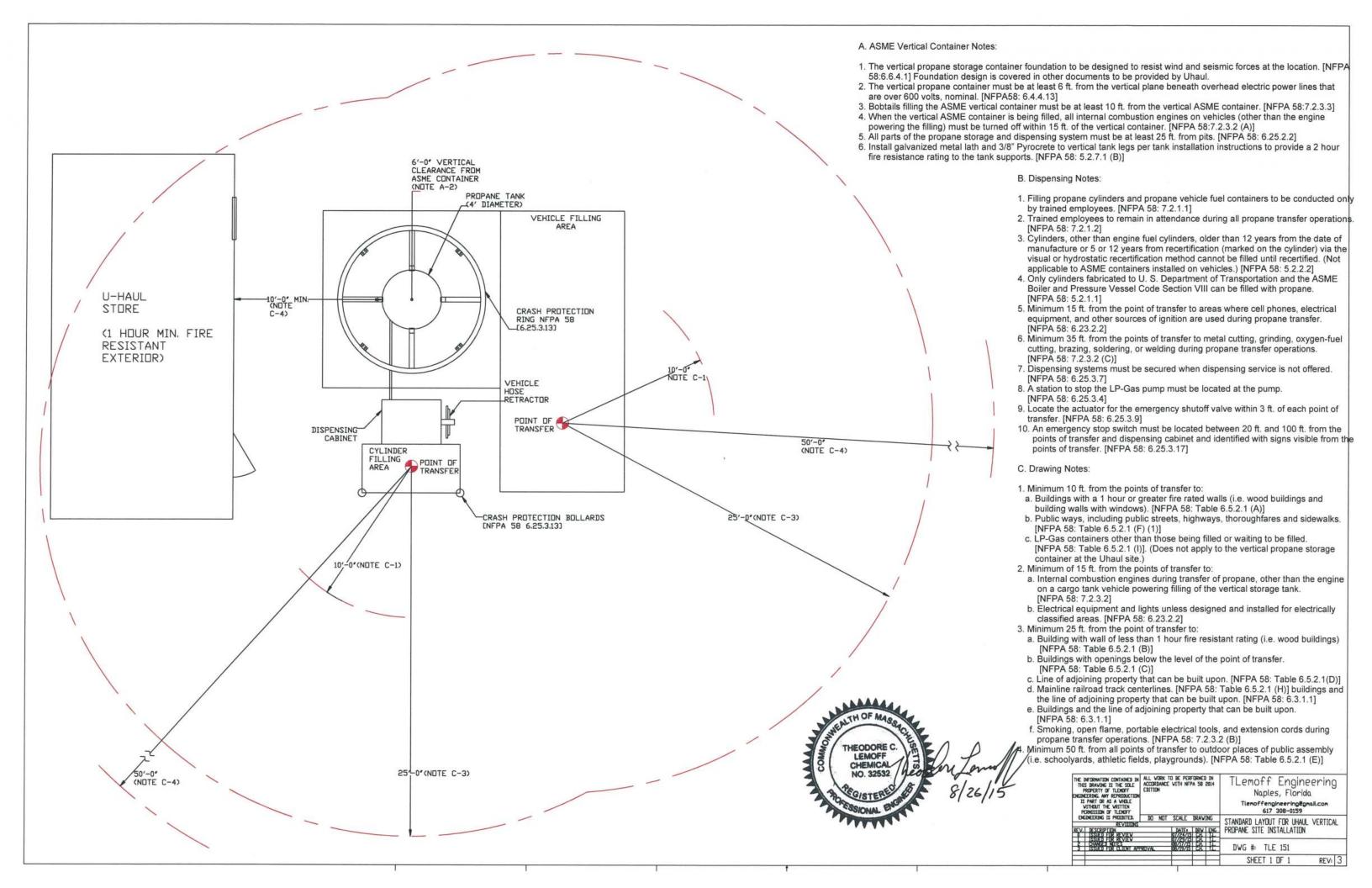
E-mail: <u>publicrelations@uhaul.com</u> Phone: 602-263-6981

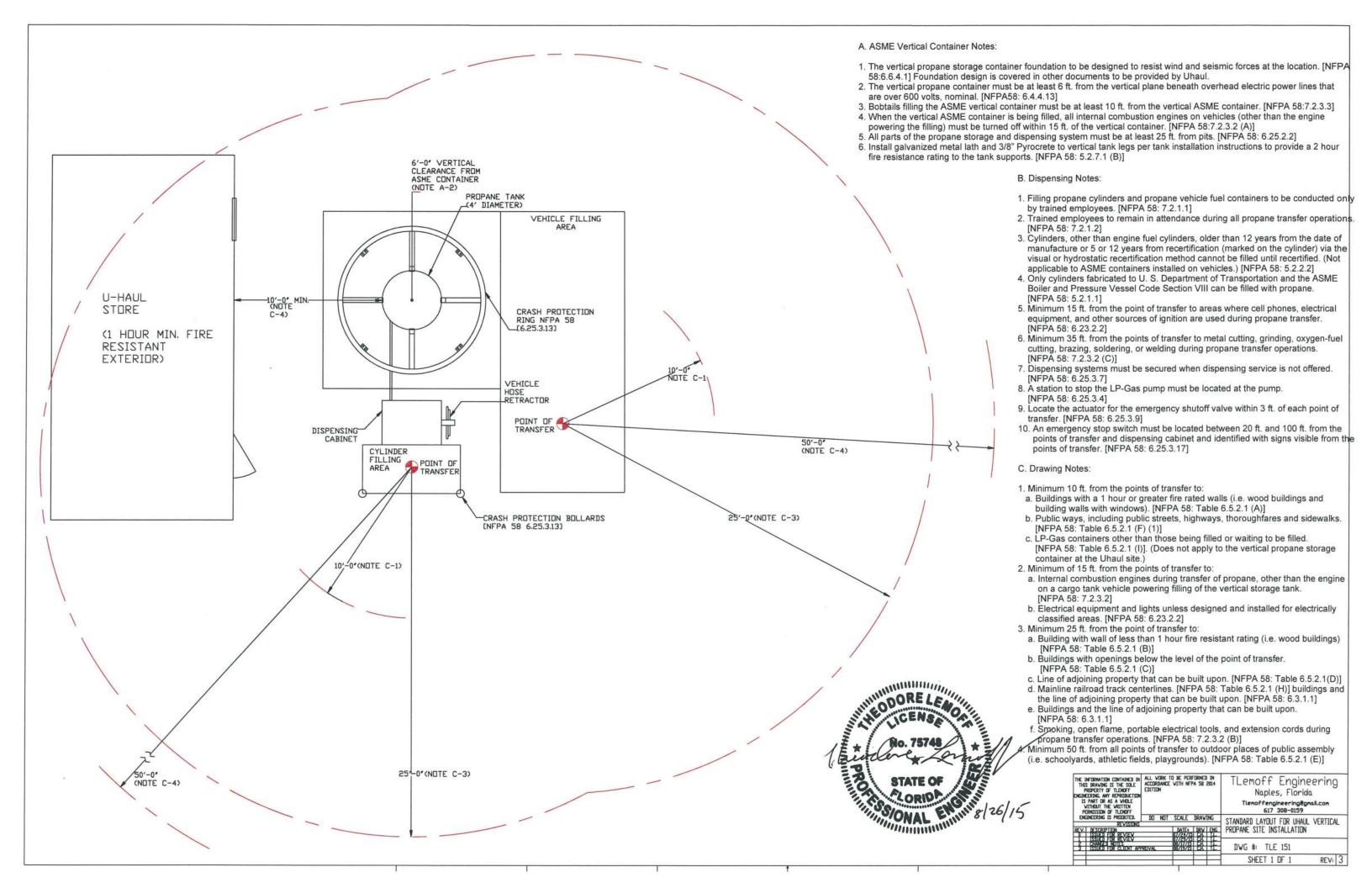
Phone: 602-263-698 Website: uhaul.com

NFPA 58

NFPA-(NATIONAL FIRE PROTECTION ASSOCIATION) 58-(LIQUID PETROLEUM-GAS)







DOT Cylinder Refilling

DOT Cylinders can be refilled

Do not fill:

- Canadian cylinders (marked TC Transport Canada). (They can be used.)
- Cylinders that are out of date: New cylinders can be filled for 12 years from the date of manufacture (usually stamped into the collar)

Cylinders that have been re-qualified can be filled for the following periods:

Requalification Method	Identification Date (month - year)	Refill allowed for:
Visual	12-20	5 years
Proof Pressure	12-20 S	7 years
Volumetric Expansion	12-20 E	12 years



This applies only to refilling, not use from cylinders.

Cylinders with any of the following should not be filled.





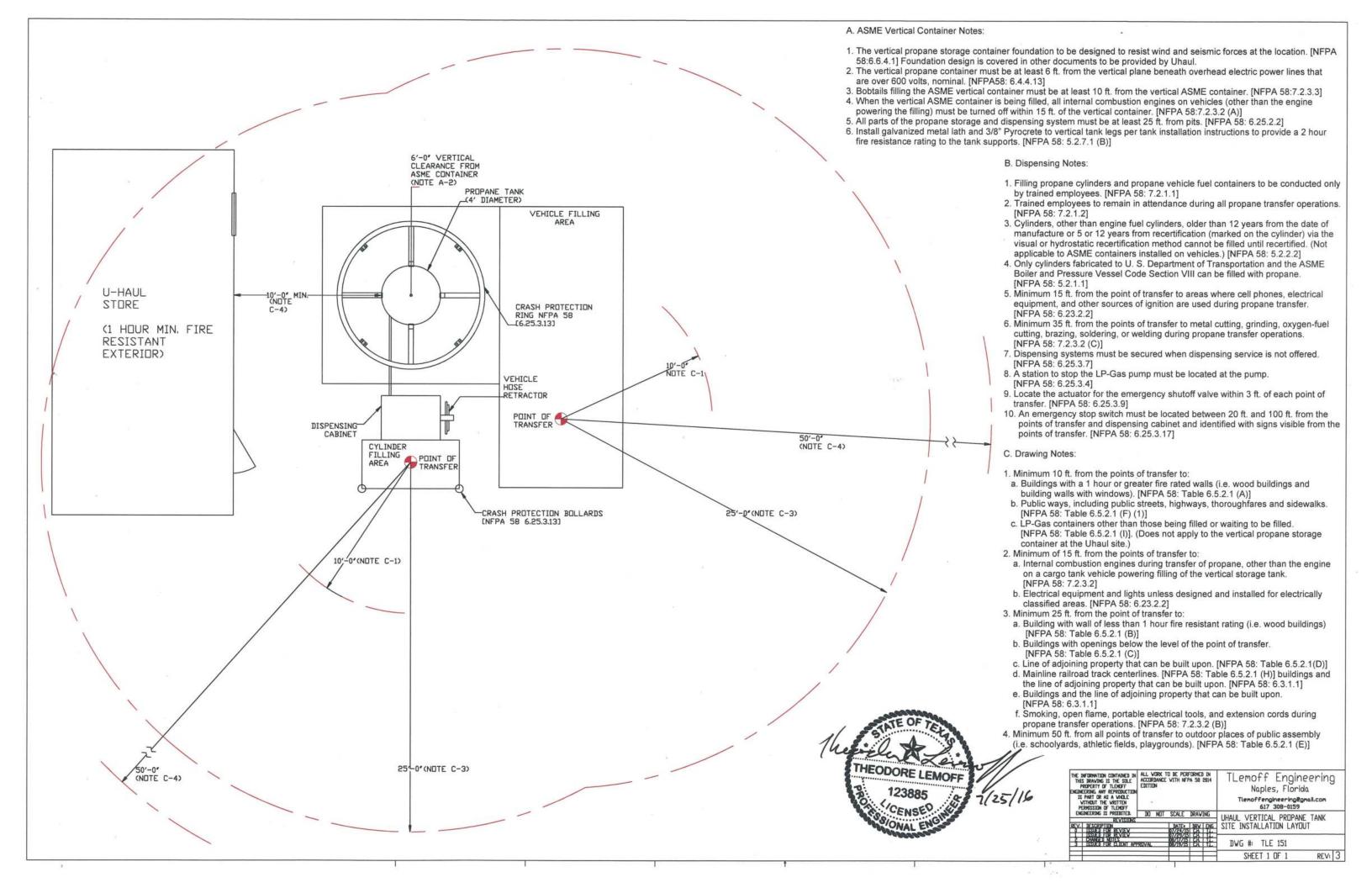
Fire Damaged, bulged Cylinder

Offer to sell the customer a new cylinder or refer them to a location that requalifies cylinders. (Note that it may cost more to requalify a 20 lb. cylinder than to purchase a new one.

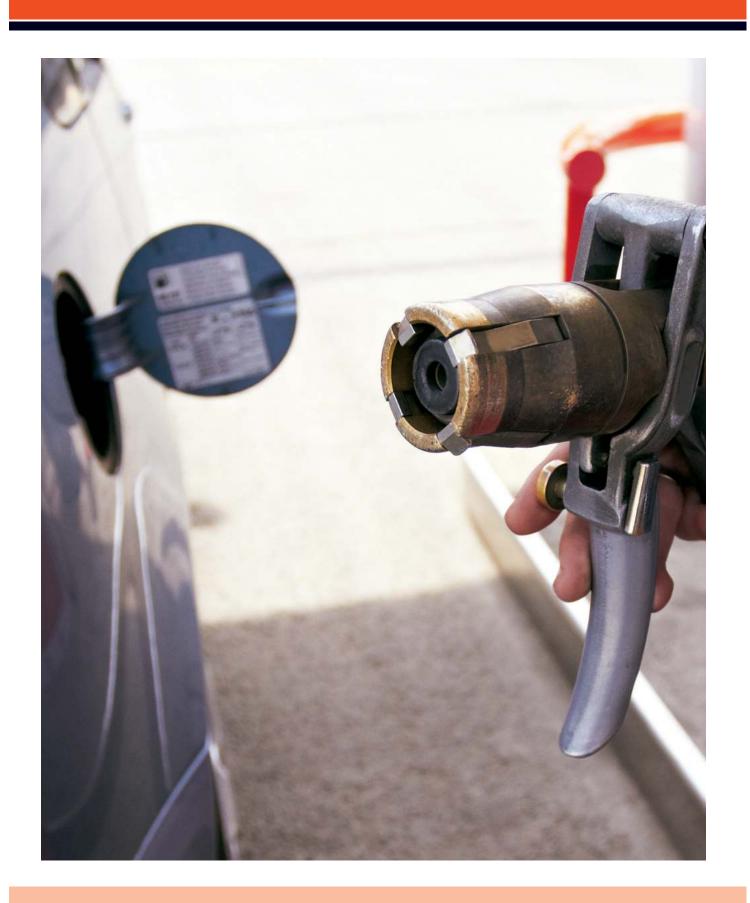


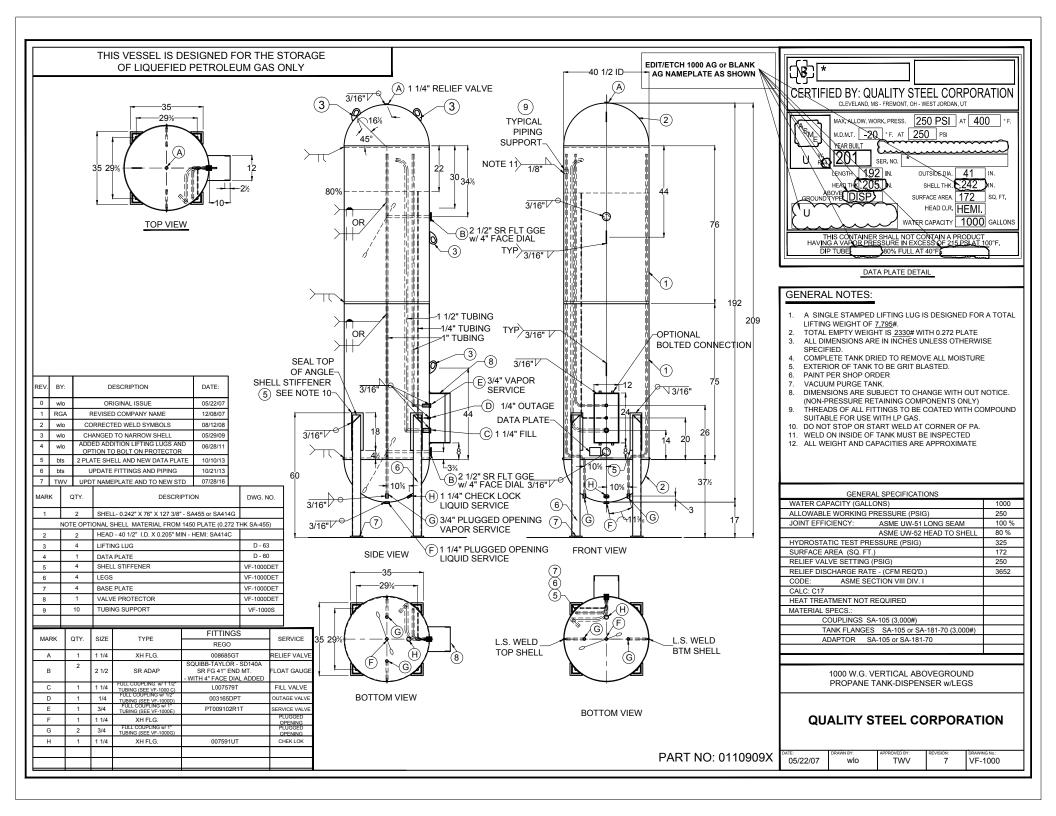
Excessive Corrosion

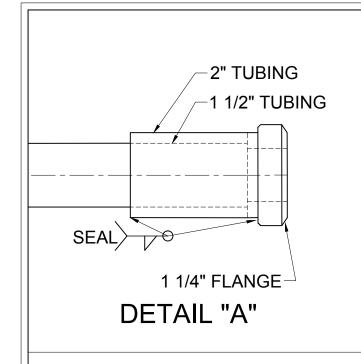
Also, do not fill cylinders that lean, cylinders with welded attachments, and gouged cylinders

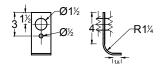


TANK



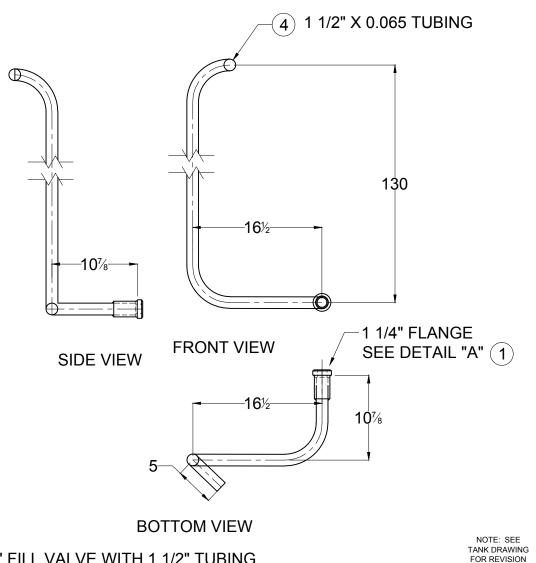






SUPPORT BRACKET (x 5) DETAIL

MARK	QTY.	DESCRIPTION					
1	1	1 1/4" XH FLANGE (SA-105)					
2	1	1/4" COUPLING w/ #54 HOLE (SA-105)					
3	3	3/4" XH FLANGE (SA-105)					
4	1	1 1/2" TUBING X 0.065 X 166 (130" OAL AFTER BENDING)					
5	2	1" TUBING X 0.065 X 175 (163" OAL AFTER BENDING)					
6	1	1" TUBING X 0.065 X 144 (121" OAL AFTER BENDING)					
7	1	1/2" TUBING X 0.049 X 128 (108" OAL AFTER BENDING)					
8	10	L 1 1/2" x 1 1/2" x 3/16" (SA-36)					
9	2	1/2" EMT ONE HOLE PIPE SUPPORT					
10	6	1" EMT ONE HOLE PIPE SUPPORT					
11	2	1 1/2" EMT ONE HOLE PIPE SUPPORT					

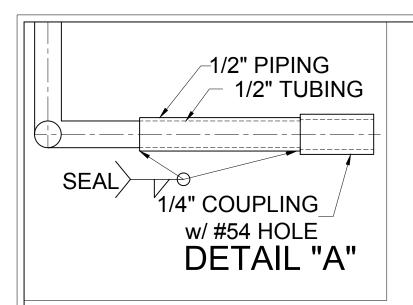


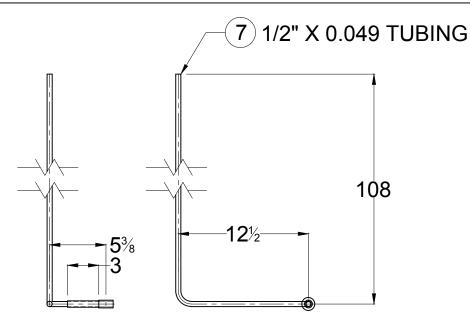
C 1 1/4" FILL VALVE WITH 1 1/2" TUBING 1 EACH (166" OF TUBING)

1000 W.G. VERTICAL ABOVEGROUND PROPANE TANK-DISPENSER w/LEGS

BLOCK

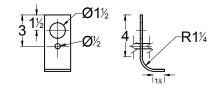
= = ==							
DATE:	DRAWN BY:	APPROVED BY:	REVISION:	DRAWING No.:	_		
05/22/07	wlo	TWV	7	VF-1000			



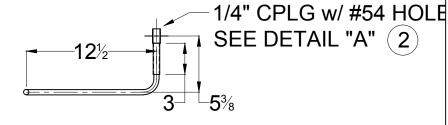


SIDE VIEW

FRONT VIEW



SUPPORT BRACKET (x 5)
DETAIL



BOTTOM VIEW

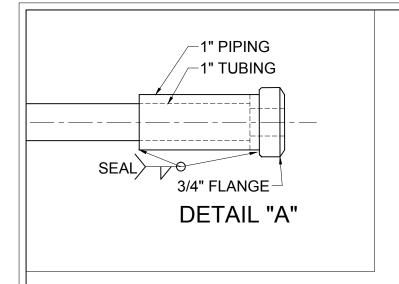
D 1/4" OUTAGE WITH 1/2" TUBING 1 EACH (128" OF TUBING)

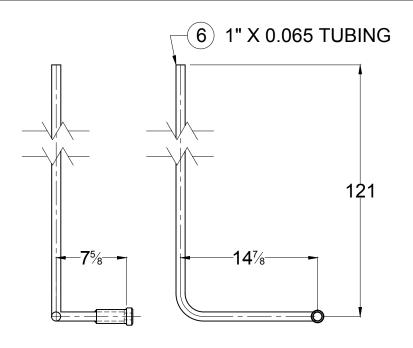
NOTE: SEE TANK DRAWING FOR REVISION BLOCK

MARK	QIY.	DESCRIPTION
1	1	1 1/4" XH FLANGE (SA-105)
2	1	1/4" COUPLING w/ #54 HOLE (SA-105)
3	3	3/4" XH FLANGE (SA-105)
4	1	1 1/2" TUBING X 0.065 X 166 (130" OAL AFTER BENDING)
5	2	1" TUBING X 0.065 X 175 (163" OAL AFTER BENDING)
6	1	1" TUBING X 0.065 X 144 (121" OAL AFTER BENDING)
7	1	1/2" TUBING X 0.049 X 128 (108" OAL AFTER BENDING)
8	10	L 1 1/2" x 1 1/2" x 3/16" (SA-36)
9	2	1/2" EMT ONE HOLE PIPE SUPPORT

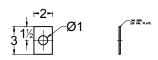
1" EMT ONE HOLE PIPE SUPPORT 1 1/2" EMT ONE HOLE PIPE SUPPORT 1000 W.G. VERTICAL ABOVEGROUND PROPANE TANK-DISPENSER w/LEGS

DATE:	DRAWN BY:	APPROVED BY:	REVISION:	DRAWING No.:	
05/22/07	wlo	TWV	7	VF-1000	D

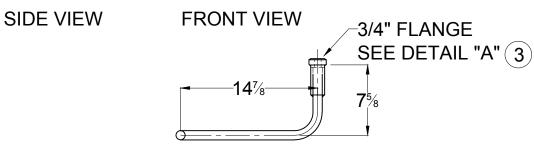




BOTTOM VIEW



SUPPORT BRACKET (x 4)
DETAIL



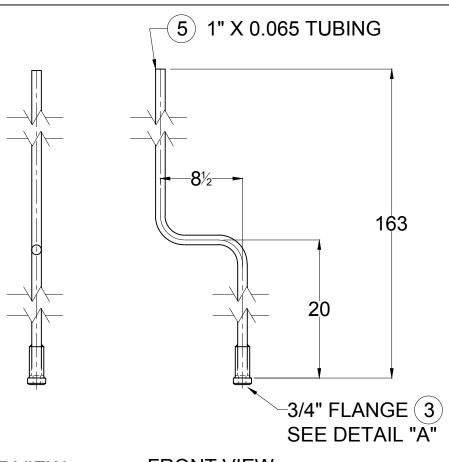
E 3/4" VAPOR SERVICE WITH 1" TUBING 1 EACH (144" OF TUBING)

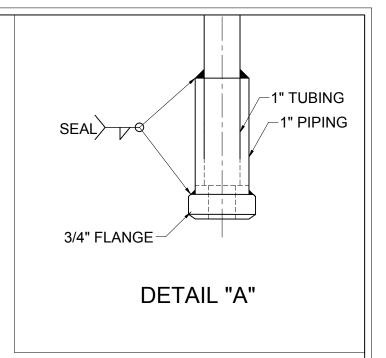
NOTE: SEE TANK DRAWING FOR REVISION BLOCK

MARK	QTY.	DESCRIPTION				
1	1	1 1/4" XH FLANGE (SA-105)				
2	1	1/4" COUPLING w/ #54 HOLE (SA-105)				
3	3	3/4" XH FLANGE (SA-105)				
4	1	1 1/2" TUBING X 0.065 X 166 (130" OAL AFTER BENDING)				
5	2	1" TUBING X 0.065 X 175 (163" OAL AFTER BENDING)				
6	1	1" TUBING X 0.065 X 144 (121" OAL AFTER BENDING)				
7	1	1/2" TUBING X 0.049 X 128 (108" OAL AFTER BENDING)				
8	10	L 1 1/2" x 1 1/2" x 3/16" (SA-36)				
9	2	1/2" EMT ONE HOLE PIPE SUPPORT				
10	6	1" EMT ONE HOLE PIPE SUPPORT				
11	2	1 1/2" EMT ONE HOLE PIPE SUPPORT				

1000 W.G. VERTICAL ABOVEGROUND PROPANE TANK-DISPENSER w/LEGS

DATE:	DRAWN BY:	APPROVED BY:	REVISION:	DRAWING No.:	
05/22/07	wlo	TWV	7	VF-1000	F

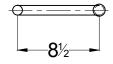




SIDE VIEW

DESCRIPTION

FRONT VIEW



BOTTOM VIEW

NOTE: SEE TANK DRAWING FOR REVISION BLOCK

1	1	1 1/4" XH FLANGE (SA-105)
2	1	1/4" COUPLING w/ #54 HOLE (SA-105)
3	3	3/4" XH FLANGE (SA-105)
4	1	1 1/2" TUBING X 0.065 X 166 (130" OAL AFTER BENDING)
5	2	1" TUBING X 0.065 X 175 (163" OAL AFTER BENDING)
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7	1	1/2" TUBING X 0.049 X 128 (108" OAL AFTER BENDING)
8	10	L 1 1/2" x 1 1/2" x 3/16" (SA-36)
q	2	1/2" EMT ONE HOLE PIPE SUPPORT

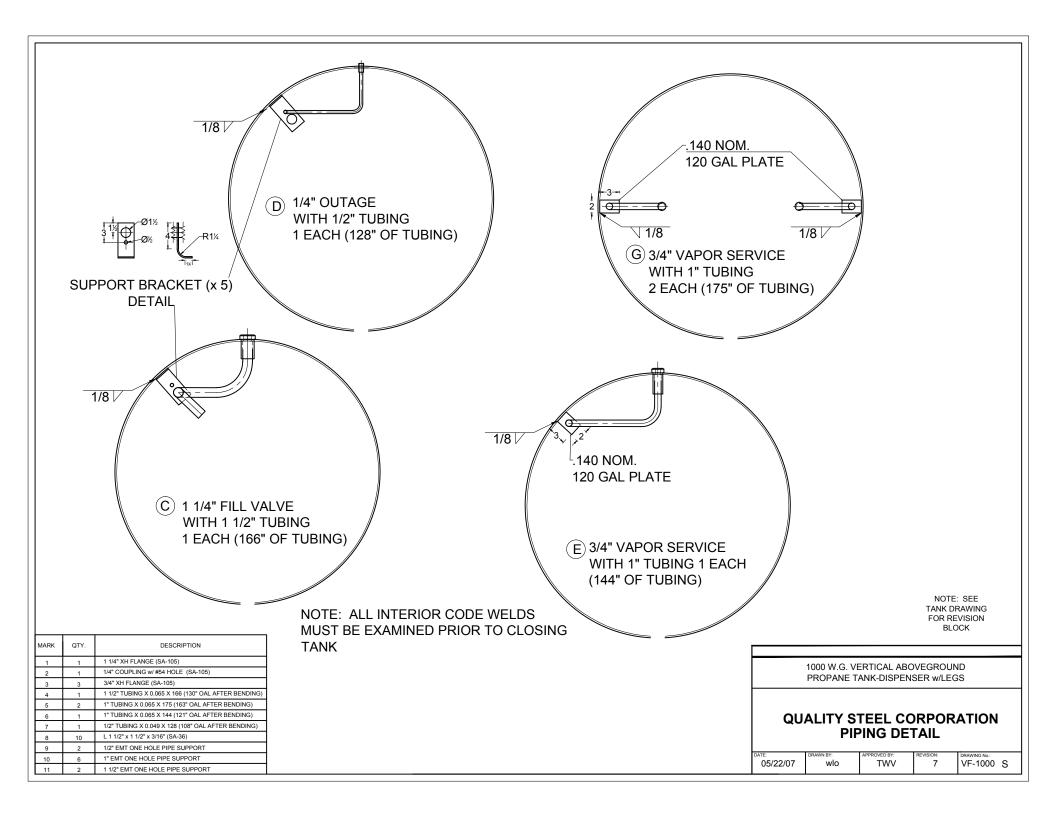
1" EMT ONE HOLE PIPE SUPPORT 1 1/2" EMT ONE HOLE PIPE SUPPORT

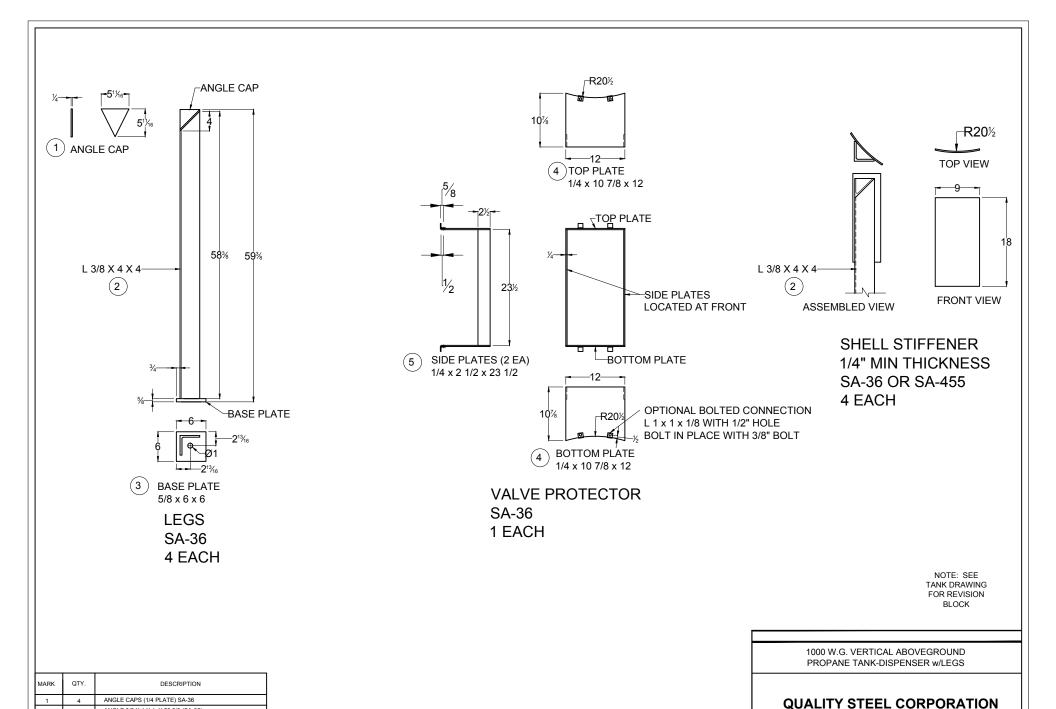
MARK QTY.

G 3/4" VAPOR SERVICE WITH 1" TUBING 2 EACH (175" OF TUBING)

1000 W.G. VERTICAL ABOVEGROUND PROPANE TANK-DISPENSER w/LEGS

DATE:	DRAWN BY:	APPROVED BY:	REVISION:	DRAWING No.:	
05/22/07	wlo	TWV	7	VF-1000	G





DETAILS

TWV

05/22/07

wlo

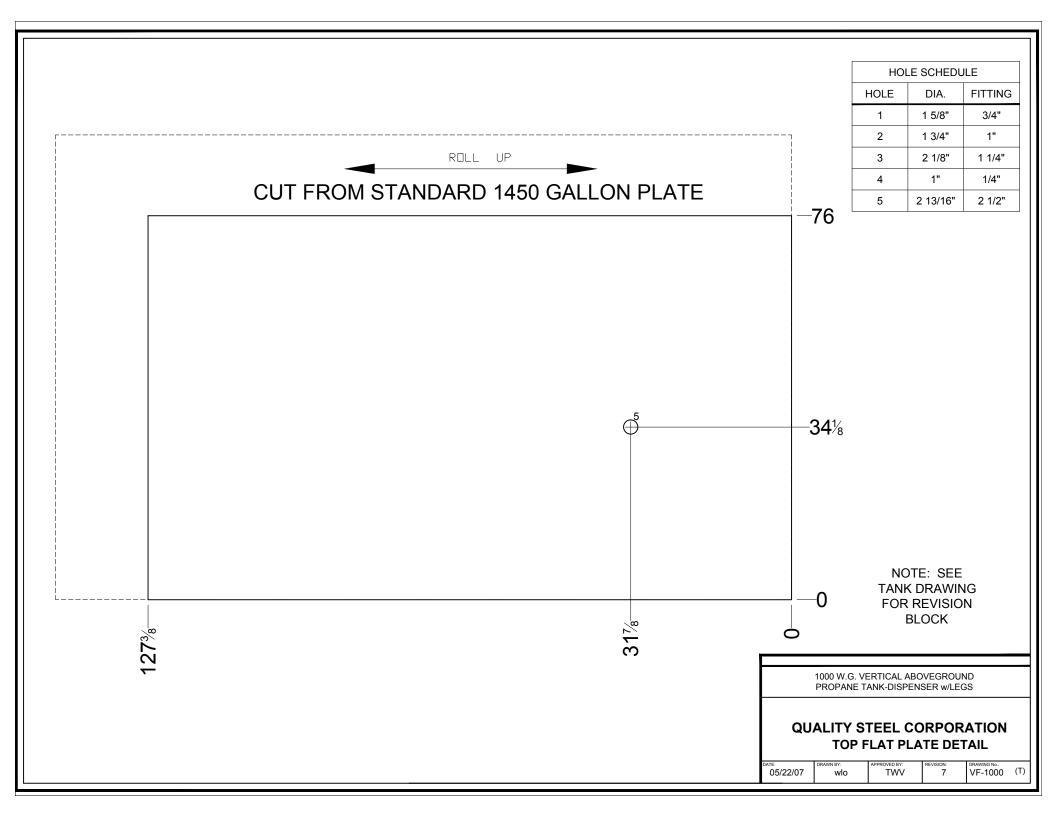
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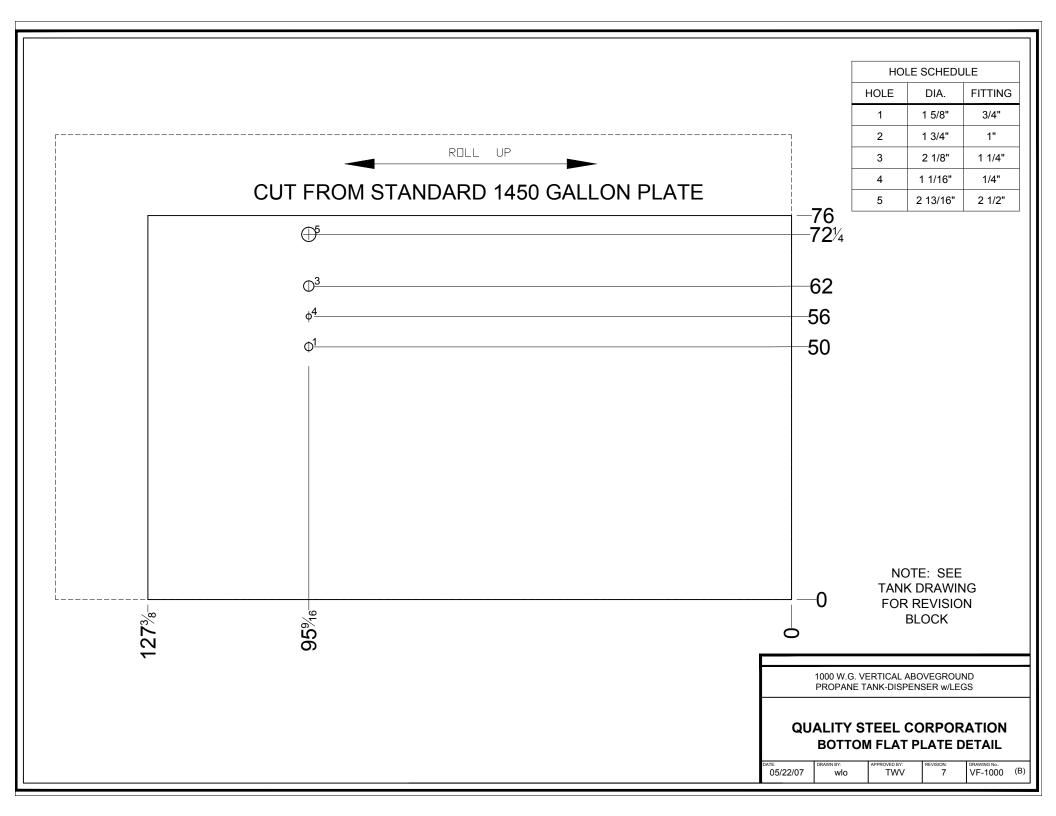
VF-1000 - DET

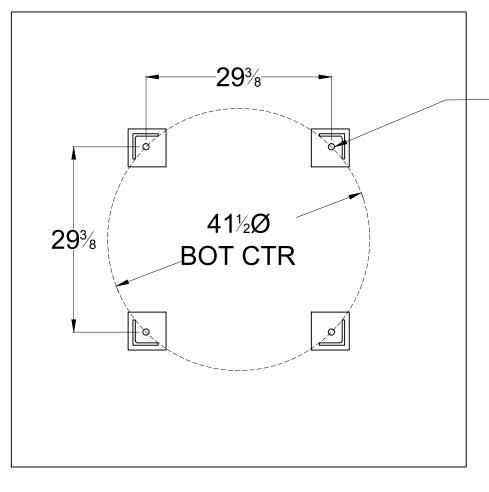
ANGLE 3/8 X 4 X 4 X 58 3/8 (SA-36)

SHELL STIFFENER 1/4 MIN X 9 X 18 (SA-36 OR SA-455)

BASE PLATE 5/8 X 6 X 6 (SA-36) TOP & BOTTOM PLATE 1/4 X 10 7/8 X 12 (SA-36) SIDE PLATE 1/4 X 2 1/2 X 23 1/2 (SA-36)







-7/8" Ø ANCHOR BOLT TYPICAL 4 PLACES

> NOTE: SEE TANK DRAWING FOR REVISION BLOCK

TOP VIEW

1000 W.G. VERTICAL ABOVEGROUND PROPANE TANK-DISPENSER w/LEGS

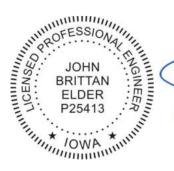
QUALITY STEEL CORPORATION
ANCHOR BOLT PATTERN

DATE:	DRAWN BY:	APPROVED BY:	REVISION:	DRAWING No.:
05/22/07	wlo	TWV	7	VF-1000

SAFETY







I hereby certify that this engineering document was prepared by me or under

my direct personal supervision and that I am a duly licensed Professional Engineer

under the laws of the State of Iowa.

01/03/2024

(signature)

(date)

SEAL

John Brittan Elder

License number #P25413

My license renewal date is December 31, 2024.

Pages or sheets covered by this seal:

Uhaul Propane IA Structural Calculations

PROJECT ADDRESS 1100 EAST HICKMAN WAUKEE, IA 50263

ISSUE DATE 1/2024

ENGINEER SS

PROJECT NUMBER 23668

United Structural Design LLC

2058 S. Dobson Rd. Ste 10 Mesa, AZ 480-454-6408

JOB NO. 23688	SHEET NO.
CALCULATED BY SS	DATE
CHECKED BY	DATE

2 of 26

JOB TITLE Uhaul Propane

CS2021 Ver 2023-01-21 <u>www.struware.com</u>

STRUCTURAL CALCULATIONS

FOR

Uhaul Propane

0.0650

Project Title: Engineer: Project ID: Project Descr:

ASCE 7-16 Seismic Base Shear						Project File: 23668.ec6
LIC# : KW-06012847, Build:20.23.10.02 DESCRIPTION: Seismic Base Shear A	nalysis	United S	Structu	ral Design		(c) ENERCALC INC 1983-2023
Specific Description: Seismic Forces						
Risk Category						Calculations per ASCE 7-16
Risk Category of Building or Other Structure : "III to I	" : Building human life	s and other	er stru	ctures that real failure.	epresent a substa	intial hazard ^{SCE 7-16, Page 4, Table 1.5-1}
Seismic Importance Factor =	1.25					ASCE 7-16, Page 5, Table 1.5-2
Gridded Ss & S1values from ASCE 7-16						ASCE 7-16 11.4.2
Max. Ground Motions, 5% Damping				Location	n 1Maukaa IA E	2262
S _S = 0.06092 g, 0.2 sec response					n :Waukee, IA 50	
S ₁ = 0.05083 g, 1.0 sec response				Latitude		41.602 deg North
For the closest datapoint grid location Latitude = 41.600 deg Nort Longitude = 93.860 deg Wes				Longitud	de =	93.862 deg West
Site Class, Site Coeff. and Design Cated	gory					
Classification: "D": Shear Wave Velocity 600 to 1,	200 ft/sec		=	D (Based	d on Testing)	ASCE 7-16 Table 20.3-1
Site Coefficients Fa & Fv (using straight-line interpolation from table val		Fa Fv	= =	1.60 2.40		ASCE 7-16 Table 11.4-1 & 11.4-2
Maximum Considered Earthquake Accelerat	S _{MS} =	Fa * Ss	=	0.097		ASCE 7-16 Eq. 11.4-1
•	S _{M1} =	Fv * S1	=	0.122		ASCE 7-16 Eq. 11.4-2
Design Spectral Acceleration	S _{DS} = S	MS * 2/3	=	0.065		ASCE 7-16 Eq. 11.4-3
		_{M1} * 2/3	=	0.081		ASCE 7-16 Eq. 11.4-4
Seismic Design Category			=	В		ISCE 7-16 Table 11.6-1 & -2
Resisting System						ASCE 7-16 Table 12.2-1
				ns detailed to		ecific classification
Response Modification Coefficient "I = 1.	25	_	-	ht Limits :		
System Overstrength Factor " Wo " = 1.	25	Catego	ory "A	. & B" Limit: " Limit:	Limit = 35 Limit = 35	
Deflection Amplification Factor " Cd ' = 1.	25)" Limit:	Not Permitted	.i
NOTE! See ASCE 7-16 for all applicable footno		Catego	orý "E	" Limit: " Limit:	Not Permitted Not Permitted	•
Lateral Force Procedure						ASCE 7-16 Section 12.8.2
Equivalent Lateral Force Procedure The "Equivalent Lateral Force Procedure	rce Proced	lure" is bei	ing us	ed according	to the provisions	of ASCE 7-16 12.8
Determine Building Period						Use ASCE 12.8-7
Structure Type for Building Period CalculaAll Other " Ct " value = 0.020 " h " x " value = 0.75 " Ta " Approximate fundemental period using Ed	nn " : Heigh q. 12.8-7 :	nt from bas	se to h	nighest leve	20.0 ft 0.189 sec	
"TL" : Long-period transition period per ASCE 7	- to iviaps				8.000 sec	
		Build	ding F	eriod " Ta " (Calculated from A	pproximate Method sel= 0.189
" Cs " Response Coefficient						ASCE 7-16 Section 12.8.1.1
S _{DS} : Short Period Design Spectral Response "R": Response Modification Factor "I": Seismic Importance Factor	= =	0.065 1.25 1.25		From Ed	•	nary Cs = 0.065 γ, Cs need not exceε = 0.430 γ, Cs not be less than = 0.010

Cs : Seismic Response Coefficient =

Project Title: Engineer: Project ID: Project Descr:

ASCE 7-16 Seismic Base Shear

LIC#: KW-06012847, Build:20.23.10.02

Project File: 23668.ec6 (c) ENERCALC INC 1983-2023

DESCRIPTION: Seismic Base Shear Analysis

Seismic Base Shear ASCE 7-16 Section 12.8.1

United Structural Design

Cs = 0.0650 from 12.8.1.1 W (see Sum Wi below) = 7.60 k Seismic Base Shear V = Cs * W = 0.49 k

Vertical Distribution of Seismic Forces

ASCE 7-16 Section 12.8.3

k ": hx exponent based on Ta = Table of building Weights by Floor Level...

Level #	Wi : Weight	Hi : Height	(Wi * Hi^k)	Cvx	Fx=Cvx * V	Sum Story Shear	Sum Story Moment
1	7.60	10.00	76.00	1.0000	0.49	0.49	0.00
Sum Wi =	7.60 k	Sum Wi * Hi =	76.00 k-ft		Total Base Shear =	0.49 k Base Moment =	4.9 k-ft

Diaphragm Forces: Seismic Design Category "B" to "F"

ASCE 7-16 12.10.1.1

Level #	Wi	Fi	Sum Fi	Sum Wi	Fpx : Calcd	Fpx : Min	Fpx : Max	Fpx	Dsgn. Force
1	7.60	0.49	0.49	7.60	0.49	0.12	0.25	0.25	0.49

Wpx..... Weight at level of diaphragm and other structure elements attached to it.

Fi Design Lateral Force applied at the level.

Sum Fi Sum of "Lat. Force" of current level plus all levels above

MIN Req'd Force @ Level . . . $0.20 * S_{DS} * I * Wpx$ MAX Req'd Force @ Level . . . 0.40 * S _{DS} * I * Wpx

Fpx: Design Force @ Level. Wpx * SUM(x->n) Fi / SUM(x->n) wi, x = Current level, n = Top Level

United Structural Design LLC

2058 S. Dobson Rd. Ste 10 Mesa, AZ 480-454-6408

JOB	TITLE	Uhaul	Pro	pane
		0		P G

JOB NO. 23688 SHEET NO. CALCULATED BY SS DATE CHECKED BY DATE

5 of 26

Wind Loads - MWFRS all h (Except for Open Buildings)

Roof Angle (θ) = 1.2 deg Bldg dim normal to ridge = 100.0 ft qi = qh

Roof tributary area: h = 20.0 ftWind normal to ridge = (h/2)*L: 1500 sf ridge ht = 21.0 ft

Wind normal to ridge =(h/2)*L: 1500 sf ridge ht = 21.0 f Wind parallel to ridge =(h/2)*L: 1000 sf

Ultimate Wind Surface Pressures (psf)

		• • • • • • • • • • • • • • • • • • • •			· · · · · · · · · · · · · · · · · · ·				
		Wind Normal to Ridge				Wind Parallel to Ridge			
	L/B =	0.67	h/L =	0.20		L/B =	1.50	h/L =	0.13
Surface	Ср	q_hGC_p	w/+q _i GC _{pi}	w/-q _h GCpi	Dist.*	Ср	q_hGC_p	w/ +q _i GC _{pi}	w/ -q _h GC _{pi}
Windward Wall (WW)	0.80	18.6	see tab	le below		0.80	18.6	see	able below
Leeward Wall (LW)	-0.50	-11.6	-16.5	-6.7		-0.40	-9.3	-14.2	-4.4
Side Wall (SW)	-0.70	-16.3	-21.2	-11.3		-0.70	-16.3	-21.2	-11.3
Leeward Roof (LR)		**				In	cluded in w	indward roof	
Neg Windward Roof: 0 to h/2*	-0.90	-20.9	-25.8	-16.0	0 to h/2*	-0.90	-20.9	-25.8	-16.0
h/2 to h*	-0.90	-20.9	-25.8	-16.0	h/2 to h*	-0.90	-20.9	-25.8	-16.0
h to 2h*	-0.50	-11.6	-16.5	-6.7	h to 2h*	-0.50	-11.6	-16.5	-6.7
> 2h*	-0.30	-7.0	-11.9	-2.0	> 2h*	-0.30	-7.0	-11.9	-2.0
Pos/min windward roof press.	-0.18	-4.2	-9.1	0.7	Min press.	-0.18	-4.2	-9.1	0.7

^{**}Roof angle < 10 degrees. Therefore, leeward roof

is included in windward roof pressure zones.

*Horizontal distance from windward edge

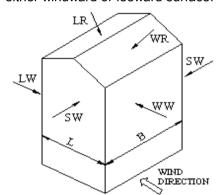
For monoslope roofs, entire roof surface is either windward or leeward surface.

Parapet			
Z	Kz	Kzt	qp (psf)
0.0 ft	0.85	1.00	0.0

Windward parapet: 0.0 psf (GCpn = +1.5) Leeward parapet: 0.0 psf (GCpn = -1.0)

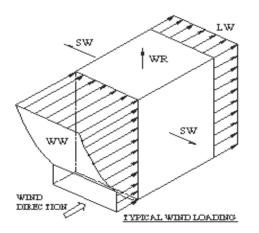
Windward roof overhangs: 18.6 psf (upward - add to windward roof pressure)

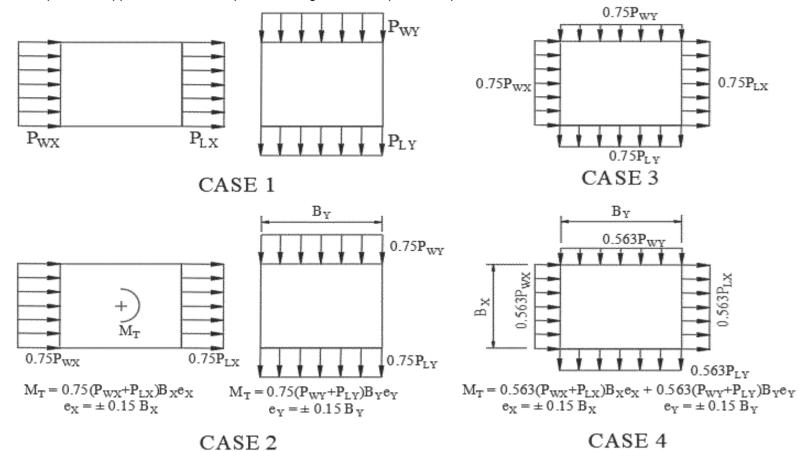
	<u>Windwar</u>	d Wall Pre		Combined WW + LW				
				V	Vindward Wa	Wind Normal	Wind Parallel	
	z	Kz	Kzt	q_zGC_p	$w/+q_iGC_{pi}$	$w/-q_hGC_{pi}$	to Ridge	to Ridge
•	0 to 15'	0.85	1.00	17.5	12.6	22.4	29.1	26.8
h=	20.0 ft	0.90	1.00	18.6	13.7	23.5	30.2	27.9
ridge =	21.0 ft	0.91	1.00	18.8	13.9	23.7	30.4	28.1



WR WR WR LW SW WIND DIRECTION

WIND PARALLEL TO RIDGE





Wind Forces at Floors

Building dimension (parallel with ridge) = 150.0 ft e = 22.50 ft

Total Floors = 1 Building dimension (normal to ridge) = 100.0 ft e = 15.00 ft

T/Fdn (dist below grade) = 2.0 ft L is the building dimension parallel to the wind direction

Wind Normal to Ridge Wind Parallel to Ridge Elevation Height of Above Centroid Applied Story Overturning Applied Story Overturning Grade (ft) to Fdn (ft) В Area (sf) Force (k) Shear (k) Force (k) Shear (k) Level Moment ('k) Moment ('k) Area Equip,etc 0.00wind on equip, screenwalls, etc = 0.00.00 0.0 0.0 Parapet 0.000.00.0 T/Ridge 0.000.000.0 0.0 0.00.0 0.017.00 150.0 Roof 15.00 100.0 1,125.0 32.7 32.7 0.0 750.0 20.1 20.1 0.00.00 2.00 100.0 150.0 1,125.0 32.7 65.5 491.1 750.0 20.1 40.2 301.3 FDN 0.00622.1 381.6



Uhaul Propane Tank Calcs

Loads

Empty tank weight = 2330#
Capacity = 1000 gallons
Weight = 4.25#*1000 = 4250#
Weight of tank legs + misc. = 170#
Total weight = 7600#

Seismic Loads R = 2.5

Lateral seismic force = 0.196*weight = 1490#

Wind Loads

Wind Pressure = 31 psf (see attached printout)

Tank area = 3.5'*20' = 70 sq ft Total wind load = 31*70 = 2170 #

Therefore wind load governs.

Worst case loads

Empty tank + Wind

Overturning moment = 2170*10' = 21700 #ft

Spacing between anchor locations = 15"

Resisting moment = 2300*15/12 = 2875 #ft

Net moment = 18825 #ft

Net uplift = 18825/(30/12) = 7530 #

Net uplift per bolt = 3765 #

7 of 26

Sheet No.



STRUCTURAL DESIGN LLC	Project No.	23668
Project Name_ Uhaul Propane IA	Date _	10/18/2023
Subject	Computed By _	SS

Crash Post Design			
Height = 4' Loads = 3k at 3' height Designed for vehicle cra	sh loads		
See attached detail and crash post design	printout for		

8 of 26

Sheet No. _

Project File: 23668.ec6

Project Title: Engineer: Project ID: Project Descr:

Analysis/Design Settings

Combined Footing

LIC#: KW-06012847, Build:20.23.10.02 United Structural Design (c) ENERCALC INC 1983-2023

DESCRIPTION: Tank Footing

Code References

Calculations per ACI 318-14, IBC 2018, CBC 2019, ASCE 7-16

Load Combinations Used: IBC 2018

General Information Material Properties

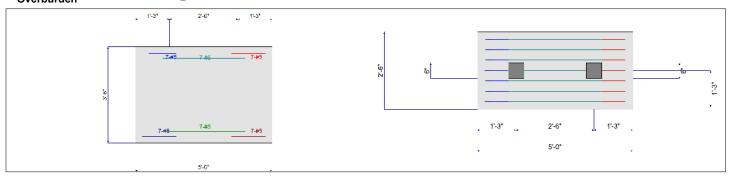
f'c : Concrete 28 day s	strength	3.0	ksi	Calculate footing weight as dead load?	Yes
fy : Rebar Yield		60.0	ksi	Calculate Pedestal weight as dead load?	No
Éc : Concrete Elastic	Modulus	3,122.0	ksi	Min Steel % Bending Reinf (based on 'd')	
Concrete Density		145.0	pcf	Min Allow % Temp Reinf (based on thick)	0.00180
் Phi Values ்	Flexure:	0.90		Min. Overturning Safety Factor	1.0: 1
Ψ	Shear :	0.750		Min. Sliding Safety Factor	1.0: 1
Soil Information					
Allowable Soil Bearing		2.0	ksf	Soil Bearing Increase	
Increase Bearing By Foo	ting Weight	No		Footing base depth below soil surface Increases based on footing Depth	ft
Soil Passive Sliding Resi	stance	250.0	pcf	Allowable pressure increase per foot	ksf
(Uses entry for "	Footing base depth	below soil surl	ace" for fo		ft
Coefficient of Soil/Concre	ato Eriction	0.30		Increases based on footing Width	
Coefficient of Son/Concre	ete Friction	0.30		Allowable pressure increase per foot	ksf
				when maximum length or width is greater tha	ft
				Maximum Allowed Bearing Pressure	10.0 ksf
				(A value of zero implies no limit)	
				Adjusted Allowable Soil Bearing	2.0 ksf
				(Allowable Soil Bearing adjusted for footing weig depth & width increases as specified by user.)	ght and

Dimensions & Reinforcing

Distance Left of Column #1 Between Columns	= -	1.250 ft 2.50 ft	Pedestal di	men			Bars left of Col #1	Count	Size #	As Provided	As Req'd
Distance Right of Column #2	= .	1.250 ft			Col #1	Col #2	Bottom Bars	7.0	5	2.170	2.268 in^2
Total Footing Length		5.0 ft	Sq. Dim.	=	6.0	6.0 in	Top Bars	7.0	5	2.170	2.268 in^2
Total Footing Length	_	3.010	Height	=		in	Bars Btwn Cols				
Footing Width	=	2.50 ft	•				Bottom Bars	7.0	5	2.170	2.268 in^2
Footing Thickness	=	42.0 in					Top Bars	7.0	5	2.170	2.268 in^2
· ·		72.0111					Bars Right of Col #	‡2			
Rebar Center to Concrete Edg	e @ Top		= 3.0	0 in			Bottom Bars	7.0	5	2.170	2.268 in^2
Rebar Center to Concrete Edg	e @ Bottom	ו :	= 3.0	0 in			Top Bars	7.0	5	2.170	0.0 in^2

Applied Loads

Applied @ Left Column		D	Lr	L	S	W	E	Н
Axial Load Downward	=	-3.760						k
Moment (+CW)	=							k-ft
Shear (+X)	=							k
Applied @ Right Column								
Axial Load Downward	=	3.80						k
Moment (+CW)	=							k-ft
Shear (+X)	=							k
Overhurden	=							



Project Title: Engineer: Project ID: Project Descr:

Combined Footing

LIC#: KW-06012847, Build:20.23.10.02 United Structural Design

Project File: 23668.ec6
(c) ENERCALC INC 1983-2023

DESCRIPTION: Tank Footing

DESIG	N SUMM	Design OK			
Facto	or of Safety	Item	Applied	Capacity	Governing Load Combination
PASS	1.462	Overturning	14.10 k-ft	20.609 k-ft	D Only
PASS I	No Sliding	Sliding	0.0 k	1.915 k	No Sliding
PASS	2.698	Uplift	3.760 k	10.144 k	D Only
Utiliz	zation Ratio	Item	Applied	Capacity	Governing Load Combination
PASS	0.8330	Soil Bearing	1.666 ksf	2.0 ksf	D Only
PASS	0.01167	1-way Shear - Col #1	0.9588 psi	82.158 psi	+1.40D
PASS	0.01167	1-way Shear - Col #2	0.9589 psi	82.158 psi	+1.40D
PASS	0.002938	2-way Punching - Col #1	0.4827 psi	164.317 psi	+1.40D
PASS	0.003650	2-way Punching - Col #2	0.5997 psi	164.317 psi	+1.40D
PASS	0.002325	Flexure - Left of Col #1 - Top	-0.8661 k-ft	372.525 k-ft	+1.40D
PASS N	No Bending	Flexure - Left of Col #1 - Bottom	0.0 k-ft	0.0 k-ft	N/A
PASS	0.001832	Flexure - Between Cols - Top	-0.6823 k-ft	372.525 k-ft	+1.40D
		Flexure - Between Cols - Bottom	2.171 k-ft	372.525 k-ft	+1.40D
PASS N	No Bendina	Flexure - Right of Col #2 - Top	0.0 k-ft	0.0 k-ft	N/A
PASS	_	Flexure - Right of Col #2 - Bottom	1.676 k-ft	372.525 k-ft	+1.40D

Soil Bearing

		Eccentricity	Actual Soil Bea	Actual / Allow		
Load Combination	Total Bearing	from Ftg CL	@ Left Edge	@ Right Edge	Allowable	Ratio
D Only	6.38 k	1.480 ft	0.00 ksf	1.67 ksf	2.00 ksf	0.833
+0.60D	3.83 k	1.480 ft	0.00 ksf	1.00 ksf	2.00 ksf	0.500

Overturning Stability

	Vlom	Moments about Left Edg€ k-ft			loments about Right Edg k-ft			
Load Combination	Overturning	Resisting	Ratio	Overturning	Resisting	Ratio		
D Only	4.70	30.11	6.406	14.10	20.61	1.462		
+0.60D	2.82	18.07	6.406	8.46	12.37	1.462		

Sliding Stability

Load Combination	Sliding Force	Resisting Force	Sliding SafetyRatio
D Only	0.00 k	1.92 k	999
+0.60D	0.00 k	1.15 k	999
Z-Axis Footing Flexure - Maximum V	alues for Load Combination		

		Distance	Tension		Governed	Actual As	Phi*Mn	Mu / PhiMn
Load Combination	Mu	from left	Side	As Req'd	by			
	(ft-k)	(ft)		(in^2)		(in^2)	(ft-k)	
+0.60D	0.000	0.000	0	0.000	0	0.000	0.000	0.000
+0.60D	0.000	0.013	0	0.000	0	0.000	0.000	0.000
+0.60D	0.000	0.025	0	0.000	0	0.000	0.000	0.000
+0.60D	0.000	0.038	0	0.000	0	0.000	0.000	0.000
+0.60D	0.000	0.050	0	0.000	0	0.000	0.000	0.000
+0.60D	0.000	0.063	0	0.000	0	0.000	0.000	0.000
+0.60D	0.000	0.075	0	0.000	0	0.000	0.000	0.000
+0.60D	0.000	0.088	0	0.000	0	0.000	0.000	0.000
+0.60D	0.000	0.100	0	0.000	0	0.000	0.000	0.000
+1.40D	-0.011	0.113	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.014	0.125	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.017	0.138	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.020	0.150	Top	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.023	0.163	Top	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.027	0.175	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.031	0.188	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.036	0.200	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.040	0.213	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.045	0.225	Top	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.050	0.238	Top	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.056	0.250	Top	2.268	Min Temp %	2.170	372.525	0.000

Combined Footing

LIC#: KW-06012847, Build:20.23.10.02 United Structural Design

Project File: 23668.ec6
(c) ENERCALC INC 1983-2023

DESCRIPTION: Tank Footing

Load Combination	Mu	Distance from left	Tension Side	As Req'd	Governed by	Actual As	Phi*Mn	Mu / PhiMr
	(ft-k)	(ft)		(in^2)	•	(in^2)	(ft-k)	
+1.40D	-0.061	0.263	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.067	0.275	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.073	0.288	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.080	0.300	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.087	0.313	Top	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.094	0.325	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.101	0.338	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.109	0.350	Top	2.268 2.268	Min Temp %	2.170 2.170	372.525 372.525	0.000
+1.40D +1.40D	-0.117 -0.125	0.363 0.375	Top Top	2.268	Min Temp % Min Temp %	2.170	372.525 372.525	0.000 0.000
+1.40D	-0.123	0.373	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.142	0.400	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.151	0.413	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D	-0.160	0.425	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.170	0.438	Top	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.180	0.450	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	-0.190	0.463	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.200	0.475	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.211	0.488	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.222	0.500	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.233	0.513	Top	2.268	Min Temp %	2.170	372.525	
+1.40D	-0.245	0.525	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.257	0.538	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.269 0.281	0.550	Top	2.268	Min Temp %	2.170	372.525	0.001
+1.40D +1.40D	-0.281 -0.294	0.563 0.575	Top Top	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.001 0.001
+1.40D	-0.294	0.588	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.320	0.600	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.333	0.613	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D	-0.347	0.625	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.361	0.638	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.375	0.650	Top	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.390	0.663	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.405	0.675	Top	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.420	0.688	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.435	0.700	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.451	0.713	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.467	0.725	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.483	0.738	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D +1.40D	-0.500 -0.516	0.750 0.763	Top Top	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.001 0.001
+1.40D +1.40D	-0.533	0.763	Тор	2.268	Min Temp %	2.170	372.525 372.525	0.001
+1.40D	-0.551	0.773	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.568	0.800	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D	-0.586	0.813	Тор	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.604	0.825	Тор	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.623	0.838	Top	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.642	0.850	Top	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.661	0.863	Тор	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.680	0.875	Top	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.700	0.888	Тор	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.719	0.900	Top	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.740	0.913	Тор	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.760	0.925	Top	2.268	Min Temp %	2.170	372.525	0.002
+1.40D +1.40D	-0.781 0.802	0.938	Top	2.268	Min Temp %	2.170	372.525 372.525	0.002
+1.40D +1.40D	-0.802 -0.823	0.950	Top Top	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.002 0.002
+1.40D +1.40D	-0.823 -0.844	0.963 0.975	Тор	2.268	Min Temp %	2.170	372.525 372.525	0.002
+1.40D +1.40D	-0.866	0.973	Тор	2.268	Min Temp %	2.170	372.525	0.002
+1.40D +1.40D	-0.888	1.000	Тор	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.910	1.013	Тор	2.268	Min Temp %	2.170	372.525	0.002
	-0.930	1.025	Тор	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.930	1.023	100	∠.∠∪∪				

Combined Footing

LIC#: KW-06012847, Build:20.23.10.02 United Structural Design

Project File: 23668.ec6
(c) ENERCALC INC 1983-2023

DESCRIPTION: Tank Footing

Load Combination	Mu	Distance from left	Tension Side	As Req'd	Governed by	Actual As	Phi*Mn	Mu / PhiMr
	(ft-k)	(ft)		(in^2)	•	(in^2)	(ft-k)	
+1.40D	-0.966	1.050	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-0.982	1.063	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D	-0.997	1.075	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.010	1.088	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.022	1.100	Top	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.033	1.113	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.042	1.125	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.050 1.056	1.138	Top	2.268 2.268	Min Temp %	2.170 2.170	372.525 372.525	0.003
+1.40D +1.40D	-1.056 -1.061	1.150 1.163	Top Top	2.268	Min Temp % Min Temp %	2.170	372.525 372.525	0.003 0.003
+1.40D	-1.065	1.175	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.067	1.188	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.068	1.200	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D	-1.068	1.213	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.066	1.225	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.063	1.238	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.059	1.250	Top	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.053	1.263	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.046	1.275	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D	-1.037	1.288	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.027	1.300	Top	2.268	Min Temp %	2.170	372.525	
+1.40D	-1.016	1.313	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-1.003	1.325	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-0.989 0.074	1.338	Top	2.268	Min Temp %	2.170	372.525	0.003 0.003
+1.40D +1.40D	-0.974 -0.957	1.350 1.363	Тор Тор	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.003
+1.40D	-0.939	1.375	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-0.919	1.388	Тор	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	-0.898	1.400	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D	-0.876	1.413	Top	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.853	1.425	Тор	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.828	1.438	Top	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.801	1.450	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D	-0.774	1.463	Top	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.745	1.475	Тор	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.714	1.488	Top	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.682	1.500	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D	-0.650	1.513	Тор	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	-0.618	1.525	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D +1.40D	-0.586 -0.555	1.538 1.550	Top Top	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.002 0.001
+1.40D +1.40D	-0.523	1.563	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.492	1.575	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.462	1.588	Тор	2.268	Min Temp %	2.170	372.525	
+1.40D	-0.431	1.600	Top	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.401	1.613	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.371	1.625	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.342	1.638	Top	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.312	1.650	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.283	1.663	Top	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.255	1.675	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.226	1.688	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.198	1.700	Тор	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	-0.170	1.713	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D +1.40D	-0.142 0.115	1.725	Top	2.268	Min Temp %	2.170	372.525	0.000
+1.40D +1.40D	-0.115 -0.088	1.738 1.750	Top Top	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.000 0.000
+1.40D +1.40D	-0.088 -0.061	1.750	Тор	2.268	Min Temp %	2.170	372.525 372.525	0.000
+1.40D +1.40D	-0.035	1.703	Тор	2.268	Min Temp %	2.170	372.525	0.000
+1.40D +1.40D	0.000	1.773	10р 0	0.000	0	0.000	0.000	0.000
+1.40D	0.018	1.800	Bottom	2.268	Min Temp %	2.170	372.525	0.000
	0.043	1.813	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	U.U 4 .5	[.013	DOLLOIII	Z.ZUU				

Combined Footing

LIC#: KW-06012847, Build:20.23.10.02 United Structural Design

Project File: 23668.ec6
(c) ENERCALC INC 1983-2023

DESCRIPTION: Tank Footing

Load Combination	Mu	Distance from left	Tension Side	As Reg'd	Governed by	Actual As	Phi*Mn	Mu / PhiMn
Load Combination	(ft-k)	(ft)	Side	(in^2)	Бу	(in^2)	(ft-k)	WIG / FIIIWIII
+1.40D	0.094	1.838	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.119	1.850	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.143	1.863	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.168	1.875	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.192	1.888	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.215	1.900	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.239	1.913	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.262	1.925	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.285	1.938	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.308	1.950	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.330	1.963	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.352	1.975	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.374	1.988	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.396	2.000	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.417	2.013	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.438	2.025	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.459	2.038	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.479	2.050	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.500	2.063	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.520	2.075	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.539	2.088	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.559	2.100	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.578	2.112	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.598	2.125	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.616	2.137	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.635	2.150	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.654	2.162	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.672	2.175	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.690	2.187	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.708	2.200	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.725	2.212	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.743	2.225	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.760	2.237	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.777	2.250	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.794 0.811	2.262	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D +1.40D	0.827	2.275	Bottom	2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.002 0.002
+1.40D +1.40D	0.844	2.287 2.300	Bottom Bottom	2.268 2.268	Min Temp %	2.170	372.525	0.002
+1.40D +1.40D	0.860	2.312	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.876	2.325	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.892	2.323	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.908	2.350	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.923	2.362	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.938	2.375	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.954	2.387	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	0.969	2.400	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	0.984	2.412	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	0.999	2.425	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.013	2.437	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.028	2.450	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.042	2.462	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.057	2.475	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.071	2.487	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.085	2.500	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.099	2.512	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.113	2.525	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.126	2.537	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.140	2.550	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.154	2.562	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.167	2.575	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.180	2.587	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.194	2.600	Bottom	2.268	Min Temp %	2.170	372.525	0.003
1.700	1.207	2.612		2.268	Min Temp %	2.170	372.525	0.003

Combined Footing

LIC#: KW-06012847, Build:20.23.10.02 United Structural Design

Project File: 23668.ec6
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DESCRIPTION: Tank Footing

Load Combination	Mu	Distance from left	Tension Side	As Req'd	Governed by	Actual As	Phi*Mn	Mu / PhiMr
	(ft-k)	(ft)		(in^2)	-	(in^2)	(ft-k)	
+1.40D	1.220	2.625	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.233	2.637	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.246	2.650	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.259	2.662	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.272	2.675	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.285	2.687	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.298 1.310	2.700	Bottom	2.268	Min Temp % Min Temp %	2.170 2.170	372.525	0.003 0.004
+1.40D +1.40D	1.323	2.712 2.725	Bottom Bottom	2.268 2.268	Min Temp %	2.170	372.525 372.525	
+1.40D +1.40D	1.336	2.723	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.348	2.750	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.361	2.762	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.373	2.775	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.386	2.787	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.398	2.800	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.411	2.812	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.423	2.825	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.435	2.837	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.448	2.850	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.460	2.862	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.473	2.875	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D +1.40D	1.485 1.497	2.887 2.900	Bottom Bottom	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.004
+1.40D +1.40D	1.510	2.900	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D +1.40D	1.522	2.925	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.535	2.937	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.547	2.950	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.559	2.962	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.572	2.975	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.584	2.987	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.597	3.000	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.610	3.012	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.622	3.025	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.635	3.037	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.648	3.050	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.660	3.062	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D +1.40D	1.673 1.686	3.075 3.087	Bottom Bottom	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.004 0.005
+1.40D +1.40D	1.699	3.100	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D +1.40D	1.712	3.112	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.725	3.125	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.739	3.137	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.752	3.150	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.765	3.162	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.779	3.175	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.792	3.187	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.806	3.200	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.819	3.212	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.833	3.225	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.847	3.237	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.861	3.250	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.875	3.262	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D +1.40D	1.890	3.275	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D +1.40D	1.904 1.919	3.287 3.300	Bottom Bottom	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.005 0.005
+1.40D +1.40D	1.933	3.312	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D +1.40D	1.948	3.325	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.963	3.337	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.978	3.350	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.993	3.362	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	2.009	3.375	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	2.024	3.387	Bottom	2.268	Min Temp %	2.170	372.525	0.005
· 1.40B	2.040							

Combined Footing LIC#: KW-06012847, Build:20.23.10.02

United Structural Design

Project File: 23668.ec6 (c) ENERCALC INC 1983-2023

DESCRIPTION: Tank Footing

Load Cambination	NA	Distance	Tension	An Dowld	Governed	Actual Ac	Dhi*Mn	M / Db:M.
Load Combination	Mu (ft-k)	from left (ft)	Side	As Req'd (in^2)	by	Actual As (in^2)	Phi*Mn (ft-k)	Mu / PhiM
+1.40D	2.055	3.412	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.071	3.425	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.088	3.437	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.104	3.450	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.120	3.462	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.137	3.475	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.154	3.487	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.171	3.500	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.187	3.512	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D +1.40D	2.202	3.525	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D +1.40D	2.216			2.268	Min Temp %	2.170	372.525	
	2.210	3.537	Bottom				372.323	
+1.40D	2.228	3.550	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.238	3.562	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.247	3.575	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.255	3.587	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.261	3.600	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.266	3.612	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.269	3.625	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.271	3.637	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.271	3.650	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.270	3.662	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.268	3.675	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.264	3.687	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	2.258	3.700	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.252	3.712	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.243	3.725	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D +1.40D	2.234			2.268	Min Temp %	2.170	372.525	0.006
	2.234	3.737	Bottom					
+1.40D	2.223	3.750	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.211	3.762	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	2.197	3.775	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.182	3.787	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	2.165	3.800	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.147	3.812	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.128	3.825	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.107	3.837	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.085	3.850	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.062	3.862	Bottom	2.268	Min Temp %	2.170	372.525	0.006
+1.40D	2.037	3.875	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	2.011	3.887	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.984	3.900	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.955	3.912	Bottom	2.268	Min Temp %	2.170	372.525	
+1.40D	1.924	3.925	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.893	3.937	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.860	3.950	Bottom	2.268	Min Temp %	2.170	372.525	0.005
		3.962				2.170		
+1.40D	1.826		Bottom	2.268	Min Temp %		372.525	0.005
+1.40D	1.790	3.975	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.753	3.987	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.715	4.000	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.676	4.012	Bottom	2.268	Min Temp %	2.170	372.525	0.005
+1.40D	1.638	4.025	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.600	4.037	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.562	4.050	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.525	4.062	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.488	4.075	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.451	4.087	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.415	4.100	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.379	4.112	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.344	4.125	Bottom	2.268	Min Temp %	2.170	372.525	0.004
+1.40D	1.308	4.137	Bottom	2.268	Min Temp %	2.170	372.525	0.004
	1.300							
+1.40D	1.274	4.150	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.239	4.162	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D +1.40D	1.205 1.172	4.175 4.187	Bottom Bottom	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.003 0.003

Combined Footing

LIC#: KW-06012847, Build:20.23.10.02 United Structural Design

Project File: 23668.ec6
(c) ENERCALC INC 1983-2023

DESCRIPTION: Tank Footing

Load Combination	8.4	Distance	Tension	An Daniel	Governed	Actual Ac	Db:#44	M., / Dh:Na
Load Combination	Mu (ft-k)	from left (ft)	Side	As Req'd	by	Actual As (in^2)	Phi*Mn (ft-k)	Mu / PhiMn
+1.40D	1.138	4.200	Bottom	(in^2) 2.268	Min Town 0/	2.170	372.525	0.003
+1.40D +1.40D	1.106	4.212	Bottom	2.268	Min Temp % Min Temp %	2.170	372.525 372.525	0.003
+1.40D	1.073	4.225	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.041	4.237	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	1.010	4.250	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	0.978	4.262	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	0.948	4.275	Bottom	2.268	Min Temp %	2.170	372.525	0.003
+1.40D	0.917	4.287	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.887	4.300	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.858	4.312	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.829	4.325	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.800	4.337	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.772	4.350	Bottom	2.268	Min Temp % Min Temp %	2.170	372.525	0.002 0.002
+1.40D +1.40D	0.744 0.717	4.362 4.375	Bottom Bottom	2.268 2.268	Min Temp %	2.170 2.170	372.525 372.525	0.002
+1.40D	0.690	4.387	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.663	4.400	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.637	4.412	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.612	4.425	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.587	4.437	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.562	4.450	Bottom	2.268	Min Temp %	2.170	372.525	0.002
+1.40D	0.538	4.462	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.514	4.475	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.491	4.487	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.469	4.500	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.446	4.512	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.425 0.403	4.525 4.537	Bottom	2.268	Min Temp % Min Temp %	2.170	372.525	0.001
+1.40D +1.40D	0.403	4.557 4.550	Bottom Bottom	2.268 2.268	Min Temp %	2.170 2.170	372.525 372.525	0.001 0.001
+1.40D	0.363	4.562	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.343	4.575	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.324	4.587	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.305	4.600	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.287	4.612	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.269	4.625	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.252	4.637	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.235	4.650	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.219	4.662	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.204	4.675	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D	0.189	4.687	Bottom	2.268	Min Temp %	2.170	372.525	0.001
+1.40D +1.40D	0.174 0.161	4.700 4.712	Bottom	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.000
+1.40D +1.40D	0.147	4.712	Bottom Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.134	4.737	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.122	4.750	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.110	4.762	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.099	4.775	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.089	4.787	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.079	4.800	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.069	4.812	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.061	4.825	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.052	4.837	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.045	4.850	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.038	4.862	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.031	4.875	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D +1.40D	0.025 0.020	4.887 4.900	Bottom Bottom	2.268 2.268	Min Temp % Min Temp %	2.170 2.170	372.525 372.525	0.000
+1.40D +1.40D	0.020	4.900	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.013	4.925	Bottom	2.268	Min Temp %	2.170	372.525	0.000
+1.40D	0.000	4.937	0	0.000	0	0.000	0.000	0.000
+1.40D	0.000	4.950	Ő	0.000	Ö	0.000	0.000	0.000
		4.962	Ö	0.000	Ö	0.000	0.000	0.000
+1.40D	0.000	4.902	U	0.000			0.000	0.000

Project File: 23668.ec6

Project Title: Engineer: Project ID: Project Descr:

Combined Footing

LIC#: KW-06012847, Build:20.23.10.02 United Structural Design (c) ENERCALC INC 1983-2023

DESCRIPTION: Tank Footing

		Distance	Tension		Governed			
Load Combination	Mu	from left	Side	As Req'd	by	Actual As	Phi*Mn	Mu / PhiMn
	(ft-k)	(ft)		(in^2)		(in^2)	(ft-k)	
+1.40D	0.000	4.987	0	0.000	0	0.000	0.000	0.000
+1.40D	0.000	5.000	0	0.000	0	0.000	0.000	0.000
One Way Shear					Punching	Shear		
Load Combination	Phi Vn	vu @	Col #1	vu @ Col #2	Phi Vn	vu @ C	ol #1 v	u @ Col #2
+1.40D	82.16 ps	i 0.	96 psi	0.96 psi	164.32 p	si 0.48	psi	0.60 psi
+1.20D	82.16 ps	i 0.	82 psi	0.82 psi	164.32 p	si 0.41 ₁	psi	0.51 psi
+0.90D	82.16 ps	i 0.	62 psi	0.62 psi	164.32 p	si 0.31	psi	0.39 psi

Project File: 23668.ec6

Project Title: Engineer: Project ID: Project Descr:

Pole Footing Embedded in Soil

DESCRIPTION: Crash Post footing

Code References

Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

Load Combinations Used: IBC 2018

General Information

 Allow Passive
 350.0 pcf

 Max Passive
 1,500.0 psf

Controlling Values

Governing Load Combination Only

Lateral Load 3.0 k Moment 9.0 k-ft

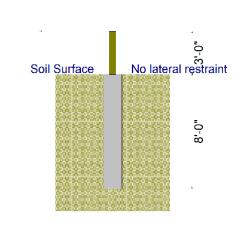
NO Ground Surface Restraint

Pressures at 1/3 Depth

Actual 930.31 psf Allowable 930.86 psf

Minimum Required Depth	8.0 ft
------------------------	--------

Footing Base Area 1.396 ft^2 Maximum Soil Pressure 0.0 ksf



Applied Loads

Lateral Concentrated Lo	ad (k)	Lateral Distributed Loads (k	Vertical Load (k)
D : Dead Load	3.0 k	k/ft	k
Lr : Roof Live	k	k/ft	k
L : Live	k	k/ft	k
S : Snow	k	k/ft	k
W : Wind	k	k/ft	k
E : Earthquake	k	k/ft	k
H : Lateral Earth	k	k/ft	k
Load distance above		TOP of Load above ground surface	
ground surface	3.0 ft	ft	
		BOTTOM of Load above ground surface	
		ft	

Load Combination Results

	Forces @	Ground Surface	Required	Pressure at	1/3 Depth	Soil Increase
Load Combination	Loads - (k)	Moments - (ft-k)	Depth - (ft)	Actual - (psf)	Allow - (psf)	Factor
D Only	3.000	9.000	8.00	930.3	930.9	1.000
+0.60D	1.800	5.400	6.50	745.7	746.8	1.000



Company:	Date:	10/18/2023
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Project:		•
Address:		
Phone:		
E-mail:		

1.Project information

Customer company: Customer contact name: Customer e-mail: Comment: Project description: Location: Fastening description:

2. Input Data & Anchor Parameters

General

Design method:ACI 318-14 Units: Imperial units

Anchor Information:

Anchor type: Cast-in-place

Material: AB

Diameter (inch): 0.875

Effective Embedment depth, hef (inch): 5.000

Anchor category: -Anchor ductility: Yes h_{min} (inch): 7.38 C_{min} (inch): 5.25 S_{min} (inch): 5.25

Base Material

Concrete: Normal-weight Concrete thickness, h (inch): 12.00 State: Uncracked Compressive strength, f'c (psi): 3000

Ψ_{c,V}: 1.0

Reinforcement condition: B tension, B shear

Supplemental reinforcement: No Reinforcement provided at corners: No Ignore concrete breakout in tension: No Ignore concrete breakout in shear: No Ignore 6do requirement: No

Build-up grout pad: No

Base Plate

Length x Width x Thickness (inch): 6.00 x 6.00 x 0.25

Recommended Anchor

Anchor Name: PAB Pre-Assembled Anchor Bolt - PAB7 (7/8"Ø)





Company:	Date:	10/18/2023
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Address:		
Phone:		
E-mail:		

Load and Geometry Load factor source: ACI 318 Section 5.3

Load combination: not set Seismic design: No

Anchors subjected to sustained tension: Not applicable

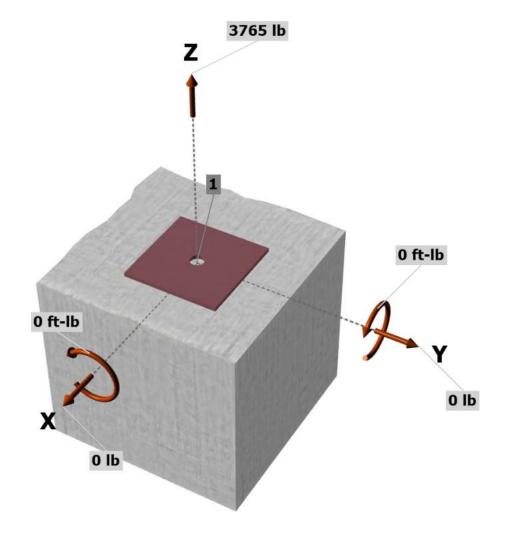
Apply entire shear load at front row: No

Anchors only resisting wind and/or seismic loads: No

Strength level loads:

Nua [lb]: 3765 V_{uax} [lb]: 0 V_{uay} [lb]: 0 M_{ux} [ft-lb]: 0 M_{uy} [ft-lb]: 0

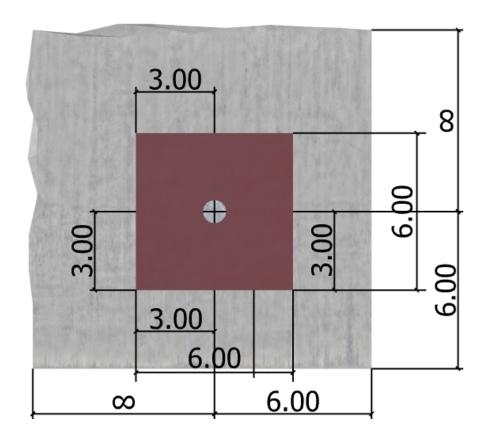
<Figure 1>





Company:	Date:	10/18/2023
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Address:		
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E-mail:		

<Figure 2>





Company:	Date:	10/18/2023
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Phone:		
E-mail:		

3. Resulting Anchor Forces

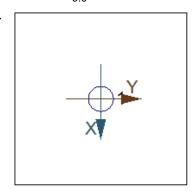
Anchor	Tension load, N _{ua} (lb)	Shear load x, V _{uax} (lb)	Shear load y, V _{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	3765.0	0.0	0.0	0.0
Sum	3765.0	0.0	0.0	0.0

Maximum concrete compression strain (‰): 0.00 Maximum concrete compression stress (psi): 0

Resultant tension force (lb): 3765 Resultant compression force (lb): 0

Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00 Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension (Sec. 17.4.1)

Nsa (lb)	ϕ	$\phi \mathcal{N}_{sa}$ (lb)
26795	0.75	20096

5. Concrete Breakout Strength of Anchor in Tension (Sec. 17.4.2)

 $N_b = k_c \lambda_a \sqrt{f'_c h_{ef}^{1.5}}$ (Eq. 17.4.2.2a)

Kc	λa	f′c (psi)	h _{ef} (In)	N _b (lb)					
24.0	1.00	3000	5.000	14697					
$\phi N_{cb} = \phi (A_N)$	$_{lc}$ / $A_{Nco})$ $\Psi_{ed,N}$ $\Psi_{c,l}$	$_{N}\Psi_{cp,N}N_{b}$ (Sec. 1	7.3.1 & Eq. 17.	4.2.1a)					
A_{Nc} (in ²)	A_{Nco} (in ²)	c _{a,min} (in)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$arPsi_{c ho,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)	
216.64	225.00	6.00	0.940	1.25	1.000	14697	0.70	11639	

6. Pullout Strength of Anchor in Tension (Sec. 17.4.3)

 $\phi N_{\rho n} = \phi \Psi_{c,P} N_{\rho} = \phi \Psi_{c,P} 8 A_{brg} f'_{c}$ (Sec. 17.3.1, Eq. 17.4.3.1 & 17.4.3.4)

$\Psi_{C,P}$	A_{brg} (in ²)	f_c (psi)	ϕ	ϕN_{pn} (lb)
1.4	4.07	3000	0.70	95609



Company:	Date:	10/18/2023
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Project:	=	•
Address:		
Phone:		
E-mail:		

11. Results

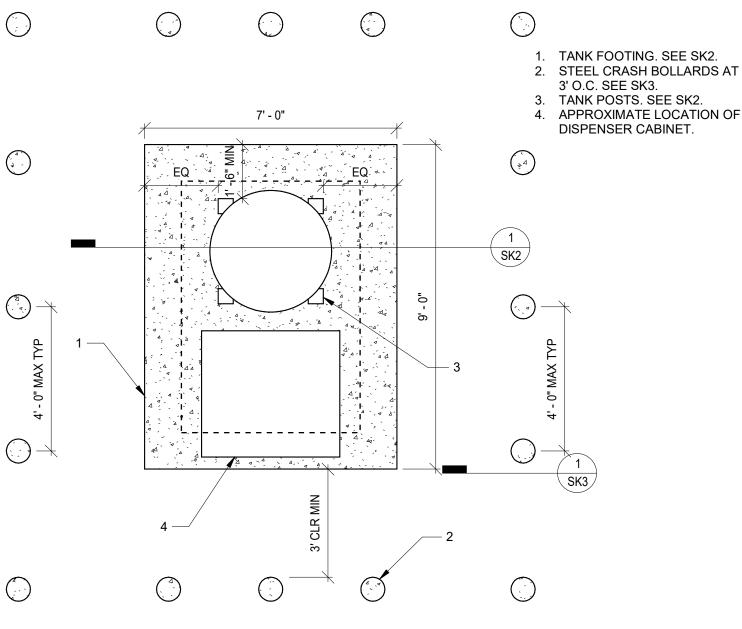
11. Interaction of Tensile and Shear Forces (Sec. D.7)?

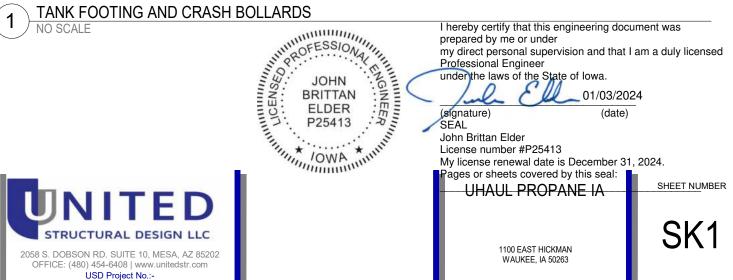
Tension	Factored Load, N _{ua} (lb)	Design Strength, øNn (lb)	Ratio	Status
Steel	3765	20096	0.19	Pass
Concrete breakout	3765	11639	0.32	Pass (Governs)
Pullout	3765	95609	0.04	Pass

PAB7 (7/8"Ø) with hef = 5.000 inch meets the selected design criteria.

12. Warnings

- Designer must exercise own judgement to determine if this design is suitable.





Project No.:-

1. 7'-0"x9'-0"x1-6" THICK SQUARE

REINFORCING IN SHORT

DIRECTION BOTTOM OF

PLATE BY OTHERS.

TANK COLUMNS AND BASE

7/8" DIA. ANCHOR BOLT AT EACH COLUMN. MIN. 12" EMBEDMENT.(2) STANDARD

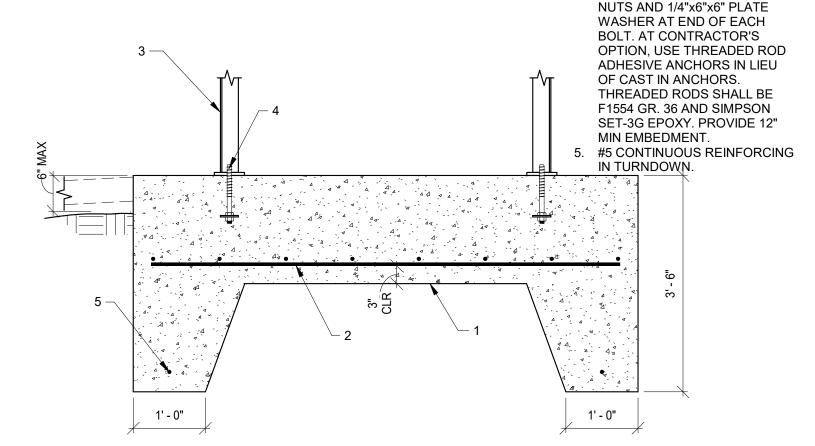
(8) #5 REINFORCING IN LONG DIRECTION AND (10) #5

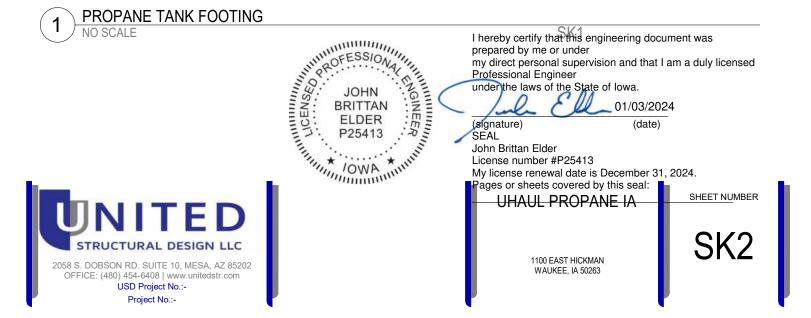
FOOTING.

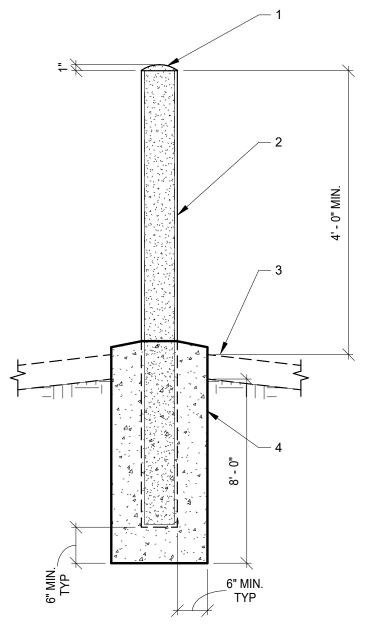
FOOTING.

DESIGN CRITERIA:

fc= 4,500 PSI Fy = 60.000 KSI soil bearing pressure = 1,500 PSF







- 1. FILL WITH GROUT AND CROWN TOP.
- 2. 4" STD STEEL POST. SCHEDULE 40; GALVANIZED.
- 3. FINISHED GRADE, CONCRETE SLAB, OR ASPHALT AS OCCURS.
- 4. 16" DIA. CONCRETE FOOTING (CLASS B) F'c = 2,500.

NOTES:

- SAFETY POST SHALL COMPLY WITH THE MINIMUM REQUIREMENTS OF NFP 58, CITY, AND AHJ.
- BOLLARD SPACING SHALL NOT EXCEED 4 FEET BETWEEN POSTS ON CENTER.
- BOLLARDS SHALL BE LOCATED MINIMUM 3 FEET CLEAR FROM PROPANE TANK.

STEEL CRASH POST (BOLLARD)

NO SCALE

3251-1S-07

192-01

192-01

192-01

INDESSIONALITIES

BRITTAN

BRITTAN

BRITTAN

P25413

AND PASSIONALITIES

P25413

I hereby certify that this engineering document was prepared by me or under

my direct personal supervision and that I am a duly licensed Professional Engineer

under the laws of the State of Iowa.

SK1

01/03/2024 (date)

(signature) SEAL

John Brittan Elder License number #P25413

My license renewal date is December 31, 2024.

Pages or sheets covered by this seal:

UHAUL PROPANE IA

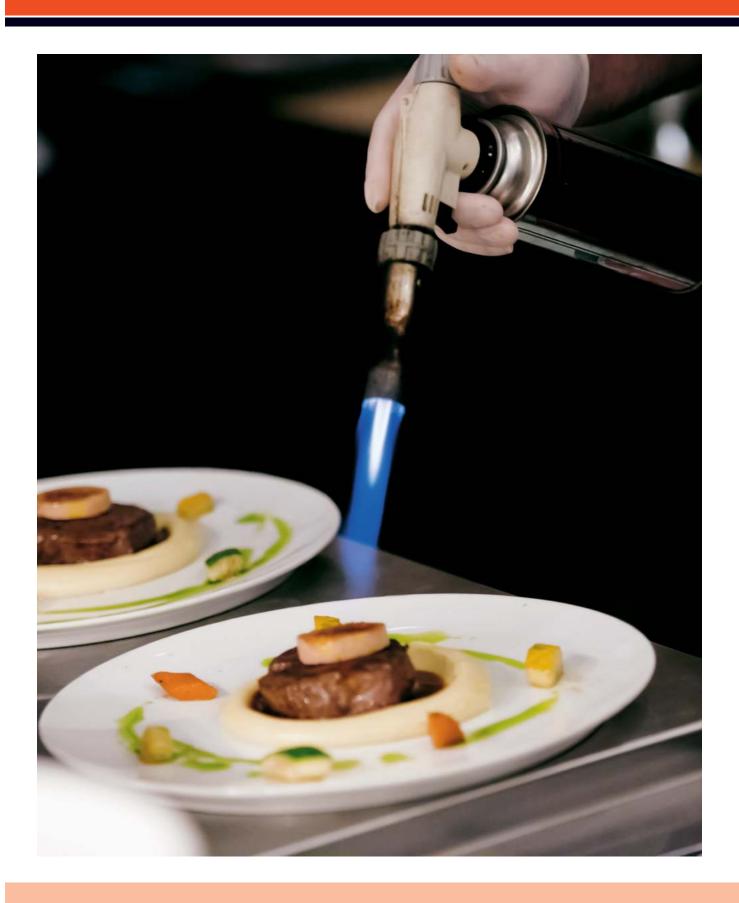
SHEET NUMBER

SK3

1100 EAST HICKMAN WAUKEE, IA 50263



PUMP





Spec Sheet 551-001

Section: 551
Effective: April 2015
Replaces: October 2014

Ebsray RC Series – Models RC20 & RC25 Regenerative Turbine Pump for LPG Applications



Design

The Ebsray RC Series Regenerative Turbine Pumps are designed and precision-built for high-pressure transfer of LPG, autogas, propane, and butane.

Applications

- LPG Autogas dispensers, single or two hoses (RC25)
- Industrial dispensing
- · Autogas refueling
- Marine dispensing
- Portable tanks
- Cylinder filling
- Forklift refueling
- · Direct burner or vaporizer feed

Features & Benefits

- Quiet, vibration-free operation
- Low maintenance, single-stage impeller
- Close coupled to standard NEMA C-face motors. IEC C-face adapters available.
- Simple installation with C-face close coupled mounting
- Versatile 3-port arrangement, self-venting design
- Bypass valve connection port direct on pump
- Balanced mechanical seal, unique cartridge design for simplicity of assembly/maintenance
- Throttle bushing for secondary sealing

Assured Quality & Performance

ISO 9001 Quality System assures compliance with the high safety and quality standards demanded by the LPG industry

Pumps are listed by Underwriters Laboratories for LP-gas service.



Ebsray RC Series – Models RC20 & RC25

Regenerative Turbine Pump for LPG Applications

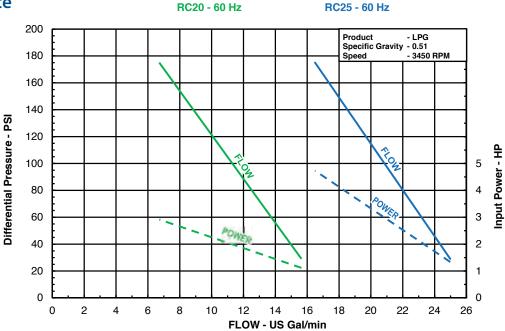
Maximum Operating Limits

Pump Mod	Flov	w Rate	Differer	ntial Press	ureHydi Tost I	rostatic	Po	wer	Pump Speed	We	eight
Pump Mod	gpm	L/min		bar	psi	bar	HP	kW	rpm	lbs	kg
RC20	15	58	175	12	1,015	70	2.9	2.2	3,500	43	19.5
RC25	25	94	175	12	1,015	70	4.8	3.6	3,500	43	19.5

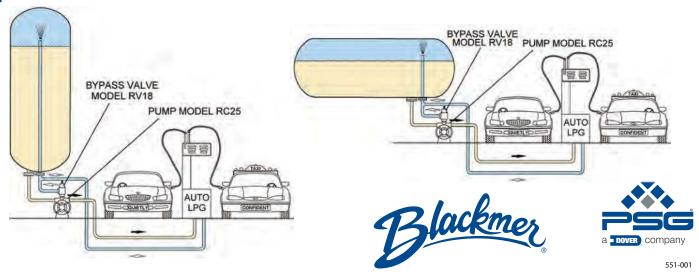
Porting:

Inlet: NPT 1" 90° and/or 180° Discharge: NPT 1" 90° and/or 180°

Performance



Typical Installations





Atlanta GA (800) 241-4155 Kansas City MO (800) 821-5062

Dallas TX (800) 821-1829 Little Rock AR (800) 643-8222

Fayetteville NC (800) 447-1625 Orlando FL (800) 821-0631

Houston TX (800) 334-7816 **Richmond VA** (800) 368-4013

Indianapolis IN (800) 241-1971 St. Louis MO (800) 423-4685

www.gasequipment.com

email: info@gasequipment.com



Ebsray RV Series – Model RV18 Bypass Valve for LPG Applications



Design

In-line design Bypass/Pressure Relief Valves are used for a wide variety of LPG services. Adjustable differential pressure is attained for accurate and repeatable performance in return-to-tank or bypass systems. This enables full pump flow while maintaining controlled preset maximum pressure.

Features & Benefits

- · CBS Constant Bleed System
- Chatter-free quiet operation
- 90° porting arrangement
- 1" NPT tapped ports. 1" ANSI 300 flanged option.
- · Adjustable pressure setting
- · Low pressure rise
- VRS Vapor Removal System

Spec Sheet 551-007

551 April 2015

Replaces: October 2014

Section:

Effective:

Assured Quality & Performance

ISO9001 Quality System assures compliance with the high safety and quality standards demanded by the LPG industry

Pumps are listed by Underwriters Laboratories for LP-gas service.



Ebsray RV Series – Model RV18 Bypass Valve for LPG Applications

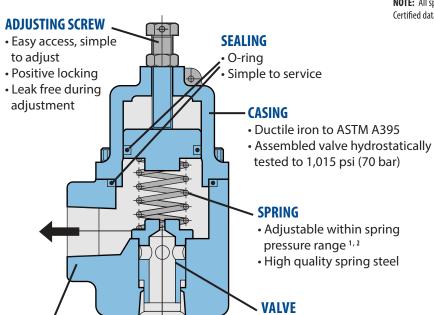
Maximum Operating Limits

Pump Mod	Flov	v Ra t e	Differen	tial Pres s ur	e Hydi Test I	rostatic Pressure
	gpm	L/min	psi	bar	psi	bar
RV18	52	200	203	14	1,015	70

Porting:

- 1" NPT tapped
- Downstream system resistance will affect differential pressure.
- Spring selection to suit required pressure range.
- Pressure rise is dependent upon flow through Bypass Valve

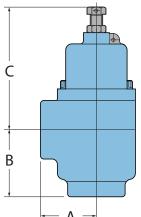
NOTE: All specifications and illustrations are typical only and subject to revision without notice. Certified data available upon request.

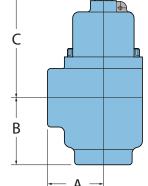


- Spool type quiet operation
- CBS (Constant Bleed System) Standard (optional VRS)

Dimensions

Pum	p Mod	el A	В	С	Ports	Weigh
D\/10	in	2.17	2.6	5.3	1" NPT	13.9 lbs
RV18	mm	55	66	135	Tapped	6.3 kg







551-007



Optional

• 1" NPT tapped

PORTS

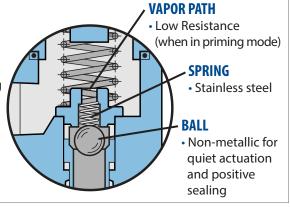
Integral "excess flow" type VRS. (Vapor Removal System)

Rapid Vapor Clearing

GAS EQUIPMENT CO., INC.

• Ease of installation service

- Efficiency after vapor clearing is completed "excess flow" valve closes fully. This ensures full pump outlet is available at discharge point.
- · Interchangeable with standard Spool Valve. (CBS)





SINCE 1937

Atlanta GA (800) 241-4155 Cansas City MO (800) 821-5062

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Houston TX (800) 334-7816 **Richmond VA** (800) 368-4013

Indianapolis IN (800) 241-1971 St. Louis MO (800) 423-4685

www.gasequipment.com

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MOTOR / ELECTRIC

Motor / Electric





LPG UNIT ELECTRICAL INSTALLATION GUIDELINES & NOTES

Page Number	011-037
Effective	Feb 2012
Replaces	New
Section	

This document is to serve as a guideline to assist in the installation, startup, and troubleshooting of the following pump and motor units – LGL1.25, LGL1.5 and LGL150 Series pumps. Only qualified personnel trained in the safe installation and operation of the equipment should install the unit. When connecting a unit to power please follow NEC (National Electric Code) and any other (country specific) local electrical codes that may apply during installation. Please verify all electrical information prior to startup of unit. This document is not intended to be used as a reference or authority for design, construction, or application of electrical systems.

Motor Wire Sizing:

Figure 1 contains a table of motor sizes and the respective recommended wire size depending upon the distance between the source and the load. As the distance increases from the source to the load, the voltage drops, caused by the resistance and reactance of a particular size of the wire. The wire must be sized properly to allow for this voltage drop to remain within an acceptable range. This is especially important for single phase motor applications. The following guidelines are minimums.

		Recon	nmended Motor	Wiring		
	Mo	otor		Recomm	nended Wire Size	e, AWG
HP	Motor Phase	Voltago	Full Load	Ler	ngth of Run in Fe	et
ПЕ	WOUNT Fliase	Voltage	Amperes	0-100	To 200	To 300
	1	120	42.5	4	2	1/0
3	l	240	21.25	10	8	6
3		240	12	<mark>12</mark>	<mark>12</mark>	10
	3	480	6	12	12	12
	4	120	70	3	1/0	2/0
5	I	240	35	8	6	4
5	2	240	19	12	10	8
	3	480	9.5	12	12	12
7.5	3	240	27.5	10	8	6
7.5	3	480	13.75	12	12	12

Figure 1: Recommended Motor Wiring*

Phased Power:

It is recommended to use three phase power where applicable. The three phase motor is a simpler design, more efficient by design, and also less costly than the single phase motor. The three phase motor allows for a higher starting torque, smoother operation, and allows the use of a smaller wire size over greater distances. Single phase power can be converted to three phase power by using a phase converter, which is readily available and inexpensive.

^{*} Information collected from standard voltage drop calculator, with a 3% allowable decrease in voltage drop or less using standard conditions. For conditions other than listed, consult NEC handbook, local standards, or engineering handbook. Wire sizes are expressed in AWG (American Wire Gauge). For other distances consult the Blackmer factory.

System Design:

Systems shall be designed according to NFPA standards and local codes. It is recommended that a Blackmer manufactured bypass valve be used in the system as they are designed to allow the optimum system performance and stability. Below is a list of informational bulletins that also guide installation of a Blackmer pump and bypass valve.

Application Bulletin 500-001: Liquefied Gas Handbook

Installation, Operation, and Maintenance 501-K00: LGL150 Series Pumps

Installation, Operation, and Maintenance 501-B00: LGL1.25 & LGL1.5 Series Pumps

Installation, Operation, and Maintenance 505-A01, A02, A03: Bypass Valves



SIEMENS

NEMA Motor Data

Ordering data:

1MB2221-1CB11-4AA3

Client order no. :

Order no.: Offer no. :

Item no.:

Consignment no. :

Project:

Remarks:

		Namepla	ite Data				Mour	nting and motor p	rotection
Туре	XP100 ID	1 - Class I, Gro	up D, Division			Type of c	onstruct	ion (A) Foot mounte	d - End shield
HP	3.0		Rating	Cont.		Motor pro	otection	(A) No winding pr	otection
Voltage	(14) 208-2	30/460V STD	Ins. Class	Insulation cl	ass F	Terminal	box des	ign (3) Mounting - F-1	
Amps	8.0 / 4.0 A		S.F.	1.15					
FL RPM	1760		Amb. Temp.	55 deg C				Bearing Data	
FL Efficiency	89.5 %		Temp. Rise	Class B				DE	ODE
FRAME	182T		kVA Code	K		Bearing Si	ze	6206 ZZ C3 S0	6206 ZZ C3 S0
DE AFBMA	30BC02JF	PP30	NEMA Des	В		Bearing Ty		Ball Bearing	Ball Bearing
ODE AFBMA	30BC02JF	PP30	Mtr WT	120		AFBMA	F-7-	30BC02JPP30	30BC02JPP30
60 Hertz	3 Ph	TEFC	IP	65					50500201 50
	~				1			Mechanical Dat	а
Load	No Load	Performan	/4 Full Loa	ad LRC		SAFE STA	LL TIME	HOT (s) 17	COLD (s) 29
***************************************	NO LOAG		4 % 89.5 %			Rtr wt (lbs)	23.7	Rtr WK2 0.300	00
Efficiency				0		FLT (ft-lbs)		LRT 21.0	BDT 32.0
Power Factor	0.4.4	racce a	78.5			rer (it-ios)	3.0	LN1 21.0	BD1 32.0
Current (A)	2.1 A		3 A 8.0 / 4.0			Ext Load Ir	nertia (W	(K2) Capability 17.0	
Inverter Duty	VT	20:1	CT	4:1					
				Typical	Noise D	ata			
A-weighted So	und	00	ctave Band Cer	nter Frequenci	es Hertz (H	lz)			
Pressure Level	63	125	250 50	00 1000	2000	4000	8000	SPL	63
at 3 feet		33	51 5	4 60	58	48	39	SPwrL	72
	Wiring Co	nnection In	formation					Special design :	
Description		3 PHASE -	9 LEAD - WYE						
Voltage	L1 L	.2 L3	Connecte	d					
LOW T	1 T7 T2	T8 T3 T9		T6 YY					
HIGH	T1 T	2 T3	T4 T7-T5 T8	тето У					

Lubrication Information

Manufacturer

Mobil Polyrex EM or equal

Type

Polyurea (standard)

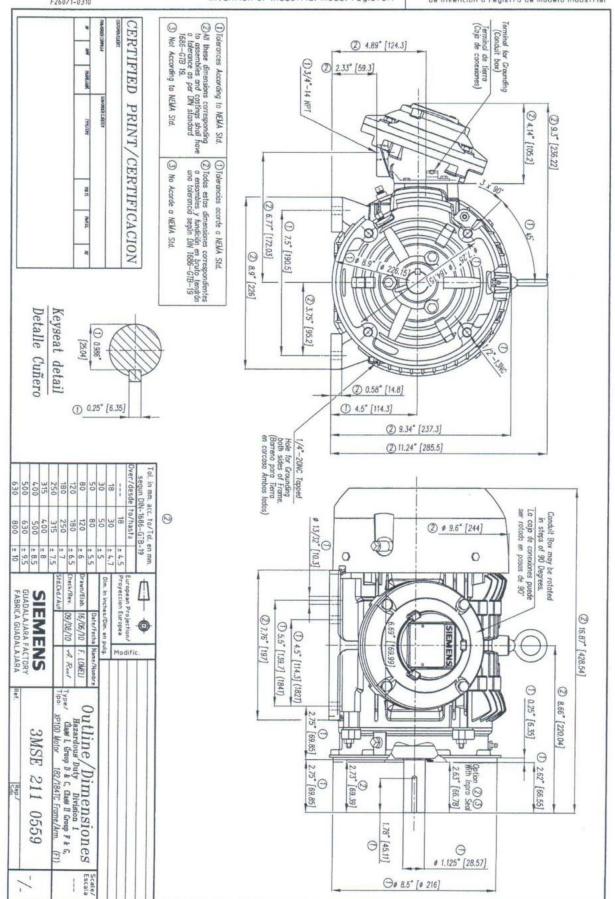
DE Capacity (oz.)

0.20

ODEnd Capacity (oz.)

0.20

Relubricate bearings every six months (more frequent if conditions require). See Instruction Manual.



File E120739 Project 09NK16907

January 24, 2011

REPORT

on

Motors for Use in Hazardous Locations

Siemens S A De C V Guadalajara, Mexico

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File E120739 Vol. 2 Sec. 1 Page 1 Issued: 2011-01-24 and Report

DESCRIPTION

PRODUCT COVERED:

USL, CNL XP100 Series Electric motors for use in Hazardous Locations, Class I, Groups C and D; Class II, Groups E, F, and G, Frame sizes 143, 145, 182, 184, 213, 215.

USL, CNL XP100 ID1 Series Electric motors for use in Hazardous Locations, Class I, Group D, Frame sizes 143, 145, 182, 184, 213, 215.

Motors are followed by suffixes T, TC, or TZ which denote length of shaft or length of shaft and flange design, respectively.

GENERAL:

These motors are squirrel cage TEFC electric motors for use in hazardous locations. The XP100 ID1 Series motors are identical to the XP100 Series motors except that they are provided without temperature limiting devices. Ratings and Markings differences are detailed in the description below.

RATINGS:

Maximum Horsepower	See Table 1 below
Maximum rpm	3600
Number of poles	2, 4, 6, 8
Service Factor	1.0 and 1.15 on sinusoidal power 1.0 on inverter power
Duty Rating	Continuous
Insulation Class	When marked Class F on nameplate, lead wires are Class F and the remaining components are Class H When marked Class H on nameplate, all components are Class H
Temperature Rise By Resistance	80°C by resistance
Ambient Temperature Rating	XP100 Series - 40°C XP100 ID1 Series - 60°C Maximum
Operating Temperature or Operating Temperature Code (External Surfaces)	T3C when motor has temperature limiting devices installed T2A when motor has no temperature limiting devices
Maximum Voltage Rating	600

EFS Non-Sealed Tumbler Switches

Explosionproof, Dust-Ignitionproof

Malleable Iron Body and Cover. Furnished with Internal Ground Screw.

Class I, Division 1 and 2, Groups C, D Class II, Division 1 and 2, Groups E, F, G Class III NEMA 7CD, 9EFG

Applications

- Designed to prevent arcing of enclosed switches in ignitable atmospheres during connect and disconnect operation of lighting and light power loads,
- For use in classified areas where ignitable vapors, gases or highly combustible dusts are present.
- · For installation in:
 - Chemical plants
 - Petrochemical plants
 - Refineries
 - Other process industries

Features

- · Enclosures have external mounting lugs for ease of mounting.
- Smooth, rounded integral bushing in each hub protects conductor insulation.
- · Enclosures furnished with internal ground screw.
- 20 Amp and 30 Amp units available for use with 120-277 Vac.
- Smooth ground mating surfaces assure flame-tight joint between cover and mounting enclosure.
- Stainless steel hex head cap screws for attaching cover to mounting enclosure.
- Choice of front-operating or side rocker arm handle—each may be locked in ON or OFF position.
- Each handle has close-tolerance threaded stainless steel shaft to meet explosionproof requirements.
- · Enclosures furnished with internal ground screw.

Options

- 1- or 2-gang copperfree (4/10 of 1% max.) aluminum bodies and covers available. Add suffix – A.
- NPBRKT nameplate mounting bracket to make circuit description/identification easy.
 - Pre-drilled holes in bottom of bracket allow direct mounting to control stations with existing cover bolts.
 - Pre-drilled holes in middle of bracket allow mounting of customer's circuit identification nameplate; epoxy glue may also be used for mounting (phenolic nameplate not included).
 - Bracket eliminates costly field installation of drilling and tapping to accommodate circuit identification nameplate.
 - Brackets fit side-by-side on 2-, 3- and 4-gang boxes and 3-devices.

Standard Materials

- · Body and cover: malleable iron
- Handle: nylon 6/6
- Optional nameplate mounting bracket: corrosion resistant stainless steel

Standard Finishes

 Tumbler switch body: triple-coat—(1) zinc electroplate, (2) chromate, and (3) epoxy powder coat

Certifications and Compliances

- UL Standards: UL 894, UL 1203
- UL Listed: E10523, E81751

Ordering Information for "Custom" Units

- Devices, covers and bodies may be ordered separately so that a different EFS switch may be used in each gang.
- Order components separately as follows:
 (1) select body catalog number,







Rocker Arm Operated

Illustrated Features





Handles may be locked in ON or OFF position

- (2) select cover catalog number, and
- (3) select switch or switch assembly catalog number (1-pole, 2-pole, 3-way or 4-way available in listings).

How to Order Hub Arrangements

 Simply send sketch indicating sizes and locations for brazed hubs on body or bodies selected from catalog listings. Orient sketch so that cover opening faces front and mounting lugs face upward and downward (box wall opposite cover should be referred to as the back of box).

Bodies and Hubs Available

- Tumbler switches may be ordered in single thru five gang deep malleable iron blank bodies with brazed hubs as specified at any location.
- Tumbler switches may be ordered with tandem malleable iron boxes with additional brazed hubs as specified.
- Standard malleable iron single and 2-gang tumbler switches may be ordered with additional brazed hubs as specified.
- Single and 2-gang tumbler switches may be ordered with aluminum boxes with additional brazed hubs as specified.

Related Products

 For classified-location push button, pilot light and selector switch control stations, see Explosionproof Control Stations Section. TS-510 Rev. B

Mechanical Flowmeter Transmitters Digital: Models VR and VRHR





DIGITAL TRANSMITTERS

Digital transmitters produce signals that exist only in one of two states: ON or OFF. These states may also be referred to as HIGH or LOW, or 1 or 0 (zero).

MODEL VR7697 (Models 35 & 45)

This economical and versatile bidirectional digital pulse

transmitter provides 10 pulses per revolution with excitation power of 115-250 VAC or 12-36 VDC, making it compatible with most remote read-out equipment.

MODEL VR7671 (HR) (Models 35 HR & 45 HR)

This solid state Hall Effect digital pulse transmitter provides 100 pulses per revolution. Note that input (excitation) power is limited to 10-15 VDC.

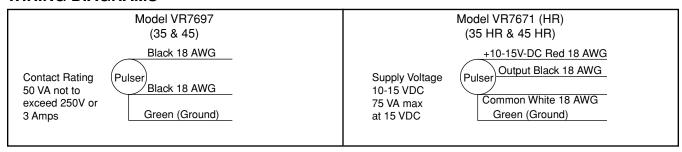
NEPTUNE DIGITAL PULSE ELECTRONIC TRANSMITTER DATA

Model No.	Type Of Device	Contact	Pulses per Revolution	Max Speed: Hz (RPM) (2)	Contact Rating (2)	Enclosure Rating	Input Voltage	Remarks
VR7697	Dry Reed Bi- directional	SP/ST	10	50 (300)	50 VA resistive (not to exceed 250v or 3 amp)	U.L., CSA X-proof Class I, Div 1 Groups C&D	110 & 250 VAC 12-36 VDC	Models 35 and 45
VR7671 (HR)	Hall Effect Uni- directional	Solid State	100	1000 (600)	.75 VA max. non- inductive (not to exceed 15VDC or .05A)	U.L., CSA X-proof Class 1, Div. 1 Groups C&D	10-15 VDC	Models 35 HR and 45 HR

Notes:

- (1) All above units are compatible with Batchmate 1500 Solid State Controller (see TS 500)
- (2) a. Max speed in pulses per revolution, Hz, and RPM limits from Manufacturers' data

WIRING DIAGRAMS



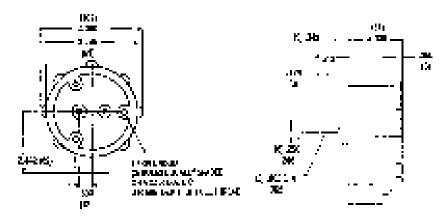
NEPTUNE ELECTRONIC TRANSMITTER Operating and Storage Temperature Data

Model Environment		VR7697 (35 & 45)	VR 7671 (HR) (35 HR & 45 HR)
Operating	°C	-40 to +71	-40 to +82
	°F	-40 to +160	-40 to +180
Storage	°C		-55 to +125
	°F		-67 to +257

DIMENSIONS

in (mm)

Model VR7697 & VR7671 (HR) (35 & 45) (35 HR & 45 HR)



CURRENT SOURCING -vs- CURRENT SINKING

Current Sourcing: sensor supplies the voltage to the count input. Sourcing sensors are PNP transistor outputs or a contact closure to V+.

Current Sinking: sensor provides a path to DC common for the count input. Sinking sensors are NPN transistor outputs or a contact closure to DC common.

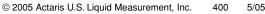
Compatibility: Both sourcing and sinking digital pulse transmitters offered by Neptune are fully compatible with the Neptune BATCHMATE 1500™ electronic batch controllers, which can be set by DIP switches in the device at the factory or in the field to match the transmitter.



U.S.A./International

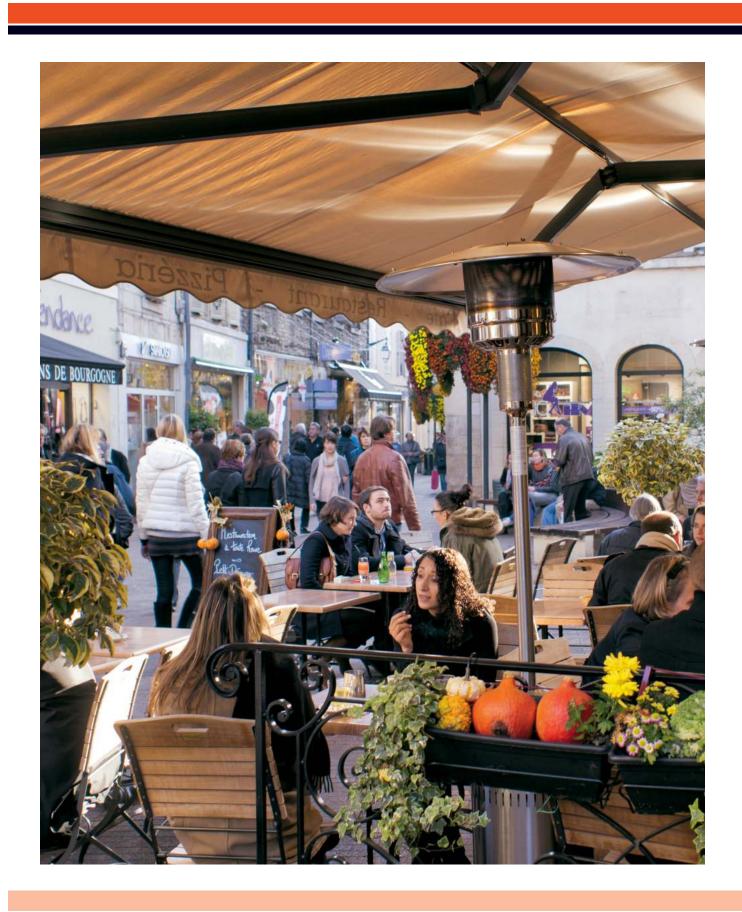
1310 Emerald Road Greenwood, SC 29646-9558 Tel.: Toll-Free (800) 833-3357

(864) 223-1212 Fax: (864) 223-0341





METER

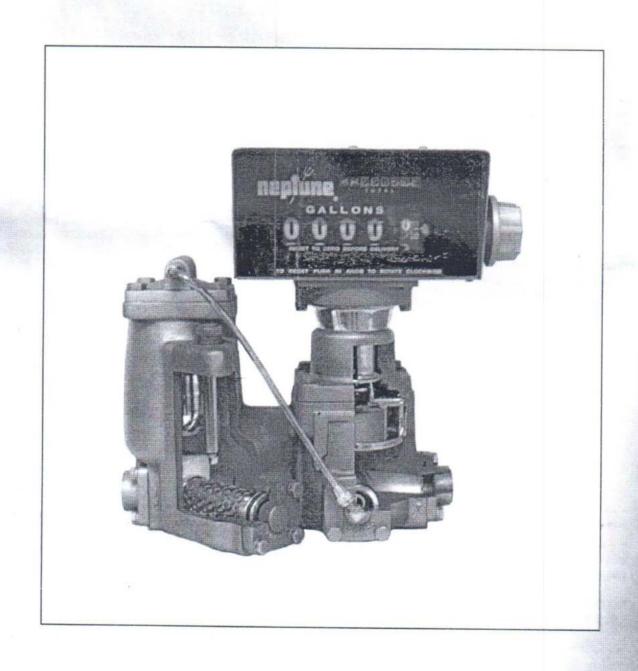




M-285 Rev. H P.D. Oscillating Piston Flowmeter 1" 4D-MD LP Gas

RED SEAL MEASUREMENT

Operating and Maintenance Manual LPG





4D-MD LP-GAS COMPACT FLOWMETERS

GENERAL INFORMATION

This manual covers the installation and maintenance of the Type 4D-MD LP-Gas Compact Flowmeter (Figure 1) which includes a Strainer, Vapor Release, Differential Valve and Automatic Temperature Compensator.

The housing and pressure components of the 4D-MD are constructed of A356 aluminum with T6 heat treatment. Nominal line connections of 3/4" and 1" (ductile iron connections) are available. The meter is fully rated to 350 psi and has been approved by UL.

The strainer, housed in the Vapor Release at the intake of the flowmeter, is of a fine (either an 80-84 mesh or special 30 micron) mesh double sleeve construction with O-rings for positive sealing. It is accessible by removing the strainer cover.

The Vapor Release, which prevents entrapped vapor from passing through the flowmeter, has a float-operated valve. When vapor collects in the Vapor Release, the valve opens venting vapor to the supply tank establishing pump pressure to close the Differential Valve. The vapor release employs a sleeve-type valve that permits a constant "leak" flow of approximately 0.2 gpm from the vapor vent back to the supply tank.

The Differential Valve is piston, plug type construction and opens when at least 15-psi pump pressure is established. This valve serves three functions to assure system measurement accuracy by requiring: (1) pump operation for delivery, (2) adequate back pressure to prevent product vaporization during measurement, and (3) blockage of flow when the Vapor Release valve opens.

The type 4D-MD is available with outlet/inlet flanges of 3/4" and 1" diameters to permit connection to varying pipe dimensions. Please refer to the current price list or your RSM distributor for additional information.

The optional temperature compensator, by sensing product temperature, controls the readout drive ratio to provide a registration compensated by 15°C (60°F).

The Type 4D-MD is available with a choice of 600 or 800 Series mechanical resettable totalizing registers. Pulse output is also optionally available.

The recommended temperature range for operation of the 4D-MD is -23° to 60°C (-10° to 140°F) or -23°C to 52°C (-10° to 125°F) for automatic temperature compensator equipped meter.

INSTALLATION

- 1. Plan the installation for maximum rate of delivery, sizing the supply tank outlet, piping and valve for free gravity flow to the pump suction. To accomplish this, locate the pump as close as possible to the supply tank and use short inlet connections with few restrictions. Keep the number of elbows to a minimum, and use large radius elbows, wherever possible. To further reduce the likelihood of causing vapor in the pump suction line, install a pump bypass valve in a return line to the supply tank as shown in the installation drawing. (See Figure 2).
- 2. Locate the flowmeter at any convenient place in the pump discharge line. If the flowmeter is to be operated under extremes of environment (dirt, water, physical damage, etc.), an enclosure or other protection should be provided. Allow sufficient clearances for removal of the register, strainer and vapor release as shown in Figure 14. Do not install any bypass around the flowmeter; the valve in such a line might eventually leak, work open, or be left open causing improper measurement.

To conform with Weights and Measures requirements, install flowmeter so that the flowmeter nameplate is visible.

NOTE

All piping on the inlet side of the flowmeter should be very thoroughly cleaned out. Flush out all lines thoroughly before installing the flowmeter.

While the installation is still new, the strainer should be cleaned once per month minimally for the first three (3) months. After the system has been thoroughly flushed of foreign material, only periodic (minimum annually) cleaning is recommended.

The majority of service calls on new installations would be eliminated if these directions were followed.

GENERAL INFORMATION

INSTALLATION Before Installing the Flowmeter



TYPE 4D-MD L.P. GAS FLOWMETER 1" ALUMINUM BODY DISPENSER METER

DESCRIPTION

The Red Seal 1" Type 4D-MD meter, with double case design has been specifically designed for the custody transfer of liquefied propane and butane gas (LPG). This meter utilizes the oscillating piston positive displacement measuring chamber technology. The 1" Type 4D-MD is particularly suited for filling portable gas bottled and fuel containers for portable burners, pavement heaters, weed burners, fork lift trucks and motor fuel tanks.

The standard unit includes the base meter with the choice of either a 600 Series totalizing register with a resettable counter or an 800 Series printer register. A differential control valve, combination vapor eliminator/strainer, continuous bleed pressure relief valve and tubing kit are also included. An optional automatic temperature compensator (ATC) is available. The ATC senses product temperature and adjusts the readout to result in registration that is compensated to 15°C (60°F).

DESIGN FEATURES

SUPERIOR ACCURACY

The Neptune designed oscillating piston measuring chamber is both accurate and reliable. The piston is treated with a special coating which protects it from damage by impurities and adds lubricity for smooth performance at low flow and high operating pressures.

FLEXIBILITY

Rugged outer body components in a compact design make the 1" Type 4D-MD useable in a wide variety of installation configurations. The meter is also available with several different register options, and in temperature compensated and uncompensated versions.

UNITS OF MEASURE

Neptune 600 and 800 Series registers offer a full range of options for calibration in U.S. gallons, Litres and Imperial gallons, with 5 digit reset and an 8 digit non-resettable totalizer.



1" 4D-MD with 600 Series Register

OPERATING SPECIFICATIONS

Flow Rate Maximum Minimum	68 11	US Gal./Min. 18 3	
Operating Pressure Maximum	Bars 24	PSI 350	
Minimum	See Note		
Operating Temperature (without ATC)	°C	°F	
Maximum	60	140	
Minimum	-23	-10	

Temperature Compensation (ATC)

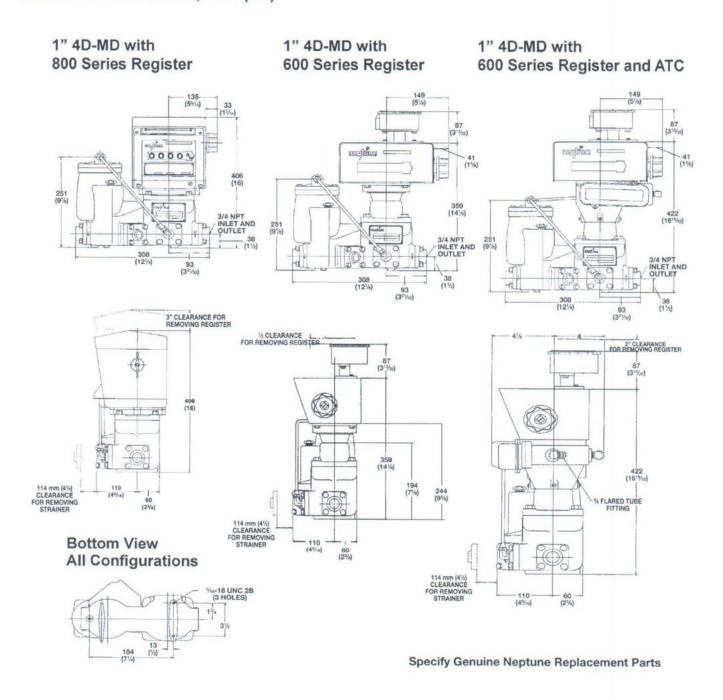
Compensates to a basepoint of 15°C (60°F) Range: -23°C to 52°C (-10°F to 125°F)

Connections

Ductile iron companion flange tapped for 3/4" std. pipe
Optional ductile iron companion flange tapped for 1" std. pipe

Note: A minimum of 1.034 bars (15 psi) is needed to open the differential control valve, plus pressure loss in the system.

DIMENSIONAL DATA, mm (in.)



Accuracy of all Neptune Type 4D Custody Transfer Meters for use with L.P. Gas and Butane meets or exceeds N.I.S.T. Handbook 44 Parameters.

1310 Emerald Road Greenwood, SC 29646 USA

Phone: 1.800.833.3357 Fax: 1.864.223.0341

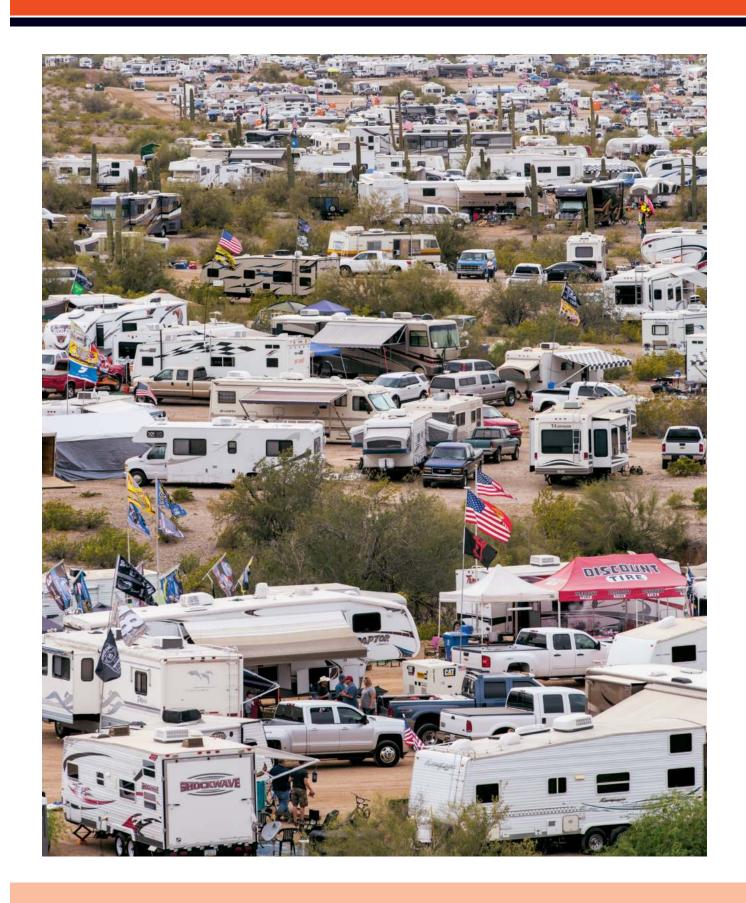


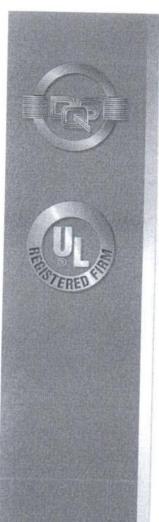




VALV







CERTIFICATE



This is to certify that

Engineered Controls International, LLC

100 Rego Drive Elon, NC 27244 United States of America

with the organizational units/sites as listed in the annex

has implemented and maintains a Quality Management System.

Scope:

The design and manufacture of valves, regulators and fittings for the L.P. Gas, Anhydrous Ammonia, LNG, and Compressed Gas Industries.

Through an audit, documented in a report, it was verified that the management system fulfills the requirements of the following standard:

ISO 9001: 2008

Certificate registration no. 1

10001523 QM08

Date of original certification

1994-10-04

Date of revision

2013-12-08

Date of certification

2012-12-22

Valid until

2015-12-21

UL DQS Inc.

Ganesh Rao Managing Director





Annex to Certificate Registration No. 10001523 QM08

Engineered Controls International, LLC

100 Rego Drive Elon, NC 27244 United States of America

Location

10003889
Engineered Controls International, LLC
3181 Lear Drive
Burlington, NC 27215
United States of America

10003890 Engineered Controls International, LLC 911 Industrial Drive S.W. Conover, NC 28613 United States of America





In its continuing quest for safety, REGO® publishes a series of bulletins explaining the hazards associated with the use, misuse, and aging of LP-Gas valves and regulators. It is hoped that these factual bulletins will make clear to LP-Gas dealer managers and service personnel, that the utmost care and attention must be used in the installation, inspection, and maintenance of these products, or problems could occur which would result in injuries and property damage.

The National Fire Protection Association NFPA 58 Liquified Petroleum Gas Code - 2014 Edition states in Section 4 Qualification of Personnel; "Persons whose duties fall within the scope of this code shall be provided with training that is consistent with the scope of their job activities and that includes proper handling and emergency response procedures... Refresher training shall be provided at least every 3 years, initial and subsequent training shall be documented". These "RegO® Safety Warnings" may be useful in training new employees and reminding older employees of hazards that can occur. It is recommended that all employees complete the Propane Education Research Council's Certified Employee Training Program.

Nature of Warnings

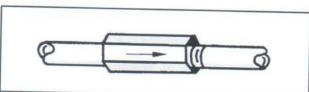
It is recognized that warnings should be as brief as possible, but the factors involved in excess flow valve failures to perform are not simple. They need to be fully understood. If there is a simple warning, it would be:

Make sure that the excess flow valve really closes when the flow exceeds normal transfer flow.

This bulletin is not intended to be an exhaustive treatment of excess flow valves, and certainly does not cover all safety practices that should be followed in installation, operation and maintenance of LP-Gas systems which include excess flow valves.

Selection and Installation

The selection of a given closing rating of an excess flow valve involves an analysis of the complete piping system and is beyond the scope of this bulletin.



It is sufficient to say that an excess flow valve must be installed in the correct direction and will close only if the flow of liquid or vapor exceeds its designed closing rating. Many valves have been installed with closing ratings considerably higher than any flow that could be obtained by a downstream rupture in piping or hoses and thus give none of the protection for which they are intended.

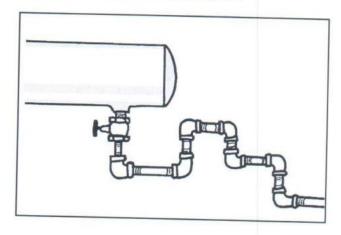
REGO® provides excess flow valves with a number of closing ratings. REGO® obviously can take no responsibility for the proper selection or correct installation of any valve.

Excess flow valves do not provide complete shut-off because there is a bleed at the check to permit pressure equalization.

Causes of Failure to Close

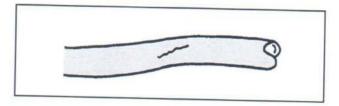
Installers, LP-Gas plant managers and service personnel should be aware that the excess flow valves may not close if these conditions are present.

1. The piping system restrictions (due to pipe length, branches, reduction in pipe size or number of other valves) decrease the flow rate to less than the valve's closing flow.

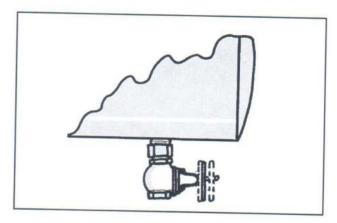


LP-Gas Excess Flow Valves

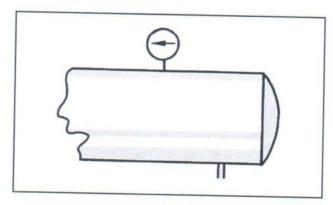
2. The break or damage to the downstream line is not large enough to allow enough flow to close the valve.



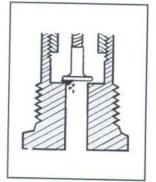
3. A shut-off valve in the line is only partially open and will not allow enough flow to close the excess flow valve.



4. LP-Gas pressure upstream of the excess flow valve, particularly due to low temperature, is not high enough to produce a closing flow rate.



5. Foreign matter (such as welding slag, scale or sludge) is lodged in the valve and prevents closing.



Because of these limitations, it is good industry practice to NOT rely entirely on excess flow valves for protection. Installation of emergency shut-off valves with remote controls is recommended in addition to excess flow valves.

Testina

The National Propane Gas Association Safety Bulletin #113-78 states:

"In order to test an excess flow valve in a piping system, the flow through the valve must be made to exceed the valve's closing rating. This testing should only be attempted by trained personnel familiar with the process. If no one at the facility has experience in proper testing, outside expert help should be obtained. The exact procedure used may vary with the installation, advisability of gas discharge and availability of equipment.

In general, most testing makes use of the fact that excess flow valves are "surge sensitive" and will close quicker under a sudden flow surge than under steady flow. A sufficient surge can often be created by using a quick open/close valve to control sudden, momentary flow into a tank or piping section containing very low pressure. An audible click from the excess flow valve (and corresponding stoppage of flow) indicates its closure.

A test involving venting gas to the atmosphere is hazardous and may be impractical, or illegal.

Any test of any excess flow valve will not prove that the valve will close in an emergency situation, due to reasons cited before. This test will only check the valve's condition, and the flow rate sizing for those test conditions."

General Warning

All REGO® products are mechanical devices that will eventually become inoperative due to wear, contaminants, corrosion and aging of components made of materials such as metal and rubber.

The environment and conditions of use will determine the safe service life of these products. Periodic testing at least once a year when tank pressures are low and maintenance, as required, are essential.

Because REGO® products have a long and proven record of quality and service, LP-Gas dealers may forget the hazards that can occur because an excess flow valve is used beyond its safe service life. Life of an excess flow valve is determined by the environment in which it "lives". The LPGas dealer knows better than anyone what this environment is.

NOTE: There is a developing trend in state legislation and in proposed national legislation to make the owners of products responsible for replacing products before they reach the end of their safe useful life. LPGas dealers should be aware of legislation which could effect

Excess Flow Valves

General Information

RegO® Excess Flow Valves have been designed, developed, and manufactured for a wide variety of industry needs for more than three

Throughout the years, those concerned with installing and operating bulk plant facilities have looked to RegO® products with confidence for reliable, long-lasting valves as required by the National Fire Protection Association (NFPA) Standards 58 and 59, as well as any state, provincial, and local regulations.

It is a responsibility we have not taken lightly. RegO® products continue to not only assess the most effective designs, but anticipate and meet the industry's changing requirements. Toward that goal, RegO® products include over fifty different types and sizes of excess flow valves (most of which are listed by Underwriters Laboratories) to meet the needs of the LP-Gas and anhydrous ammonia industries.

An Explanation and Warning

An excess flow valve is a spring-loaded check valve which will close only when the flow of fluid through the valve generates sufficient force to overcome the power of the spring holding it open. Each valve has a closing rating in gallons per minute and CFH/air.

The selection of a proper closing rating is critical. It requires a technical understanding of the flow characteristics of the piping system, including restrictions of the piping and other valves and fittings downstream of the excess flow valve.

System designers and operating people must understand why an excess flow valve, which remains open in normal operations, may fail to close when an accident occurs.

Warning: A downstream break in piping or hoses may not result in sufficient flow to close the valve.

How They Work

Excess flow valves permit the flow of liquid or vapor in either direction. This flow is controlled in only one direction (the direction of the arrow stamped on the valve). If the flow in that direction exceeds a predetermined rate (shown in this catalog for each valve), the valve automatically closes.

The valve disc is held in the open position by a spring. When the flow creates a pressure drop across the valve disc that overcomes the preset load on the spring, the valve disc moves to the closed position. It remains closed until the force on both sides of the valve disc are approximately equal (a small bleed hole in the disc of each valve permits equalization), then the spring automatically reopens the valve. When a line is completely broken, the pressure cannot equalize and the excess flow valve remains closed until the line is repaired. Because the bleed hole in each valve disc permits equalization of pressure, excess flow valves do not provide a 100 percent type shut-off.

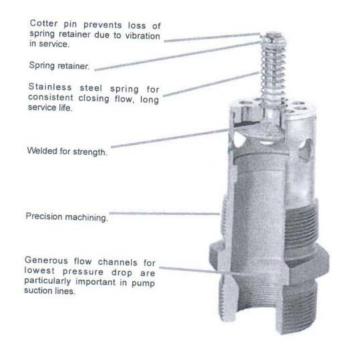
Proper Installation

Since excess flow valves depend on flow in order to close, the line downstream of the excess flow valve should be large enough not to excessively restrict the flow. If the piping is too small, unusually long or restricted by too many elbows, tees and other fittings, consideration should be given to the use of larger size pipe fittings.

An excess flow valve in a pump suction line cannot be expected to close in the case of a clean break in the line beyond the pump, as the pump constitutes too great a restriction, even if running.

Good piping practices dictate the selection of an excess flow valve with a rated closing flow of approximately 50 percent greater than the anticipated normal flow. This is important because valves which have a rated closing flow very close to the normal flow may chatter or slug closed when surges in the line occur during normal operation, or due to the rapid opening of a control valve.

All installations must be in accordance with NFPA Standards 58 and 59, as well as state, provincial and local regulations.



P

The Limitations of Excess Check Valves for LP-Gas

Excess flow check valves have been of help in limiting gas loss in many incidents involving breakage of hoses and transfer piping. Thus, they do provide a useful safety function in LP-Gas systems. However, there have also been transfer system accidents where excess flow valves have been ineffective in controlling gas loss due to a variety of conditions and to the inherent limitations of these valves. This bulletin explains what protection excess flow valves can offer, points out conditions which can interfere with that protection, and offers suggestions for effective excess flow valve installation.

An excess flow valve is a protective device to help control the discharge of product in the event of complete breakage of pipe lines or hose rupture. However, an excess flow valve can only offer limited protection from gas discharge, because it will only close under those conditions which cause the flow through the valve to exceed its rated closing flow, and even when closed it necessarily allows some "bleed" past the valve.

An excess flow valve is not designed to close and thus may not provide protection, if any of the following conditions are present:

- The piping system restrictions (due to pipe length, branches, reduction in pipe size, or number of other valves) decrease the flow rate to less than the valve's closing flow. (Valve should be selected by closing flow rating — not just by pipe size).
- The break or damage to the downstream line is not large enough to allow enough flow to close the valve.
- A shut-off valve in the line is only partially open and will not allow enough flow to close the excess flow valve.
- LP-Gas pressure upstream of the excess flow valve, particularly due to low temperature, is not high enough to produce a closing flow rate.
- Foreign matter (such as welding slag) is lodged in the valve and prevents its closing.
- A buildup of process material (sludge), which may be found in LPGas, may occur over a period of time and cause the valve to stick open.
- The piping break or damage occurs upstream of an in-line excess flow valve, so the escaping product is not passing through the valve.
- The flow through the valve is in the wrong direction. (Excess flow valves only respond to flow in one direction.)
- The excess flow valve has been damaged, or is otherwise not in operating condition.

Because of these limitations of excess flow valves, they should not be relied upon as the only means of controlling the escape of product in the event of piping damage. When possible, shut-off protection by quick closing valves, with shut-off controls accessible in spite of likely line damage, should be provided in addition to, or instead of excess flow valves.

Where excess flow valves are installed, they should be checked to see that:

- They are installed in the correct direction the arrow on the valve indicates the shut-off direction.
- 2. The flow rating on the valve is proper for the installation. The rating must be above the normal system flow, but not higher than necessary to prevent "nuisance" closing in normal conditions. If the manufacturer's catalog information is not sufficient, the valve suppliers can provide sizing assistance.
- In-line excess flow valves are installed so likely piping damage will occur downstream of the valve and will not separate the valve from the upstream piping.

When the excess flow valves can be examined separate from the line (before the installation or if removed for system maintenance), they should be checked to see that the parts are in good condition and that the poppet can be pushed fully closed.

Testing of Excess Flow Valves

In order to test an excess flow valve in a piping system, the flow through the valve must be made to exceed the valve's closing rating.

This testing should only be attempted by trained personnel familiar with the process. If no one at the facility has experience in proper testing, outside expert help should be obtained. The exact procedure used may vary with the installation, advisability of gas discharge, and availability of equipment.

In general, most testing makes use of the fact that excess flow valves are "surge sensitive" and will close quicker under a sudden flow surge than under steady flow. A sufficient surge can often be created by using a quick-closing valve to control sudden, momentary flow into a tank or piping section containing very low pressure. An audible click from the excess flow valve (and corresponding stoppage of flow) indicates its closure.

A test involving venting gas to the atmosphere is hazardous and may be impractical, or illegal.

Any test of any excess flow valve will not prove that the valve will close in an emergency situation, due to reasons cited before. This test will only check the valve's condition, and the flow rate sizing for those test conditions.

For additional information on excess flow valves and other means of

shut-off protection, contact REGO® and refer to NFPA 58.

Prepared by NATIONAL PROPANE GAS ASSOCIATION

The purpose of this bulletin is to set forth general safety practices for the installation, operation, and maintenance of LP-Gas equipment. It is not intended to be an exhaustive treatment of the subject, and should not be interpreted as precluding other procedures which would enhance safe LP-Gas operations. The National Propane Gas Association assumes no liability for reliance on the contents of this bulletin.

HOSES





Technical Advisory

Parker Hannifin Corporation Industrial Hose Division 30242 Lakeland Boulevard Wickliffe, OH 44092-1747

Telephone: (440) 833-2120 Fax: (440) 833-2230 www.safehose.com

PRODUCT UPDATE LP Gas Hose/Assemblies — Permeation

Permeation of high-pressure gas (such as LP Gas/propane, anhydrous ammonia and steam) through a rubber hose is a common but often misunderstood phenomenon. During the manufacturing process, small perforations – sometimes called pinpricks – are applied to the cover of the hose. The perforations allow a path for the gas to safely permeate through the hose wall and into the atmosphere. Without this path, undesirable amounts of gas could accumulate in the hose body, blistering the cover and leading to premature hose failure.

The permeation process is invisible in most circumstances. However, when the hose is moist or sits in water, bubbles may be observed emerging from the pinprick holes in the cover. Or bubbles may be observed slowly escaping from the area where the ferrule attaches to the coupling stem. These emissions may be perceived as leakage.

The most common perceived leakage is the "normal" escape of permeating gas:

- Through the hose wall. The pinprick holes concentrate the permeation to specific areas of the cover. Due to the
 presence of moisture, this concentration of permeation may be observed as bubbling.
- Through the interface of the ferrule and coupling. In some instances the permeating gas may travel down the reinforcement of the hose and escape from the end of the hose encased by the coupling.

Another common perceived leakage is the escape of air from the hose reinforcement through the hose all, most commonly noticed during the pressure testing of a hose assembly. During the manufacturing process, air may become trapped in the reinforcement of the hose. During the hose assembly testing process, the trapped air may be squeezed through the pinprick holes in the cover, or from the end of the hose encased by the coupling. In the presence of moisture, the venting air may be apparent as bubbling. The escape of trapped air through the pinprick holes and/or at the coupling should diminish over time, and should disappear after one to four hours of pressurization. Generally, air escaping from the pinprick holes will dissipate much more rapidly than air escaping at the coupling.

The question that remains: How can one differentiate between a hose that is leaking or excessively permeating LP Gas, a hose that is appropriately permeating LP Gas, and a hose that is venting trapped air?

When testing a new LP Gas hose assembly, only escaping air can be mistaken for leakage (because propane has not yet entered the hose). Two methods for assuring that the escaping air is not from a leak are:

- 1) Use water as the test media. A "true" leak will be a water leak and not an air leak.
- 2) Increase the test time. A test of sufficient duration will allow the escaping air to be purged. Note:
 - a. The use of a rubber cement or epoxy to seal the hose end may eliminate air escaping from the stem/ferrule lock-on area of the coupling.
 - The Parker 7661-LAR coupling in the 1-inch size is designed to prevent gas from escaping from the stem/ferrule lock-on area of the coupling.

When testing a hose in service, it is much more difficult to differentiate between a "true" leak and normal permeation. Generally, leaking propane will create a frosting or icing on the surface of the hose or coupling. On the other hand, permeation is generally at such a low rate that it can be detected only by the slow escape of bubbles. It is important to note that the rate of permeation is dependent on temperature. As the environmental temperature increases so does the rate at which the gas permeates through the hose. Therefore, on hot, rainy days, the likelihood of observing permeation is much higher. If the rate of escaping gas is enough to cause concern, the best way to determine whether a hose is leaking or not is to remove it from service and perform a hydrostatic pressure test.

In the transfer of LP Gas, the allowable permeation rate is controlled by the Underwriters Laboratories Standard UL 21 for LP Gas Hose. Per UL 21, the "Maximum Allowable Permeation Rate" for LP Gas hose is 171 cm³/ft/hr. Testing of standard Parker LP Gas hose has produced permeation rates which are five times better than the allowed maximum.

If there are any questions please contact Parker Customer Service toll-free at:

866.810.HOSE (4673) Wickliffe, OH • Eastern USA

800.242.HOSE (4673) South Gate, CA · Western USA



GasGuard "GG20" Nozzle Range GG20, GG20H & GG20DN

Nozzles in the GasGuard "GG20" series are designed to reach into, and connect to, deep-seated filler valves, as associated with forklift truck cylinders and RV filler valves in similarly difficult locations. This is possible due to the extended connector on the outlet of the nozzle which allows customers to connect to fill points with a more difficult access point. There are three different nozzles in the UL listed GG20 range, the GG20, the GG20H and the GG20DN, which cater for differing customer needs. With a 35mm longer connector the nozzles are engineered with the same function as their shorter GG1E, GG1EH and GG1DN counterparts. With a lightweight & well balanced construction, the GG20 series design has seen significant improvements in operational performance and reduced maintenance requirements, and like all GasGuard nozzles, they are fully repairable.

Standard Specifications for GG1 series nozzles:

Connector thread coupling: 13/4" ACME x 6 TPI form

Swivel Inlet thread:

15mm (1/2") or 20mm (3/4") N.P.T. female

Nett mass:

2.0kgs (4.4lbs)

Max. operating pressure:

2450 KPa (350 psi)

Operating temperature:

-40 to +110 deg. C

Standard features on all GasGuard Autogas Nozzles:

- Safety: Cannot discharge LPGas to the atmosphere when not coupled and lever is actuated.
- Safe connection: Nozzle will safely seal with filler valve, even if its sealing gasket is missing.
- Swivel: Option of either 15mm (1/2"), 20mm (3/4") N.P.T. internal thread to the inlet swivel to the Nozzle.
- Latching: An optional lever hold-open latch is available (not UL listed).
- Robust: High strength aluminium alloy connector casting with a stainless steel ACME thread Insert provides long service without distortion.

GG20 Nozzle Characteristics

Nozzle is used for industrial refueling of forklift truck cylinders and RV filler valves in similarly difficult locations. It uses a single nose piece to achieve high flow rates.

- Flow rate of 63L/min at 12bar system pressure
- Release Volume on valve closure of 1.9cm3
- Customer experiences a low lever pressure
- Magnet option for dispensers with reed switch technology
- New guided extended thread assists with alignment and connection to fill point
- A fine filter comes standard in all nozzles
- Long Connector Nut to access "hard to reach" fill points
- UL Listed





GasGuard "GG20" Nozzle Range GG20, GG20H & GG20DN

GG20H Nozzle Characteristics

Nozzle is used for industrial refueling of forklift truck cylinders and RV filler valves in similarly difficult locations. It incorporates a new "hybrid" nose piece to reduce the lever pressure experienced by the customer.

- Flow rate of 60L/min at 12bar system pressure
- Release Volume on valve closure of 1.7cm 3
- Customer experiences a lower lever pressure than GG20
- Magnet option for dispensers with reed switch technology
- New guided extended thread assists with alignment and connection to fill point
- A fine filter comes standard in all nozzles
- Long Connector Nut to access "hard to reach" fill points
- UL Listed



GG20DN Nozzle Characteristics

The GG20DN nozzle is suited for refueling of passenger vehicles by untrained personnel. It incorporates a patented Dual Nose piece which significantly reduces the amount of user error when operating the nozzle. It creates a positive seal to the customer's vehicles even if they have not tightly screwed the nozzle to the fill point. If the nozzle is not screwed on completely and the lever is pulled, there is no effect of flow rate as the Dual Nose piece compensates for the changed operating situation.

- Flow rate of 60L/min at 12bar system pressure
- Release Volume on valve closure of 1.7cm 3
- A Dual Nose piece for added customer safety
- Customer experiences a lower lever pressure than GG20
- Magnet option for dispensers with reed switch technology
- New guided extended thread assists with alignment and connection to fill point
- A fine filter comes standard in all nozzles
- Long Connector Nut to access "hard to reach" fill points
- UL Listed



POMECO 102 Spring Balance Single Hose Retractors

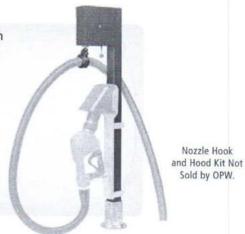
POMECO 102 Spring Balance Single Hose Retractors keep excess hose off the ground and out of the way, prolonging hose life and reducing potential hazards. The POMECO 102 is a California Air Resources Board (CARB) certified Stage II component for use with single and dual hose dispensers as per Executive Order G-70-52-AM.



Materials

Housing: Cast aluminum Cable: Black polyester

Post: Aluminum



Features

- Easy to Use the spring-loaded reel and stretch-resistant cable provide smooth and steady tension throughout hose extension and return.
- Easy to maintain the removable sideplate provides full access to the mechanism for easy tension adjustment and unit maintenance. A convenient safety thumb screw is provided to lock the reel in place during tension adjustment.
- Field Adjustable for Various Hose, Nozzle, Swivel, Breakaway Combinations - no need for upgrading components if a breakaway or swivel is added to the hose assembly. Simply change the tension setting on the spring-loaded hose reel.
- Multiple Mounting Options the POMECO 102 retractor housing is tapped on the top for bolting to overhead crossbars, and on the side for mounting to vertical posts. The 102 is available as a retractor kit (including post, retractor and mounting hardware) or as separate components. Models are also available for aboveground storage tank (AST) applications. AST models include a 44" (112 cm) post with a freestanding base.

102 Spring Balance Hose Retractor Instruction Sheet Order Number: H15853PA

NOTE: See OPW's Website at www.opwglobal.com for product instruction sheets, trouble-shooting guides, how-to-use guide and to view the Do's & Don'ts at the Gas Pump video.

Ordering Specifications

Vertical Retractor Kits (Box, Post, Bracket, Foot & Hardware)

Model Number	Mounting Method	Clamp Fits	Weight	
		Clamp Fits	lbs.	kg
6102-1039P	39" Retractor/Post Kit	(Hose Clamp Not Included)	12	5.4
6102-1078P	78" Retractor/Post Kit	(Hose Clamp Not Included)	14	6.4
6102-1100	78" Retractor/Post Kit	(Hose Clamp Not Included)	14	6.4
6102-AST	AST	(Hose Clamp Not Included)	9	4.1

Ordering Specifications

Separate Retractor Components (Box Only)

Madel	Mounting Method	Clamp Fits				W-1-ha	
Model Number		Hose O.D.		Hose I.D.			Weight
		in.	mm	in.	mm	lbs.	kg
6102-1000	Overhead Crossbar/Verticle Post		(Hose Clam	p Not Included)		7	3.2
6102-4000	Overhead Crossbar/Verticle Post	13/4"	35	1"	25	7	3.2
6102-6000	Overhead Crossbar	11/12"	26	3/8" or 3/4"	16 or 19	7	3.2
6102-8000	Overhead Crossbar	1"	25	3/8 "	16	7	3.2
6102-CNG	Hose Retractor Kit, CNG						
6102-CNG2	Hose Retractor Kit, CNG2						

^{*}POMECO recommends using CO5238M, CO5261M or P100-3F/P100-44/P100-2AST for use with 102 Series retractors. Other size tubes and clamps available upon request.



Hose Clamp

Ordering Specifications Hose Clamps

Hose Clamp Size †		
Standard 1%" O.D. Hose (1" I.D.)		
Standard 11/4" O.D. Hose (1/4" I.D.)		
Standard 11/12" O.D.Hose (1/6" or 3/4" I.D.)		
Standard 1" O.D. Hose (%" I.D.)		
Balanced Coaxial, Goodyear Premier		

[†] Other sizes available upon request

Options Replacement Parts

Model Number	Hose Clamp Size			
C05238M	Post Kit, 39"(99 cm), 11/4" x 2"			
C05261M	Post Kit, 78"(198 cm), 11/4" x 2"			
H15212M	10 ft. Replacement Cable			
P338SPOOL	Spool of Retractor Cable, 338 ft.			
H15210M (P102-02)	Replacement Cable Guide			
H15211M	Replacement Reel			
P100-3F	AST Replacement Base			
P100-2AST	Sliding Bracket (AST)			
	MUM WHITEST STATES			

RESUME





Resume

THEODORE C. LEMOFF

Current Position: Engineering Consultant

Education B.E. (Chemical Engineering), City College of New York,

New York, NY, 1967

M.B.A. (Business Administration), Xavier University,

Cincinnati, OH, 1979

<u>Certifications</u> Registered Professional Engineer, Florida and Massachusetts

Experience

2010 – Present <u>Principal, TLemoff Engineering.</u>

Code consultation: Provide opinions on the applicability of gas code provisions in specific cases. Work includes review of history of code text to identify the intent of code provisions, providing verbal and written explanations, and follow-up with officials and other parties as required.

Code expert in legal cases: Provide written explanation of the intent of code requirements, when cited by other parties. Incident site visits to determine code compliance or non-compliance and opinion as the relevance thereof. Review depositions for accuracy of code related statements. Provide testimony at depositions or trials as needed.

Product support: Provide assistance to manufacturers on product specific code requirements, and propane industry practices. Assist with liaison with approval laboratories. Work with local officials on product acceptance.

Seminars: Presented talks and seminars on NFPA 54 and NFPA 58 in the United States, Santa Cruz, Bolivia, and Doha, Qatar.

1985 - 2010 <u>National Fire Protection Association</u>, Quincy, MA

Principal Gases Engineer

Staff liaison to all gases committees administering LP-Gas, Fuel Gas, and Liquid Natural Gas, and Ovens and Furnaces committee. Duties in addition to the administration of the standards making process include information interpretations as requested, speaking engagements and technical advice to NFPA books, films and other products.

NFPA representative to technical committees of the American Gas Association, National Propane Gas Association, and Compressed Gas Association, and the U. S. Department of Transportation Pipeline Advisory Committee. Voting member of the Uniform Plumbing Code and Uniform Mechanical Code committees.

Developed and maintained formal training programs on NFPA 58, Liquefied Petroleum Gas Code and NFPA 54, National Fuel Gas Code. Seminars presented throughout the United States

1980 - 1985 <u>Badger Engineers, Inc.</u>, Cambridge, MA and The Hague, Holland

Senior Project Engineer

Various assignments in the Cambridge, MA and the Hague, Holland offices covering the full range of project engineering activities including coordination, design, flow diagrams, equipment bid evaluation and selection.

1978 - 1980 <u>Table Talk Pies, Division of Squibb Corporation, Worcester, Ma</u>

Plant Engineer

Responsible for all engineering and maintenance for the bakery, freezer warehouse, distribution centers, and truck fleet.

1973 - 1978 <u>Sun Chemical Corporation</u>, Staten Island, NY and Cincinnati, OH

Engineering Manager

Responsible for all fire protection engineering and maintenance for the manufacturing facilities and associated offices and laboratories.

1967 - 1973 The Proctor and Gamble Company. Cincinnati, OH

Process Engineer

Broad range of assignments in detergents R&D.

Memberships and Affiliations

NFPA Technical Committee on National Fuel Gas Code (NFPA 54) NFPA Technical Committee on Liquefied Petroleum Gases (NFPA 58) American Institute of Chemical Engineers, Member Society of Fire Protection Engineers, Member National Fire Protection Association, Member National Propane Gas Association, Member

Publications

Editor, Liquefied Petroleum Gases Handbook, 8 editions Editor, National Fuel Gas Code Handbook, 6 editions Co Author, NFPA Pocket Guide to Fuel Gas Storage and Use

Patent

Spray-Dried Detergent Composition, US # 3,801,511 (Assigned to the Proctor and Gamble Company)