

TECHNICAL MEMORANDUM

| То: | Mr. Brian Pensack |
|----------|--|
| From: | Annjanette Dodd, PhD, CA PE #77756 |
| Date: | November 9, 2021 |
| Subject: | Groundwater Hydrology – 2185 Ogulin Canyon Road, Clearlake, CA |

PURPOSE AND BACKGROUND

The purpose of this Technical Memorandum is to provide an evaluation of the potential impacts the proposed project would have on the surrounding groundwater resources. The project is located at 2185 Ogulin Canyon Road, Clearlake, Lake County, California. The project proposes 0.5-acres of mixed-light cannabis cultivation, 10,000 sq. ft. of manufacturing, processing, and distribution, and a 3,000 sq. ft. office, retail, and delivery building (Figure 1). A Water Availability Analysis (WAA) was prepared for the project in June 2021 by Richard Knoll Consulting and submitted to the City of Clearlake.

The estimated project water demand for cultivation (300-day cultivation period) was estimated in the WAA using standard industry values for cultivation (3,000 gallons per acre per day, or 2.1 gallons per minute) and warehouse demand (0.85 gallons per square foot, or 11,000 gallons per month). The project proposes ten employees, water demand based on the number of employees is equivalent to sanitary sewer generation for factories with shower facilities. According to the Lake County Rules and Regulations for On-Site Sewage Disposal (Lake County, 2010), the demand would be 35 gallons per day, per person. Thus, the proposed project employee demand would be 350 gallons per day or about 10,500 gallons per month, which corroborates the employee estimate provided in the WAA. The total estimated water demand for the proposed project provided in the WAA is 582,000 gallons per year or 1.8 acre-feet per year. The daily demand is about 1.3 gallons per minute (gpm).

WATER SOURCE AND SUPPLY

There is one (1) existing, permitted groundwater well (Permit Number: WE 5569AG) that will be used for cultivation (Lat/Long 38.983147, -122.604709). The well is approximately 375 feet deep and was drilled in March 2021. The well is screened between 280- and 375-feet below the ground surface. During the drilling of the well, the depth of first water was at 280-feet below the ground surface (bgs) and the static water level was estimated to be 280-feet bgs (Attachment 1 – Well Log).

The well was estimated to have a yield of 80 gpm (129.0 acre-feet per year). The potential daily demand of 1.3 gpm represents approximately 1.6% of the well yield and 2.5% of the annual well production in acre-feet.



GROUNDWATER BASIN INFORMATION AND HYDROGEOLOGY

The well site is in the Burns Valley Groundwater Basin (Basin #5-17). According to the California Department of Water Resources (DWR), almost all the groundwater in the Burns Valley Basin is derived from rain that falls within the 12.5 square mile Burns Valley Watershed drainage area (DWR Bulletin 118).

The Burns Valley Basin is within the Burns Valley Watershed. The Franciscan Formation borders the Burns Valley Basin on the north, Clear Lake borders the basin on the west, and the Cache Formation borders the basin on the south and east. The valley is drained by Burns Valley Creek, flowing southwest, and eventually into Clearlake. There are three water bearing formations in the Burns Valley Basin, the Quaternary Alluvium, Quaternary Terrace Deposits, and Lower Lake Formation. The Quaternary Alluvium located in the valley lowlands in the southern end of the valley are composed of silt, sand, and gravel with a thickness up to 50 feet. Groundwater in this formation is unconfined and typically provides water for domestic use. Quaternary Terrace Deposits have been deposited on the sides of the alluvial plain in the Burns Valley Basin. The terrace deposits are approximately 15 feet above the valley floor and slope up the valley to a similar elevation as the foothill exposures of the Cache Formation. Groundwater in this formation is not well understood. The *Lower Lake Formation*, consisting of lake deposits, underlies the alluvial and terrace deposits in the basin. The formation consists of fine sands, silts, and thick interbeds of marl and limestone, and has a maximum thickness of 200 feet. The formation has low permeability and provides water to wells at up to a few hundred gallons per minute. Based on the depth of the well, it is likely in the deeper, higher yielding, water bearing formation. The California Department of Water Resources (DWR) estimated a storage capacity of the Burns Valley Basin as 4,000 AF with a usable storage capacity of 1,400 AF. Well depths mostly range between 25- and 425-feet. (CDM 2006 and California DWR 2003, 2021)

The Burns Valley Groundwater Basin has not been identified by the California Department of Water Resources (DWR) as critically overdrafted basins. Critically overdrafted is defined by DWR as, "A basin subject to critical overdraft when continuation of present water management practices would probably result in significant adverse overdraft-related environmental, social, or economic impacts." In addition, as part of the California Statewide Groundwater Elevation Monitoring (CASGEM) Program, DWR created the CASGEM Groundwater Basin Prioritization statewide ranking system to prioritize California groundwater basins in order to help identify, evaluate, and determine the need for additional groundwater level monitoring. California's groundwater basins were classified into one of four categories high-, medium-, low-, or very low-priority. The Burns Valley Groundwater Basin is ranked as very low-priority basins by the CASGEM ranking system. (DWR, 2021)

Recharge Rate

The annual recharge can be estimated using a water balance equation, where recharge is equal to precipitation (P) less runoff (Q) and abstractions that do not contribute to infiltration (e.g., evapotranspiration). A simple tool that can be used to estimate runoff and abstractions, that uses readily available data, is the Natural Resources Conservation Service (NRCS) Curve Number (CN) Method (NRCS, 1986). Determination of the CN depends on the watershed's soil and cover conditions, cover type, treatment, and hydrologic condition. The CN Method runoff equation is

$$Q = \frac{(P - I_a)^2}{(P - I_a) + S}$$

Where,

Q = runoff (inches)
P = rainfall (inches)
S = potential maximum retention after runoff begins (inches) and
I_a = initial abstraction (inches)

The initial abstraction (I_a) represents all losses before runoff begins, including initial infiltration, surface depression storage, evapotranspiration, and other factors. The initial abstraction is estimated as $I_a = 0.2S$. *S* is related to soil and cover conditions of the watershed through the CN, determined as S = 1000/CN - 10. Using these relations, the runoff equation becomes:

$$Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

The CN is estimated based on hydrologic soil group (HSG), cover type, condition, and land use over the area of recharge, which is estimated as the area of the Burns Valley Watershed. However, to be conservative, the project parcel area of 21.3 acres was used as the recharge area.

The recharge area soils are classified into four HSGs (A, B, C, and D) according to the soils ability to infiltrate water; where HSG A has the highest infiltration potential and HSG D has the lowest infiltration potential. HSGs are based on soil type and can be determined from the NRCS Web Soil Survey (Attachment 2). The recharge area is comprised of HSG C. The land use is undeveloped with a cover type of woods with grassland in fair condition (50% to 75% ground cover) and has a CN of 76 for HSG C.

The PRISM Climate Group gathers climate observations from a wide range of monitoring networks and provides time series values of precipitation for individual locations (https://prism.oregonstate.edu/explorer/). Using the annual precipitation from 1895 to 2020, as predicted by PRISM, the annual average precipitation over this period is 27.6 inches and the minimum precipitation over this period is 6.5 inches (Attachment 3).

Using the above information, and assuming that 50% of the initial abstraction infiltrates and the remainder is evapotranspiration (0.31 inches or 0.56 AF), the estimated annual recharge over the recharge area of 21.3 acres is 5.6 AF during an average year and 4.2 AF during a dry year (Table 1).

| Recharge | | | | | | Recharge = | |
|----------|----------|----|----------|----------|----------|-------------------|----------|
| Area | Р | | S | Ia | Q | $P - Q - 0.5*I_a$ | Recharge |
| (acres) | (inches) | CN | (inches) | (inches) | (inches) | (inches) | (AF) |
| 21.3 | 6.5 | 76 | 3.16 | 0.63 | 3.81 | 2.37 | 4.2 |
| 21.3 | 27.6 | 76 | 3.16 | 0.63 | 24.17 | 3.14 | 5.6 |

Table 1. Estimated annual recharge over the recharge area of the project's well.

CUMULATIVE IMPACT TO SURROUNDING AREAS

Annual water demand of the proposed project is approximately 1.8 AF per year. The demand represents

approximately 32% and 43% of the annual recharge during an average and dry year, respectively. Recharge in the Burns Valley Groundwater Basin is derived from rain that falls within the 12.5 square mile Burns Valley Watershed. The area used to estimate the recharge for the proposed project is only 0.3% of the entire recharge area. Thus, the recharge estimate is a conservative (low) estimate of the available recharge over the entire recharge area. Overall, there is sufficient recharge, on an annual basis, to meet the project's demand during both a dry year and average year.

The estimated storage capacity of the Burns Valley Basin is 4,000 AF, with a usable storage capacity of 1,400 AF. According to DWR, the groundwater in the Burns Valley Basin is derived from rain that falls within the 12.5 square mile Burns Valley Watershed drainage area. The project's demand is only 0.1% of the usable storage capacity of the Burns Valley Groundwater Basin.

According to the Lake County Groundwater Management Plan, there are 86 domestic wells and 9 irrigation wells in the Burns Valley Groundwater Basin and the agricultural demand in the basin during an average year is 105 AF per year; of this, 14 AF is supplied from groundwater. The Groundwater Management Plan is dated 2006, and does not include the demand from additional proposed cannabis cultivation projects in the Burns Valley Groundwater Basin. The total additional proposed cannabis cultivation is unknown. Assuming there is the potential for approximately 20 to 40 acres of new cannabis cultivation, the annual agricultural demand could increase by an additional 66.3 AF. Cumulatively, with the proposed project at 2185 Ogulin Canyon Road, the annual demand could increase to 82.1 AF or up to 6.0% of the usable storage capacity of the Burns Valley Basin. However, the demand of the proposed project is only 2% of the potential future demand.

Since there is sufficient recharge and supply to meet the project's demand during average and dry years; the project's demand is only 0.1% of the usable storage capacity of the Burns Valley Groundwater Basin; and the potential future cannabis demand in the basin is a fraction of the usable storage capacity. Thus, the proposed project water use would have little to no cumulative impact on the surrounding area.

Additionally, if needed in the future to create water redundancy for the project, the project could install storage for rainwater catchment. The project proposes 31,750 sq. ft. of footprint that could be utilized as rainwater catchment. The rainwater catchment potential is approximately 0.39 acre-feet (129,000 gallons) during a dry year and up to 1.7 acre-feet (546,000 gallons) during a wet year.

QUALIFICATIONS OF AUTHOR

I have a PhD in Water Resources Engineering. In addition, I am a registered Professional Engineer with the State of California with 30-years of experience practicing and teaching Water Resources Engineering, including over 15 years of teaching, practicing, and modeling surface and groundwater hydrology.

LIMITATIONS

The study of groundwater hydrology is very complex and often relies on limited data, especially in rural areas. Recommendations and conclusions provided herein are based on professional judgment made using information of the groundwater systems and geology in Lake County, which is limited and allows only for a general assessment of groundwater aquifer conditions and recharge. NorthPoint Consulting Group, Inc. is making analyses, recommendations, and conclusions based on readily available data, including studies and reports conducted by other professionals, Lake County, the State of California, and

other consultants hired by the project proponent to prepare technical studies for the proposed project. If additional information or data becomes available for the project area, the recommendations and conclusions presented herein may be subject to change.

ATTACHMENTS

- 1. Well Completion Report
- 2. NRCS Soil Survey Results
- 3. PRISM Climate Precipitation 1985-2020

REFERENCES

- Bauer S, Olson J, Cockrill A, van Hattem M, Miller L, Tauzer M, et al. (2015). Impacts of Surface Water
 Diversions for Marijuana Cultivation on Aquatic Habitat in Four Northwestern California
 Watersheds. PLoS ONE 10(9): e0137935. https://doi.org/10.1371/journal.pone.0137935
- CDFA (2017) CalCannabis Cultivation Licensing Program Draft Program Environmental Impact Report. State Clearinghouse #2016082077. Prepared by Horizon Water and Environment, LLC, Oakland, California. 484 pp.
- California DWR (2003). California's Groundwater Bulletin 118 Update 2003. October 2003. https://water.ca.gov/-/media/DWR-Website/Web-Pages/Programs/Groundwater-Management/Bulletin-118/Files/Statewide-Reports/Bulletin 118 Update 2003.pdf
- California DWR (2003). California's Groundwater Bulletin 18, Update 2003. October 2003.
- California DWR (2021). California's Groundwater. <u>https://water.ca.gov/programs/groundwater-management/bulletin-118</u>
- California DWR California Statewide Groundwater Monitoring Program (CASGEM) (2021). https://water.ca.gov/Programs/Groundwater-Management/Groundwater-Elevation-Monitoring--CASGEM. Accessed August 2021.
- CDM (2006). Lake County Water Inventory Analysis. Prepared for the Lake county Watershed Protection District. March 2006.

http://www.lakecountyca.gov/Assets/Departments/WaterResources/Groundwater+Management/ Lake+County+Water+Inventory+and+Analysis+w+Appendices.pdf

CDM (2006). Lake County Groundwater Management Plan. Prepared for the Lake county Watershed Protection District. March 2006.

http://www.lakecountyca.gov/Assets/Departments/WaterResources/IRWMP/Lake+County+Groun dwater+Managment+Plan.pdf

Gupta, R.S. (2008). Hydrology and Hydraulic Systems, 3rd Edition. Waveland Press, Long Grove IL.

Natural Resources Conservation Service, NRCS< (1986) Urban Hydrology for Small Watersheds. USDFA NRCS Technical Release 55. June 1986.

https://www.nrcs.usda.gov/Internet/FSE_DOCUMENTS/stelprdb1044171.pdf

ATTACHMENT 1 PROJECT'S WELL COMPLETION REPORT

| COUNTY OF LAKE HEALTH SERVICES DEPARTMENT Division of Environmental Health 922 Bevins Court, Lakeport, CA 95453-9739 Telephone 707/263-1164 FAX: 263-1681 | Denise Pomeroy Health Services Director Erin Gustafson .Public Health Officer |
|--|--|
| | Jasjit Kang Environmental Health Director |
| SEAL WITHOUT | WITNESS |
| Permit Number: WE 5569AC | |
| Site Address: 2185 Ogylin Canyon 1 | Rd. clearlake CA |
| Assessor's Parcel No: 010 _ 044 _ 17 | |
| Owner Name: Cegulin Fills Holdings | |
| Date: 4-1-21 | |
| REASON FOR SEAL WITHOUT WITNESS: | |
| Emergency Seal – Explain: | |
| | |
| Inspector unable to witness | |
| Other: | |
| | |
| IMPERMEABLE LAYER in which annular space terminates: | h concrete cap Mix concrete cap |
| I hereby certify that I have installed the annular seal in accordance with the provision unless otherwise specified in the Lake County Well Ordinance, with the California Bulletin 74-81 or as modified by subsequent revisions or supplements. | s of the Lake County Well Ordinance and Department of Water Resources |
| DRILLING CONTRACTOR SIGNATURE: | |
| company will referson Well DrillingLich | ENSE NO: 100 9053 |
| | |
| | |
| Our mission is to promote and protect the health of the people of Lake | County through education and the enforcement |

| "The fre | e Adobe F | eader ma | y be used to view | wand complete th | stom to | | | | | |
|----------------------------|-----------------|----------------------|-------------------|------------------|---------------|-----------------|------------------|------------------|--|------------------------|
| I NE OR | ginal will A | DWR | | , | a mill money | er, software | must be purch | ased to com | plate, save, and reuse a save | Pri form |
| Page | 12 | of | 1. | | Well C | Ompio | alifornia | | DWR Use | Only De Not Cal |
| Owner's | s Well Nu | mber | | | Re | er lo instructa | NOU KED | Port | | |
| Date W | ork Bega | 3 | 241200 | 2) Date M | N Ended | O. XXXXXX | Cr | | State Wet | NumberiSce Number |
| Permit A | ermit Age | ncy Er | Wironm | ental H | PALTA | 21251 | 2021 | | | |
| I Crane I | winder_ | NE 5 | 569AC | 7 Permit Date | 2/22/ | 2021 | • | | | Longitude |
| - | ontest . | | Geolo | gic Log | | and | - - - | | API | TRS/Other |
| O-Hirur | Maihad | Over | ical OHo | izontal Or | Angle Spor | ifv | | | Well Owne | ſ |
| Depti | from Su | rface | Kotan | Dr | Erg Fluid | 0 | - Name_ | Daul | in Hills H | aldinas |
| Feet | to F | eel | Desc | Descrip | tion | | Mailing | Address | 037 Lindard |) St. Sto 201 |
| 0 | 4 | 0 | Brown | Clavi | Samo o | | City_ | pank | afael s | tale (A z 940AI |
| 40 | 38 | 0 | Cemen- | ted Franc | Iscan a | raver | | | Well Location | |
| F | | | | | SUAT O | MUVER | Address | 3 2185 | 5 Daulin Can | Von Ra |
| | | | | | | | City | laria | Ke, o | The Lake |
| | <u> </u> | | | | | | - Lalituce | | N Longi | hurin |
| | | | | | | | Datum | Dao, | Vin. Sec. | Dea. Min. Sec |
| | | | | | | | APN B | at all | Dec. Lat. | Dec. Long. |
| | + | | | | | | Townet | in <u>C</u> | _ Page _ 079_ | Parcel 17 |
| | | | | | | | | 1 | Kange | _ Section |
| | | -+ | | | | | (States | LOCal | tion Sketch | Activity |
| | | | | | | | 1 | | North | New Well |
| | | | | | | | -11 | | TI | O Deenen |
| | | | | | | | 11 | 1 . | ~) . | O Other |
| L | | | | | | ****** | -11 | | | O Destroy |
| | | | | | | | 11 | 10 | aut's | ander TEO DGC: DC |
| | | | | | | | 17 | A | Julia | Planned Uses |
| | | | ····· | | | | 11 - 7 | | myon KO. | Vater Supply |
| | | | | | | | | N . | 2351 | Inigation Thorbestriat |
| | | | | | | | | ~ . | u | O Cathodic Protection |
| | | | | • | | •. | 11 | | | O Dewatering |
| | | | | | | | 11 | | * <u>1</u> | O Heat Exchange |
| | | | | | | • | 11 | | (4) | O Injection |
| | | | | | | | HYC | | | O Monutaring |
| | | | | <u></u> | | | 1 | 1 | | O Sparoina |
| | | | | | | | 1. | 1 | South | O Test Weil |
| | | | | | | | illustrate or or | some clistance : | antine wat builtings larges | O Vapor Extraction |
| | | | | | | | 710342 20 20 | carson and come | lies all thind paper it minutatory Sete | O Other |
| | | | | | | | Water L | evel and | Yield of Completed V | Veli |
| | | | | | | | Depth to | first water | 280 | _ (Feet below surface) |
| Tabl | | <u> </u> | 0.0 | | | | Water L | evel a | 80 (Feel) Date | Barry 3/25/21 |
| | | ang | 30 | 50 | Feel | | Estimate | d Yietd * | SO (GPM) Test | Type Air Lift |
| I otal D | epth of Ci | ompleted | Well 3 | 15 | Feet | | Test Ler | syth | (Hours) Tota | Drawdown (Feet) |
| | | | | Casinga | | | May no | t be repres | entative of a well's long to | erm yield. |
| Depti | from | Borchole | Tumo | casings | Wall | Onteido | Fanna | Class Cl | Annu | lar Material |
| Feet u | ace Feet | Diameter (inches) | | M960131 | Thickness | Diameter | Туре | if Any | Surface F | ll Drawidle |
| 0 | 280 | 9 | FUSO | PUC. | (Inches) | (Inches) | | {inches; | Feel to Feel | |
| 280 | 375 | q | F480 | PVC | VIII | 44 | na pear | NA Na | o i con | crete seal |
| - | | | | | | 113 | PERF | -025 | 1 23 bento | inite seal |
| | | | | | | 1 | | | 22 215 51 | 10 ray gravel pack |
| | | | | | | | | | | |
| | | - 4 | <u> </u> | - | | | | | | |
| [] | | Attachn | nents | | | | (| ertificati | on Statement | |
| Li Geologic Log | | | | | | | | | | |
| Geophysical Local | | | EKRON | wei | 1 Philling | | | | | |
| Soliwater Chemical Anchese | | | 1095 | - K | elseville r | A 95451 | | | | |
| Other Signed | | | | | | at 4-1-71 5 | ine ang and the | | | |
| Allach add | ะดาล) การก | aton, d s culta | ests | | C-571-0 | ensed Water | Vell Consector | + | Data Signal | 511001033 |
| UWR 183 | REV 1/2006 | i | | IFA | DITIONAL SPAC | E IS KEFNEN | USELEXT | ACLC | Verbury and | -or License Number |

ATTACHMENT 2 NRCS SOIL SURVEY RESULTS HYDROLOGIC SOIL GROUPS



Conservation Service

Web Soil Survey National Cooperative Soil Survey



Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|---------------------------|---|--------|--------------|----------------|
| 161 | Manzanita loam, 15 to 25 percent slopes | С | 0.0 | 0.2% |
| 196 | Phipps complex, 15 to 30 percent slopes | С | 2.2 | 10.4% |
| 197 | Phipps complex, 30 to 50 percent slopes | С | 17.2 | 81.1% |
| 249 | Xerofluvents-Riverwash complex | | 1.8 | 8.3% |
| Totals for Area of Intere | est | 21.3 | 100.0% | |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



ATTACHMENT 3 PRISM PRECIPITATION 1895-2020

| 11/9/2021 | |
|------------------------|--|
| PRISM Time Series Data | |

| PRISM Time Ser | ies Data | | | | |
|--|----------------------|-----------------------|-------------|-----------------|--|
| Location: Lat: 38.9831 Lon: -122.6047 Elev: 1637ft | | | | | |
| Climate variable: ppt | | | | | |
| Spatial resolution | on: 4km | | | | |
| Period: 1895 - 2 | 020 | | | | |
| Dataset: AN81n | n | | | | |
| PRISM day define | nition: 24 hours end | ing at 1200 UTC on th | ne day show | n | |
| Grid Cell Interp | olation: On | | | | |
| Time series gen | erated: 2021-Nov-0 | 8 | | | |
| Details: http://v | www.prism.oregons | tate.edu/documents | /PRISM_data | asets.pdf | |
| Date ppt | (inches) | | | | |
| 1895 | 33.63 | | | | |
| 1896 | 39.53 | | | | |
| 1897 | 26.55 | | | | |
| 1898 | 15.13 | | | Precip (inches) | |
| 1899 | 36.1 | | Average | 27.63 | |
| 1900 | 24.89 | | Minimum | 6.49 | |
| 1901 | 26.27 | | | | |
| 1902 | 34.58 | | | | |
| 1903 | 26.84 | | | | |
| 1904 | 42.96 | | | | |
| 1905 | 23.18 | | | | |
| 1906 | 43.17 | | | | |
| 1907 | 35.74 | | | | |
| 1908 | 18.81 | | | | |
| 1909 | 45.51 | | | | |
| 1910 | 17.48 | | | | |
| 1911 | 33.96 | | | | |
| 1912 | 20.53 | | | | |
| 1913 | 26.29 | | | | |
| 1914 | 31.26 | | | | |
| 1915 | 35.72 | | | | |
| 1916 | 30.02 | | | | |
| 1917 | 12.99 | | | | |
| 1918 | 20.6 | | | | |
| 1919 | 23.04 | | | | |
| 1920 | 29.98 | | | | |
| 1921 | 24.18 | | | | |
| 1922 | 27.47 | | | | |
| 1923 | 14.73 | | | | |
| 1924 | 21.14 | | | | |
| 1925 | 26.24 | | | | |
| 1926 | 34.63 | | | | |
| 1927 | 28.51 | | | | |
| 1928 | 20.62 | | | | |
| 1929 | 15.3 | | | | |
| 1930 | 17.4 | | | | |

11/9/2021

| - | |
|------|-------|
| 1931 | 25.04 |
| 1932 | 12.78 |
| 1933 | 20.87 |
| 1934 | 18.96 |
| 1935 | 25.54 |
| 1936 | 25.52 |
| 1937 | 34.47 |
| 1938 | 31.9 |
| 1939 | 12.63 |
| 1940 | 46.05 |
| 1941 | 45.26 |
| 1942 | 32.35 |
| 1943 | 21.27 |
| 1944 | 26.51 |
| 1945 | 29.28 |
| 1946 | 14.21 |
| 1947 | 16.82 |
| 1948 | 23.43 |
| 1949 | 16.82 |
| 1950 | 34.39 |
| 1951 | 29.8 |
| 1952 | 34.49 |
| 1953 | 21.26 |
| 1954 | 29.45 |
| 1955 | 25.1 |
| 1956 | 21.25 |
| 1957 | 30.95 |
| 1958 | 35.// |
| 1959 | 20.73 |
| 1960 | 27.2 |
| 1961 | 20.06 |
| 1962 | 27.13 |
| 1903 | 28.50 |
| 1904 | 25.1 |
| 1905 | 20.00 |
| 1900 | 22.75 |
| 1907 | 27.02 |
| 1908 | 30.50 |
| 1909 | 34.10 |
| 1970 | 17 75 |
| 1972 | 19.43 |
| 1973 | Δ1 R |
| 1974 | 24.09 |
| 1975 | 24.41 |
| 1976 | 8.7 |
| 1977 | 19.25 |
| | |

11/9/2021

| 1978 | 30.31 |
|------|-------|
| 1979 | 35.17 |
| 1980 | 24.72 |
| 1981 | 31.37 |
| 1982 | 33.74 |
| 1983 | 62.67 |
| 1984 | 21.4 |
| 1985 | 16.78 |
| 1986 | 38.8 |
| 1987 | 27.96 |
| 1988 | 17.74 |
| 1989 | 21.03 |
| 1990 | 16.9 |
| 1991 | 24.2 |
| 1992 | 30.08 |
| 1993 | 36.42 |
| 1994 | 21.42 |
| 1995 | 55.55 |
| 1996 | 37.21 |
| 1997 | 30.34 |
| 1998 | 52.68 |
| 1999 | 23.66 |
| 2000 | 27.61 |
| 2001 | 36.24 |
| 2002 | 28.87 |
| 2003 | 33.08 |
| 2004 | 33.64 |
| 2005 | 39.25 |
| 2006 | 34.93 |
| 2007 | 13.8 |
| 2008 | 19.43 |
| 2009 | 17.73 |
| 2010 | 34.1 |
| 2011 | 23.25 |
| 2012 | 30.53 |
| 2013 | 6.49 |
| 2014 | 31.39 |
| 2015 | 18.19 |
| 2016 | 35.97 |
| 2017 | 43.71 |
| 2018 | 23.67 |
| 2019 | 43.27 |
| 2020 | 10 |