

TSE Engineers
136 S. State Street
Shelley, Idaho 83274
208-357-2420

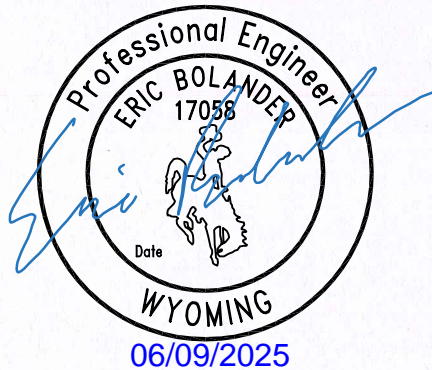
JOB TITLE		Wooden Spur Renovation
		368 Wppdem Spur Dr. Alpine Wy.
JOB NO.	225112	SHEET NO.
CALCULATED BY	EVb	DATE 6/4/25
CHECKED BY		DATE

STRUCTURAL CALCULATIONS

FOR

Wooden Spur Renovation

368 Wppdem Spur Dr. Alpine Wy.



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JOB TITLE Wooden Spur Renovation

368 Wppdem Spur Dr. Alpine Wy.

JOB NO. 225112

SHEET NO. 1 of 39

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CODE SUMMARY**Code:** International Building Code 2021**Live Loads:**

Roof 0 to 200 sf: 20 psf
200 to 600 sf: 24 - 0.02Area, but not less than 12 psf
over 600 sf: 12 psf

Typical Floor 40 psf
Partitions N/A
All other residential areas except bal 40 psf
Habitable attics & sleeping areas 30 psf
Attics without storage 10 psf
Decks (1.5 times live load) 60 psf

Dead Loads:

Floor 10.0 psf
Roof 15.0 psf

Roof Snow Loads:

Design Uniform Roof Snow load = 100.0 psf
Flat Roof Snow Load Pf = 98.0 psf
Balanced Snow Load Ps = 98.0 psf
Ground Snow Load Pg = 140.0 psf
Importance Factor I = 1.00
Snow Exposure Factor Ce = 1.00
Thermal Factor Ct = 1.00
Sloped-roof Factor Cs = 1.00
Drift Surcharge load Pd =
Width of Snow Drift w =

Earthquake Design Data:

Risk Category = II
Importance Factor I = 1.00
Mapped spectral response accelerat Ss = 110.90
S1 = 34.10
Site Class = code default
Spectral Response Coef. Sds = 0.887
Sd1 = 0.445
Seismic Design Category = D
Basic Structural System = Bearing Wall Systems
Seismic Resisting System = Light frame (wood) walls with structural wood shear panels
Seismic Response Coef. Cs = 0.136
Response Modification Factor R = 6.5
Analysis Procedure = Equivalent Lateral-Force Analysis

Rain Design Data:

Rain intensity i = 7.23 in/hr
Rain Load R = 24.4 psf

Wind Design Data:

Ultimate Design Wind Speed 120 mph
Nominal Design Wind Speed 92.95 mph
Risk Category II
Mean Roof Ht (h) 17.0 ft
Exposure Category C
Enclosure Classif. Enclosed Building
Internal pressure Coef. +/-0.18
Directionality (Kd) 0.85

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CALCULATED BY EVB DATE 6/4/25
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Component and Cladding Nominal Wind Pressures

Roof Area	Surface Pressure (psf)							
	2 sf	10 sf	20 sf	50 sf	75 sf	100 sf	200 sf	250 sf
Negative Zone 1 & 2e	-29.1	-29.1	-29.1	-17.7	-12.7	-10.0	-10.0	-10.0
Negative Zone 2n, 2r & 3e	-42.4	-42.4	-36.7	-29.1	-25.7	-23.3	-17.6	-15.8
Negative Zone 3r	-50.5	-50.5	-43.2	-33.7	-29.4	-26.4	-26.4	-26.4
Positive All Zones	11.7	10.0	10.0	10.0	10.0	10.0	10.0	10.0
Overhang Zone 1 & 2e	-33.4	-33.4	-33.4	-25.8	-22.4	-20.0	-20.0	-20.0
Overhang Zone 2n & 2r	-46.7	-46.7	-42.4	-36.7	-34.2	-32.4	-28.1	-26.7
Overhang Zone 3e	-54.7	-54.7	-47.3	-37.4	-33.0	-29.9	-22.4	-20.0
Overhang Zone 3r	-62.7	-62.7	-53.1	-40.3	-34.7	-30.7	-30.7	-30.7

Overhang soffit pressure equals adj wall pressure (which includes internal pressure of 2.4 psf)

Parapet Area	Solid Parapet Pressure (psf)					
	10 sf	20 sf	50 sf	100 sf	250 sf	500 sf
CASE A: Zone 2e :	0.0	0.0	0.0	0.0	0.0	0.0
Zone 2n, 2r & 3e :	0.0	0.0	0.0	0.0	0.0	0.0
Zone 3r :	0.0	0.0	0.0	0.0	0.0	0.0
CASE B : Interior zone :	0.0	0.0	0.0	0.0	0.0	0.0
Corner zone :	0.0	0.0	0.0	0.0	0.0	0.0

Wall Area	Surface Pressure (psf)			
	10 sf	100 sf	200 sf	500 sf
Negative Zone 4	-15.6	-13.5	-12.9	-12.0
Negative Zone 5	-19.2	-15.0	-13.7	-12.0
Positive Zone 4 & 5	14.4	12.3	11.7	10.8

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Code Search

Code: International Building Code 2021

Occupancy:

Occupancy Group = R Residential

Risk Category & Importance Factors:

Risk Category = II
Wind factor = 1.00 use 0.60 NOTE: Output will be nominal wind pressures
Snow factor = 1.00
Seismic factor = 1.00

Type of Construction:

Fire Rating:
Roof = 0.0 hr
Floor = 0.0 hr

Building Geometry:

Roof angle (θ) 2.00 / 12 9.5 deg
Building length 26.0 ft
Least width 38.0 ft
Mean Roof Ht (h) 17.0 ft
Parapet ht above grd 0.0 ft
Minimum parapet ht 0.0 ft

Live Loads:

Roof 0 to 200 sf: 20 psf
200 to 600 sf: 24 - 0.02Area, but not less than 12 psf
over 600 sf: 12 psf

Floor:

Typical Floor 40 psf
Partitions N/A
All other residential areas except balc 40 psf
Habitable attics & sleeping areas 30 psf
Attics without storage 10 psf
Decks (1.5 times live load) 60 psf

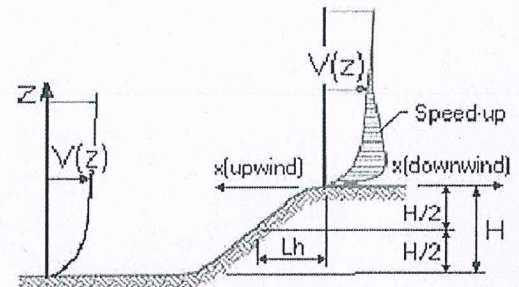
Wind Loads : ASCE 7- 16

Ultimate Wind Speed 120 mph
Nominal Wind Speed 93 mph
Risk Category II
Exposure Category C
Enclosure Classif. Enclosed Building
Internal pressure +/-0.18
Directionality (Kd) 0.85
Kh case 1 0.872
Kh case 2 0.872
Type of roof Gable

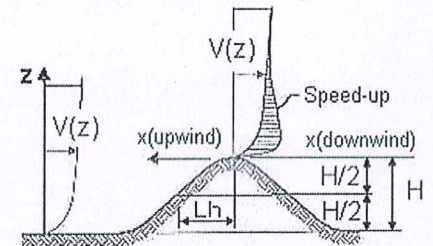
Topographic Factor (Kzt)

Topography Flat
Hill Height (H) 80.0 ft
Half Hill Length (Lh) 100.0 ft
Actual H/Lh = 0.80
Use H/Lh = 0.50
Modified Lh = 160.0 ft
From top of crest: x = 50.0 ft
Bldg up/down wind? downwind

H/Lh = 0.50 $K_1 = 0.000$
x/Lh = 0.31 $K_2 = 0.792$
z/Lh = 0.11 $K_3 = 1.000$
At Mean Roof Ht:
 $K_{zt} = (1 + K_1 K_2 K_3)^2 = 1.00$



ESCARPMENT



2D RIDGE or 3D AXISYMMETRICAL HILL

Gust Effect Factor

h = 17.0 ft
B = 38.0 ft
lz (0.6h) = 15.0 ft

Flexible structure if natural frequency < 1 Hz (T > 1 second).

If building h/B > 4 then may be flexible and should be investigated.

h/B = 0.45 Rigid structure (low rise bldg)

G = 0.85 Using rigid structure formula

Rigid Structure

$\bar{e} = 0.20$
 $\ell = 500$ ft
 $z_{min} = 15$ ft
c = 0.20
 $g_Q, g_v = 3.4$
 $L_z = 427.1$ ft
Q = 0.92
 $I_z = 0.23$
G = 0.88 use G = 0.85

Flexible or Dynamically Sensitive Structure

Natural Frequency (η_1) = 0.0 Hz
Damping ratio (β) = 0
/b = 0.65
/a = 0.15
Vz = 101.3
 $N_1 = 0.00$
 $R_n = 0.000$
 $R_h = 28.282$ $\eta = 0.000$ h = 17.0 ft
 $R_B = 28.282$ $\eta = 0.000$
 $R_L = 28.282$ $\eta = 0.000$
 $g_R = 0.000$
R = 0.000
Gf = 0.000

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Enclosure Classification

Test for Enclosed Building: $A_o < 0.01A_g$ or 4 sf, whichever is smaller

Test for Open Building: All walls are at least 80% open.
 $A_o \geq 0.8A_g$

Test for Partially Enclosed Building: Predominately open on one side only

Input		Test	
Ao	180.0 sf	$A_o \geq 1.1A_{oi}$	NO
Ag	286.0 sf	$A_o > 4'$ or $0.01A_g$	YES
Aoi	308.0 sf	$A_{oi} / A_{gi} \leq 0.20$	NO
Agi	858.0 sf		

Building is NOT Partially Enclosed

Conditions to qualify as Partially Enclosed Building. Must satisfy all of the following:

$$A_o \geq 1.1A_{oi}$$

$$A_o > \text{smaller of } 4' \text{ or } 0.01 A_g$$

$$A_{oi} / A_{gi} \leq 0.20$$

Where:

A_o = the total area of openings in a wall that receives positive external pressure.

A_g = the gross area of that wall in which A_o is identified.

A_{oi} = the sum of the areas of openings in the building envelope (walls and roof) not including A_o .

A_{gi} = the sum of the gross surface areas of the building envelope (walls and roof) not including A_g .

Test for Partially Open Building: A building that does not qualify as open, enclosed or partially enclosed.
(This type building will have same wind pressures as an enclosed building.)

Reduction Factor for large volume partially enclosed buildings (R_i) :

If the partially enclosed building contains a single room that is unpartitioned , the internal pressure coefficient may be multiplied by the reduction factor R_i .

Total area of all wall & roof openings (A_{og}): 0 sf
Unpartitioned internal volume (V_i) : 0 cf
 $R_i = 1.00$

Ground Elevation Factor (K_e)

Grd level above sea level = 5664.0 ft
Constant = 0.00256
Adj Constant = 0.00209
 $K_e = 0.8146$

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Wind Loads - MWFRS $h \leq 60'$ (Low-rise Buildings) except for open buildings

$K_z = K_h$ (case 1) = 0.87
Base pressure (qh) = **13.3 psf**
GCpi = +/-0.18

Edge Strip (a) = 3.0 ft
End Zone (2a) = 6.0 ft
Zone 2 length = 13.0 ft

Wind Pressure Coefficients

Surface	CASE A			CASE B		
	GCpf	$\theta = 9.5 \text{ deg}$ w/-GCpi	w/+GCpi	GCpf	w/-GCpi	w/+GCpi
1	0.44	0.62	0.26	-0.45	-0.27	-0.63
2	-0.69	-0.51	-0.87	-0.69	-0.51	-0.87
3	-0.40	-0.22	-0.58	-0.37	-0.19	-0.55
4	-0.33	-0.15	-0.51	-0.45	-0.27	-0.63
5				0.40	0.58	0.22
6				-0.29	-0.11	-0.47
1E	0.67	0.85	0.49	-0.48	-0.30	-0.66
2E	-1.07	-0.89	-1.25	-1.07	-0.89	-1.25
3E	-0.58	-0.40	-0.76	-0.53	-0.35	-0.71
4E	-0.49	-0.31	-0.67	-0.48	-0.30	-0.66
5E				0.61	0.79	0.43
6E				-0.43	-0.25	-0.61

Nominal Wind Surface Pressures (psf)

1	8.3	3.5	-3.6	-8.4
2	-6.8	-11.6	-6.8	-11.6
3	-3.0	-7.8	-2.5	-7.3
4	-2.0	-6.8	-3.6	-8.4
5			7.7	2.9
6			-1.5	-6.3
1E	11.3	6.5	-4.0	-8.8
2E	-11.9	-16.7	-11.9	-16.7
3E	-5.3	-10.1	-4.7	-9.5
4E	-4.2	-9.0	-4.0	-8.8
5E			10.5	5.7
6E			-3.3	-8.1

Parapet

Windward parapet = 0.0 psf (GCpn = +1.5)
Leeward parapet = 0.0 psf (GCpn = -1.0)

Windward roof overhangs = 9.3 psf (upward) add to windward roof pressure

Horizontal MWFRS Simple Diaphragm Pressures (psf)

Transverse direction (normal to L)

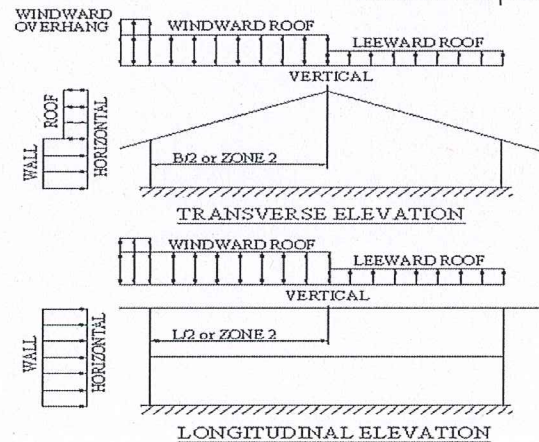
Interior Zone: Wall 10.3 psf
Roof -3.8 psf **
End Zone: Wall 15.5 psf
Roof -6.6 psf **

Longitudinal direction (parallel to L)

Interior Zone: Wall 9.2 psf
End Zone: Wall 13.9 psf

** NOTE: Total horiz force shall not be less than that determined by neglecting roof forces (except for MWFRS moment frames).

The code requires the MWFRS be designed for a min ultimate force of 16 psf multiplied by the wall area plus an 8 psf force applied to the vertical projection of the roof.

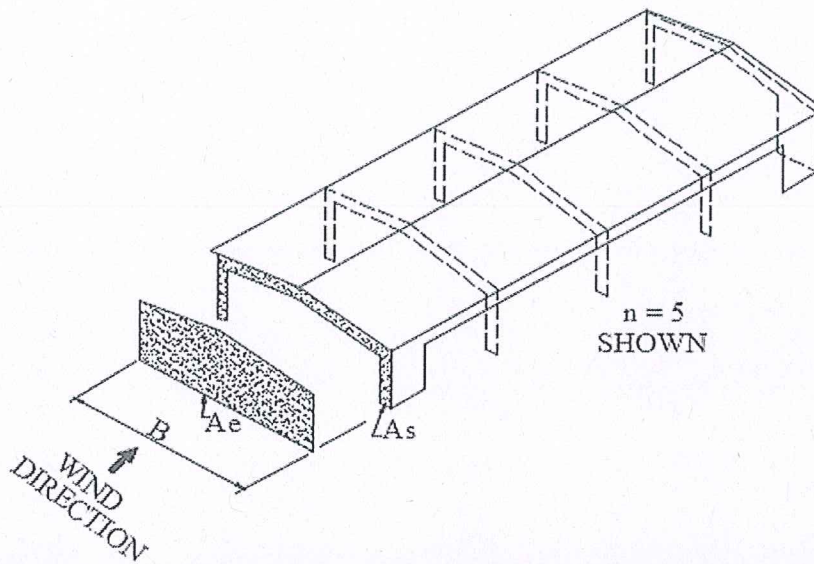


Wind Loads - $h \leq 60'$ Longitudinal Direction MWFRS On Open or Partially

Enclosed Buildings with Transverse Frames and Pitched Roofs

Base pressure (q_h) = **13.3 psf**
 GCpi = ± 0.18 Enclosed bldg, procedure doesn't apply
 Roof Angle (θ) = 9.5 deg

ASCE 7-16 procedure

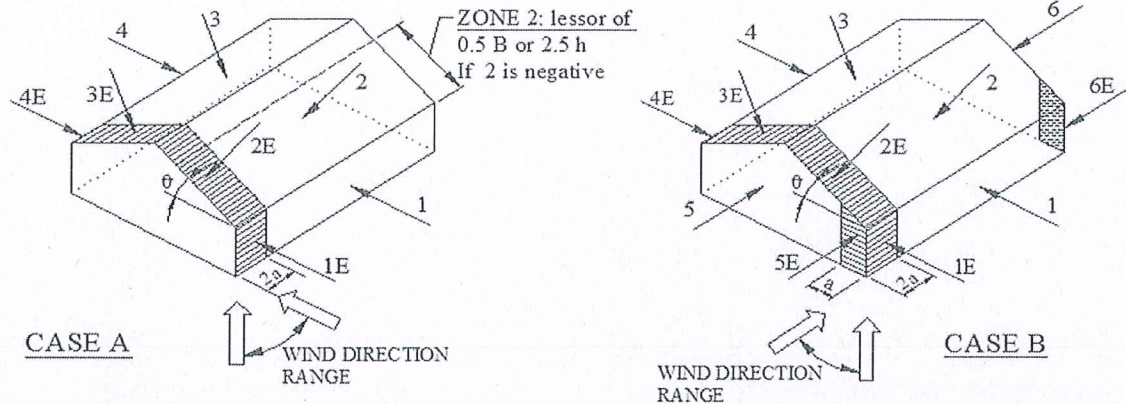


$B = 38.0$ ft
 # of frames (n) = 5
 Solid area of end wall including fascia (A_s) = 1,500.0 sf
 Roof ridge height = 20.2 ft
 Roof eave height = 17.0 ft
 Total end wall area if solid (A_e) = 706.2 sf

Longitudinal Directional Force (F) = $p A_e$
 $p = q_h [(GC_{pf})_{windward} - (GC_{pf})_{leeward}] K_B K_S$
 Solidarity ratio (Φ) = 2.124
 $n = 5$
 $K_B = 1.42$
 $K_S = 5.597$
 Zones 5 & 6 area = 653 sf
 5E & 6E area = 53 sf
 $(GC_{pf})_{windward} - (GC_{pf})_{leeward} = 0.716$
 $p = 76.0$ psf

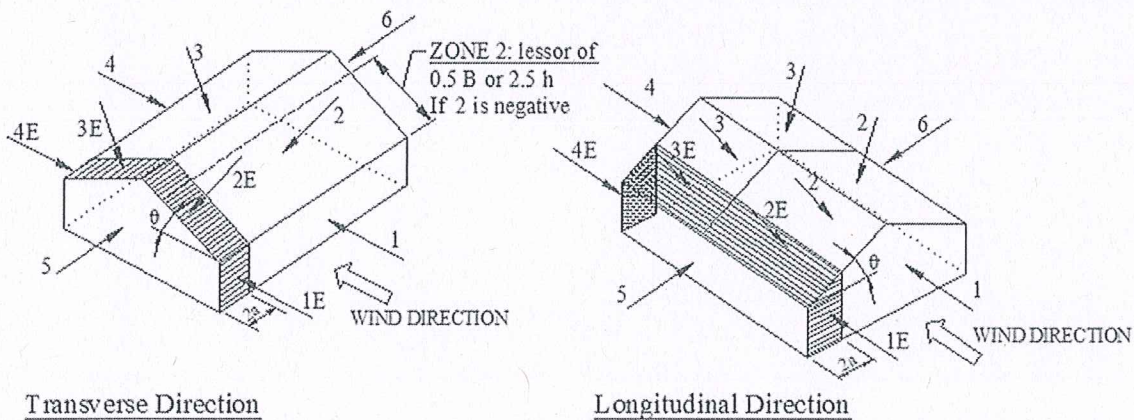
Total force to be resisted by MWFRS (F) = **53.7 kips** applied at the centroid of the end wall area A_e

Note: The longitudinal force acts in combination with roof loads calculated elsewhere for an open or partially enclosed building.



NOTE: Torsional loads are 25% of zones 1 - 6. See code for loading diagram.
Exception: One story buildings $h < 30'$ and 1 to 2 story buildings framed with light-frame construction or with flexible diaphragms need not be designed for the torsional load case.

ASCE 7-98 & ASCE 7-10 (& later) - MWFRS wind pressure zones



NOTE: Torsional loads are 25% of zones 1 - 4. See code for loading diagram.
Exception: One story buildings $h < 30'$ and 1 to 2 story buildings framed with light-frame construction or with flexible diaphragms need not be designed for the torsional load case.

ASCE 7-02 and ASCE 7-05 - MWFRS wind pressure zones

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Nominal Wind Pressures

Wind Loads - Components & Cladding : $h \leq 60'$

Kh (case 2) = 0.87 h = 17.0 ft
 Base pressure (qh) = 13.3 psf a = 3.0 ft
 Minimum parapet ht = 0.0 ft GCpi = +/-0.18
 Roof Angle (θ) = 9.5 deg qi = qh = 13.3 psf
 Type of roof = Gable

Roof	Area	Surface Pressure (psf)						
		2 sf	10 sf	20 sf	50 sf	75 sf	100 sf	200 sf
Negative Zone 1 & 2e		-29.1	-29.1	-29.1	-17.7	-12.7	-10.0	-10.0
Negative Zone 2n, 2r & 3e		-42.4	-42.4	-36.7	-29.1	-25.7	-23.3	-17.6
Negative Zone 3r		-50.5	-50.5	-43.2	-33.7	-29.4	-26.4	-26.4
Positive All Zones		11.7	10	10	10	10.0	10.0	10.0
Overhang Zone 1 & 2e		-33.4	-33.4	-33.4	-25.8	-22.4	-20.0	-20.0
Overhang Zone 2n & 2r		-46.7	-46.7	-42.4	-36.7	-34.2	-32.4	-28.1
Overhang Zone 3e		-54.7	-54.7	-47.3	-37.4	-33.0	-29.9	-22.4
Overhang Zone 3r		-62.7	-62.7	-53.1	-40.3	-34.7	-30.7	-30.7

Overhang pressures in the table above assume an internal pressure coefficient (GCpi) of 0.0
 Overhang soffit pressure equals adj wall pressure (which includes internal pressure of 2.4 psf)

User input	
25 sf	50 sf
-26.3	-17.7
-34.8	-29.1
-40.9	-33.7
10.0	10.0
-31.5	-25.8
-41.0	-36.7
-44.8	-37.4
-50.0	-40.3

Parapet

qp = 0.0 psf

Solid Parapet Pressure		Surface Pressure (psf)				
		10 sf	20 sf	50 sf	100 sf	250 sf
CASE A:	Zone 2e :	0.0	0.0	0.0	0.0	0.0
	Zone 2n, 2r & 3e :	0.0	0.0	0.0	0.0	0.0
	Zone 3r :	0.0	0.0	0.0	0.0	0.0
CASE B :	Interior zone :	0.0	0.0	0.0	0.0	0.0
	Corner zone :	0.0	0.0	0.0	0.0	0.0

User input	
50 sf	
0.0	
0.0	
0.0	
0.0	
0.0	
0.0	

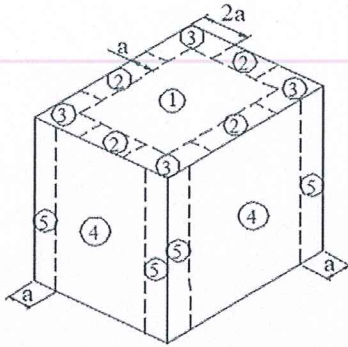
Walls

Area	GCp +/- GCpi				Surface Pressure at h			
	10 sf	100 sf	200 sf	500 sf	10 sf	100 sf	200 sf	500 sf
Negative Zone 4	-1.17	-1.01	-0.96	-0.90	-15.6	-13.5	-12.9	-12.0
Negative Zone 5	-1.44	-1.12	-1.03	-0.90	-19.2	-15.0	-13.7	-12.0
Positive Zone 4 & 5	1.08	0.92	0.87	0.81	14.4	12.3	11.7	10.8

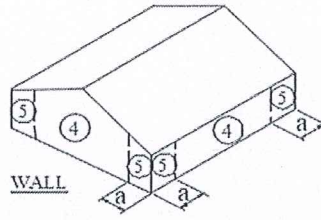
Note: GCp reduced by 10% due to roof angle ≤ 10 deg.

User input	
21 sf	50 sf
-14.9	-14.1
-17.8	-16.3
13.7	12.9

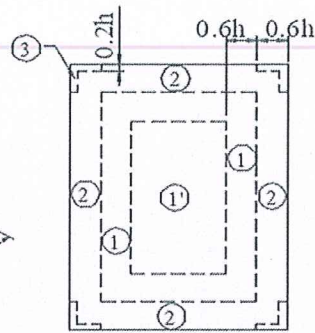
Location of C&C Wind Pressure Zones - ASCE 7-16



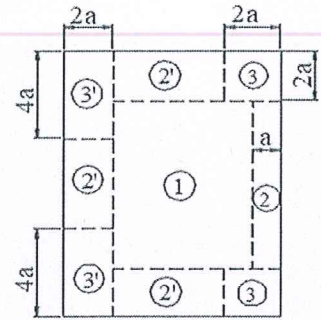
Roofs w/ $\theta \leq 10^\circ$
 and all walls
 $h > 60'$



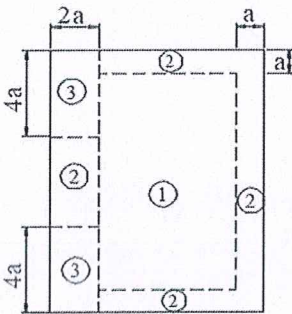
Walls $h \leq 60'$
 & alt design $h < 90'$



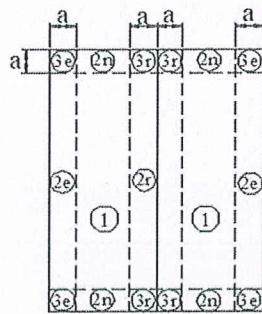
Gable, Sawtooth and
 Multispan Gable $\theta \leq 7$ degrees &
 Monoslope ≤ 3 degrees
 $h \leq 60'$ & alt design $h < 90'$



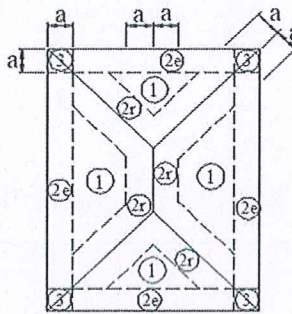
Monoslope roofs
 $3^\circ < \theta \leq 10^\circ$
 $h \leq 60'$ & alt design $h < 90'$



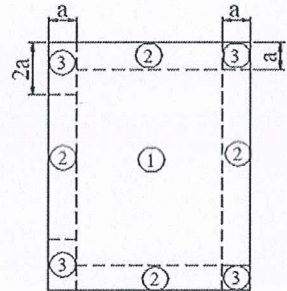
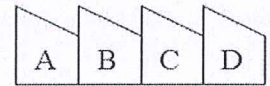
Monoslope roofs
 $10^\circ < \theta \leq 30^\circ$
 $h \leq 60'$ & alt design $h < 90'$



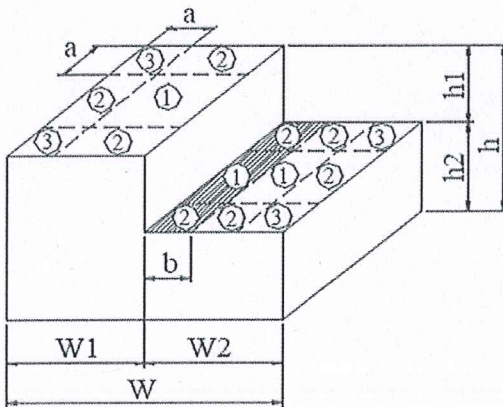
Multispan Gable &
 Gable $7^\circ < \theta \leq 45^\circ$



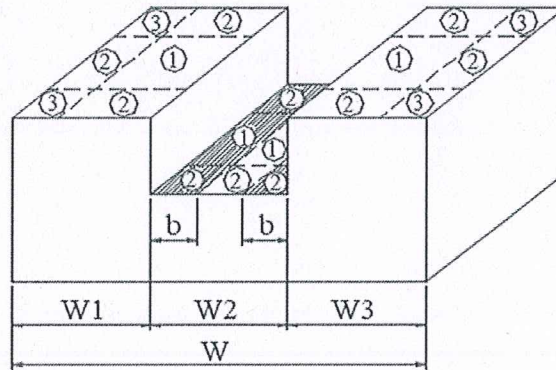
Hip $7^\circ < \theta \leq 27^\circ$



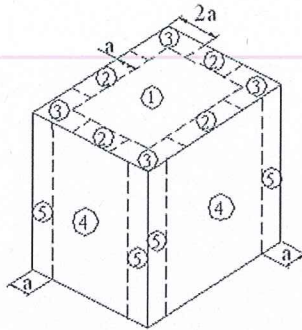
Sawtooth $10^\circ < \theta \leq 45^\circ$
 $h \leq 60'$ & alt design $h < 90'$



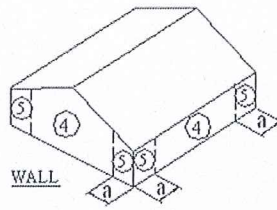
Stepped roofs $\theta \leq 3^\circ$
 $h \leq 60'$ & alt design $h < 90'$



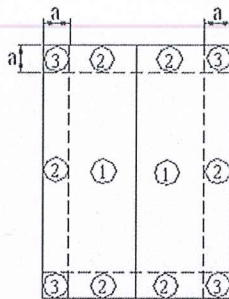
Location of C&C Wind Pressure Zones - ASCE 7-10 & earlier



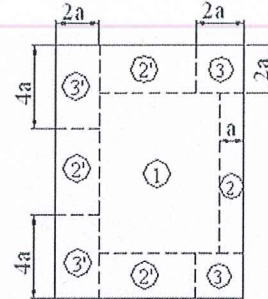
Roofs w/ $\theta \leq 10^\circ$
 and all walls
 $h > 60'$



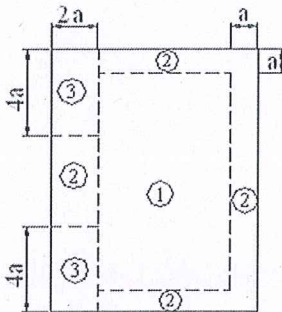
Walls $h \leq 60'$
 & alt design $h < 90'$



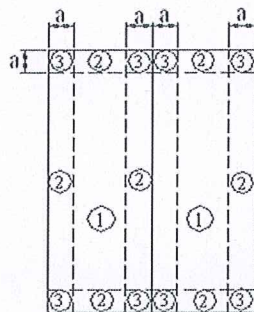
Gable, Sawtooth and
 Multispan Gable $\theta \leq 7$ degrees &
 Monoslope ≤ 3 degrees
 $h \leq 60'$ & alt design $h < 90'$



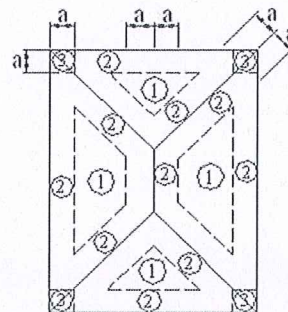
Monoslope roofs
 $3^\circ < \theta \leq 10^\circ$
 $h \leq 60'$ & alt design $h < 90'$



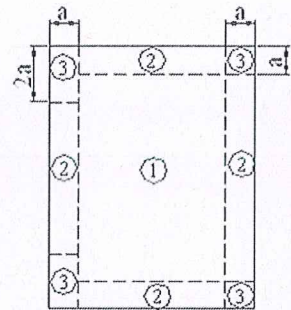
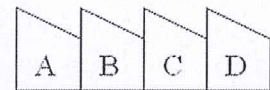
Monoslope roofs
 $10^\circ < \theta \leq 30^\circ$
 $h \leq 60'$ & alt design $h < 90'$



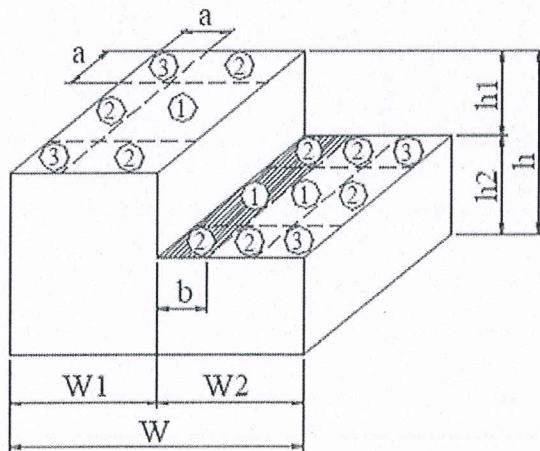
Multispan Gable &
 Gable $7^\circ < \theta \leq 45^\circ$



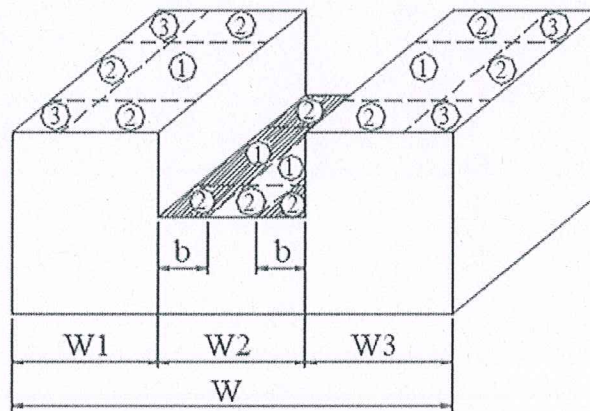
Hip $7^\circ < \theta \leq 27^\circ$



Sawtooth $10^\circ < \theta \leq 45^\circ$
 $h \leq 60'$ & alt design $h < 90'$



Stepped roofs $\theta \leq 3^\circ$
 $h \leq 60'$ & alt design $h < 90'$



Snow Loads : ASCE 7- 16

Nominal Snow Forces

Roof slope = 9.5 deg
Horiz. eave to ridge dist (W) = 19.0 ft
Roof length parallel to ridge (L) = 26.0 ft

Type of Roof Hip and gable w/ trussed systems
Ground Snow Load $P_g = 140.0$ psf
Risk Category = II
Importance Factor $I = 1.0$
Thermal Factor $C_t = 1.00$
Exposure Factor $C_e = 1.0$

$P_f = 0.7 \cdot C_e \cdot C_t \cdot I \cdot P_g = 98.0$ psf
Unobstructed Slippery Surface no

Sloped-roof Factor $C_s = 1.00$
Balanced Snow Load = 98.0 psf

Near ground level surface balanced snow load = 140.0 psf

Rain on Snow Surcharge Angle 0.38 deg
Code Maximum Rain Surcharge 5.0 psf
Rain on Snow Surcharge = 0.0 psf
Ps plus rain surcharge = 98.0 psf
Minimum Snow Load $P_m = 20.0$ psf

Uniform Roof Design Snow Load = 98.0 psf use 100.0

NOTE: Alternate spans of continuous beams shall be loaded with half the design roof snow load so as to produce the greatest possible effect - see code for loading diagrams and exceptions for gable roofs..

Unbalanced Snow Loads - for Hip & Gable roofs only

Required if slope is between 7 on 12 = 30.26 deg
and 2.38 deg = 2.38 deg Unbalanced snow loads must be applied

Windward snow load = 29.4 psf = $0.3P_s$
Leeward snow load from ridge to 16.88' = 129.7 psf = $hdy / \sqrt{S} + P_s$
Leeward snow load from 16.88' to the eave = 98.0 psf = P_s

Windward Snow Drifts 1 - Against walls, parapets, etc

Up or downwind fetch $l_u = 40.0$ ft
Projection height $h = 6.0$ ft
Projection width/length $l_p = 18.0$ ft
Snow density $g = 30.0$ pcf
Balanced snow height $h_b = 3.27$ ft
 $h_d = 2.73$ ft
 $h_c = 2.73$ ft

$h_c/h_b > 0.2 = 0.8$ Therefore, design for drift

Drift height (h_c) = 2.73 ft
Drift width $w = 10.95$ ft
Surcharge load: $pd = \gamma \cdot h_d = 82.0$ psf
Balanced Snow load: = 98.0 psf

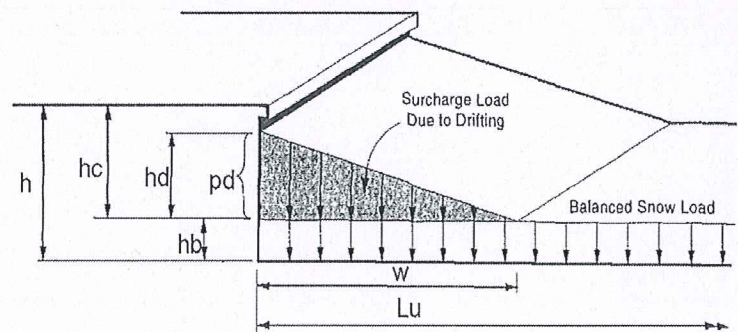
180.0 psf

Windward Snow Drifts 2 - Against walls, parapets, etc

Up or downwind fetch $l_u = 12.0$ ft
Projection height $h = 6.0$ ft
Projection width/length $l_p = 18.0$ ft
Snow density $g = 30.0$ pcf
Balanced snow height $h_b = 3.27$ ft
 $h_d = 1.94$ ft
 $h_c = 2.73$ ft

$h_c/h_b > 0.2 = 0.8$ Therefore, design for drift

Drift height (h_d) = 1.94 ft
Drift width $w = 7.75$ ft
Surcharge load: $pd = \gamma \cdot h_d = 58.2$ psf
Balanced Snow load: = 98.0 psf
156.2 psf



Note: If bottom of projection is at least 2 feet above h_b then snow drift is not required.

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Seismic Loads:

IBC 2021

Strength Level Forces

Risk Category : II
Importance Factor (Ie) : 1.00

Site Class : D - code default

Ss (0.2 sec) = 110.90 %g
S1 (1.0 sec) = 34.10 %g

A site specific ground motion analysis is required for seismically isolated structures or with damping systems, see ASCE7 11.4.8

Fa =	1.200	Sms =	1.331	S _{DS} =	0.887	Design Category =	D
Fv =	1.959	Sm1 =	0.668	S _{D1} =	0.445	Design Category =	D

Seismic Design Category = D
Redundancy Coefficient p = 1.30
Number of Stories: 1

Structure Type: All other building systems

Horizontal Struct Irregularities: No plan Irregularity
Vertical Structural Irregularities: No vertical Irregularity

Flexible Diaphragms: Yes

Building System: **Bearing Wall Systems**

Seismic resisting system: **Light frame (wood) walls with structural wood shear panels**

System Structural Height Limit: **65 ft**

Actual Structural Height (hn) = 17.0 ft

See ASCE7 Section 12.2.5 for exceptions and other system limitations

DESIGN COEFFICIENTS AND FACTORS

Response Modification Coefficient (R) = 6.5
Over-Strength Factor (Ωo) = 2.5
Deflection Amplification Factor (Cd) = 4
S_{DS} = 0.887
S_{D1} = 0.445

Seismic Load Effect (E) = $E_h \pm E_v = \rho Q_E \pm 0.2 S_{DS} D$ = $1.3 Q_E \pm 0.177 D$ Q_E = horizontal seismic force
Special Seismic Load Effect (Em) = $E_m h \pm E_v = \Omega_o Q_E \pm 0.2 S_{DS} D$ = $2.5 Q_E \pm 0.177 D$ D = dead load

PERMITTED ANALYTICAL PROCEDURES

Simplified Analysis - Use Equivalent Lateral Force Analysis

Equivalent Lateral-Force Analysis - Permitted

Building period coef. (C _T) =	0.020	Cu =	1.40
Approx fundamental period (Ta) =	C _T h _n ^{1/4} = 0.167 sec	x =	0.75
User calculated fundamental period =	0.500 s	Tmax = CuTa =	0.234 sec
Long Period Transition Period (TL) =	ASCE7 map = 8 sec	T =	0.234 sec

Seismic response coef. (Cs) = S_{ds}/R = 0.136 ASCE7 11.4.8 exception 2 equations used
but not less than Cs = 0.044S_{ds} = 0.039
USE Cs = 0.136

Design Base Shear V = 0.136W

Model & Seismic Response Analysis - Permitted (see code for procedure)

ALLOWABLE STORY DRIFT

Structure Type: All other structures

Allowable story drift Δa = 0.020hsx where hsx is the story height below level x

Total Stories = 1
 Building length L = 26.0 ft
 Building width W = 38.0 ft
 hn = 17.0 ft
 k = 1.000
 V = 0.136W

Floor Dead Load = 40.0 psf
 Floor LL to include = 0.0 psf
 Floor Equip wt = 0.0 kips
 Partition weight = 10.0 psf
 Ext Wall Weight = 0.0 psf

Roof Dead Load = 20.0 psf
 Roof Snow Load = 20.0 psf
 Roof Equip wt = 0.0 kips
 Parapet weight = 0.0 psf
 Parapet height = 0.0 ft

Bottom Floor is a slab on grade

Diaphragm shall be designed for level force F_x ,
 but not less than $F_{px} = (\sum F_i / \sum w_i) w_{px}$, but :
 $F_{px} \min = 0.2 S_{DS}$ le $w_{px} = 0.177 w_{px}$
 $F_{px} \max = 0.4 S_{DS}$ le $w_{px} = 0.355 w_{px}$

Seismic Forces Normal to Building Length

EL. above		Level		$C_{vx} =$	V = 5.4k					
Seismic Base		Weight	$W_x h_x^k$	$\frac{W_x h_x^k}{\sum W_i h_i^k}$	Base Shear Distribution			Diaphragm Force F_{px}		
Level (x)	h_x (ft)	W_x (kips)	(ft-kips)	$\sum W_i h_i^k$	$F_x = C_{vx} V$	$\sum F_x$ (k)	Story M	$\sum W_i$ (k)	F_{px}	Design F_{px}
Roof	15.00	40	593	1.000	5.39	5.4	0	40	5.4	7.0
1	2.00	0	0	0.000	0.00	0.0	0	0	0.0	0.0
Base		40		1.000		5.4	81			
							81 = Base M			

81 = Base M

Seismic Forces Parallel to Building Length

Level (x)	h_x (ft)	W_x (kips)	$W_x h_x^k$	$C_{vx} =$	V = 5.4k Base Shear Distribution			Diaphragm Force F_{px}		
					$F_x = C_{vx} V$	$\sum F_x$ (k)	Story M	$\sum W_i$ (k)	F_{px}	Design F_{px}
Roof	15.00	40	593	1.000	5.39	5.4	0	40	5.4	7.0
1	2.00	0	0	0.000	0.00	0.0	0	0	0.0	0.0
Base	0.00	40		1.000		5.4	81			

81 = Base M

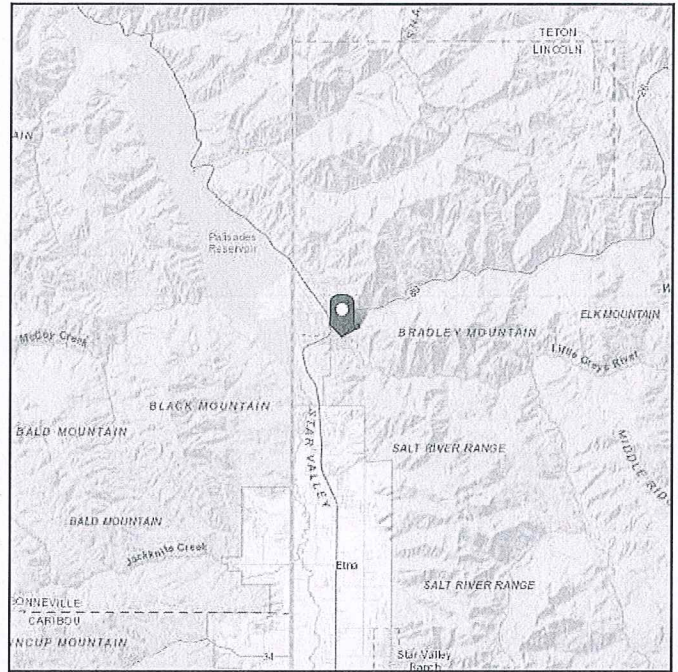
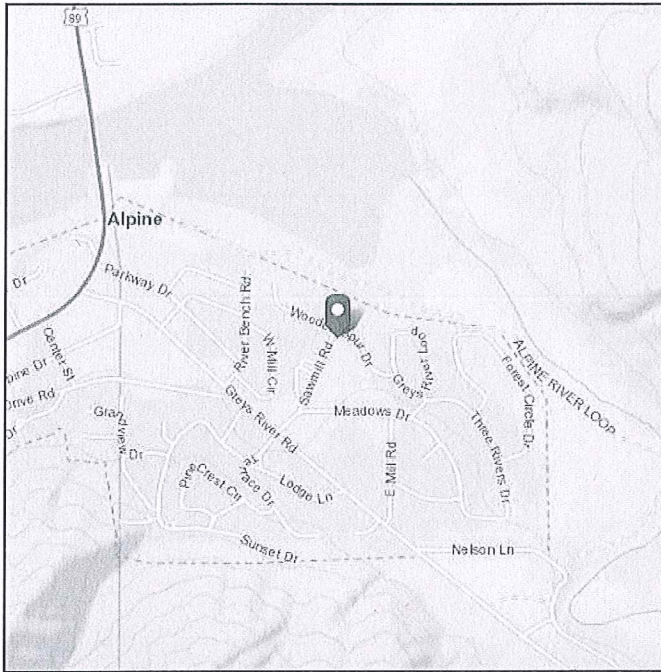


ASCE Hazards Report

Address:
368 Wooden Spur Dr
Alpine, Wyoming
83128

Standard: ASCE/SEI 7-16
Risk Category: II
Soil Class: D - Default (see
Section 11.4.3)

Latitude: 43.16238
Longitude: -111.008836
Elevation: 5666.142041756172 ft
(NAVD 88)





Seismic

Site Soil Class: D - Default (see Section 11.4.3)

Results:

S_s :	1.109	S_{D1} :	N/A
S_1 :	0.341	T_L :	6
F_a :	1.2	PGA :	0.477
F_v :	N/A	PGA_M :	0.572
S_{MS} :	1.331	F_{PGA} :	1.2
S_{M1} :	N/A	I_e :	1
S_{DS} :	0.888	C_v :	1.322

Ground motion hazard analysis may be required. See ASCE/SEI 7-16 Section 11.4.8.

Data Accessed: Wed Jun 04 2025

Date Source: USGS Seismic Design Maps

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JOB TITLE Wooden Spur Renovation
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 CHECKED BY DATE

Roof Design Loads

Items	Description	Multiple	psf (max)	psf (min)
Roofing	Asphalt Shingles w/roll roofing		3.0	2.0
Decking	5/8" plywood/OSB		2.2	1.8
Framing	Wood Trusses @ 24"		3.0	2.5
Insulation	R-40 Fiberglass insul.	x 1.4	1.8	1.7
Ceiling	5/8" gypsum		2.8	2.5
			0.0	0.0
			0.0	0.0
			0.0	0.0
Actual Dead Load			12.8	10.5
Use this DL instead			15.0	9.0
Live Load			20.0	0.0
Snow Load			100.0	0.0
Ultimate Wind (zone 2 - 100sf)			16.0	-38.9
ASD Loading				
D + S			115.0	-
D + 0.75(0.6*W + S)			97.2	-
0.6*D + 0.6*W			-	-17.9
LRFD Loading				
1.2D + 1.6 S + 0.5W			186.0	-
1.2D + 1.0W + 0.5S			84.0	-
0.9D + 1.0W			-	-30.8

Roof Live Load Reduction

Roof angle 2.00 / 12 9.5 deg

0 to 200 sf: 20.0 psf
 200 to 600 sf: $24 - 0.02 \text{Area}$, but not less than 12 psf
 over 600 sf: 12.0 psf

300 sf 18.0 psf
 400 sf 16.0 psf
 500 sf 14.0 psf
 User Input: 450 sf 15.0 psf

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 368 Wppdem Spur Dr. Alpine Wy.
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Floor Design Loads

Items	Description	Multiple	psf (max)	psf (min)
Flooring	Carpet & pad		1.0	1.0
	None		0.0	0.0
Decking	3/4" plywood/OSB		2.7	2.3
Framing	TJI @ 24"	x 1.4	2.8	1.4
	None		0.0	0.0
Ceiling	5/8" gypsum		2.8	2.5
	None		0.0	0.0
	None		0.0	0.0
	None		0.0	0.0
Actual Dead Load			9.3	7.2
Use this DL instead			10.0	8.0
Partitions			15.0	0.0
Live Load			40.0	0.0
Total Live Load			55.0	0.0
Total Load			65.0	7.2

FLOOR LIVE LOAD REDUCTION (not including partitions)

NOTE: Not allowed for assembly occupancy or LL>100psf or passenger car garages, except may reduce members supporting 2 or more floors & non-assembly 20%.

$L = L_o(0.25 + 15/\sqrt{K_{LL}A_T})$

Unreduced design live load: $L_o =$ 40 psf

Floor member & 1 floor cols $K_{LL} =$ 2

Tributary Area $A_T =$ 300 sf

Reduced live load: $L =$ 34.5 psf

Columns (2 or more floors) $K_{LL} =$ 4

Tributary Area $A_T =$ 500 sf

Reduced live load: $L =$ 23.4 psf

IBC alternate procedure

Smallest of:

$R = .08(SF - 150)$

$R = 23.1(1 + D/L) =$ 28.9%

$R = 40\%$ member supports 1 floor

$R = 60\%$ member supports ≥ 2 floors

$R =$ 12.0%

Reduced live load: $L =$ 35.2 psf

$R =$ 28.0%

Reduced live load: $L =$ 28.8 psf

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JOB TITLE Wooden Spur Renovation
368 Wooden Spur Dr. Alpine, Wyoming
JOB NO. 225112
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SHEET NO.
DATE
DATE

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6/4/2025

Wood Header Design Or Wood Beam (Not Laterally Supported)
NDS 2018

Mark: HDR1

Mark: HDR1			Load Factors		Loading							
Span(ft)= 18		Dead 1.00		DL (psf)		LL (psf)		trib (ft)		DLw(plf)	LLw(plf)	TLw(plf)
LL Deflection<L/ 360		Floor Live 1.00		roof	15	100		16		240	1600	1840
Total Deflection<L/ 240		Roof Live/Snow 1.00		floor						0	0	0
CD= 1		Misc. 1.00		wall						0	0	0
				misc.						0	0	0
				Total						240.0	1600.0	1840

				Load Factors Applied		Reactions		
	Load	DL(lbs)	LL(lbs)	x(ft)(left)	DL	LL		
Point Load 1	roof				0	0	Uniform	RDL= 2160 2160
Point Load 2	roof				0	0		RLL= 14400 14400
							Point Loads	P1DL= 0 0
								P1LL= 0 0
								P2DL= 0 0
								P2LL= 0 0
								RTL= 16560 16560
							Max Shear=	16.6 k
Wood Species=		Douglas Fir #2	Douglas Fir #1	LVL	24F-V4			
Option 1	No Single Ply	4x None	No Single Ply	3.125 x None				

DIM TIMBER LVL GLB

Wood Species=	Douglas Fir #2	Douglas Fir #1	LVL	24F-V4
Option 1	No Single Ply	4x None	No Single Ply	3.125 x None
Option 2	No Double Ply	6x None	No Double Ply	5.125x22.5
Option 3	No Triple Ply	8x None	No Triple Ply	6.75x19.5
Option 4	No Four Ply	10x None	(4) 1.75x18	8.75x18
Option 5	-	12x None	-	10.75x16.5
Option 6	-	14x None	-	-
Option 7	-	16x18	-	-

Moment			
	Center	Point Load 1	Point Load 2
RDL=	9720	0	0
RLL=	64800	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	74520	0	0
Max M=	74.5	k-ft	

Mark: HDR2

Mark: HDR2		Load Factors		Loading						
Span(ft)= 3		Dead	1.00	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)	
LL Deflection<L/ 360		Floor Live	1.00	roof	15	100	4	60	400	460
Total Deflection<L/ 240		Roof Live/Snow	1.00	floor				0	0	0
CD= 1		Misc.	1.00	wall				0	0	0
				misc.				0	0	0
				Total				65.2	434.8	500

				Load Factors Applied		Reactions		
	Load	DL(lbs)	LL(lbs)	x(ft)(left)	DL	LL		
Point Load 1	roof				0	0	Uniform	RDL= 98 98
Point Load 2	roof				0	0		RLL= 652 652
							Point Loads	P1DL= 0 0
								P1LL= 0 0
								P2DL= 0 0
								P2LL= 0 0
								RTL= 750 750
								Max Shear= 0.8 k
Wood Species=	Douglas Fir #2	Douglas Fir #1	LVL	24F-V4				
Option 1	(1) 2x6	4x4	(1) 1.75x5.5	3.125x9				

DIM TIMBER LVL GLB

Wood Species=	Douglas Fir #2	Douglas Fir #1	LVL	24F-V4
Option 1	(1) 2x6	4x4	(1) 1.75x5.5	3.125x9
Option 2	(2) 2x4	6x6	(2) 1.75x5.5	5.125x6
Option 3	(3) 2x4	8x8	(3) 1.75x5.5	6.75x9
Option 4	(4) 2x4	10x10	(4) 1.75x5.5	8.75x9
Option 5	-	12x12	-	10.75x12
Option 6	-	14x14	-	-
Option 7	-	16x16	-	-

Moment			
	Center	Point Load 1	Point Load 2
RDL=	73	0	0
RLL=	489	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	563	0	0
Max M=	0.6	k-ft	

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JOB TITLE Wooden Spur Renovation

368 Wooden Spur Dr. Alpine, Wyoming

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Wood Header Design Or Wood Beam (Not Laterally Supported)
NDS 2018

Mark: HDR3

Mark: HDR3		Load Factors		Loading						
Span(ft)=	8	Dead	1.00	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)	
LL Deflection<L/	360	Floor Live	1.00	roof	15	100	14	210	1400	1610
Total Deflection<L/	240	Roof Live/Snow	1.00	floor				0	0	0
CD=	1	Misc.	1.00	wall				0	0	0
				misc.				0	0	0
Total							210.0	1400.0	1610	

Load Factors Applied				Reactions	
Load	DL(lbs)	LL(lbs)	x(ft)(left)	DL	LL
Point Load 1				0	0
Point Load 2				0	0

DIM TIMBER LVL GLB

Wood Species=	Douglas Fir #2	Douglas Fir #1	LVL	24F-V4
Option 1	No Single Ply	4x None	No Single Ply	3.125x12
Option 2	No Double Ply	6x12	(2) 1.75x11.875	5.125x9
Option 3	No Triple Ply	8x12	(3) 1.75x9.5	6.75x9
Option 4	No Four Ply	10x10	(4) 1.75x9.5	8.75x9
Option 5	-	12x12	-	10.75x12
Option 6	-	14x14	-	-
Option 7	-	16x16	-	-

Reactions		Left (lbs)	Right (lbs)
Uniform	RDL=	840	840
	RLL=	5600	5600
Point Loads	P1DL=	0	0
	P1LL=	0	0
	P2DL=	0	0
	P2LL=	0	0
	RTL=	6440	6440
	Max Shear=	6.4	k

Moment			
	Center	Point Load 1	Point Load 2
RDL=	1680	0	0
RLL=	11200	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	12880	0	0
	Max M=	12.9	k-ft

Mark: HDR4

Mark: HDR4		Load Factors		Loading						
Span(ft)=	3	Dead	1.00	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)	
LL Deflection<L/	360	Floor Live	1.00	roof	15	100	14	210	1400	1610
Total Deflection<L/	240	Roof Live/Snow	1.00	floor				0	0	0
CD=	1	Misc.	1.00	wall				0	0	0
				misc.				0	0	0
Total							210.0	1400.0	1610	

Load Factors Applied				Reactions	
Load	DL(lbs)	LL(lbs)	x(ft)(left)	DL	LL
Point Load 1				0	0
Point Load 2				0	0

DIM TIMBER LVL GLB

Wood Species=	Douglas Fir #2	Douglas Fir #1	LVL	24F-V4
Option 1	No Single Ply	4x8	(1) 1.75x9.5	3.125x9
Option 2	(2) 2x8	6x6	(2) 1.75x5.5	5.125x6
Option 3	(3) 2x6	8x8	(3) 1.75x5.5	6.75x9
Option 4	(4) 2x6	10x10	(4) 1.75x5.5	8.75x9
Option 5	-	12x12	-	10.75x12
Option 6	-	14x14	-	-
Option 7	-	16x16	-	-

Reactions		Left (lbs)	Right (lbs)
Uniform	RDL=	315	315
	RLL=	2100	2100
Point Loads	P1DL=	0	0
	P1LL=	0	0
	P2DL=	0	0
	P2LL=	0	0
	RTL=	2415	2415
	Max Shear=	2.4	k

Moment			
	Center	Point Load 1	Point Load 2
RDL=	236	0	0
RLL=	1575	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	1811	0	0
	Max M=	1.8	k-ft

TSE Engineers
136 S State Street
Shelley, ID 83274
208-357-2420

JOB TITLE Wooden Spur Renovation
368 Wooden Spur Dr. Alpine, Wyoming
JOB NO. 225112 SHEET NO. 21 of 39
CALCULATED BY EVB DATE 6/4/2025
CHECKED BY 0 DATE

Wood Header Design Or Wood Beam (Not Laterally Supported)
NDS 2018

Mark: HDR5

Load Factors		Loading					
Span(ft)=	Dead	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)
4	1.00	15	100	4	60	400	460
LL Deflection<L/	Floor Live				0	0	0
360	1.00				0	0	0
Total Deflection<L/	Roof Live/Snow				0	0	0
240	1.00				0	0	0
CD=	Misc.				0	0	0
1	1.00						
Total					65.2	434.8	500

Load Factors Applied				Reactions	
Load	DL(lbs)	LL(lbs)	x(ft)(left)	Left (lbs)	Right (lbs)
Point Load 1					
Point Load 2					
roof	0	0		Uniform RDL=	130
roof	0	0		Uniform RLL=	870
				Point Loads P1DL=	0
				Point Loads P1LL=	0
				Point Loads P2DL=	0
				Point Loads P2LL=	0
				Point Loads RTL=	1000
				Point Loads Max Shear=	1.0

DIM TIMBER LVL GLB

Wood Species=	Douglas Fir #2	Douglas Fir #1	LVL	24F-V4
Option 1	(1) 2x8	4x4	(1) 1.75x5.5	3.125x9
Option 2	(2) 2x6	6x6	(2) 1.75x5.5	5.125x6
Option 3	(3) 2x4	8x8	(3) 1.75x5.5	6.75x9
Option 4	(4) 2x4	10x10	(4) 1.75x5.5	8.75x9
Option 5	-	12x12	-	10.75x12
Option 6	-	14x14	-	-
Option 7	-	16x16	-	-

Moment			
	Center	Point Load 1	Point Load 2
RDL=	130	0	0
RLL=	870	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	1000	0	0
Max M=	1.0		k-ft

Mark: HDR6

Load Factors		Loading					
Span(ft)=	Dead	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)
3	1.00	15	100	4	60	400	460
LL Deflection<L/	Floor Live				0	0	0
360	1.00				0	0	0
Total Deflection<L/	Roof Live/Snow				0	0	0
240	1.00				0	0	0
CD=	Misc.				0	0	0
1	1.00						
Total					65.2	434.8	500

Load Factors Applied				Reactions	
Load	DL(lbs)	LL(lbs)	x(ft)(left)	Left (lbs)	Right (lbs)
Point Load 1					
Point Load 2					
roof	0	0		Uniform RDL=	98
roof	0	0		Uniform RLL=	652
				Point Loads P1DL=	0
				Point Loads P1LL=	0
				Point Loads P2DL=	0
				Point Loads P2LL=	0
				Point Loads RTL=	750
				Point Loads Max Shear=	0.8

DIM TIMBER LVL GLB

Wood Species=	Douglas Fir #2	Douglas Fir #1	LVL	24F-V4
Option 1	(1) 2x6	4x4	(1) 1.75x5.5	3.125x9
Option 2	(2) 2x4	6x6	(2) 1.75x5.5	5.125x6
Option 3	(3) 2x4	8x8	(3) 1.75x5.5	6.75x9
Option 4	(4) 2x4	10x10	(4) 1.75x5.5	8.75x9
Option 5	-	12x12	-	10.75x12
Option 6	-	14x14	-	-
Option 7	-	16x16	-	-

Moment			
	Center	Point Load 1	Point Load 2
RDL=	73	0	0
RLL=	489	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	563	0	0
Max M=	0.6		k-ft

TSE Engineers
136 S State Street
Shelley, ID 83274
208-357-2420

JOB TITLE: Wooden Spur Renovation
368 Wooden Spur Dr. Alpine, Wyoming
JOB NO. 225112 SHEET NO. 22 of 39
CALCULATED BY EVB DATE 6/4/2025
CHECKED BY 0 DATE

Wood Header Design Or Wood Beam (Not Laterally Supported)
NDS 2018

Mark: HDR7

Mark: HDR7		Load Factors		Loading						
Span(ft)=	3	Dead	1.00	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)	
LL Deflection<L/	360	Floor Live	1.00	roof	15	100	7	105	700	805
Total Deflection<L/	240	Roof Live/Snow	1.00	floor				0	0	0
CD=	1	Misc.	1.00	wall				0	0	0
				misc.				0	0	0
Total							105.0	700.0	805	

Load Factors Applied				Reactions		
Load	DL(lbs)	LL(lbs)	x(ft)(left)	DL	LL	
Point Load 1				0	0	
Point Load 2				0	0	
Reactions				Left (lbs)		
Uniform				RDL=	158	158
				RLL=	1050	1050
Point Loads				P1DL=	0	0
				P1LL=	0	0
				P2DL=	0	0
				P2LL=	0	0
				RTL=	1208	1208
Max Shear=					1.2	k

DIM TIMBER LVL GLB

Wood Species=	Douglas Fir #2	Douglas Fir #1	LVL	24F-V4
Option 1	(1) 2x8	4x4	(1) 1.75x5.5	3.125x9
Option 2	(2) 2x6	6x6	(2) 1.75x5.5	5.125x6
Option 3	(3) 2x4	8x8	(3) 1.75x5.5	6.75x9
Option 4	(4) 2x4	10x10	(4) 1.75x5.5	8.75x9
Option 5	-	12x12	-	10.75x12
Option 6	-	14x14	-	-
Option 7	-	16x16	-	-

Moment			
	Center	Point Load 1	Point Load 2
RDL=	118	0	0
RLL=	788	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	906	0	0
Max M=	0.9	k-ft	

Mark: HDR8

Mark: HDR8		Load Factors		Loading						
Span(ft)=	3	Dead	1.00	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)	
LL Deflection<L/	360	Floor Live	1.00	roof	15	100	9	135	900	1035
Total Deflection<L/	240	Roof Live/Snow	1.00	floor				0	0	0
CD=	1	Misc.	1.00	wall				0	0	0
				misc.				0	0	0
Total							135.0	900.0	1035	

Load Factors Applied				Reactions		
Load	DL(lbs)	LL(lbs)	x(ft)(left)	DL	LL	
Point Load 1				0	0	
Point Load 2				0	0	
Reactions				Left (lbs)		
Uniform				RDL=	203	203
				RLL=	1350	1350
Point Loads				P1DL=	0	0
				P1LL=	0	0
				P2DL=	0	0
				P2LL=	0	0
				RTL=	1553	1553
Max Shear=					1.6	k

DIM TIMBER LVL GLB

Wood Species=	Douglas Fir #2	Douglas Fir #1	LVL	24F-V4
Option 1	(1) 2x10	4x6	(1) 1.75x5.5	3.125x9
Option 2	(2) 2x6	6x6	(2) 1.75x5.5	5.125x6
Option 3	(3) 2x6	8x8	(3) 1.75x5.5	6.75x9
Option 4	(4) 2x4	10x10	(4) 1.75x5.5	8.75x9
Option 5	-	12x12	-	10.75x12
Option 6	-	14x14	-	-
Option 7	-	16x16	-	-

Moment			
	Center	Point Load 1	Point Load 2
RDL=	152	0	0
RLL=	1013	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	1164	0	0
Max M=	1.2	k-ft	

JOB TITLE	Wooden Spur Renovation		
368 Wooden Spur Dr. Alpine, Wyoming			
JOB NO.	225112	SHEET NO.	23 of 39
CALCULATED BY	EVb	DATE	6/4/2025
CHECKED BY		DATE	

Moment			
	Center	Point Load	Point Load 2
RDL=	1553	0	0
RLL=	10350	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	11903	0	0
Max M=	11.9		k-ft

TSE Engineers
136 S State Street
Shelley, ID 83274
208-337-2420

JOB TITLE Wooden Spur Renovation
368 Wooden Spur Dr. Alpine, Wyoming
JOB NO. 225112
CALCULATED BY EVB
CHECKED BY 0

SHEET NO. 24 of 39
DATE 6/4/2025
DATE

Wood Joist/Rafters (simple span)
NDS 2018

Mark: RFT1

Span(ft)=	8.5
Spacing (in)=	16
LL Deflection<L/	360
Total Deflection<L/	240

C _p =	1
C _r =	1.15

	Loading					
	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)
roof	15	100	1.33	20.0	133.3	153.3
floor			1.33	0.0	0.0	0.0
misc.			1.33	0.0	0.0	0.0
Total				20.0	133.3	153.3

Reactions			Moment	
Left (lbs)		Right (lbs)		
RDL=	85	85	RDL=	181
RLL=	567	567	RLL=	1204
RTL=	652	652	MTL=	1385
Max Shear (k)=	0.7		Max M (k-ft)=	1.4

DIM TJI BCI

Wood Species= Douglas Fir #1

Single Ply	(1) 2x8	9 1/2" 110	9 1/2" 5000
Double Ply	(2) 2x6	9 1/2" 210	9 1/2" 6000
4x	4x6	9 1/2" 230	9 1/2" 6500
6x	6x6	11 7/8" 360	11 7/8" 60
8x	8x8	11 7/8" 560	11 7/8" 90
10x	10x10		
12x	12x12		
14x	14x14		
16x	16x16		

Mark: RFT 2

Span(ft)=	10
Spacing (in)=	16
LL Deflection<L/	360
Total Deflection<L/	240

C _p =	1
C _r =	1.15

	Loading					
	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)
roof	15	100	1.33	20.0	133.3	153.3
floor			1.33	0.0	0.0	0.0
misc.		60	1.33	0.0	80.0	80.0
Total				20.0	213.3	233.3

Reactions			Moment	
Left (lbs)		Right (lbs)		
RDL=	100	100	RDL=	250
RLL=	1067	1067	RLL=	2667
RTL=	1167	1167	MTL=	2917
Max Shear (k)=	1.2		Max M (k-ft)=	2.9

DIM TJI BCI

Wood Species= Douglas Fir #1

Single Ply	(1) 2x12	11 7/8" 110	11 7/8" 5000
Double Ply	(2) 2x8	9 1/2" 210	9 1/2" 6000
4x	4x8	9 1/2" 230	9 1/2" 6500
6x	6x8	11 7/8" 360	11 7/8" 60
8x	8x8	11 7/8" 560	11 7/8" 90
10x	10x10		
12x	12x12		
14x	14x14		
16x	16x16		

Mark: FLR 1

Span(ft)=	10
Spacing (in)=	16
LL Deflection<L/	480
Total Deflection<L/	240

C _p =	1
C _r =	1.15

	Loading					
	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)
roof			1.33	0.0	0.0	0.0
floor	10	40	1.33	13.3	53.3	66.7
misc.			1.33	0.0	0.0	0.0
Total				13.3	53.3	66.7

Reactions			Moment	
Left (lbs)		Right (lbs)		
RDL=	67	67	RDL=	167
RLL=	267	267	RLL=	667
RTL=	333	333	MTL=	833
Max Shear (k)=	0.3		Max M (k-ft)=	0.8

DIM TJI BCI

Wood Species= Douglas Fir #2

Single Ply	(1) 2x8	9 1/2" 110	9 1/2" 5000
Double Ply	(2) 2x6	9 1/2" 210	9 1/2" 6000
4x	4x6	9 1/2" 230	9 1/2" 6500
6x	6x6	11 7/8" 360	11 7/8" 60
8x	8x8	11 7/8" 560	11 7/8" 90
10x	10x10		
12x	12x12		
14x	14x14		
16x	16x16		

TSE Engineers
136 S State Street
Shelley, ID 83274
208-716-2426

JOB TITLE Wooden Spur Renovation
368 Wooden Spur Dr. Alpine, Wyoming
JOB NO. 225112 SHEET NO. 25 of 39
CALCULATED BY EVB DATE 6/4/2025
CHECKED BY DATE

Wood Beam Design (Lateral Supported Fully)
NDS 2018

Mark: BM21

Mark: BM21			Load Factors			Loading				
Span(ft)=	18	Dead	1.00	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)	
LL Deflection<L/	360	Floor Live	0.00	roof	15	100	7	105	700	805
Total Deflection<L/	240	Roof Live/Snow	1.00	floor	10	40	5	50	0	50
CD=	1	Misc.	1.00	wall				0	0	0
				misc.		60	5	0	300	300
				Total			155	1000	1155	

Load Factors Applied					Reactions		
Load	DL(lbs)	LL(lbs)	x(ft)(left)	DL	LL	Left (lbs)	Right (lbs)
Point Load 1	roof			0	0	Uniform	RDL= 1395 1395
Point Load 2	floor			0	0		RLL= 9000 9000
						Point Loads	P1DL= 0 0
							P1LL= 0 0
							P2DL= 0 0
							P2LL= 0 0
							RTL= 10395 10395
							Max Shear= 10.4 k

	DIM	TIMBER	LVL	GLB
Wood Species=	Douglas Fir #2	Douglas Fir #2	LVL	24F-V4
Option 1	No Single Ply	4x None	No Single Ply	3.125 x None
Option 2	No Double Ply	6x None	No Double Ply	5.125x18
Option 3	No Triple Ply	8x None	(3) 1.75x18	6.75x16.5
Option 4	No Four Ply	10x None	(4) 1.75x16	8.75x15
Option 5	-	12x None	-	10.75x13.5
Option 6	-	14x18	-	-
Option 7	-	16x18	-	-

Moment			
	Center	Point Load	Point Load 2
RDL=	6278	0	0
RLL=	40500	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	46778	0	0
Max M=	46.8	k-ft	

Mark: BM 21

Mark: BM 21		Load Factors		Loading						
Span(ft)= 18		Dead	1.00	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)	
LL Deflection<L/	360	Floor Live	0.75	roof	15	100	7	105	525	630
Total Deflection<L/	240	Roof Live/Snow	0.75	floor	10	40	5	50	150	200
CD= 1		Misc.	0.75	wall				0	0	0
				misc.		60	5	0	225	225
				Total			155	900	1055	

Load Factors Applied					Reactions		
Load	DL(lbs)	LL(lbs)	x(ft)(left)	DL	LL	Left (lbs)	Right (lbs)
Point Load 1	roof			0	0	Uniform	RDL= 1395 1395
Point Load 2	floor			0	0		RLL= 8100 8100
						Point Loads	P1DL= 0 0
							P1LL= 0 0
							P2DL= 0 0
							P2LL= 0 0
							RTL= 9495 9495
							Max Shear= 9.5 k

	DIM	TIMBER	LVL	GLB
Wood Species=	Douglas Fir #2	Douglas Fir #2	LVL	24F-V4
Option 1	No Single Ply	4x None	No Single Ply	3.125x21
Option 2	No Double Ply	6x None	No Double Ply	5.125x18
Option 3	No Triple Ply	8x None	(3) 1.75x18	6.75x16.5
Option 4	No Four Ply	10x None	(4) 1.75x16	8.75x15
Option 5	-	12x None	-	10.75x13.5
Option 6	-	14x18	-	-
Option 7	-	16x18	-	-

Moment			
	Center	Point Load	Point Load 2
RDL=	6278	0	0
RLL=	36450	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	42728	0	0
Max M=	42.7	k-ft	

TSE Engineers
136 S State Street
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JOB TITLE Wooden Spur Renovation
368 Wooden Spur Dr. Alpine, Wyoming
JOB NO. 225112 SHEET NO. 26 of 39
CALCULATED BY EVB DATE 6/4/2025
CHECKED BY DATE

Wood Beam Design (Lateral Supported Fully)
NDS 2018

Mark: BM22

Mark: BM22			Load Factors		Loading						
Span(ft)= 10		Dead	1.00		DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)	
LL Deflection<L/ 360		Floor Live	0.00		roof	15	100	4	60	400	460
Total Deflection<L/ 240		Roof Live/Snow	1.00		floor	10	40	1	10	0	10
CD= 1		Misc.	1.00		wall				0	0	0
					misc.		60	4	0	240	240
					Total				70	640	710

Load Factors Applied					Reactions		
Load	DL(lbs)	LL(lbs)	x(ft)(left)	DL	LL	Left (lbs)	Right (lbs)
Point Load 1 roof				0	0	Uniform	RDL= 350
Point Load 2 floor				0	0		RLL= 3200

	DIM	TIMBER	LVL	GLB
Wood Species=	Douglas Fir #2	Douglas Fir #2	LVL	24F-V4
Option 1	No Single Ply	4x None	(1) 1.75x11.875	3.125x10.5
Option 2	No Double Ply	6x14	(2) 1.75x9.5	5.125x9
Option 3	No Triple Ply	8x12	(3) 1.75x9.5	6.75x9
Option 4	(4) 2x12	10x10	(4) 1.75x9.5	8.75x9
Option 5	-	12x12	-	10.75x12
Option 6	-	14x14	-	-
Option 7	-	16x16	-	-

Point Loads	P1DL=	0	0
	P1LL=	0	0
	P2DL=	0	0
	P2LL=	0	0
	RTL=	3550	3550
	Max Shear=	3.6	k

Moment			
	Center	Point Load	Point Load 2
RDL=	875	0	0
RLL=	8000	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	8875	0	0
	Max M=	8.9	k-ft

Mark: BM 22

Mark: BM 22			Load Factors		Loading				
Span(ft)= 10	Dead	1.00		DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)
LL Deflection<L/ 360	Floor Live	0.75	roof	15	100	4	60	300	360
Total Deflection<L/ 240	Roof Live/Snow	0.75	floor	10	40	1	10	30	40
CD= 1	Misc.	0.75	wall				0	0	0
			misc.		60	4	0	180	180
			Total				70	510	580

Load Factors Applied					Reactions		
Load	DL(lbs)	LL(lbs)	x(ft)(left)	DL	LL	Left (lbs)	Right (lbs)
Point Load 1 roof				0	0	Uniform	RDL= 350
Point Load 2 floor				0	0		RLL= 2550

	DIM	TIMBER	LVL	GLB
Wood Species=	Douglas Fir #2	Douglas Fir #2	LVL	24F-V4
Option 1	No Single Ply	4x None	(1) 1.75x11.875	3.125x10.5
Option 2	No Double Ply	6x12	(2) 1.75x9.5	5.125x9
Option 3	No Triple Ply	8x10	(3) 1.75x9.5	6.75x9
Option 4	(4) 2x12	10x10	(4) 1.75x7.25	8.75x9
Option 5	-	12x12	-	10.75x12
Option 6	-	14x14	-	-
Option 7	-	16x16	-	-

Point Loads	P1DL=	0	0
	P1LL=	0	0
	P2DL=	0	0
	P2LL=	0	0
	RTL=	2900	2900
	Max Shear=	2.9	k

Moment			
	Center	Point Load	Point Load 2
RDL=	875	0	0
RLL=	6375	0	0
P1DL=	0	0	0
P1LL=	0	0	0
P2DL=	0	0	0
P2LL=	0	0	0
MTL=	7250	0	0
	Max M=	7.3	k-ft

Project Wooden Spur Renovation

Project # 225112

Title Roof Frame

By EUB Ck'd

Code IBC 2021 Jurisdiction City of Alpine wy

Sheet 27 of 39

$$SL = 100 \quad DL = 15$$

$$\text{Priftty / sliding} = 100 \text{ psf}$$

Rafters

$$L = 5' \text{ can't}$$

$$W = (100 + 100 + 15) (16/12) = 287$$

$$M = 3.6$$

$$V = 1.4$$

$$W = (100 + 100 + 15) (1) =$$

$$M =$$

$$V =$$

$$1\frac{3}{4} \times 7\frac{1}{4} \text{ LVL}$$

$$7.11$$

$$4.8$$

$$110$$

$$\Delta = 0.19''$$

$$\frac{L}{323}$$

$$\underline{\underline{OK}}$$

$$1\frac{3}{4} \times 7\frac{1}{4} \text{ LVL @ } 16'' \text{ o.c.}$$

max span

$$L = ?$$

$$W = (100 + 100 + 15) (16/12) = 287$$

$$VA = 4800$$

$$MA = 7110$$

$$\Delta = \frac{1}{360}$$

$$V = 4800 = \frac{(287)(L)}{2}$$

$$L = 33'$$

$$M = 7110 = \frac{287 (L)^2}{8}$$

$$L = 14'$$

$$\Delta = \frac{L (12)}{360} = \frac{5 (287/12) ((L)(12))^4}{384 (1100000) (110)}$$

$$L = 10'$$

$$\text{max span} = 10'-0''$$

$$1\frac{3}{4} \times 7\frac{1}{4} \text{ LVL @ } 16'' \text{ o.c.}$$

(99) Beam

$$L = 6'$$

$$W = (100 + 100 + 15) (8/12 + 5) = 1935$$

$$M = 8.7$$

$$V = 5.8$$

$$5\frac{1}{8} \times 9$$

$$13.8$$

$$8.1$$

$$310$$

$$\Delta = 0.10''$$

$$\frac{L}{712}$$

$$5\frac{1}{8} \times 9 \text{ LVL}$$

(100) Floor Beam

$$L = 5'-0" \text{ can't}$$

$$W = (60 + 10) \left(\frac{14}{12} \right) = 500$$

$$M = 6.3$$

$$V = 2.5$$

$$5'8 \times 10 \frac{1}{2}$$

$$18.8$$

$$9.5$$

$$490$$

$$D = 0.0001$$

$$5'8 \times 10 \frac{1}{2} \text{ can't}$$

(101) Beam

$$L = 14'$$

$$W = ?$$

(3) $1 \frac{3}{4} \times 7 \frac{1}{4}$ LVL

$$I = 170$$

$$VA = 7230$$

$$7230 = \frac{W (14)}{2} = 1032$$

$$MA = 10700$$

$$10700 = \frac{W (14)^2}{8} = 436$$

$$D = 0.25"$$

$$0.25 = \frac{5W ((14)(12))^4}{384 (1900000) (170)} = 7.785(12) = 93 \text{ plf}$$

(3) $1 \frac{3}{4} \times 9 \frac{1}{2}$ LVL

$$I = 380$$

$$VA = 9480$$

$$VU = 1354$$

$$MA = 17700$$

$$W = 722$$

$$D = 0.25"$$

$$W = 208$$

Use (3) $1 \frac{3}{4} \times 9 \frac{1}{2}$ LVL

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Wood Joist/Rafters (simple span)
NDS 2018

Mark: FLR 2

Span(ft)=	14
Spacing (in)=	12
LL Deflection<L/	360
Total Deflection<L/	240

C _D =	1
C _r =	1.15

Loading

	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)
roof	10	60	1.00	10.0	60.0	70.0
floor			1.00	0.0	0.0	0.0
misc.			1.00	0.0	0.0	0.0
Total				10.0	60.0	70.0

Reactions

Moment

	Left (lbs)	Right (lbs)		
RDL=	70	70	RDL=	245
RLL=	420	420	RLL=	1470
RTL=	490	490	MTL=	1715
Max Shear (k)=	0.5		Max M (k-ft)=	1.7

DIM

TJI

BCI

Wood Species= Douglas Fir S.S.

Single Ply	(1) 2x10	9 1/2" 110	9 1/2" 5000
Double Ply	(2) 2x8	9 1/2" 210	9 1/2" 6000
4x	4x8	9 1/2" 230	9 1/2" 6500
6x	6x6	11 7/8" 360	11 7/8" 60
8x	8x8	11 7/8" 560	11 7/8" 90
10x	10x10		
12x	12x12		
14x	14x14		
16x	16x16		

Mark:

Span(ft)=	
Spacing (in)=	16
LL Deflection<L/	360
Total Deflection<L/	240

C _D =	1
C _r =	1.15

Loading

	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)
roof	15	100	1.33	20.0	133.3	153.3
floor			1.33	0.0	0.0	0.0
misc.		60	1.33	0.0	80.0	80.0
Total				20.0	213.3	233.3

Reactions

Moment

	Left (lbs)	Right (lbs)		
RDL=	0	0	RDL=	0
RLL=	0	0	RLL=	0
RTL=	0	0	MTL=	0
Max Shear (k)=	0.0		Max M (k-ft)=	0.0

DIM

TJI

BCI

Wood Species= Douglas Fir #1

Single Ply	(1) 2x4	9 1/2" 110	9 1/2" 5000
Double Ply	(2) 2x4	9 1/2" 210	9 1/2" 6000
4x	4x4	9 1/2" 230	9 1/2" 6500
6x	6x6	11 7/8" 360	11 7/8" 60
8x	8x8	11 7/8" 560	11 7/8" 90
10x	10x10		
12x	12x12		
14x	14x14		
16x	16x16		

Mark:

Span(ft)=	
Spacing (in)=	16
LL Deflection<L/	480
Total Deflection<L/	240

C _D =	1
C _r =	1.15

Loading

	DL (psf)	LL(psf)	trib (ft)	DLw(plf)	LLw(plf)	TLw(plf)
roof			1.33	0.0	0.0	0.0
floor	10	40	1.33	13.3	53.3	66.7
misc.			1.33	0.0	0.0	0.0
Total				13.3	53.3	66.7

Reactions

Moment

	Left (lbs)	Right (lbs)		
RDL=	0	0	RDL=	0
RLL=	0	0	RLL=	0
RTL=	0	0	MTL=	0
Max Shear (k)=	0.0		Max M (k-ft)=	0.0

DIM

TJI

BCI

Wood Species= Douglas Fir #2

Single Ply	(1) 2x4	9 1/2" 110	9 1/2" 5000
Double Ply	(2) 2x4	9 1/2" 210	9 1/2" 6000
4x	4x4	9 1/2" 230	9 1/2" 6500
6x	6x6	11 7/8" 360	11 7/8" 60
8x	8x8	11 7/8" 560	11 7/8" 90
10x	10x10		
12x	12x12		
14x	14x14		
16x	16x16		

Project Wooden Spur Renovation

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Title Foundation

By EUB Ck'd

Code IBC2021 Jurisdiction City of Alpine Wyo.

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$$q_A = 1500$$

Footings Exterior

$$W = 1610$$

Try 10x24

$$P = 5.9 \text{ k}$$

$$q = \frac{1610(1)}{(24/12)(1)} + \frac{5900}{(24/12)(6)} = 1296 < 1500 \quad \underline{\underline{OK}}$$

$$A_s = 0.0018(10)(24) = 0.43 \text{ in}^2$$

$$(3) \#4 = 0.6 \text{ in}^2$$

∴ 10x24 w/(3) #4 long.

$$W = 1840$$

Try 10x20

$$P = 16.6$$

$$q = \frac{1840(1)}{(20/12)(1)} + \frac{16600}{(20/12)(6)} = 2300 > 1500 \text{ Fails USC}$$

Spot Footings for Point Load

$$q = \frac{1840(1)}{(20/12)(1)} = 1104 < 1500 \quad \underline{\underline{OK}}$$

$$A_s = 0.0018(10)(20) = 0.36 \text{ in}^2$$

$$(3) \#4 = 0.6 \text{ in}^2$$

∴ 10x20 w/(3) #4 long.

Spot Footings $q_A = 1500$

Size	PA
2'-0"	6.0
2'-6"	9.4
3'-0"	13.5
3'-6"	18.4
4'-0"	24.0

Project Wooden Spar Renovation

Project # 225112

Title Lateral Loads

By EV3 Ck'd

Code TBC2021 Jurisdiction City of Alpine Wy.

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Seismic

RCUT

$I = 1.0$

$SS = 110.9$

$S_1 = 34.1$

$SC = 0$

$Sds = 0.887$

$Sd_1 = 0.445$

$SDC = 0$

$R = 6.5$

$CS = 0.135$

$V = 0.136$ w (ultimate)

Garage $W = (29)(29)(15) + (29)(29)(100)(0.2) = 29435$

$V = 0.136 (29435) / 1.4 / 2 = 1.4$

Coverd Patio $W = (15)(29)(15) + (15)(29)(100)(0.2) = 15225$

$V = 0.136 (15225) / 1.4 / 2 = 0.8$

Son Room $W = (21)(12)(15) + (21)(12)(100)(0.2) = 8820$

$V = 0.136 (8820) / 1.4 / 2 = 0.4$

Existy House

$W = (40)(30)(15) + (40)(30)(100)(0.2) = 42000$

$V = 0.136 (42000) / 1.4 / 2 = 2.0$

Existy Garage

$W = (30)(22)(20) + (30)(22)(100)(0.2) = 26400$

$V = 0.136 (26400) / 1.4 / 2 = 1.3$

Project Warden Spar Renovation

Title Lateral Loads

Code IBC 2021 Jurisdiction City of Alpine Wyo.

Date JUN 04 2025

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By EUB Ck'd

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Wind 115 mph Exp=C RC=II Z_a=6'

P_w=15.5; 10.3 P_G=13.9; 9.2 P_E=-0.6; -3.8

$$(W1) V = (13.9(6) + 10(26/2 - 6)) (11/2 + 2 + 5.5/2) = 1.6$$

$$(W2) V = (15.5(6) + 10.3(26/2 - 6)) (11/2 + 2) + 10(26/2)(5.5) = 2.0$$

$$(W3) V = (15.5(6) + 10.3(26/2 - 6)) (11/2 + 4) + 10(26/2)(5.5) = 2.3$$

$$(W4) V = (10)(2)(15) = 0.3$$

$$(W5) V = (15.5(6) + 10.3(18/2 - 6)) (8/2) + 10(18/2)(2) = 0.7$$

$$(W6) V = (13.9(6) + 10.3(10/2 - 6)) (8/2 + 2 + 3/2) = 0.4$$

$$(W7) V = (15.5(6) + 10.3(49/2 - 6)) (8/2) + 10(49/2)(8.5) = 2.6$$

$$(W8) V = (15.5(6) + 10.3(22/2 - 6)) (9/2 + 3) + 10(22/2)(8.5) = 2.0$$

$$(W9) V = (13.9(6) + 10.3(30/2 - 6)) (10/2 + 3 + 8.5/2) = 2.2$$

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Wood Shear Walls w/ Wood Studs (Top Story)
NDS 2021 (ASD Loading)
Total Length of walls (ft) = 8.00

Shear Line:	SW1
Seismic Load (lb):	1400
S _{ps}	0.887
Wind Load (lb):	1600

Roof DL (psf)	15
Floor DL (psf)	10
Wall Self (psf)	8

	Segment 1	Segment 2	Segment 3	Segment 4	Segment 5	Segment 6	Segment 7
length (ft)	4	4					
height (ft)	11	11					
roof trib. (ft)	16	16					
floor trib. (ft)	0	0					
Distance from HD to end of wall (in)	3	3					
Aspect Ratio:	2.75	2.75					
Aspect Ratio Factor (WSP):	0.91	0.91					
Seismic							
shear flow (plf)	175.0	175.0					
F (lbs)	700	700					
Seismic Factor	0.73	0.73					
Adjusted Shear Flow (plf)	240.63	240.63					
MOT (ft-lb)	7700	7700					
DL Factor A=	1.12	1.12					
A x wDL (plf)	369	369					
End Post Compression (lb)	2175	2175					
DL Factor B=	0.48	0.48					
B x wDL (plf)	156	156					
End Post Uplift for HDs (lb)	1035	1035					
Wind							
shear flow (plf)	200	200					
F (lb)	800	800					
MOT (ft-lb)	8800	8800					
wDL (plf)	328	328					
End Post Compression (lb)	3003	3003					
DL Factor	0.6	0.6					
wDL (plf)	196.8	197					
End Post Uplift for HDs (lb)	2121	2121					
Max Compression	3003	3003					
Max Uplift	2121	2121					
Max Shear Flow	241	241					
Max Shear Flow Due to Wind or Seismic (W/S)	S	S					
Sheathing Nails	7/16 w/ 8d @ 4" O.C.	7/16 w/ 8d @ 4" O.C.					
# of Layers	1	1					
Shear Flow Allowable (plf)	317	317					
Check	Adequate	Adequate					
Sheathing Staples	7/16 w/ 1 1/2" 16 ga. @ 3" O.C.	7/16 w/ 1 1/2" 16 ga. @ 3" O.C.					
Shar Flow Allowable (plf)	310	310					
Check	Adequate	Adequate					
Recommended Holdown @ Foundation 8" wall	HDU2	HDU2					
Strap Style (Midwall)	LSTHD8	LSTHD8					
Strap Style (End Wall)	LSTHD8	LSTHD8					
Recommended Holdown @ Wood Wall	MSTC40	MSTC40					
Strap Nailing Req'd	(32) 16d	(32) 16d					
# OF Minimum End Post	2	2					

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Wood Shear Walls w/ Wood Studs (Top Story)
NDS 2021 (ASD Loading)
Total Length of walls (ft) = 9.00

Shear Line:	SW2
Seismic Load (lb):	2900
Sos	0.887
Wind Load (lb):	1900

Roof DL (psf)	15
Floor DL (psf)	10
Wall Self (psf)	8

	Segment 1	Segment 2	Segment 3	Segment 4	Segment 5	Segment 6	Segment 7
length (ft)	9						
height (ft)	11						
roof trib. (ft)	13						
floor trib. (ft)	0						
Distance from HD to end of wall (in)	3						
Aspect Ratio:	1.22						

Seismic	shear flow (plf)	322.2
	F (lbs)	2900
	Seismic Factor	1.00
	Adjusted Shear Flow (plf)	322.22
	MOT (ft-lb)	31900
	DL Factor A=	1.12
	A x wDL (plf)	318
	End Post Compression (lb)	3984
	DL Factor B=	0.48
	B x wDL (plf)	135
	End Post Uplift for HDs (lb)	1875

Wind	shear flow (plf)	211
	F (lb)	1900
	MOT (ft-lb)	20900
	wDL (plf)	283
	End Post Compression (lb)	3662
	DL Factor	0.6
	wDL (plf)	169.8
	End Post Uplift for HDs (lb)	1695
	Max Compression	3984
	Max Uplift	1875
	Max Shear Flow	322
	Max Shear Flow Due to Wind or Seismic (W/S)	5

	Sheathing Nails	7/16 w/ 8d @ 3" O.C.
	# of Layers	1
	Shear Flow Allowable (plf)	450
	Check	Adequate
	Sheathing Staples	7/16 w/ 1 1/2" 16 ga. @ 2" O.C.
	Shar Flow Allowable (plf)	395
	Check	Adequate
	Recommended Holdown @ Foundation 8" wall	HDU2
	Strap Style (Midwall)	LSTD8
	Strap Style (End Wall)	LSTD8
	Recommended Holdown @ Wood Wall	MSTA49
	Strap Nailing Req'd	(26) 10d
	# OF Minimum End Post	2

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Wood Shear Walls w/ Wood Studs (Top Story)
NDS 2021 (ASD Loading)
Total Length of walls (ft) = 20.00

Shear Line:	SW3
Seismic Load (lb):	2200
S _{DS}	0.887
Wind Load (lb):	2000

Roof DL (psf)	15
Floor DL (psf)	10
Wall Self (psf)	8

	Segment 1	Segment 2	Segment 3	Segment 4	Segment 5	Segment 6	Segment 7
length (ft)	20						
height (ft)	11						
roof trib. (ft)	4						
floor trib. (ft)	0						
Distance from HD to end of wall (in)	3						
Aspect Ratio:	0.55						

Seismic	shear flow (plf)	110.0
	F (lbs)	2200
	Seismic Factor	1.00
	Adjusted Shear Flow (plf)	110.00
	MOT (ft-lb)	24200
	DL Factor A=	1.12
	A x wDL (plf)	166
	End Post Compression (lb)	2522
	DL Factor B=	0.48
	B x wDL (plf)	70
	End Post Uplift for HDs (lb)	143

Wind	shear flow (plf)	100
	F (lb)	2000
	MOT (ft-lb)	22000
	wDL (plf)	148
	End Post Compression (lb)	2594
	DL Factor	0.6
	wDL (plf)	88.8
	End Post Uplift for HDs (lb)	240
	Max Compression	2594
	Max Uplift	240
	Max Shear Flow	110
	Max Shear Flow Due to Wind or Seismic (W/S)	5

	Sheathing Nails	7/16 w/ 8d @ 6" O.C.
	# of layers	1
	Shear Flow Allowable (plf)	240
	Check	Adequate
	Sheathing Staples	7/16 w/ 1 1/2" 16 ga. @ 6" O.C.
	Shar Flow Allowable (plf)	155
	Check	Adequate
	Recommended Holdown @ Foundation 8" wall	not reqd.
	Strap Style (Midwall)	not reqd.
	Strap Style (End Wall)	not reqd.
	Recommended Holdown @ Wood Wall	not reqd.
	Strap Nailing Req'd	not reqd.
	# OF Minimum End Post	not reqd

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Wood Shear Walls w/ Wood Studs (Top Story)
NDS 2021 (ASD Loading)
Total Length of walls (ft) = 15.00

Shear Line:	SW4
Seismic Load (lb):	2200
S _{DS}	0.887
Wind Load (lb):	2000

Roof DL (psf)	15
Floor DL (psf)	10
Wall Self (psf)	8

	Segment 1	Segment 2	Segment 3	Segment 4	Segment 5	Segment 6	Segment 7
length (ft)	9	6					
height (ft)	11	11					
roof trib. (ft)	4	4					
floor trib. (ft)	0	0					
Distance from HD to end of wall (in)	3	3					
Aspect Ratio:	1.22	1.83					

Seismic	shear flow (plf)	146.7	146.7
	F (lbs)	1320	880
	Seismic Factor	1.00	1.00
	Adjusted Shear Flow (plf)	146.67	146.67
	MOT (ft-lb)	14520	9680
	DL Factor A=	1.12	1.12
	A x wDL (plf)	166	166
	End Post Compression (lb)	1910	1678
	DL Factor B=	0.48	0.48
	B x wDL (plf)	70	70
	End Post Uplift for HDs (lb)	812	918

Wind	shear flow (plf)	133	133
	F (lb)	1200	800
	MOT (ft-lb)	13200	8800
	wDL (plf)	148	148
	End Post Compression (lb)	2175	1974
	DL Factor	0.6	0.6
	wDL (plf)	88.8	89
	End Post Uplift for HDs (lb)	1153	1334

	Max Compression	2175	1974
	Max Uplift	1153	1334
	Max Shear Flow	147	147
	Max Shear Flow Due to Wind or Seismic (W/S)	5	5

Sheathing Nails	7/16 w/ 8d @ 6" O.C.	7/16 w/ 8d @ 6" O.C.					
# of Layers	1	1					
Shear Flow Allowable (plf)	240	240					
Check	Adequate	Adequate					

Sheathing Staples	7/16 w/ 1 1/2" 16 ga. @ 6" O.C.	7/16 w/ 1 1/2" 16 ga. @ 6" O.C.					
Shar Flow Allowable (plf)	155	155					
Check	Adequate	Adequate					

Recommended Holdown @ Foundation 8" wall	HDU2	HDU2					
Strap Style (Midwall)	LSTHD8	LSTHD8					
Strap Style (End Wall)	LSTHD8	LSTHD8					
Recommended Holdown @ Wood Wall	MSTC28	MSTC28					
Strap Nailing Req'd	(16) 16d	(16) 16d					
# OF Minimum End Post	2	2					

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Wood Shear Walls w/ Wood Studs (Top Story)
NDS 2021 (ASD Loading)
Total Length of walls (ft) = 5.00

Shear Line:	SW5
Seismic Load (lb):	400
S _{DS}	0.887
Wind Load (lb):	400

Roof DL (psf)	15
Floor DL (psf)	10
Wall Self (psf)	8

	Segment 1	Segment 2	Segment 3	Segment 4	Segment 5	Segment 6	Segment 7
length (ft)	2.5	2.5					
height (ft)	7	7					
roof trib. (ft)	7	7					
floor trib. (ft)	0	0					
Distance from HD to end of wall (in)	3	3					
Aspect Ratio:	2.80	2.80					
Aspect Ratio Factor (WSP):	0.90	0.90					
Seismic							
shear flow (plf)	80.0	80.0					
F (lbs)	200	200					
Seismic Factor	0.71	0.71					
Adjusted Shear Flow (plf)	112.00	112.00					
MOT (ft-lb)	1400	1400					
DL Factor A=	1.12	1.12					
A x wDL (plf)	181	181					
End Post Compression (lb)	662	662					
DL Factor B=	0.48	0.48					
B x wDL (plf)	77	77					
End Post Uplift for HDs (lb)	296	296					
Wind							
shear flow (plf)	80	80					
F (lb)	200	200					
MOT (ft-lb)	1400	1400					
wDL (plf)	161	161					
End Post Compression (lb)	823	823					
DL Factor	0.6	0.6					
wDL (plf)	96.6	97					
End Post Uplift for HDs (lb)	579	579					
Max Compression	823	823					
Max Uplift	579	579					
Max Shear Flow	112	112					
Max Shear Flow Due to Wind or Seismic (W/S)	5	5					
Sheathing Nails	7/16 w/ 8d @ 6" O.C.	7/16 w/ 8d @ 6" O.C.					
# of Layers	1	1					
Shear Flow Allowable (plf)	216	216					
Check	Adequate	Adequate					
Sheathing Staples	7/16 w/ 1 1/2" 16 ga. @ 6" O.C.	7/16 w/ 1 1/2" 16 ga. @ 6" O.C.					
Shar Flow Allowable (plf)	155	155					
Check	Adequate	Adequate					
Recommended Holdown @ Foundation 8" wall	not reqd.	not reqd.					
Strap Style (Midwall)	not reqd.	not reqd.					
Strap Style (End Wall)	not reqd.	not reqd.					
Recommended Holdown @ Wood Wall	not reqd.	not reqd.					
Strap Nailing Req'd	not reqd.	not reqd.					
# OF Minimum End Post	not reqd	not reqd					

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6/4/2025

Wood Shear Walls w/ Wood Studs (Top Story)

NDS 2021 (ASD Loading)

Total Length of walls (ft) = 8.00

Shear Line:	SWG
Seismic Load (lb):	1300
S_{ps}	0.887
Wind Load (lb):	2000

Roof DL (psf)	15
Floor DL (psf)	10
Wall Self (psf)	8

	Segment 1	Segment 2	Segment 3	Segment 4	Segment 5	Segment 6	Segment 7
length (ft)	8						
height (ft)	9						
roof trib. (ft)	4						
floor trib. (ft)	1						
Distance from HD to end of wall (in)	3						
Aspect Ratio:	1.13						

Seismic	shear flow (plf)	162.5
	F (lbs)	1300
	Seismic Factor	1.00
	Adjusted Shear Flow (plf)	162.50
	MOT (ft-lb)	11700
	DL Factor A=	1.12
	A x wDL (plf)	160
	End Post Compression (lb)	1695
	DL Factor B=	0.48
	B x wDL (plf)	68
	End Post Uplift for HDs (lb)	753

Wind	shear flow (plf)	250
	F (lb)	2000
	MOT (ft-lb)	18000
	wDL (plf)	142
	End Post Compression (lb)	2891
	DL Factor	0.6
	wDL (plf)	85.2
	End Post Uplift for HDs (lb)	2059
	Max Compression	2891
	Max Uplift	2059
	Max Shear Flow	250
	Max Shear Flow Due to Wind or Seismic (W/S)	W

Sheathing Nails	2/16 w/ 8d @ 6" O.C.						
# of Layers	1						
Shear Flow Allowable (plf)	335						
Check	Adequate						
Sheathing Staples	2/16 w/ 1 1/2" 16 ga. @ 4" O.C.						
Shar Flow Allowable (plf)	322						
Check	Adequate						
Recommended Holdown @ Foundation 8" wall	HDU2						
Strap Style (Midwall)	LSTHD8						
Strap Style (End Wall)	LSTHD8						
Recommended Holdown @ Wood Wall	MSTC40						
Strap Nailing Req'd	(32) 16d						
# OF Minimum End Post	2						

TSE Engineers
136 S State Street
Shelley, ID 83274
208-357-2420

JOB TITLE Wooden Spur Renovation
368 Wooden Spur Dr. Alpine, Wyoming
JOB NO. 225112
CALCULATED BY EVB
CHECKED BY 0

SHEET NO. 37 of 39
DATE 6/4/2025

Wood Shear Walls w/ Wood Studs (Top Story)
NDS 2021 (ASD Loading)
Total Length of walls (ft) = 16.50

Shear Line:	SW7
Seismic Load (lb):	3300
S _{DS}	0.887
Wind Load (lb):	4600
Roof DL (psf)	15
Floor DL (psf)	10
Wall Self (psf)	8

	Segment 1	Segment 2	Segment 3	Segment 4	Segment 5	Segment 6	Segment 7
length (ft)	8	8.5					
height (ft)	8	8					
roof trib. (ft)	4	4					
floor trib. (ft)	2	2					
Distance from HD to end of wall (in)	3	3					
Aspect Ratio:	1.00	0.94					

Seismic	shear flow (plf)	200.0	200.0
	F (lbs)	1600	1700
	Seismic Factor	1.00	1.00
	Adjusted Shear Flow (plf)	200.00	200.00
	MOT (ft-lb)	12800	13600
	DL Factor A=	1.12	1.12
	A x wDL (plf)	162	162
	End Post Compression (lb)	1804	1842
	DL Factor B=	0.48	0.48
	B x wDL (plf)	69	69
	End Post Uplift for HDs (lb)	846	829

Wind	shear flow (plf)	279	279
	F (lb)	2230	2370
	MOT (ft-lb)	17842	18958
	wDL (plf)	144	144
	End Post Compression (lb)	2878	2910
	DL Factor	0.6	0.6
	wDL (plf)	86.4	86
	End Post Uplift for HDs (lb)	2033	2002
	Max Compression	2878	2910
	Max Uplift	2033	2002
	Max Shear Flow	279	279
	Max Shear Flow Due to Wind or Seismic (W/S)	W	W

Sheathing Nails	7/16 w/ 8d @ 6" O.C.	7/16 w/ 8d @ 6" O.C.					
# of Layers	1	1					
Shear Flow Allowable (plf)	335	335					
Check	Adequate	Adequate					
Sheathing Staples	7/16 w/ 1 1/2" 16 ga. @ 4" O.C.	7/16 w/ 1 1/2" 16 ga. @ 4" O.C.					
Shar Flow Allowable (plf)	322	322					
Check	Adequate	Adequate					
Recommended Holdown @ Foundation 8" wall	HDU2	HDU2					
Strap Style (Midwall)	LSTHD8	LSTHD8					
Strap Style (End Wall)	LSTHD8	LSTHD8					
Recommended Holdown @ Wood Wall	MSTC40	MSTA49					
Strap Nailing Req'd	(32) 16d	(26) 10d					
# OF Minimum End Post	2	2					